## User's Manual

## பSER'S <br> MANபAL

# FRENIC-VG Series 

Stack Type Edition

# High Performance Vector Control Inverter FRENIC-VG 

User's Manual
(Stack Type Edition)

| Revision History | Revision Symbol | Year and Month of Change | Description |
| :---: | :---: | :---: | :---: |
| First Edition | - | 2013-03 | - |
| Second Edition | a | 2016-03 | 1. Inverters <br> - 400 V series $\rightarrow 630 \mathrm{~kW}$ to 800 kW units added (external views, etc.) <br> - 690 V series added $\rightarrow 90 \mathrm{~kW}$ to 450 kW <br> 2. Converters (diode rectifiers) <br> - 690V series added. <br> 3. Converters (PMW converters) <br> - 400 V series $\rightarrow 630 \mathrm{~kW}$ to 800 kW units added (external views, etc.) <br> 4. Filter stacks <br> - 400 V series added. <br> 5. Other <br> - Content renewed (addition of sections added at later date, etc.) |
| Third Edition | b | 2017-03 | 1. Converters (PMW converters) <br> - 690V series added. <br> 2. Converters (filter stacks) <br> - 690V series added. <br> 3. Other <br> - Content renewed (addition of sections added at later date, etc.) |
| 4th Edition | c | 2019-02 | Content renewed. |
| 5th Edition | d | 2019-07 | Content renewed. |

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The information in this manual is correct at the time of publication. However, if concerns arise or if mistakes are found, please contact the retailing store of purchase or a sales office of Fuji Electric Co., Ltd. listed at the end of this document

## Preface

This manual describes information on the installation of FRENIC-VG series stack type inverters and converters and the selection of peripheral devices, with specialization in hardware. Please refer to the separate volume user's manual for operation methods such as function setup.
Please read this manual thoroughly for correct operation. Improper handling may result in prevention of normal operation, decrease of service life, or cause of failure.

The table below lists other materials related to the use of the FRENIC-VG series. Read them in conjunction with this manual as necessary.

| Name |  |  | Material Number | Description |
| :---: | :---: | :---: | :---: | :---: |
| Catalog |  |  | 24A1- $\square-0002^{*}$ (Formerly MH659) | Product overview, features, specifications, external dimensions, options, etc. |
|  | Unit Type Function Code Edition |  | 24A7-■-0019* <br> (Formerly MHT286) | 1) Description of function codes, keypad operating instructions, etc. for the FRENIC-VG series (unit type/stack type) <br> 2) Overview of the FRENIC-VG unit type, features, specifications, replacement documentation, etc. |
|  | Option Edition |  | 24A7-■-0045* <br> (Formerly MHT286) | Functional description of various option cards for the FRENIC-VG series, the RS-485, etc. <br> * For information on the functional safety option (OPC-VG1-SAFE), refer to the manual of the option card. The functions and other aspects of other options are described in this manual. |
|  | Stack Type Edition (this manual) |  | 24A7- $\square-0018$ * | Features, specifications, cabinet design materials, etc. for the FRENIC-VG stack type inverters and converters |
|  | UPAC Option Edition |  | 24A7- $\square$-0044* | UPAC option card specifications, description of the interface between the inverter and UPAC, description of application package software (orientation, dancer type winder), etc. |
|  | FRENIC-VG st | ack type (400V) | INR-SI47-1721*- $\square$ | Inspection upon delivery, installation and wiring of the product, keypad operating instructions, troubleshooting, maintenance and inspection, specifications, etc. |
|  | FRENIC-VG st | tack type (690V) | INR-SI47-1841*- $\square$ |  |
|  | RHD-D stack typ | pe (400V) | INR-SI47-1786*- $\square$ |  |
|  | RHD-D stack type (690V) |  | INR-SI47-1852*- $\square$ |  |
|  | RHC-D stack type (400V) |  | INR-SI47-1722*- $\square$ |  |
|  | RHC-D stack type (690V) |  | INR-SI47-1944*- $\square$ |  |
|  | RHF-D stack type (400V) |  | INR-SI47-1770*- $\square$ |  |
|  | RHF-D stack type (690V) |  | INR-SI47-1945*- $\square$ |  |
| FRENIC-VG Loader Instruction Manual |  | WPS-VG1-STR | INR-SI47-1588*- $\square$ | Instructions for use of the inverter support loader software, FRENIC-VG Loader (free-of-charge version) |
|  |  | WPS-VG1-PCL | INR-SI47-1616*- $\square$ | Instructions for use of FRENIC-VG Loader (paid version) Includes tracing functions in addition to all the functions of the free-of-charge version (WPS-VG1-STR). |

Note 1) Placeholders " $\square$ " appearing in material numbers in the table above will be replaced with symbols such as $J$ (Japanese), E (English), C (Chinese).
Asterisks (*) appearing in material numbers will be replaced with a revision number (a, b, c...).
Note 2) The materials are subject to change without notice. Be sure to obtain the latest editions before use.

[^0]For more information, refer to Appendix 7 of this manual.

## Structure of this manual

This manual is structured as follows.

## Chapter 1 Overview

This chapter describes the overview, features and the control system of the FRENIC-VG stack type inverter and the recommended configuration for the inverter and peripheral devices.

## Chapter 2 Specifications

Rated output, control method, product overview, specifications for the specialized motor, protective function details, basic connection diagrams, and terminal functions of the FRENIC-VG are described. Additionally, descriptions for the operating environment, storage environment, product quality assurance, precautions for use, external dimensions, examples of basic connections, and protective function details are provided.

## Chapter 3 Transportation and Storage

Descriptions of the transportation method for the FRENIC-VG, converter stack and the cabinet, the FRENIC-VG name plate, storage environment, and storage method are provided.

## Chapter 4 Installation and Wiring

Cabinet construction design documents and wiring specifications, conditions and precautions for the selection of electrical lines and crimped terminals are described for installation the FRENIC-VG and converter on the cabinet.

## Chapter 5 Peripherals

The purpose of peripheral devices and options, connection configuration, and precautions for the FRENIC-VG are described.

## Chapter 6 Converter System

The specifications, protective function details, and basic connection diagrams are described for the PWM converter (RHC-D series), which is the converter providing input to FRENIC-VG, and for the diode rectifier (RHD-D series). Additionally, the selection method for the peripheral devices and electrical wiring sizes for the converters are described. Lastly, the resistance regenerative braking unit and the braking resistance are described.

## Chapter $7 \quad$ EMC Compatible Peripherals

Introduction and operation of devices with noise countermeasures as well as noise countermeasures are described.

## Chapter 8 Operation

Provides references to the operating method for the FRENIC-VG described in the separate volume, "FRENIC-VG unit Type Function Code Edition" (24A7- $\square$-0019).

## Chapter $9 \quad$ Selecting Model

The selection method for the motor and inverter capacities is described. The inverter output torque characteristics required when selecting the capacity, the procedure for capacity selection, and the equation for capacity selection are described. In addition, the braking resistor selection needed in choosing the capacity, MD/LD specification selection, and the control method selection methods are shown.
Lastly, function setup, connection configuration, and reduced unit operation are explained for the case of direct parallel connection control method.

## Chapter 10 Maintenance and Inspection

The daily inspection, periodic inspection, and periodic part replacement for using the inverter in the long term are described. In addition, the maintenance for the air filter used in the cabinet is explained.

## Chapter 11 Troubleshooting

The troubleshooting procedures for inverter malfunctions, alarms, and minor failures are described.
The content guides the user to the individual troubleshooting steps after determining the event as an alarm or a failure based on the displayed content.

## Chapter 12 Cabinet Construction

Introduction of the protection level and the cooling method selection matching the installation environment of the cabinet housing the inverter are provided.

## Appendix

The guidelines concerning safety in Japan, overview of JEM standards, harmonics guideline, and case studies of inverter noise countermeasures are shown.

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## Safety precautions

Please read the instructions manual carefully before installation, wiring (connection), operating, or performing maintenance checkup, and operate the product correctly. Additionally, ensure that you have sound knowledge of the device and familiarize yourself with all safety information and precautions.
Safety precautions are classified into the following categories in this manual.


Failure to heed the information indicated by this symbol may lead to dangerous conditions, possibly resulting in death or serious bodily injuries.

Failure to heed the information indicated by this symbol may lead to dangerous conditions, possibly resulting in medium level or minor bodily injuries and/or substantial property damage.

Following the cautionary advices contained under the CAUTION title may still cause serious consequences.
These safety precautions are of utmost importance and must be observed at all times.

## Application

(1) FRENIC-VG stack type inverter

$$
\begin{aligned}
& \text { - The FRENIC-VG is an equipment to drive } 3 \text { phase motors. The inverter may not be used for single-phase motors } \\
& \text { and other purposes. } \\
& \text { - The FRENIC-VG cannot drive } 3 \text { phase motors independently by connecting to a commercial power supply. } \\
& \text { Use the PWM converters or diode rectifiers specified by Fuji Electric Co., Ltd in combination with the FRENIC-VG. } \\
& \text { Otherwise, fire or accidents may occur. } \\
& \text { - FRENIC-VG may not be used for applications directly related to human safety such as life supporting systems. } \\
& \text { - Although the product is manufactured under strict quality control, install safety devices for applications where } \\
& \text { serious accidents or property damages are foreseen in relation to the failure of the inverter. } \\
& \text { Otherwise, accidents may occur. }
\end{aligned}
$$

(2) RHC-D (PWM converter)

## $\triangle$ WARNING

- RHC-D (PWM converter) is an equipment to be used in combination with Fuji Electric's inverter to drive 3 phase motors. It may not be used for other purposes.
Otherwise, fire or accidents may occur.
- The RHC-D may not be used for applications directly related to human safety such as life supporting systems.
- Although the product is manufactured under strict quality control, install safety devices for applications where serious accidents or property damages are foreseen in relation to the failure of the inverter.
Otherwise, accidents may occur.
(3) RHD-D (diode rectifier)


## 〔 WARNING

- RHD-D (diode rectifier) is an equipment to be used in combination with Fuji Electric's inverter to drive 3 phase motors. It may not be used for other purposes.
Otherwise, fire or accidents may occur.
- The RHD-D may not be used for applications directly related to human safety such as life supporting systems.
- Although the product is manufactured under strict quality control, install safety devices for applications where serious accidents or property damages are foreseen in relation to the failure of the inverter.
Otherwise, accidents may occur.
(4) RHF-D (filter stack dedicated to RHC-D)

| - The RHF-D (filter stack dedicated to RHC-D) is an equipment to be used in combination with Fuji Electric's PWM |
| :--- |
| converter (RHC-D) and inverter to drive 3 phase motors. It may not be used for other purposes. |
| Otherwise, fire or accidents may occur. |
| - The RHF-D may not be used for applications directly related to human safety such as life supporting systems. |
| - Although the product is manufactured under strict quality control, install safety devices for applications where |
| serious accidents or property damages are foreseen in relation to the failure of the inverter. |
| Otherwise, accidents may occur. |

## Installation

- Install the inverter on a base made of metal or other non-flammable material.
- Do not install close to flammable objects.
Otherwise, fire may occur.
- The protection structure of the product body is IP00, and contact with the main circuit terminal block (live part) is
possible. For this reason, implement measures such as installation in locations where individuals cannot easily
contact.
Otherwise, it could cause electric shock and injury.


## $\triangle$ CAUTION

- Do not support the product by its front cover during transportation.

Otherwise, it could cause the product to drop, resulting in injury.

- Prevent foreign materials such as lint, paper fibers, sawdust, dust, and metallic chips from entering the product and from accumulating on the cooling fins.
- Install by using screws and bolts at the defined tightening torque, following the specified installation method.

Otherwise, fire or accidents may occur.

- Do not install or operate products which are damaged internally or externally.

Otherwise, it could cause fire, accidents and injuries.

## Wiring

## WARNING $\wedge$

- Shutdown of the entire power supply system caused by functioning of the ground-fault relay in the upstream power supply line is operationally undesirable. When appropriate earth leakage (zero phase current) detecting devices are not installed in the power supply system, install an earth leakage circuit breaker (ELCB) on the input side of each converter (diode rectifier, PWM converter, filter stack).
- Connect to the power supply through molded-case circuit-breakers and earth leakage circuit breakers (with overcurrent protection) on each converter (diode rectifier, PWM converter, filter stack). Use recommended devices with the recommended capacities for the molded-case circuit-breaker and earth leakage breaker.
- Use wires in the specified size.
- Tighten terminals with the specified torque.
- When multiple combinations of inverters and motors exist, do not use multicore cables for the purpose of handling the wiring together.
- Do not connect surge killers to the inverter output (secondary) circuit.

Otherwise, fire may occur.

- Perform C type grounding construction following the supply voltage systems for the converter (diode rectifier, PWM converter, filter stack).
- Always connect the grounding terminal [ $\quad \mathrm{G}$ ] to an earthing conductor or earthing copper bar for the converter (diode rectifier, PWM converter, filter stack) and the FRENIC-VG.
Otherwise, electric shock or fire may occur.
- Qualified electricians should carry out wiring.
- Be sure to perform wiring after turning the power OFF.

Otherwise, electric shock may occur.

- Always wire after the product is installed.

Otherwise, it could cause electric shock and injury.

- Confirm that the phase number and the rated voltage of the power supply input to the converter (diode rectifier, PWM converter, filter stack) matches the phase number and voltage of the power supply to connect.
- Do not connect the power supply lines to the output terminals ( $\mathrm{P}, \mathrm{N}$ ) of the converter (diode rectifier, PWM converter).
- Do not connect the power supply lines to the inverter output terminals ( $\mathrm{U}, \mathrm{V}$, and W ).

Otherwise, fire or accidents may occur.

- In general, sheaths of the control signal wires are not specifically designed to withstand high voltage (i.e., reinforced insulation is not applied). Therefore, if a control signal wire comes into direct contact with a live conductor of the main circuit, the insulation of the sheath may be damaged. In this case, the main circuit high voltage may be applied on the control signal wire, so make sure that the control signal wires do not come into contact with live conductors of the main circuit.

Otherwise, it could cause an accident or an electric shock.

```
|WARNING © 
- When moving the switches, check that the voltage between the major terminals \(P(+)\) and \(N(-)\) has fallen to a safe voltage (below \(\mathrm{DC}+25 \mathrm{~V}\) ) using a tester after confirming that the LED monitor and the charge lamp have turned off and after 10 minutes has elapsed.
The diode rectifier or filter stack does not contain the LED monitoring function.
Otherwise, electric shock may occur.
```

- Electric noise is generated from FRENIC-VG, PWM converter, filter stack, motor, and wiring. This may cause malfunction in the peripheral sensors and devices. To prevent malfunctions, implement noise countermeasures.

Otherwise, accidents may occur.

Operation

## WARNING ©

- Be sure to mount the front cover of the product before turning the power ON. Do not remove the cover when the power is ON.
- Do not operate the switches with wet hands.

Otherwise, electric shock may occur.

## <FRENIC-VG stack type inverter>

- If the auto-reset function has been selected, the inverter may automatically restart and drive the motor depending on the cause of tripping. Design the machine so that safety for human and the surroundings is ensured after restarting.
- If the stall prevention function (torque limiter) has been selected, the inverter may operate with acceleration/deceleration times and speed different from the setup. Design the machine so that safety is ensured even in these cases.


## Otherwise, accidents may occur.

- The keypad (woy keys are enabled only when the keypad operation is selected by F02 function code. Emergency shut down switch should be prepared separately. When the operation command method is switched from keypad operation command using link operation selection "LE", the keys are disabled.
- After the cause of protective function actuation is removed, confirm that the run command is OFF and release the alarm. If the run command is ON when the alarm is released, the inverter will start supplying power to the motor. The motor may rotate, which could be dangerous.


## Otherwise, accidents may occur.

- If the "Restart mode after momentary power failure" (Function code F14 = 3 to 5 ) is selected, then the inverter automatically restarts running the motor when the power is recovered. Design the machine so that human safety is ensured after restarting.
- Set up the function codes after completely understanding this user's manual. When the equipment is operated while the function code date is changed indiscriminately, motor may rotate at torques and speed which the machine cannot tolerate.


## Otherwise, accidents or injuries may occur.

- Even if the inverter has interrupted power to the motor, voltage may be output to inverter output terminals $\mathrm{U}, \mathrm{V}$, and W if voltage is applied to the main input power supply of the PWM converter and the diode rectifier.
- Even if the motor is stopped by direct current braking or pre-excitation, voltage is output to inverter output terminals $\mathrm{U}, \mathrm{V}$, and W.
Otherwise, electric shock may occur.
- The inverter can be readily set up for high speed operation. When changing the speed setting, carefully check the specifications of motors and the machine beforehand.
Otherwise, it could cause injury.


## <Diode rectifier, PWM converter, filter stack>

- When the protective function of the PWM converter is activated, confirm that the run command is OFF. Remove the cause of the protective function activation, and release the alarm. If the alarm is released while the run command is ON, the inverter may restart abruptly, which can be dangerous.
Otherwise, accidents may occur.
- Voltage is applied to the individual main terminals $P(+)-N(-)$ even while the FRENIC-VG is stopped when the input supply voltage is applied to the converter (diode rectifier, PWM converter, filter stack).
Otherwise, electric shock may occur.
- While the filter stack is operating, an electromagnetic sound is generated from the reactors and resistors in it. If the product is installed in an area with noise restrictions, implement sound insulation.


## CAUTION

- Do not touch the cooling fins as they become hot.

Risk of burn exists.

## <FRENIC-VG stack type inverter>

- The brake function of the inverter does not provide mechanical holding.
- The digital input terminal contains functions for run, stop, and speed commands such as operation command "FWD" and coast-to-stop command "BX". The speed may change drastically or operation may start abruptly with changes in the function code setting through the digital input terminals. Perform changes to the function code settings after adequately securing safety.
- The manipulation method of the operation commands and the function to switch the speed commanding methods ("SS1, 2, 4, 8", "N2/N1", "KP/PID", "IVS", "LE", others) can be assigned to the digital input terminal. When switching these signals, the operation may start abruptly or the speed may change drastically depending on the conditions.
Otherwise, accidents or injuries may occur.
<Diode rectifier, PWM converter, filter stack>
- Do not touch the reactor (filter reactor, pressurizing reactor, DC reactor, etc.) and the braking resistor as they become hot.
Otherwise, it could cause injury.


## Maintenance checkup and parts replacement

## $\triangle$ WARNING $\triangle$

- When moving the switches at checkup, check that the voltage between the major terminals $\mathrm{P}(+)$ and $\mathrm{N}(-)$ has fallen to a safe voltage (below DC +25 V ) using a tester after confirming that the LED monitor and the charge lamp have turned off and after 10 minutes has elapsed. The diode rectifier or filter stack does not contain the LED monitoring function.

Otherwise, electric shock may occur.

- Be sure to perform the daily inspection and periodic inspection described in the instruction manual. Lengthy use of the product without inspection could result in inverter failure and damage, or accident and fire.
- A periodic inspection cycle of 1 to 2 years is recommended, however, the cycle may be reduced depending on usage conditions.
- It is recommended that parts for periodic replacement be replaced after the standard number of years indicated in the instruction manual. Lengthy use of the product without without replacing parts could result in inverter failure and damage, or accident and fire.


## Risk of burn exists.

## <FRENIC-VG stack type inverter>

- Contact outputs [30A/B/C] and [Y5A/C] use relays, and may remain ON or OFF, or in an indefinite state when the life is reached. In the interests of safety, equip the product with an external protection function.
- Continued use of the product with battery consumed may result in loss of data.


## Risk of accident

## <Diode rectifier>

- Contact outputs [73A/C], [1,2], and [ONA/C] use relays, and may remain ON or OFF, or in an indefinite state when the life is reached. In the interests of safety, equip the product with an external protection function.
Risk of accident


## <PWM converter>

- Contact outputs [30A/B/C], [Y5A/C], and [73A/C] use relays, and may remain ON or OFF, or in an indefinite state when the life is reached. In the interests of safety, equip the product with an external protection function.


## Risk of accident

## $\triangle$ WARNING $\Delta$

## <Filter stack>

- Contact outputs [1, 2] and [ONA/B/C] use relays, and may remain ON or OFF, or in an indefinite state when the life is reached. In the interests of safety, equip the product with an external protection function.


## Risk of accident

- Maintenance checkup and parts replacement should be conducted only by qualified personnel.
- Take off watches, rings, and other metallic objects before starting work.
- Use insulated tools.
- Never modify the product.

Otherwise, it could cause electric shock and injury.

## Disposal

## $\triangle$ CAUTION

- Treat the FRENIC-VG and converter (diode rectifier, PWM converter, filter stack) as industrial waste when disposing of them.
Otherwise, it could cause injury.
- The batteries used in the FRENIC-VG fall under "primary batteries". Discard following the procedures for disposal defined by each municipality.


## Speed control mode

## $\triangle$ CAUTION

## <FRENIC-VG stack type inverter>

- If the control parameters of the automatic speed regulator (ASR) are not appropriately configured under speed control, turning the run command OFF may not decelerate the motor due to hunting caused by high gain setting. Stop conditions may not be reached and the motor may continue running.
- Hunting state may be realized by high response in low speed regions during deceleration. The detected speed deviates from the zero speed area before the zero speed control duration (F39) elapses, and the stop conditions are not reached. The inverter enters the deceleration mode again and continues running.


## Otherwise, it could cause accidents or injuries.

$\Rightarrow$ Adjust the ASR control parameter to an appropriate value. Also implement countermeasures such as causing the alarm to trip when deviation results between the commanded speed and actual speed by using the speed mismatch alarm function. Additional measures may include switching by ASR control constant speed or determination of stopping speed detection by the commanded value.

## Torque control mode

| <FRENIC-VG stack type inverter> |
| :--- |
| - When the motor is rotated by load-side torque exceeding the torque command under torque control, turning the run |
| command OFF may not bring the stop conditions so that the inverter may continue running. |
| Otherwise, it could cause accidents or injuries. |
| $\Rightarrow$ To cut off the inverter output, switch to speed control and decelerate to stop, or issue the coast-to-stop command |
| and cut off the output. |

## General Precautions

## $\triangle$ CAUTION

Part of the illustrations listed in this user's manual and the instruction manual bundled with the product may be shown without covers or shields in order to describe the details.
When operating the product, be sure to reinstall the covers and shields exactly as specified, and operate it in accordance with the instruction manual.

## Icons

The following icons are used throughout this manual.
Note This icon indicates information which, if not heeded, can result in the inverter not operating to full efficiency, as well as information concerning incorrect operations and settings which can result in accidents.

Tip This icon indicates information that can prove handy when performing certain settings or operations.
(1) This icon indicates a reference to more detailed information.

## FRENIC-VG

## 1

## Chapter 1 Overview

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### 1.1 Product introduction

## Inverter (Unit Type)



This type consists of the converter and inverter circuits. The inverter can be operated using a commercial power supply. - DC power can also be supplied without using the converter circuit.

## Structure

- Built-in converter (rectifier)
- Built-in control circuit
- External DC reactor as standard*
- DC input is available.
* Available for 75 kW or higher capacity models


## Features

Easier arrangement for small-scale system


## Converter

Diode rectifier (Stack Type)
RHD-D series


This converter is used where no electric power regeneration is required.

PMW converter (Unit Type) PMW converter (Stack Type) Filter stack (Stack Type) RHC-C series*
 RHC-D series ${ }^{\star}(400 \mathrm{~V} / 690 \mathrm{~V}$ ) RHF-D series ( $400 \mathrm{~V} / 690 \mathrm{~V}$ )


This converter is used where electric power regeneration or harmonic control is required. Peripheral devices are separately required.

- D series and C series differ in form but show identical function and performance Please use them according to the installation space and purposes.
- Line-up features unit type and stack type, facilitating easy construction of large-capacity systems.
- The stack type offers support for up to the following capacities through direct parallel connection.

Three-phase 400 V series: Max. 2400 kW (MD spec.), 3000 kW (LD spec.)
Three-phase 690V series: Max. 1200 kW (MD spec.), 1200 kW (LD spec.)


Three-phase 400V series


Three-phase 690V series

| Type | Series name | Form | Specifications *1 (applicable load) | Nominal applied motor [kW] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 50 | 100 | 500 | 5000 |  |
| Stack | Inverter (FRENIC-VG) | Standard stack | $\begin{aligned} & \text { MD } \\ & \text { (LD) } \end{aligned}$ |  | $\begin{gathered} 90 \mathrm{~kW} \\ (110 \mathrm{~kW}) \end{gathered}$ | $450 \mathrm{~kW}(450 \mathrm{~kW})$ <br> Direct parallel Multiwinding motor | 1200kW(1200kW)$2700 \mathrm{~kW}(2700 \mathrm{~kW})$ |  |
|  | PWM Converter (RHC-D) | Standard stack | $\begin{aligned} & \text { MD } \\ & \text { (LD) } \end{aligned}$ |  | $\begin{gathered} 132 \mathrm{~kW} \\ (160 \mathrm{~kW}) \end{gathered}$ | $450 \mathrm{~kW}(450 \mathrm{~kW})$ <br> Isolation-less <br> Isolation | $\begin{array}{r} 1200 \mathrm{~kW}(1200 \\ 2700 \mathrm{~kW} \\ \hline \end{array}$ | kW) <br> (2000kW) |
| 4 | Filter stack (RHF-D) | Standard stack | - |  | $160 \mathrm{~kW}$ | $450 \mathrm{~kW}$ |  |  |
| - | Diode rectifier (RHD-D) | Standard stack | $\begin{aligned} & \text { MD } \\ & \text { (LD) } \end{aligned}$ |  | $\begin{array}{r} 220 \mathrm{~kW} \\ (250 \mathrm{~kW}) \\ \hline \end{array}$ | 450kW <br> Parallel connection | 2000kW |  |

"1 Refer to "Ratings for intended use" on page 6 for specifications (applicable load).
Unit type inverters have built-in brake circuits as standard ( 160 kW or less),

* Configuration: Standard unit $\rightarrow$ Can be used with one set. Stack by phase $\rightarrow$ Categorized by phase, and one inverter set consists of three stacks.
* Multiple inverters can be connected with a single PWM converter and diode rectifier.
* Inverters can also be supplied with DC power (with generator, etc.) without the use of a converter circuit.
- Capacity expansion (parallel operation)

Inverters

- Direct parallel connection: One single-winding motor is driven by multiple inverters. (Drive is possible with up to three inverters)
- Multi-winding motor drive: Specialized motor drive system with multiple windings around a single motor. (Drive is possible with up to six inverters)

PWM converters

- Transformer isolation (parallel system): System used to isolate the receiving power supply system and converter with a transformer. It is necessary to equip each converter
input with a transformer. (No. of parallel connection units: max. 6)
Transformerless (parallel system): System in which a PWM converter is connected directly to the receiving power supply system. There is no need to isolate with a transformer (No. of parallel connection units: max. 3)
-Filter circuits if used with transformerless parallel system (multiple units operating in parallel)
Standard stack: Use a filter stack. (Filter circuits cannot be configured with peripheral equipment.)
Stack by phase: Use peripheral equipment.


### 1.2 Features

### 1.2.1 A wide range of applications

### 1.2.1.1 Control method

Not only induction motors but also synchronous motors can be driven, and for induction motors, you can select the most suitable control method according to your individual needs.

| Target motors | Control method |
| :--- | :--- |
| Induction motor | - Vector control with a speed sensor <br> - Vector control without a speed sensor <br> - V/f Control |
| Synchronous motor | Vector control with a speed sensor (including magnetic pole position detection) |

### 1.2.1.2 Product arrangement and easier change

The stack type inverters have an arrangement with consideration for the installation of the product into the cabinet and easier change.
(1) The inverters ( 132 to 800 kW ) can easily be installed to the cabinet or changed because they have casters.
(2) With the inverters ( 630 to 800 kW ), stacks are divided for each output phase ( $\mathrm{U}, \mathrm{V}$ and W ), which has realized the lighter weight.

| Nominal applied motor capacity <br> [kW] (MD spec) | 30 to 110 | 132 to 450 | 630 to 800 |
| :---: | :---: | :---: | :---: |
| Type | 400V: FRN30SVG1S-4 to FRN110SVG1S-4 <br> 690V: FRN90SVG1S-69 to FRN110SVG1S-69 | 400V: FRN132SVG1S-4 to FRN315SVG1S-4 <br> 690V: FRN132SVG1S-69 to FRN450SVG1S-69 | FRN630BVG1S-4 $\square$ to FRN800BVG1S-4 |
| Categoly | Single unit | Single unit | Stack by phase |
| Wheels | Not provided | Provided | Provided |
| Arrangement |  |  |  |
| Maintenance | The weight of one stack is reduced ( 50 kg or less) to give consideration to replacement work. | The models where each stack is heavy have wheels in order to change the stacks easily. A lifter for replacement is available. | Trim weight by dividing the stack into 3 parts by each output phase ( $\mathrm{U}, \mathrm{V}$ and W ). In the event of a breakdown, only the target phase needs to be replaced with a new one. The stack to be replaced should be an exclusive part. |
| Approx.weight [kg] | 30 to 45 | 95 to 135 | $135 \times 3$ |

### 1.2.1.3 Ratings for intended use

The operation mode for the motor is selected according to motor load condition. Motors one or two frame larger than inverter can be driven for light load (LD) use.

| Specification | Applied <br> load | Feature | Applicable <br> overload rating | Power supply <br> voltage | Applicable motor <br> capacity [kW] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MD | Middle Duty <br> Spec |  | $150 \%, 1 \mathrm{~min}$ | 400 V | 30 to 800 |
|  | LD | Low Duty <br> Spec | Can drive motors of frames <br> one or two sizes larger. | $110 \%, 1$ min | 400 V |
|  |  |  | 69 to 450 |  |  |

### 1.2.1.4 Style designed specifically for installation in a panel

Fits in smaller panels
Designed specifically for installation in a panel, the stack type inverters fit in smaller panels than the conventional models.
For crane systems, the panel width can be reduced by $34 \%$, compared with the conventional models.
Also, the inverters can be easily installed in a panel and replaced, thanks to the dedicated design.
<Example of panel configuration for a crane system>


### 1.2.1.5 How to expand the capacity range of the inverters

Direct parallel connection system and multiwinding motor drive system are provided for driving a large capacity motor.

| System |  | Direct parallel connection system | Multiwinding motor drive system |
| :---: | :---: | :---: | :---: |
| Features | Drive motor | Single-winding motor | Multiwinding motor (Exclusive use for multiwinding motors) |
|  | Restriction of wiring length | The minimum wiring length ( $L$ ) varies with the capacity. | There is no particular limit. |
|  | Reduced capacity operation *2 | Available | Available <br> (However, the wiring should be switched over.) |
| Number of inverters to be connected |  | 2 to 3 inverters | 2 to 6 inverters |
| Arrangement diagram |  | When 2 inverters are connected | When 2 inverters are connected |

Configuration table for direct parallel connection
*1) OPC-VG1-TBSI is separately required.
*2) Reduced capacity operation. If a stack fails in case of direct parallel connection, the operation continues with lower output power using the stacks that have not failed.


Example) If one inverter fails when $200 \mathrm{~kW} \times 2$ inverters are driving a 355 kW motor, the operation can continue with the 200kW inverter (capacity of one inverter).
Note) To start the reduced capacity operation, consideration is needed to the switch over operation of PG signals or motor constants and sequence circuit. For details, refer to chapter 9 of direct parallel.

2 or even 3 inverters of the same capacity can be connected in parallel to increase capacity or facilitate system redundancy. Typical combinations are shown in Table 1, however, other configurations are also possible.

Table 1 Direct parallel combination example ( 400 V series, MD specification)

| Connection system | Standard stack |  |  |  | Stack by phase |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| Capacity [kW] | Applicable inverter | Applicable inverter | No. of units | Current [A] | Applicable inverter | Applicable inverter | No. of units | Current [A] |
| 30 | FRN30SVG1 |  |  |  |  |  |  |  |
| 37 | FRN37SVG1 |  |  |  |  |  |  |  |
| 45 | FRN45SVG1 |  |  |  |  |  |  |  |
| 55 | FRN55SVG1 |  |  |  |  |  |  |  |
| 75 | FRN75SVG1 |  |  |  |  |  |  |  |
| 90 | FRN90SVG1 |  |  |  |  |  |  |  |
| 110 | FRN110SVG1 |  |  |  |  |  |  |  |
| 132 | FRN132SVG1 |  |  |  |  |  |  |  |
| 160 | FRN160SVG1 |  |  |  |  |  |  |  |
| 200 | FRN200SVG1 |  |  |  |  |  |  |  |
| 220 | FRN220SVG1 |  |  |  |  |  |  |  |
| 250 | FRN250SVG1 |  |  |  |  |  |  |  |
| 280 | FRN280SVG1 |  |  |  |  |  |  |  |
| 315 | FRN315SVG1 |  |  |  |  |  |  |  |
| 355 |  | FRN200SVG1 | 2 | 716 |  |  |  |  |
| 400 |  | FRN220SVG1 | 2 | 789 |  |  |  |  |
| 500 |  | FRN280SVG1 | 2 | 988 |  |  |  |  |
| 630 |  | FRN220SVG1 | 3 | 1183 | FRN630BVG1 |  |  |  |
| 710 |  | FRN280SVG1 | 3 | 1482 | FRN710BVG1 |  |  |  |
| 800 |  | FRN280SVG1 | 3 | 1482 | FRN800BVG1 |  |  |  |
| 1000 |  |  |  |  |  | FRN630BVG1 | 2 | 2223 |
| 1200 |  |  |  |  |  | FRN630BVG1 | 2 | 2223 |
| 1500 |  |  |  |  |  | FRN800BVG1 | 2 | 2812 |
| 1800 |  |  |  |  |  | FRN630BVG1 | 3 | 3335 |
| 2000 |  |  |  |  |  | FRN710BVG1 | 3 | 3905 |
| 2400 |  |  |  |  |  | FRN800BVG1 | 3 | 4218 |

*1) OPC-VG1-TBSI is required for each stack.
For more information, refer to:
(1) • "2.1.2. Multi-drive system" in Chapter 2

- "9.4.8.1. Direct parallel connection combinations and wiring lengths" in Chapter 9


### 1.2.1.6 How to expand the total capacity of the converter

You can expand the total capacity of the PWM converter (RHC-D) using either a "transformer isolation-less parallel system" or a "transformer insulation type parallel system".

| System | Transformer isolation-less parallel system | Transformer insulation type parallel system |
| :---: | :---: | :---: |
|  | This system involves connecting converter inputs to the power supply without isolating with a transformer, etc. | This system involves isolating respective converter inputs with a transformer. |
| Reduced capacity operation | Available | Available |
| Number of converter to be connected | 2 to 3 converters | 2 to 6 converters |
| Arrangement diagram | When 2 converters are connected | When 2 converters are connected |

*2) OPC-VG7-SIR is required for each stack. *3) OPC-VG7-SI is required for each stack.

## Transformerless parallel system configuration table

2 or 3 converters of the same capacity can be connected in parallel to increase capacity or facilltate system redundancy. Typical combinations are shown in Table 2, however, other configurations are also possible.

Table 2 Transformerless parallel system combination example ( 400 V series, MD specification)

| Connection system | Standard stack |  |  | Stack by phase |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | upply |  |  |  |
| Capacity [kW] | Applicable converter | Applicable converter | No. of units | Applicable converter | Applicable converter | No. of units |
| 132 | RHC132S-4D |  |  |  |  |  |
| 160 | RHC160S-4D |  |  |  |  |  |
| 200 | RHC200S-4D |  |  |  |  |  |
| 220 | RHC220S-4D |  |  |  |  |  |
| 280 | RHC280S-4D |  |  |  |  |  |
| 315 | RHC315S-4D |  |  |  |  |  |
| 355 |  | RHC200S-4D | 2 |  |  |  |
| 400 |  | RHC200S-4D | 2 |  |  |  |
| 500 |  | RHC280S-4D | 2 |  |  |  |
| 630 |  | RHC315S-4D | 2 | RHC630B-4D |  |  |
| 710 |  | RHC280S-4D | 3 | RHC710B-4D |  |  |
| 800 |  | RHC280S-4D | 3 | RHC800B-4D |  |  |
| 1000 |  |  |  |  | RHC630B-4D | 2 |
| 1200 |  |  |  |  | RHC630B-4D | 2 |
| 1500 |  |  |  |  | RHC800B-4D | 2 |
| 1800 |  |  |  |  | RHC630B-4D | 3 |
| 2000 |  |  |  |  | RHC710B-4D | 3 |
| 2400 |  |  |  |  | RHC800B-4D | 3 |

*2) OPC-VG7-SIR is required for each stack.
For more information, refer to:

- $\mathbb{C l}$ - PWM converter (RHC-D): "6.3.13. Parallel system (capacity expansion)" in Chapter 6
- Diode rectifier (RHD-D): "6.2.9. Multi-unit connection (capacity expansion)" in Chapter 6


### 1.2.1.7 A wide range of options

- A wide range of options are available that support high speed communication and other various interfaces.
- You can use option cards by just inserting them into the connectors provided inside the inverter. You can install up to four option cards.
(There are some restrictions on the combinations of option cards. For more information, refer to "5.4.2. Restrictions on mounting control option cards and others" in Chapter 5.)

| Categoly | Name |  | Type |
| :---: | :---: | :---: | :---: |
| Analog card | Synchronized interface |  | OPC-VG1-SN |
|  | F/V converter*1 |  | OPC-VG1-FV |
|  | Analog input/output interface expansion card |  | OPC-VG1-AIO |
| Digital card (for 8-bit bus) | Di interface card |  | OPC-VG1-DI |
|  | Dio extension card |  | OPC-VG1-DIO |
|  | PG interface card | +5V line driver | OPC-VG1-PG |
|  |  | Open collector | OPC-VG1-PGo |
|  |  | ABS encoder with 17-bit high resolution | OPC-VG1-SPGT |
|  | PG card for synchronous motor drive | Line driver | OPC-VG1-PMPG |
|  |  | Open collector | OPC-VG1-PMPGo |
|  | T-Link communication card |  | OPC-VG1-TL |
|  | CC-Link communication card |  | OPC-VG1-CCL |
|  | High-speed serial communication card (for UPAC)*1 |  | OPC-VG1-SIU |
| Digital card (for 16-bit bus) | SX bus communication card |  | OPC-VG1-SX |
|  | E-SX bus communication card |  | OPC-VG1-ESX |
|  | User programming card |  | OPC-VG1-UPAC |
|  | PROFINET-IRT communication card |  | OPC-VG1-PNET |
| Safety card | Functional safety card |  | OPC-VG1-SAFE |
| Field bus interface card | PROFIBUS-DP communication card |  | OPC-VG1-PDP |
|  | DeviceNet communication card |  | OPC-VG1-DEV |
| Control circuit terminal | Terminal block for high-speed communications |  | OPC-VG1-TBSI |

[^1]
### 1.2.2 Easier maintenance and greater reliability

### 1.2.2.1 Upgraded PC loader functions


[Fault diagnosis using the trace back function]


- Internal data, time and date around the fault are recorded. The real-time clock (clock function) is built-in as standard.
- Data are backed up by battery.

Trace data can be stored in the memory even while the power is off. *Battery: 30 kW or more (built-in as standard), up to 22 kW (available as option: OPK-BP)

- Trace waveform can be checked on the PC loader


## [Easy edit and detail monitor]

Data editing and detailed data monitor analysis operations are much easier than with a conventional PC loader.

Function code setting User-defined displays (customized displays), data explanation display for each code.

Trace function
Real-time trace: for long-term monitoring
Historical trace: for detailed data diagnosis for short periods
Trace back: for fault analysis (last three times)
*The paid-for loader software (WPS-VG1-PCL) supports real-time tracing and historical tracing.
*The paid-for loader software (WPS-VG1-STR) is contained in the CD-ROM provided with the product. (Can be downloaded from the Fuji website.)

### 1.2.2.2 Multifunctional Keypad

- Wide 7 -segment LED ensures easy view.
- The back-light is incorporated in the LCD panel, which enables easy inspection in a dark control panel.
- Enhanced copy feature

Function codes can be easily copied to other inverters.
(Three patterns of function codes can be stored.)
Copying data in advance reduces restoration time when problems occur, by replacing the Keypad when changing the unit.

- Remote control operation is available.

The Keypad can be remotely operated by extending the cable length at the RJ-45 connector.


- JOG (jogging) operation can be executed using the Keypad.
- The HELP key displays operation guidance.


### 1.2.2.3 More reliable functions

## Save alarm data



- The number of alarm data to be stored has been increased from the conventional model.

Thanks to the real-time clock function built-in as standard, the complete data of the latest and last 3 alarm occurences is stored: time, speed command, torque, current and others. This enables machine units to be checked for abnormalities.
$\Rightarrow$ As for previous model, new alarm data overwrote and deleted existing alarm data. This is solved with the new VG model.

## Alarm severity selection

Alarm severity (serious and minor) can be selected, eliminating the risk of critical facility stoppage due to a minor fault.

|  | 30-relay <br> output | Y-terminal <br> output | Inverter <br> output | Selection |
| :--- | :---: | :---: | :---: | :---: |
| Motor overload, <br> communications error, <br> DC fan lock, etc. | No output <br> (minor fault) | Provided | Operation <br> continued | Can be selected <br> for each function. |
| Output | Not provided | Shut off | Fixed |  |
| Blown fuse, excessive current, <br> ground fault, etc. | Output | Not provided | Shut off | Fixe |

## PG fault diagnosis

- The PG interface circuit incorporated as standard detects disconnection of the power supply line as well as the PG signal line.
- A mode was added that judges if it is a PG fault or a fault on the inverter side Simulated output mode is provided at the PG pulse output terminal (FA and FB). Operation can be checked by connecting this to the PG input terminal.


### 1.2.2.4 Easy change of the cooling fan

The cooling fan installed at the top can easily be changed without drawing the stacks out of the cabinet.
However, for the 220 to 800 kW inverter, remove the two connection bars from the DC side and change the cooling fan.


### 1.2.2.5 Components with a longer service life

For the various consumable parts inside the inverter, their designed lives have been extended to 10 years.
This also extends the equipment maintenance cycles.
<Life conditions>

| Life-limited component | Design lifetime ${ }^{-1}$ |
| :---: | :---: |
| Cooling fan |  |
| Smoothing capacitor on main circuit |  |
| Electrolytic capacitors on PCB |  |

- Ambient temperature: $30^{\circ} \mathrm{C}$
- Load factor: $100 \%$ (MD Spec), $80 \%$ (LD Spec)


### 1.2.2.6 Enhanced lifetime alarm

- Lifetime alarms can be checked easily on the Keypad and PC loader (optional).
- Facility maintenance can be performed much more easily.

| Items |  |  |  |
| :---: | :---: | :---: | :---: |
| Inverter accumulated <br> time (h) | No. of inverter <br> starts (times) | Facility maintenance warning <br> Accumulated time (h) <br> No. of starts (times) | Inverter lifetime <br> alarm information <br> is displayed. |

### 1.2.2.7 Useful functions for test run and adjustment

- You can customize the display of function codes (by showing or hiding individual items on the loader).
- A simulated fault alarm can be issued by a special function on the Keypad.
- Monitor data hold function
- Simulated operation mode

Simulated connection allows the inverter to be operated with internal parts in the same way as if they were connected to the motor, without actually being connected.

- The externally input I/O monitor and PG pulse states can be checked on the Keypad.


### 1.2.2.8 Easy wiring (removable control terminal block)

By the use of removable control terminal block:

- The terminal block can be connected to the inverter after control wiring work is completed. Wiring work is simplified.
- Restoration time for updating equipment, problem occurrence, and inverter replacement has been drastically reduced. Just mount the wired terminal block board to the replaced inverter.



### 1.2.3 Adaptation to environment and safety

### 1.2.3.1 Conforms to safety standards

- The functional safety (FS) function STO that conforms to the FS standard IEC/EN61800-5-2 is incorporated as standard.
- The FS functions STO, SS1, SLS and SBC that conform to FS standard IEC/EN 61800-5-2 can be also made available by installing the option card OPC-VG1-SAFE. (Available only when the product is used in conjunction with the MVK dedicated motor.)

|  | STO: Safe Torque Off | This function shuts off the output of the inverter (motor output torque) immediately. |
| :---: | :---: | :---: |
|  | SS1: Safe Stop 1 | This function decreases the motor speed to shut down the motor output torque (by STO FS function) after the motor reaches the specified speed or after the specified time has elapsed. |
|  | SLS: Safely Limited Speed | This function prevents the motor from rotating over the specified speed. |
|  | SBC: Safe Brake Control | This function outputs a safe signal of the motor brake control. |

### 1.2.3.2 Enhanced environmental resistance

Environmental resistance has been enhanced compared to conventional inverters.
(1) Environmental resistance of cooling fan has been enhanced.
(2) Ni and Sn plating is employed on copper bars.

* Environmental resistance has been enhanced on the FRENIC-VG compared to conventional models; however, the following environments should be examined based on how the equipment is being used.
a. Sulfidizing gas (present in some activities such as tire manufacturers, paper manufacturers, sewage treatment, and the textile industry)
b. Conductive dust and foreign particles (such as with metal processing, extruding machines, printing machines, and waste treatment)
c. Others: under unique environments not included under standard environments

Contact Fuji before using the product in environments such as those indicated above.

### 1.2.3.3 RoHS directive compliance

FRENIC-VG complies with European regulations that limit the use of specific hazardous substances (RoHS) as a standard.

## Six hazardous substances

## About RoHS

Lead, mercury, cadmium, hexavalent chromium, Directive 2002/95/EC, promulgated by the European polybrominated biphenyl (PBB), polybrominated biphenyl Parliament and European Council, limits the use of ether (PBDE)
*Does not apply to the parts of some inverter models. specific hazardous substances included in electrical and electronic devices.

### 1.2.4 Functional compatibility with previous models

The FRENIC-VG has functional compatibility with our previous models of vector control inverters.

- Compatibility with the FRENIC5000VG7S

The function codes of the FRENIC-VG are compatible with those of the VG7, and therefore the latter can be set for the FRENIC-VG without making any changes (except for the function codes for the M3).
In addition, function codes can be uploaded from the VG7 via the FRENIC-VG loader and directly copied to the FRENIC-VG.

### 1.3 Control method

### 1.3.1 Features and applications of control methods

Inverter-based speed regulators for AC motors are most commonly used to control the rotational speed of loads.
This section describes the basic configuration of some speed control methods, their characteristics, and hints about their applications.
Speed control systems are generally classified into open-loop control and closed-loop control. (Refer to Figure 1.3.1-1.)


Figure 1.3.1-1: Classification of speed control methods

### 1.3.1.1 Open-loop speed control



Figure 1.3.1-2: Basic configuration of open-loop speed control
As the basic configuration of open-loop control shown in Figure 1.3.1-2 demonstrates, this control method is designed to control the rotational speed of the load with the aid of the frequency output by the inverter, while information about the speed under control is not fed back. The "speed-torque characteristic" of an induction motor traces a slight gradient across frequencies f1 to f6, as shown in Figure 1.3.1-3. If the voltage frequency supplied to the motor is constant, the rotational speed shows little variation in response to variations in the load; for example, the slip at the rated torque is several percent. To put it another way, when controlling the speed of the motor by changing the output frequency of the inverter, "V/f control," which controls the ratio between the terminal voltage of the motor and the applied voltage, is generally applied.


Figure 1.3.1-3: Speed - Torque characteristics

Open-loop control does not require any speed sensor and is adopted mainly for general-purpose inverters. It is used to make the speed of existing motors variable or when a squared-deceleration torque load, such as a fan or pump, does not require very fast response.


Figure 1.3.1-4: Speed control using slip compensation method
The factors that determine the accuracy of the rotational speed in open-loop speed control include load torque fluctuation, the accuracy of the output frequency, and power voltage fluctuation. To deal with load torque fluctuations, a "slip compensation control method" is used, which, as shown in Figure 1.3.1-4, keeps the rotational speed constant by calculating the output torque from the terminal voltage and primary current of the motor and compensating the output frequency of the inverter based on the calculated output torque.

### 1.3.1.2 Closed-loop speed control

"Closed-loop speed control" is the method of compensating speed fluctuations by feeding back speed information. Closed-loop speed control ensures speed control with a high degree of accuracy by feeding back the rotational speed under control and can, therefore, be applied to paper machines, machine tools, etc.


Figure 1.3.1-5: Basic configuration of closed-loop speed control
Figure 1.3.1-5 shows the basic configuration of closed-loop speed control. Speed information is fed back from a speed detection sensor, such as a pulse generator (PG), compared with the speed command, and the output frequency of the inverter is controlled so that the speed command and the detected speed value will match.
As speed control methods, slip frequency control, vector control with a speed sensor, and vector control without a speed sensor are applied. This section presents an overview of each control method.
This high-performance vector control inverter FRENIC-VG series uses vector control included in closed-loop control to control speed.
a) Slip frequency control


Figure 1.3.1-6: Configuration of slip frequency control
Figure 1.3.1-6 shows the configuration of slip frequency control.
The output of the speed controller becomes a slip frequency responsive to the load, and speed fluctuations are compensated by adding this slip frequency to actual speed. Since this control method is relatively simple, it is applied to the speed control of general-purpose inverters. Note that it is suitable for applications that do not require high-speed response because $\mathrm{V} / \mathrm{f}$ control is used for basic control.

## b) Vector control with a speed sensor

Vector control is the control method that enables AC motors to respond faster.
This control method is intended to achieve an equal level of control performance to DC motors by separating the primary current of an AC motor into a magnetic flux current and a torque current to be controlled.
Compared with the V/f control method, vector control combines the following performance characteristics and is suitable for applications requiring fast response and a high degree of accuracy.
(1) Satisfactory acceleration/deceleration characteristic
(2) Broad speed control range
(3) Feasibility of torque control
(4) Fast control response


Figure 1.3.1-7: Example of configuration of vector control
Figure 1.3.1-7 shows an example of the configuration of vector control. Performance considerably depends on the accuracy of the grasping of the motor constant because the vector calculation unit uses the motor constant. In addition, variations in the motor constant due to the temperature condition also greatly affect performance. This control is complicated and thus applied mainly in combination with a dedicated inverter and a dedicated motor.

## c) Vector control without a speed sensor

Vector control with a speed sensor offers distinguished performance backed by fast response and a high degree of accuracy. On the other hand, since it requires a speed sensor, it is sometimes confronted by such issues as the mounting of the speed sensor and wiring from the speed sensor. In contrast to vector control with a speed sensor, vector control without a speed sensor is the method of performing vector control by estimating the rotational speed from the terminal voltage or primary current of the motor without using a speed sensor, and using this estimated value as a speed feedback signal. Vector control without a speed sensor is slightly inferior to vector control with a speed sensor in performance.
Figure 1.3.1-8 shows a configuration of vector control without a speed sensor.


Figure 1.3.1-8: Example of configuration of vector control without a speed sensor
The FRENIC-VG series is capable of performing this control in combination with a general-purpose motor. However, the specifications of this combination, including control performance, are lower than those of the combination of the FRENIC-VG series and a dedicated motor.

## FRENIC-VG

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### 2.1 Standard specifications

This chapter describes the standard specifications for a multi-drive system where a single-drive system of the FRENIC-VG is used in conjunction with multiple units of the FRENIC-VG.

### 2.1.1 Single-drive system

### 2.1.1.1 MD spec (for medium overloads)

## 3-phase 400V series

## - Standard stack

| Type | : FRN | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 315 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal applied motor capacity [kW] |  | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 315 |
| Rated capacity [kVA] ${ }^{* 1}$ |  | 45 | 57 | 69 | 85 | 114 | 134 | 160 | 192 | 231 | 287 | 316 | 356 | 396 | 445 |
| Rated current [A] |  | 60 | 75 | 91 | 112 | 150 | 176 | 210 | 253 | 304 | 377 | 415 | 468 | 520 | 585 |
| Overload capability |  | $150 \%$ of the rated current for 1 minute *2 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Main pow | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Auxilia input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Auxilia | - |  |  |  |  | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |  |  |  |  |  |
|  | Allowa | Voltage: +10 to $-15 \%$, Frequency: +5 to $-5 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Braking system, braking torque |  | Braking system: Depending on power regenerative braking (PWM converter), resistance regenerative braking (braking unit) <br> Braking torque: 150\% |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Carrier frequency [kHz] ${ }^{*}$ |  | 2 kHz |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approx. mass [kg] |  | 30 | 30 | 30 | 37 | 37 | 45 | 45 | 95 | 95 | 95 | 125 | 135 | 135 | 135 |
| Enclosure |  | IP00 open type |  |  |  |  |  |  |  |  |  |  |  |  |  |

- Phase-specific stack

| Type: FRN___BVG1S-4 ${ }^{* 5}$ |  | 630 | 710 | 800 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal applied motor capacity [kW] |  | 630 | 710 | 800 |  |
| Rated capacity [kVA] *1 |  | 891 | 1044 | 1127 |  |
| Rated current [A] |  | 1170 | 1370 | 1480 |  |
| Overload capability |  | $150 \%$ of the rated current for 1 minute *2 |  |  |  |
|  | Main power input | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |
|  | Auxiliary control power input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |
|  | Auxiliary fan power input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |
|  | Allowable fluctuation | Voltage: +10 to -15\%, Frequency: +5 to -5\% |  |  |  |
| Braking system, braking torque |  | Braking system: Depending on power regenerative braking (PWM converter), resistance regenerative braking (braking unit) <br> Braking torque: 150\% |  |  |  |
| Carrier frequency [ kHz$]^{*}{ }^{4}$ |  | 2 kHz |  |  |  |
| Approx. mass [kg] |  | $135 \times 3$ | $135 \times 3$ | $135 \times 3$ |  |
| Enclosure |  | IP00 open type |  |  |  |

The MD spec above applies when Function code $\mathrm{F} 80=0,2$, or 3 . The keypad display shows "HD", however, when $\mathrm{F} 80=$ 0 or 2. (Initial value $=0$ )
*1 This specification applies when the rated output voltage is 440 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 Operating synchronous motors other than Fuji Electric's standard synchronous motor (GNF2 type series) at low carrier frequency may cause demagnetization due to heating of the permanent magnet by output current harmonics. Always confirm the motor's allowable carrier frequencies.
*5 A set of three phase-specific stacks (Type: FRN___BVG1S-4 $\square$ ) for $\mathrm{U}, \mathrm{V}$ and W phases constitutes a single inverter unit. (One unit each for output phases $\mathrm{U}, \mathrm{V}$, and W)

## 3-phase 690V series

## Standard stack

| Type: FRN___SVG1S-69口 | 90 | 110 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 | 450 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal applied motor <br> capacity [kW] ${ }^{* 5}$ | 90 | 110 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 | 450 |
| Rated capacity [kVA] ${ }^{* 1}$ | 120 | 155 | 167 | 192 | 258 | 317 | 353 | 394 | 436 | 490 | 550 |
| Rated current [A] | 100 | 130 | 140 | 161 | 216 | 265 | 295 | 330 | 365 | 410 | 460 |
| Overload capability | $150 \%$ of the rated current for 1 minute ${ }^{* 2}$ |  |  |  |  |  |  |  |  |  |  |
|  | Main power input | Refer to "Diode rectifier specifications" (section 6.2.2). |  |  |  |  |  |  |  |  |  |

The MD spec above applies when Function code $\mathrm{F} 80=0$, 2, or 3 . The keypad display shows "HD", however, when F80 = 0 or 2 . (Initial value $=0$ )
*1 This specification applies when the rated output voltage is 690 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 575 to $600 \mathrm{~V}, 50 \mathrm{~Hz} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 Operation at frequencies lower than the allowable carrier frequency of the synchronous motor may cause demagnetization due to heating of the permanent magnet by output current harmonics. Always confirm your synchronous motor's allowable carrier frequencies.
*5 This nominal applied motor capacity assumes the use of a 690 V motor. When you use a motor with different voltage specifications or want to choose a motor more accurately, make sure that the inverter's rated current is higher than or equal to the motor's rated current.

### 2.1.1.2 LD spec (for light overloads)

## 3-phase 400V series

Standard stack

| Type | : FRN__ SVG1S-4■ | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 315 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal applied motor capacity [kW] |  | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 315 | 355 |
| Rated capacity [kVA] ${ }^{* 1}$ |  | 57 | 69 | 85 | 114 | 134 | 160 | 192 | 231 | 287 | 316 | 356 | 396 | 445 | 495 |
| Rated current [A] |  | 75 | 91 | 112 | 150 | 176 | 210 | 253 | 304 | 377 | 415 | 468 | 520 | 585 | 650 |
| Overload capability |  | 110\% of the rated current for 1 minute ${ }^{*}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Main power input | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Auxiliary control power input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Auxiliary fan power input | - |  |  |  |  | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |  |  |  |  |  |
|  | Allowable fluctuation | Voltage: +10 to $-15 \%$, Frequency: +5 to $-5 \%$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Braking system, braking torque |  | Braking system: Depending on power regenerative braking (PWM converter), resistance regenerative braking (braking unit) <br> Braking torque: 110\% |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Carrier frequency [kHz] ${ }^{* 4}$ |  | 2 kHz |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approx. mass [kg] |  | 30 | 30 | 30 | 37 | 37 | 45 | 45 | 95 | 95 | 95 | 125 | 135 | 135 | 135 |
| Enclosure |  | IP00 open type |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Phase-specific stack



The above specifications apply when Function code F80 = 1 (LD spec).
*1 This specification applies when the rated output voltage is 440 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 Operating synchronous motors other than Fuji Electric's standard synchronous motor (GNF2 type series) at low carrier frequency may cause demagnetization due to heating of the permanent magnet by output current harmonics. Always confirm the motor's allowable carrier frequencies.
*5 A set of three phase-specific stacks (Type: FRN___BVG1S-4 $\square$ ) for $U, V$ and $W$ phases constitutes a single inverter unit. (One unit each for output phases $\mathrm{U}, \mathrm{V}$, and W.)

## 3-phase 690V series

## - Standard stack

| Type | : FRN | 90 | 110 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal applied motor capacity [kW] ${ }^{* 5}$ |  | 110 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 | 450 |
| Rated capacity [kVA] ${ }^{* 1}$ |  | 155 | 167 | 192 | 258 | 281 | 353 | 394 | 436 | 490 | 550 |
| Rated current [A] |  | 130 | 140 | 161 | 216 | 235 | 295 | 330 | 365 | 410 | 460 |
| Overload capability |  | $110 \%$ of the rated current for 1 minute *2 |  |  |  |  |  |  |  |  |  |
|  | Main p | Refer to "Diode rectifier specifications" (section 6.2.2). |  |  |  |  |  |  |  |  |  |
|  | Auxilia <br> input | Single-phase, 575 to 690 V, $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |  |  |
|  | Auxilia | Single-phase, 660 to 690 V, $50 \mathrm{~Hz} / 60 \mathrm{~Hz}, 575$ to $600 \mathrm{~V}, 50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ *3 |  |  |  |  |  |  |  |  |  |
|  | Allowa | Voltage: +10 to $-15 \%$, Frequency: +5 to $-5 \%$ |  |  |  |  |  |  |  |  |  |
| Braking system, braking torque |  | Braking system:Depending on power regenerative braking (PWM converter), resistance regenerative braking <br> (braking unit). <br> Braking torque: $\quad 150 \%$ |  |  |  |  |  |  |  |  |  |
| Carrier frequency [kHz] *4 |  | 2 kHz |  |  |  |  |  |  |  |  |  |
| Approx. mass [kg] |  | 45 | 45 | 95 | 95 | 95 | 135 | 135 | 135 | 135 | 135 |
| Enclosure |  | IP00 open type |  |  |  |  |  |  |  |  |  |

The above specifications apply when Function code F80 $=1$ (LD spec).
*1 This specification applies when the rated output voltage is 690 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 575 to $600 \mathrm{~V}, 50 \mathrm{~Hz} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 Operation at frequencies lower than the allowable carrier frequency of the synchronous motor may cause demagnetization due to heating of the permanent magnet by output current harmonics. Always confirm your synchronous motor's allowable carrier frequencies.
*5 This nominal applied motor capacity assumes the use of a 690 V motor. When you use a motor with different voltage specifications or want to choose a motor more accurately, make sure that the inverter's rated current is higher than or equal to the motor's rated current.

### 2.1.2 Multi-drive system

To drive a motor of 315 kW or above, you can combine multiple units of the FRENIC-VG in conjunction.
Observe the specifications given in this section.

### 2.1.2.1 MD spec (for medium overloads)

## 3-phase 400V series

■ Direct parallel connection (2 or $\mathbf{3}$ parallel systems)

| Type: FRN___SVG1S-4 $\square$ | 200 | 220 | 280 | 220 | 280 | 280 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of parallel systems | 2 |  |  | 3 |  |  |
| Nominal applied motor capacity [kW] | 355 | 400 | 500 | 630 | 710 | 800 |
| Rated current [A] | 716 | 789 | 988 | 1183 | 1482 | 1482 |
| Rated capacity [kVA] ${ }^{* 1}$ | 545 | 601 | 752 | 901 | 1129 | 1129 |
| Overload capability | 150\% of the rated current for 1 minute *2 |  |  |  |  |  |
| ¢ ${ }^{\text {¢ }}$ Main power input | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |  |  |
| Auxiliary control power input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |
| Auxiliary fan power input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |  |  |
| $\triangle$ Allowable fluctuation | Voltage: +10 to $-15 \%$, Frequency: +5 to $-5 \%$ |  |  |  |  |  |
| Braking system, braking torque | Braking system: Depending on power regenerative braking (PWM converter, power regenerative), resistance regenerative braking (braking unit). <br> Braking torque: 150\% |  |  |  |  |  |
| Carrier frequency [kHz] | 2 kHz |  |  |  |  |  |
| Approx. mass [kg] | $95 \times 2$ | $125 \times 2$ | $135 \times 2$ | $125 \times 3$ | $135 \times 3$ | $135 \times 3$ |
| Enclosure | IP00 open type |  |  |  |  |  |

- Phase-specific stack + direct parallel connection (2 or 3 parallel systems)

| Type: FRN__ BVG1S-4 $\square^{*} 4$ | 630 | 630 | 800 | 630 | 710 | 800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of parallel systems | 2 |  |  | 3 |  |  |
| Nominal applied motor capacity [kW] | 1000 | 1200 | 1500 | 1800 | 2000 | 2400 |
| Rated current [A] | 2223 | 2223 | 2812 | 3335 | 3905 | 4218 |
| Rated capacity [kVA] ${ }^{* 1}$ | 1694 | 1694 | 2143 | 2541 | 2976 | 3214 |
| Overload capability | $150 \%$ of the rated current for 1 minute *2 |  |  |  |  |  |
| $\stackrel{\text { ¢ }}{ }$ Main power input | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |  |  |
| \% Auxiliary control power input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |
| $\stackrel{\rightharpoonup}{\vec{\partial}}$ Auxiliary fan power input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{*}$ |  |  |  |  |  |
| $\subseteq$ Allowable fluctuation | Voltage: +10 to $-15 \%$ (phase-to-phase unbalance rate within $2 \%{ }^{* 4}$ ), Frequency: +5 to $-5 \%$ |  |  |  |  |  |
| Braking system, braking torque | Braking system: Depending on power regenerative braking (PWM converter, power regenerative), resistance regenerative braking (braking unit). <br> Braking torque: $150 \%$ |  |  |  |  |  |
| Carrier frequency [kHz] | 2 kHz |  |  |  |  |  |
| Approx. mass [kg] | $135 \times 6$ | $135 \times 6$ | $135 \times 6$ | $135 \times 9$ | $135 \times 9$ | $135 \times 9$ |
| Enclosure | IP00 open type |  |  |  |  |  |

The MD spec above applies when Function code $\mathrm{F} 80=0,2$, or 3 . The keypad display shows "HD", however, when $\mathrm{F} 80=$ 0 or 2. (Initial value $=0$ )
*1 This specification applies when the rated output voltage is 440 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 A set of three phase-specific stacks (Type: FRN___BVG1S-4 $\square$ ) for $\mathrm{U}, \mathrm{V}$ and W phases constitutes a single inverter unit.
(Each of the U, V, W phases uses one stack, so six stacks for 2 parallel systems and nine stacks for 3 parallel systems are required.)
Note: Direct parallel connection requires the optional high-speed serial communication support terminal block (OPC-VG1-TBSI).

## 3-phase 690V series

- Direct parallel connection (2 or 3 parallel systems)

| Type: FRN___SVG1S-69 |  | 250 | 280 | 355 | 400 | 450 | 400 | 450 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of parallel systems |  | 2 |  |  |  |  | 3 |  |  |
| Nominal applied motor capacity [kW] |  | 450 | 500 | 630 | 710 | 800 | 1000 | 1200 |  |
| Rated current [A] |  | 504 | 561 | 694 | 779 | 874 | 1169 | 1311 |  |
| Rated capacity [kVA] ${ }^{* 1}$ |  | 602 | 670 | 829 | 930 | 1044 | 1397 | 1566 |  |
| Overload capability |  | $150 \%$ of the rated current for 1 minute *2 |  |  |  |  |  |  |  |
|  | Main power input | Refer to "Diode rectifier specifications" (section 6.2.2). |  |  |  |  |  |  |  |
|  | Auxiliary control power input | Single-phase, 575 to $690 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |
|  | Auxiliary fan power input | Single-phase, 660 to $690 \mathrm{~V}, 50 / 60 \mathrm{~Hz}, 575$ to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}{ }^{\text {* }}$ |  |  |  |  |  |  |  |
|  | Allowable fluctuation | Voltage: +10 to -15\%, Frequency: +5 to -5\% |  |  |  |  |  |  |  |
| Braking system, braking torque |  | Braking system: Depending on power regenerative braking (PWM converter, power regenerative), resistance regenerative braking (braking unit). <br> Braking torque: $150 \%$ |  |  |  |  |  |  |  |
| Carrier frequency [kHz] |  | 2 kHz |  |  |  |  |  |  |  |
| Approx. mass [kg] |  | $135 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 3$ | $135 \times 3$ |  |
| Enclosure |  | IP00 open type |  |  |  |  |  |  |  |

The MD spec above applies when Function code $\mathrm{F} 80=0,2$, or 3 . The keypad display shows "HD", however, when $\mathrm{F} 80=$ 0 or 2 . (Initial value $=0$ )
*1 This specification applies when the rated output voltage is 690 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 575 to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
Note: Direct parallel connection requires the optional high-speed serial communication support terminal block (OPC-VG1-TBSI).

### 2.1.2.2 LD spec (for light overloads)

## 3-phase 400V series

- Direct parallel connection (2 or 3 parallel systems)

| Type: FRN___SVG1S-4■ |  | 200 | 250 | 315 | 250 | 250 | 315 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of parallel systems |  | 2 |  |  | 3 |  |  |
| Nominal applied motor capacity [kW] |  | 400 | 500 | 630 | 710 | 800 | 1000 |
| Rated current [A] |  | 789 | 988 | 1235 | 1482 | 1482 | 1853 |
| Rated capacity [kVA] ${ }^{* 1}$ |  | 601 | 752 | 941 | 1129 | 1129 | 1412 |
| Overload capability |  | 110\% of the rated current for 1 minute *2 |  |  |  |  |  |
|  | Main power input | Refer to "Diode rectifier specifications" (section 6.2.2) and "PWM converter specifications" (section 6.3.2). |  |  |  |  |  |
|  | Auxiliary control power input | Single-phase, 380 to $480 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |
|  | Auxiliary fan power input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |  |  |
|  | Allowable fluctuation | Voltage: +10 to -15\%, Frequency: +5 to $-5 \%$ |  |  |  |  |  |
| Braking system, braking torque |  | Braking system: Depending on power regenerative braking (PWM converter, power regenerative), resistance regenerative braking (braking unit). <br> Braking torque: 110\% |  |  |  |  |  |
| Carrier frequency [ kHz ] |  | 2 kHz |  |  |  |  |  |
| Approx. mass [kg] |  | $95 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 3$ | $135 \times 3$ | $135 \times 3$ |
| Enclosure |  | IP00 open type |  |  |  |  |  |

Phase-specific stack + direct parallel connection (2 or 3 parallel systems)


The above specifications apply when Function code F80 = 1 (LD spec).
*1 This specification applies when the rated output voltage is 440 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
*4 A set of three phase-specific stacks (Type: FRN___BVG1S-4■) for $\mathrm{U}, \mathrm{V}$ and W phases constitutes a single inverter unit. (Each of the U, V, W phases uses one stack, so six stacks for 2 parallel systems and nine stacks for 3 parallel systems are required.)

Note: Direct parallel connection requires the optional high-speed serial communication support terminal block (OPC-VG1-TBSI).

## 3-phase 690V series

Direct parallel connection (2 or 3 parallel systems)

| Type: FRN___SVG1S-69 | 250 | 315 | 355 | 400 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of parallel systems | 2 |  |  |  | 3 |  |
| Nominal applied motor capacity [kW] | 500 | 630 | 710 | 800 | 1000 | 1200 |
| Rated current [A] | 561 | 694 | 779 | 874 | 1169 | 1311 |
| Rated capacity [kVA] ${ }^{* 1}$ | 670 | 829 | 930 | 1044 | 1397 | 1566 |
| Overload capability | 110\% of the rated current for 1 minute *2 |  |  |  |  |  |
| Main power input | Refer to "Diode rectifier specifications" (section 6.2.2). |  |  |  |  |  |
| 0 Auxiliary control power <br> Bo input | Single-phase, 575 to $690 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |
| 읃 Auxiliary fan power input | Single-phase, 660 to $690 \mathrm{~V}, 50 / 60 \mathrm{~Hz}, 575$ to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}{ }^{* 3}$ |  |  |  |  |  |
| Allowable fluctuation | Voltage: +10 to $-15 \%$, Frequency: +5 to $-5 \%$ |  |  |  |  |  |
| Braking system, braking torque | Braking system: Depending on power regenerative braking (PWM converter, power regenerative), resistance regenerative braking (braking unit). <br> Braking torque: $150 \%$ |  |  |  |  |  |
| Carrier frequency [kHz] | 2 kHz |  |  |  |  |  |
| Approx. mass [kg] | $135 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 2$ | $135 \times 3$ | $135 \times 3$ |
| Enclosure | IP00 open type |  |  |  |  |  |

The above specifications apply when Function code $\mathrm{F} 80=1$ (LD spec).
*1 This specification applies when the rated output voltage is 690 V .
*2 When the inverter output frequency converted is less than 1 Hz , the inverter may trip due to an overload earlier than this specification depending on the ambient temperature or other conditions.
*3 For 575 to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$, connector switching is required inside the inverter.
Note: Direct parallel connection requires the optional high-speed serial communication support terminal block (OPC-VG1-TBSI).

### 2.2 Common specifications

This section provides common specifications of the FRENIC-VG.

### 2.2.1 Installation environment and conformity with standards

| Item |  |  | Explanation |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Provided as standard | Stop function | Safe Torque Off (STO)* <br> The external digital input signal (termin output circuit on the hardware side so | al EN1 or EN2) forcibly turns off the inverter's hat the motor coasts to a stop. |
|  | Conformity with standards |  | (1) US and Canadian Safety Standards <br> (2) European Safety Standards IEC/EN <br> (3) Machinery Directive <br> (4) Low Voltage Directive <br> IEC/EN <br> (5) EMC Directives | UL, cUL (UL508C, C22.2 No. 14) <br> (400V series only) <br> 61800-5-2: SIL2 <br> 62061: SIL2 <br> 13849-1: PL-d <br> 60204-1: Stop category 0 <br> 61800-5-1 (Over voltage category: 3) <br> 61800-3, IEC/EN 61326-3-1 <br> on) EMC-filter (optional): Category C3 <br> ity) 2nd Env. |
|  | Installation location (Note 1) |  | - Shall be installed indoor (free from corrosive gases, flammable gases, dusts, oil mist). Pollution degree 2: IEC60664-1 <br> - Shall not be exposed to direct sunlight. |  |
|  | Ambient temperatures |  | -10 to $+40^{\circ} \mathrm{C}$ |  |
|  | Ambient humidity |  | 5 to 95\% RH (without condensation) |  |
|  | Altitude (Note 2) |  | - Lower than $1,000 \mathrm{~m}$ (For use in an altitude between 1,001 to $3,000 \mathrm{~m}$, the output current should be derated.) <br> - In an altitude between 2,001 to $3,000 \mathrm{~m}$, the insulation of the control circuit is degraded from reinforced insulation to basic one. |  |
|  | Vibration |  | Compliance standards: IEC61800-2 <br> Amplitude 0.3 mm : 2 to 9 Hz <br> $1 \mathrm{~m} / \mathrm{s}^{2}$ <br> : 9 to 200 Hz | Compliance standards: IEC61800-5-1 Amplitude $0.075 \mathrm{~mm}: 10$ to less than 57 Hz 1G $: 57$ to 150 Hz |
|  | Storage temperature |  | -25 to $+70^{\circ} \mathrm{C}\left(-10\right.$ to max. $+30^{\circ} \mathrm{C}$ for long-term storage) |  |
|  | Storage humidity |  | 5 to $95 \% \mathrm{RH}$ (without condensation) |  |

(Note 1) Do not install the inverter in an environment where it may be exposed to lint, cotton waste or moist dust or dirt which will clog the heat sink of the inverter.
If the inverter is to be used in such an environment, install it in a dustproof panel of your system.
(Note 2) Insulation and cooling (heat radiation) are dependent on the density of air.
Due to the atmospheric pressure, insulation breakdown easily occurs and the dielectric strength decreases. In an altitude of 2,001 to $3,000 \mathrm{~m}$, therefore, the insulation of the control circuit is degraded from reinforced insulation to basic one.
In addition, as the air is thin, the cooling effect (radiation effect) decreases so that the temperature of the heat generating devices such as inverter increases.
If you install the inverter in an altitude above $1,000 \mathrm{~m}$, apply an output current derating factor as listed in Table 2.2.1-1.

Table 2.2.1-1: Output current derating factor in relation to altitude

| Altitude | Output current derating factor |
| :--- | :--- |
| $1,000 \mathrm{~m}$ or lower | 1.00 |
| 1,001 to $1,500 \mathrm{~m}$ | 0.97 |
| 1,501 to $2,000 \mathrm{~m}$ | 0.95 |
| 2,001 to $2,500 \mathrm{~m}$ | 0.91 |
| 2,501 to $3,000 \mathrm{~m}$ | 0.88 |

### 2.2.2 Control methods

This section outlines the motor drive controls and methods.

| Item |  |  | Explanation |
| :---: | :---: | :---: | :---: |
|  | For induction motor |  | - Vector control with a speed sensor <br> - Vector control without a speed sensor <br> - V/f Control |
|  | For synchronous motor |  | Vector control with a speed sensor (incl. magnetic pole position detection) |
|  | Test mode |  | Simulation mode |
|  | Single drive |  | - Standard stack: A single standard stack drives a single motor. <br> - Phase-specific stack: A set of three phase-specific stacks drives a single motor. <br> (The control printed circuit board is mounted on the V-phase stack. As a master, the V-phase stack controls two slave stacks (U- and W-phase ones). <br> (Available under vector control with/without a speed sensor and V/f control) |
|  |  | Multiwinding motor drive | Drives a multiwinding motor (Number of windings: 2 to 6 ). <br> Note that the same number of inverters as the number of windings is required. (Available only under vector control with a speed sensor) The option OPC-VG1-TBSI should be used. |
|  |  | Direct parallel connection | Drives a single motor (single winding) with two or three inverters. (Available under vector control with a speed sensor and V/f control of induction motors) <br> The option OPC-VG1-TBSI should be used. |
|  |  | Phase-specific stack (Multi-drive function) | Drives a multiwinding motor of a large capacity with two or more inverters of phase-specific stack type. <br> Direct parallel connection is possible. <br> The option OPC-VG1-TBSI should be used. |

Figure 2.2.2-1 shows the skeleton configuration for drive systems.


Figure 2.2.2-1: Stack configuration summary by driving method

### 2.2.3 Control performance

The table below lists the control performance specifications of motors.

| Item |  |  |  | Explanation |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Setting resolution | Speed command | Analog setting: $\quad 0.005 \%$ of maximum speed Digital setting: $\quad 0.005 \%$ of maximum speed |
|  |  |  | Torque command, Torque current command | 0.01\% of the rated torque |
|  |  | Control accuracy | Speed | Analog setting: $\quad \pm 0.1 \%$ of maximum speed (at $25 \pm 10^{\circ} \mathrm{C}$ ) <br> Digital setting: $\quad \pm 0.005 \%$ of maximum speed (at -10 to $+40^{\circ} \mathrm{C}$ ) |
|  |  |  | Torque | $\pm 3 \%$ of the rated torque (when a dedicated motor is in use) |
|  |  | Control response speed |  | 100 Hz |
|  |  | Maximum speed |  | 150 Hz (when converted to the inverter output frequency) |
|  |  | Speed control range |  | 1: 1500 (When the base speed is $1500 \mathrm{r} / \mathrm{min}$ : 1 to $1500 \mathrm{r} / \mathrm{min}$ to maximum speed *1) <br> 1: 6 (Constant torque range: Constant output range) |
|  |  | Setting resolution | Speed command | Analog setting: $\quad 0.005 \%$ of maximum speed Digital setting: $\quad 0.005 \%$ of maximum speed |
|  |  |  | Torque command, Torque current command | 0.01\% of the rated torque |
|  |  | Control accuracy | Speed | Analog setting: $\quad \pm 0.1 \%$ of maximum speed (at $25 \pm 10^{\circ} \mathrm{C}$ ) <br> Digital setting: $\quad \pm 0.1 \%$ of maximum speed (at -10 to $+40^{\circ} \mathrm{C}$ ) |
|  |  |  | Torque | $\pm 5 \%$ of the rated torque |
|  |  | Control response speed |  | 20 Hz |
|  |  | Maximum speed |  | 150 Hz (when converted to the inverter output frequency) |
|  |  | Speed control range |  | 1: 250 (When the base speed is $1500 \mathrm{r} / \mathrm{min}$ : 6 to $1500 \mathrm{r} / \mathrm{min}$ to maximum speed ${ }^{* 1}$ ) <br> 1: 4 (Constant torque range: Constant output range) |
|  | $\begin{aligned} & \text { 유 } \\ & \text { O} \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | Setting resolution |  | $\begin{array}{ll}\text { Analog setting: } \quad 0.005 \% \text { of maximum frequency } \\ \text { Digital setting: } & 0.005 \% \text { of maximum frequency }\end{array}$ |
|  |  | Output frequency control accuracy |  | Analog setting: $\quad \pm 0.2 \%$ of maximum output frequency (at $25 \pm 10^{\circ} \mathrm{C}$ ) <br> Digital setting: $\pm 0.01 \%$ of maximum output frequency (at -10 to $+40^{\circ} \mathrm{C}$ ) |
|  |  | Maximum frequency |  | 150 Hz |
|  |  | Control range |  | 0.2 to 150 Hz <br> 1: 4 (Constant torque range: Constant output range) |
|  |  | Setting resolution | Speed command | Analog setting: $\quad 0.005 \%$ of maximum speed Digital setting: $\quad 0.005 \%$ of maximum speed |
|  |  |  | Torque command, Torque current command | 0.01\% of the rated torque |
|  | $\begin{aligned} & 0 \\ & \frac{1}{3} \\ & \frac{3}{3} \end{aligned}$ | Control accuracy | Speed | Analog setting: $\quad \pm 0.1 \%$ of maximum speed (at $25 \pm 10^{\circ} \mathrm{C}$ ) <br> Digital setting: $\quad \pm 0.005 \%$ of maximum speed (at -10 to $+40^{\circ} \mathrm{C}$ ) |
|  | 읃 |  | Torque | $\pm 3 \%$ of the rated torque (when a dedicated motor is in use) |
|  | $\bigcirc$ | Control response speed |  | 100 Hz |
|  | $\begin{aligned} & \text { Oib } \\ & \hline 0 \mathrm{O} \end{aligned}$ | Maximum speed |  | 150 Hz (when converted to the inverter output frequency) |
|  |  | Speed control range |  | 1: 1500 (When the base speed is $1500 \mathrm{r} / \mathrm{min}$ : 1 to $1500 \mathrm{r} / \mathrm{min}$ to maximum speed ${ }^{* 1}$ ) |

*1 In the case of the PG pulse resolution 1024 P/R.

### 2.2.4 Control functions

The table below lists the outline of the control function specifications.

| Item | Explanation |
| :---: | :---: |
| Start/stop operation | - Keypad: and keys (for forward/reverse rotation), key (for stop) <br> - Digital input signals: "Switch forward/reverse operation," "Coast to a stop," "Reset alarm," "Select multistep speed," etc. |
| Speed command | - Keypad: <br> - External potentiometer: Three-terminal variable resistor (1 to $5 \mathrm{k} \Omega$ ) <br> - Analog input signals: 0 to $\pm 10 \mathrm{~V}, 4-20 \mathrm{~mA}$ <br> - UP/DOWN control: When the digital input signal UP or DOWN is ON, the speed increases or decreases, respectively. <br> - Multistep speed: The combination of the four digital input signals SS1, SS2, SS4 and SS8 enables 15 different speeds to be selected. <br> - Digital signal: parallel signals. <br> - Serial link operation: <br> RS-485 (provided as standard). Various communication options are available. <br> - Jogging operation: <br> (Fw) and (eve keys or digital input on [FWD] and [REV] terminals in jogging mode. |
| Speed detection | (1) Induction motor <br> - $+15 \mathrm{~V},+12 \mathrm{~V}$ complementary output PG (insulation type): Maximum frequency receivable: 100 kHz <br> - +5 V line driver output PG (insulation type) ${ }^{*}{ }^{*}$ : <br> Maximum frequency <br> receivable: 500 kHz <br> (2) Synchronous motor: +5 V line driver output PG (insulation type) <br> - ABS type ${ }^{* 2}$ : Maximum frequency receivable: 100 kHz <br> - ABZ type ${ }^{{ }^{*}}$ : Maximum frequency receivable: 500 kHz <br> - High-resolution serial transmission system (TS5667N253: TAMAGAWA SEIKI, Co., Ltd.) *3: 17 bits (one rotation) +16 bits (multi-rotation) <br> *1 When the option card OPC-VG1-PG (insulation type) is mounted. <br> *2 When the option card OPC-VG1-PMPG is mounted. <br> *3 When the option card OPC-VG1-SPGT is mounted. |
| Speed control | PI calculation with feed-forward terms. <br> Switching of control parameters: Control parameters are switchable by external signals. |
| Running status signal | Transistor output signals: "Inverter running," "Speed arrival," "Speed detected," <br>  "Inverter overload early warning," "Torque limiting," etc. <br> Analog output signals: "Motor speed," "Output voltage," "Torque," "Load factor," etc. |
| Acceleration/deceleration time | Specifies the acceleration/deceleration time for a run command to the motor (soft start/stop). <br> - Four independent settings can be made for each of acceleration and deceleration. <br> - S-curve acceleration/deceleration can be selected in addition to linear acceleration/ deceleration |
| Speed setting gain | Proportional relationship between analog speed setting and motor speed can be specified in the range of 0 to $200 \%$. |
| Jump speed | Jump speed (3 points) and jump hysteresis width (1 point) can be specified. |
| Auto search for idling motor speed | Automatically searches for the idling motor speed to be harmonized and starts to drive it without stopping it. |
| Auto-restart after momentary power failure | Possible to restart the inverter after a momentary power failure without stopping the motor depending on the restart mode setting. |
| Slip compensation control | Compensates for decrease in speed according to the load for stabilized operation. (Available for IM under V/f control.) |
| Droop control | The motor speed droops in proportion to output torque. (Not available under V/f control.) |



[^2]
### 2.2.5 Configuration/display functions

This section outlines the configuration and display functions.

*1 Available when the ROM version is $\mathrm{H} 1 / 20021$ or later.

| Item |  |  | Explanation |
| :---: | :---: | :---: | :---: |
|  | When a light alarm occurs |  | The light-alarm display " 1 <br> The inverter retains the cause of the light alarm to display it. |
|  | When an alarm occurs |  | The following contents display by items. <br> - The inverter retains the latest and the last 10 alarm codes and the latest and the last three pieces of alarm detailed information to display them. <br> - It also retains the detailed contents of the latest and the last 3 alarms (including light alarms) to display them. <br> - The calendar clock function retains the date and time when an alarm occurred to display them. <br> Precision: $\pm 27$ seconds $/$ month ( $\mathrm{Ta}=25^{\circ} \mathrm{C}$ ) <br> Data retention period: At least 5 years (at surrounding temperature of $25^{\circ} \mathrm{C}$ ) |
|  | Historical trace *2 |  | Reads out the sampling data held in the inverter and shows it graphically. Sampling interval: $62.5 \mu \mathrm{~s}$ to 1 s |
|  | Real-time trace *2 |  | Reads out the current data of the running inverter and shows it graphically in real-time. <br> Sampling interval: 1 ms to 1 s |
|  | Traceback |  | Reads out the sampling data held in the inverter and shows it graphically when an alarm has occurred. <br> Sampling interval: $62.5 \mu$ s to 1 s ( $400 \mu \mathrm{~s}$ for sampling data except current) <br> The sampling data is retained in the memory by the backup battery. <br> Data retention period: At least 5 years (at the surrounding temperature $25^{\circ} \mathrm{C}$ ) |
|  | Operation monitor *2 |  | I/O monitor, system monitor, alarm history monitor, etc. |
|  | Configuration of function codes |  | Shows the configuration of the function codes, as well as enabling editing, transmitting, comparing, and initialization. |
| Charge lamp |  |  | Lights when DC power is applied to the inverter unit. Lights when only control power is ON . |
|  | Common functions |  | - Retains and displays the cumulative life of the main circuit capacitor and the cumulative run time of cooling fans. <br> - Retains and displays the inverter operation time. <br> - Retains and displays the maximum output current and the maximum internal temperature for the past one hour. |
|  | RS-485 |  | I/O terminals for RS-485 communication. <br> Up to 31 inverter units can be connected in multi-drop connection. <br> Half-duplex system |
|  | USB |  | Accessible from the front, connector type: mini B USB 2.0 Full Speed |
|  | VG7 | Function code data | Selecting the VG7 compatible mode makes it possible to use the VG7 function codes as is on the FRENIC-VG (except function codes for the VG7 3rd motor). Possible to read out VG7 function code data using the FRENIC-VG Loader and write it as is into the FRENIC-VG. (Except special inverter versions.) |
|  |  | Various communications tools | T-Link, SX-bus, and CC-Link are fully compatible with the VG7 so that software in the upper PLC is available as is. (Except special inverter versions.) |

*2 Available in the paid-for version of FRENIC-VG Loader (WPS-VG1-PCL).

### 2.2.6 Protective functions

The table below lists the name of the protective functions, their description, and what appears on the LED monitor. If an alarm code appears on the LED monitor, remove the cause of activation of the protective function referring to Chapter 11 "Troubleshooting."

| Item | $\quad$Related <br> function <br> code |  |  |
| :--- | :--- | :--- | :--- |
| DC fuse blown | If a fuse in the main DC circuit blows due to a short circuit in the IGBT <br> circuit or other reason, this protective function displays the error to prevent <br> the secondary damage. The inverter could be broken, so immediately <br> contact your Fuji Electric representative. | Display |  |
| DC fan lock | This function is activated when the DC fan stops. |  |  |

*1 Available when the ROM version is $\mathrm{H} 1 / 20021$ or later.

| Item | Explanation | Display | Related function code |
| :---: | :---: | :---: | :---: |
| Operation error | This function is activated： <br> －If two or more network options（T－Link，SX－bus，E－SX bus，and CC－Link） are mounted． <br> －If the SW configuration is the same on two or more PG options． <br> －If auto tuning（Function code $\mathbf{H 0 1 ) ~ i s ~ a t t e m p t e d ~ w h e n ~ a n y ~ o f ~ t h e ~ d i g i t a l ~}$ input signals BX，STOP1，STOP2 and STOP3 is ON． <br> －If auto tuning is selected with Function code H01 but the key on the keypad is not pressed within 20 seconds． | Eー言 | H01 |
| Output wiring fault | This function is activated if the wires in the inverter output circuit are not connected during auto－tuning． | E－7 | H01 |
| A／D converter error | This function is activated if an error occurs in the A／D converter circuit． | EーG |  |
| Speed not agreed | This function is activated if the deviation between the speed command （reference speed）and the motor speed（detected or estimated speed） becomes excessive． <br> The detection level and detection time can be specified with function codes． | に－9 | $\begin{aligned} & \text { E43, E44, } \\ & \text { E45, } \\ & \text { H108, H149 } \end{aligned}$ |
| UPAC error＊1 | This function is activated：if the UPAC option hardware fails；if a communications error with main unit controller occurs；or the backup battery is run out． | E－イ7 |  |
| Inter－inverter communications link error | This function is activated if a communications error occurs in the inverter－to－inverter communications link using a high－speed serial communication terminal block（option）． | にーム | H107 |
| Hardware error | This function is activated upon detection of an LSI failure on the printed circuit board． | に－イ゙ |  |
| Mock alarm | An alarm can be simulated by inputting an external signal（FTB），by operating the keypad，or by using FRENIC－VG Loader． | E－－ | $\begin{aligned} & \hline \text { E01-E14 } \\ & \text { H108, H142 } \end{aligned}$ |
| Start delay | This function is activated when the torque current command value exceeds the specified level（ $\mathbf{H} 140$ ）and the detected or estimated speed value drops below the specified stop speed（F37），and then the state is kept for the specified duration（H141）． <br> The detection level and detection time can be specified with function codes． | L Lill | $\begin{aligned} & \text { H108, } \\ & \text { H140, H141 } \end{aligned}$ |
| Under voltage | This function is activated if the DC intermediate circuit voltage drops to the insufficient voltage detection level or below for reasons such as a drop in the power supply voltage．Note that，if F14 is set to 3,4 or 5 ，no alarm is output even if the direct intermediate circuit voltage drops．（Auto－restart after momentary power failure） <br> Under voltage detection level <br> － 400 V series： 360 Vdc <br> － 690 V series： 470 Vdc | し＇ı＇ | F14 |
| NTC thermistor wire break error | This function is activated if the thermistor wire breaks when the NTC thermistor is selected with Function code P30／A31／A131 for motor M1／M2／M3． <br> This function works even at extremely low temperatures（approx．$-30^{\circ} \mathrm{C}$ or below）． | 11て | $\begin{aligned} & \text { P30, } \\ & \text { A31, A131, } \\ & \text { H106 } \end{aligned}$ |
| Overcurrent | This function stops the inverter output when the output current to the motor exceeds the overcurrent level of the inverter．When a synchronous motor is controlled，the function is also activated if the current output to the synchronous motor exceeds the overcurrent protection level（P44，P64， P164）． | ${ }_{\text {LIII }}$ |  |
| Heat sink overheat | This function is activated if the temperature surrounding the heat sink（that cools down the IGBTs）increases due to stopped cooling fans or other reason． | ！［－111） |  |

＊1 Available when the ROM version is $\mathrm{H} 1 / 20021$ or later．

| Item | Explanation | Display | Related function code |
| :---: | :---: | :---: | :---: |
| External alarm | This function stops the inverter with the protective function by digital input signal（THR）． <br> Connecting an alarm contact of external equipment such as a braking unit or braking resistor to the input terminal to which the THR signal is assigned activates this function according to the contact signal status． <br> The diode rectifier（RHD）can be protected from overheating by connecting the alarm output（for any alarm）to the diode rectifier（RHD）to the input terminal to which the THR signal is assigned． |  | $\begin{aligned} & \text { E01-E14, } \\ & \text { H106 } \end{aligned}$ |
| Inverter internal overheat | This function is activated if the temperature surrounding the control printed circuit board increases due to poor ventilation inside the inverter or other reason． |  |  |
| Motor overheat | This function is activated if the temperature detected by the NTC thermistor integrated in a dedicated motor for motor temperature detection exceeds the motor overheat protection level（Function code E30）． |  | E30，H106 |
| Motor 1 overload | This function is activated by the electronic thermal overload protection if the motor 1 current（inverter output current）exceeds the operation level specified by Function code F11． | ＇i11 ！ | F11，H106 |
| Motor 2 overload | This function is activated by the electronic thermal overload protection if the motor 2 current（inverter output current）exceeds the operation level specified by Function code A33． | －17\％ | A33，H106 |
| Motor 3 overload | This function is activated by the electronic thermal overload protection if the motor 3 current（inverter output current）exceeds the operation level specified by Function code A133． | ill | $\begin{aligned} & \text { A133, } \\ & \text { H106 } \end{aligned}$ |
| Inverter overload | This function is activated if the output current exceeds the overload characteristic of the inverse time characteristic． <br> It stops the inverter output depending upon the heat sink temperature and switching element temperature calculated from the output current． | －171！ | F80 |
| Output phase loss | This function detects a break in inverter output wiring during running and stops the inverter output． <br> （Available under vector control for IM with a speed sensor．） | －ハイ11 | $\begin{aligned} & \text { H103, P01 } \\ & \text { A01, A101 } \end{aligned}$ |
| Overspeed | This function is activated if the motor speed（detected or estimated speed） exceeds 120\％（adjustable with Function code H90）of the maximum speed （F03／A06／A106）． | 年年 | H90 |
| Overvoltage | This function is activated if the DC intermediate circuit voltage exceeds the overvoltage detection level for reasons such as a rise in the power supply voltage，or increase in braking power from the motor． <br> Note that the inverter cannot be protected from excessive voltage（high voltage，for example）supplied by mistake． <br> －Overvoltage detection level <br> － 400 V series： 820 Vdc <br> －690V series： 1230 Vdc | ！ill＇， |  |
| PG wire break | This function is activated if a wire breaks in the PA／PB circuit on the PG terminal or in the PGP／PGM power supply circuit．It does not work under vector control without a speed sensor or under V／f control． This function is also activated if the use of the PG interface card （OPC－VG1－PG，OPC－VG1－PMPG）is attempted with PG signal disconnection or incorrect wiring． | ！ | H104 |
| E－SX bus tact synchronizatio n error | This error occurs when the tact cycle of the E－SX bus of the MICREX－SX SPH3000 and the inverter control cycle are out of synchronization with each other． | A1， | H108 |
| Toggle abnormality error | The inverter monitors 2－bit signals of toggle signal 1 TGL1 and toggle signal 2 TGL2 which are sent from the PLC．When the inverter receives no prescribed change pattern within the time specified by H144，this error occurs． | A1， | H107 |


| Item | Explanation | Display | Related function code |
| :---: | :---: | :---: | :---: |
| Light alarm (warning) | This function displays " $/ 2-\vdash_{1}^{\prime \prime \prime}$ " on the keypad if a failure or warning registered as a light alarm occurs. It outputs the light alarm signal on the $Y$ terminal but it does not issue an alarm output (for any alarm) (30A/B/C), so the inverter continues to run. <br> Light alarm objects that can be registered (selectable individually) <br> Motor overheat (OH4), Motor overload (OL1 to OL3), <br> NTC thermistor wire break error (nrb), External alarm ( OH 2 ), <br> RS-485 communications error (Er5), Network error (Er4), <br> Toggle abnormality error (ArF), Mock alarm (Err), DC fan lock (dFA), <br> Speed mismatch (Er9 ), E-SX error (ArE), <br> Motor overheat early warning (MOH), <br> Motor overload early warning (MOL), <br> Lifetime alarm (LiF), Heat sink overheat early warning (OH), Inverter overload early warning (OL), Battery life expired (BaT), Start delay (LOC) <br> Light alarm objects can be checked on the keypad. |  | H106-H111 |
| Surge protection | This function protects the inverter against surge voltages which might appear between one of the power lines, using surge absorbers connected to the main circuit power terminals (L1/R, L2/S, L3/T) and control power terminals (RO, TO). | - |  |
| Functional safety card error *1 | Protective function for functional safety cards. For more information, refer to the functional safety card instruction manual (INR-SI47-1541). |  |  |

*1 Available when the ROM version is $\mathrm{H} 1 / 20021$ or later.

Note: All protective functions are automatically reset if the control power voltage drops to a level at which inverter control circuit operation can no longer be sustained.

- The inverter retains the latest and the last 10 alarm codes and the latest and the last three pieces of alarm detailed information. However if the DC voltage between main circuit input terminals $\mathrm{P}(+), \mathrm{N}(-)$ is lower than necessary level, alarm information will not be saved.
- Stoppage due to a protective function can be reset by the RST key on the keypad or turning OFF and then ON between the X terminal (to which RST is assigned) and the CM. This action is invalid if the cause of an alarm is not removed.
- If there are multiple alarms, the inverter cannot reset until the causes of all the alarms are removed. (The causes of alarms not removed can be checked on the keypad.)
- When an alarm categorized as a light alarm occurs, the 30A/B/C does not operate.


### 2.3 Motor specifications

### 2.3.1 Dedicated motor specifications (induction motor with a sensor)

### 2.3.1.1 Standard specifications for three-phase 400V series

| Dedicated motor rated output (kW) |  | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 300 | 315 | 355 | 400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Applicable motor type (MVK_) |  | 8187A | 8207A | 8208A | 9224A | 9254A | 9256A | 9284A | 9286A | 528 KA | 528LA | 531FA | 531GA | 531HA | 535GA | 535GA | 535HA | 535JA |
| Moment of inertia of rotor $\left[k g \cdot \mathrm{~m}^{2}\right.$ ] |  | 0.34 | 0.41 | 0.47 | 0.53 | 0.88 | 1.03 | 1.54 | 1.77 | 1.72 | 1.83 | 2.33 | 2.52 | 2.76 | 5.99 | 5.99 | 6.53 | 7.18 |
| Rotor GD ${ }^{2}$ [kg•m²] |  | 1.34 | 1.65 | 1.87 | 2.12 | 3.52 | 4.12 | 6.16 | 7.08 | 6.88 | 7.32 | 9.32 | 10.08 | 12.34 | 23.96 | 23.96 | 26.12 | 28.72 |
| Rated speed/Max. speed [r/min] |  | 1500/3000 |  |  | 1500/2400 |  | 1500/2000 |  |  |  |  |  |  |  |  |  |  |  |
| Vibration |  | V10 or less |  |  | V15 or less |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Voltage [V] | - |  |  | $400 \mathrm{~V} / 50 \mathrm{~Hz}, 400,440 \mathrm{~V} / 60 \mathrm{~Hz}$ |  |  |  |  | $\begin{gathered} 380,400,415 \mathrm{~V} / 50 \mathrm{~Hz}, \\ 400,440 \mathrm{~V} / 60 \mathrm{~Hz} \end{gathered}$ |  |  |  |  |  |  |  |  |
|  | Number of phases/poles | Three-phase, 4P |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Input power [W] | 150/210 |  |  | $\begin{aligned} & 80 / \\ & 120 \end{aligned}$ | 270/390 |  |  |  | 2200 |  | 3700 |  |  |  |  |  |  |
|  | Current [ A ] | 0.38/0.39 to 0.4 |  |  | $\begin{gathered} \hline 0.39 / \\ 0.4, \\ 0.4 \\ \hline \end{gathered}$ | 1.0/1.0,1.0 |  |  |  | 4.6/4.3,4.1 |  | 7.8/7.1,7.6 |  |  |  |  |  |  |
| Approx.mass [kg] |  | 235 | 280 | 296 | 380 | 510 | 570 | 710 | 760 | 1270 | 1310 | 1630 | 1685 | 1745 | 2230 | 2230 | 2310 | 2420 |

### 2.3.1.2 Common specifications

| Item |  |
| :--- | :--- |
| Insulation class, <br> number of poles | Class F, 4P |
| Terminal structure | Main terminal box (lug type): <br> Main circuit terminals x 3 or x 6, NTC thermistor terminal x 2 (for MVK8 series) or x 3 (for <br> MVK9 and MVK5 series; including one spare) <br> Auxiliary terminal box (terminal block): <br> Pulse encoder (PGP, PGM, PA, PB, SS), cooling fan (FU, FV, FW) |
| Mounting method | Foot mounted with bracket (IMB3), <br> Note: Contact your Fuji Electric representative for other mounting. |
| Degree of protection, <br> cooling method | IP44, totally enclosed forced-ventilation system with cooling fan motor. A cooling fan blows air <br> over the motor toward the drive-end. |
| Installation location | Indoors, 1000 m or less in altitude. |
| Ambient temperature, <br> humidity | -10 to +40ㅇ, 90\% RH or less (no condensation) |
| Finishing color | Munsell N5 |
| Standard conformity | MVK8 series: JEM1466 or JEC-2137-2000 MVK9 or MVK5 series: JEC-2137-2000 |
| Standard accessories | Pulse encoder (1024 P/R, +15 V, complementary output), NTC thermistor(s) (1 or 2), and <br> cooling fan |

Note 1: For applicable motors of 55 kW or above, the torque accuracy is $\pm 5 \%$. When higher accuracy is required, contact your Fuji Electric representative.
Note 2: For dedicated motors other than 4-pole ones with the base speed of $1500 \mathrm{r} / \mathrm{min}$, contact your Fuji Electric representative.

### 2.3.1.3 External dimensions of dedicated motors

Figure A


Figure C


Figure B


Figure D



Note 1: The MVK9224A ( 55 kW ) has an auxiliary terminal box for fan, in addition to the configuration shown in Figure B.
Note 2: Dimensional tolerance of rotary shaft height C $\mathrm{C} \leq 250 \mathrm{~mm}$ : 0 to $-0.5 \mathrm{~mm}, \mathrm{C}>250 \mathrm{~mm}$ : 0 to 1.0 mm

### 2.3.2 Dedicated motor specifications (synchronous motor with a sensor)

### 2.3.2.1 Standard specifications for three-phase 400V series

| Dedicated motor rated output [kW] |  | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Applicable motor type (GNF) |  | 2139A | 2165A | 2167A | 2185A | 2187A | 2207A | 2224B | 2226B | 2254B | 2256B |  |  |  |  |
| Moment of inertia of rotor ( $\mathrm{lkg} \cdot \mathrm{m}^{2}$ ] |  | 0.090 | 0.153 | 0.191 | 0.350 | 0.467 | 0.805 | 0.882 | 0.994 | 1.96 | 2.22 |  |  |  |  |
| Rotor GD ${ }^{2}$ <br> [kg•m²] |  | 0.360 | 0.610 | 0.763 | 1.401 | 1.868 | 3.220 | 3.53 | 3.98 | 7.84 | 8.88 |  |  |  |  |
| Base speed/Max. speed (r/min) |  | 1500/2000 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Rated current [A] |  | 57/54 | 72 | 83 | 100 | 135 | 158 | 198 | 232 | 273 | 340 | 369 | 420 | 480 | 520 |
| Vibration |  | V10 or less |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Voltage [V] <br> Frequency <br> [ Hz ] | $\begin{gathered} 200 \text { to } \\ 240 \mathrm{~V} \\ 50 / 60 \\ \mathrm{~Hz} \end{gathered}$ | 400 to $420 \mathrm{~V} / 50 \mathrm{~Hz}, 400$ to $440 \mathrm{~V} / 60 \mathrm{~Hz}$ |  |  |  |  | $\begin{gathered} 380,400,415 / 400,415,440,460 \mathrm{~V} \\ 50 / 60 \mathrm{~Hz} \end{gathered}$ |  |  |  |  |  |  |  |
|  | Number of phases/ poles | Three-p hase, 2P | Three-phase, 4P |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Input power [W] | 54 to $58 /$ 70 to 78 | 90/120 |  | 150/210 |  |  | 80/120 |  | 270/390 |  |  |  |  |  |
|  | Current [ A ] | $\begin{gathered} 0.18 / \\ 0.22 \text { to } \\ 0.21 \end{gathered}$ | $\begin{aligned} & 0.27 \text { I } \\ & 0.24 \text { to } 0.25 \end{aligned}$ |  | $\begin{aligned} & 0.38 / \\ & 0.39 \text { to } 0.4 \end{aligned}$ |  |  | $\begin{aligned} & 0.36,0.38,0.41 \\ & / 0.4,0.4,0.4,0.4 \end{aligned}$ |  | 0.95,0.95,1/1,1,1,1 |  |  |  |  |  |
| Approx.mass <br> [kg] |  | 127 | 170 | 192 | 247 | 325 | 420 | 520 | 580 | 760 | 810 |  |  |  |  |

### 2.3.2.2 Common specifications

| Item | Explanation |
| :---: | :---: |
| Insulation class, number of poles | Class F, 6P |
| Terminal structure | Main terminal box (lug type): Main circuit terminals $\times 3$ or $\times 6$, NTC thermistor terminal $\times 2$ or x 3 (for 110 kW or higher; including one spare) <br> Auxiliary terminal box (terminal block): Cooling fan (FU, FV, FW) |
|  | Pulse encoder (connector type) |
| Rotation direction | CCW when viewed from the drive side |
| Mounting method | Legs mounted (IMB3) Note: Contact your Fuji Electric representative for other mounting. |
| Overload resistance | 150\% for 1 minute |
| Time rating | S1 |
| Degree of protection, Cooling method | IP44, Totally enclosed forced-ventilation system with cooling fan motor. A cooling fan blows air over the motor toward the drive-end. |
| Installation location | Indoors, 1,000 m or less in altitude |
| Ambient temperature, humidity | -10 to $+40^{\circ} \mathrm{C}, 90 \% \mathrm{RH}$ or less (no condensation) |
| Noise | 30 kW to 90 kW : $80 \mathrm{~dB}(\mathrm{~A})$ or less at 1 m apart, 110 to 300 kW : $90 \mathrm{~dB}(\mathrm{~A})$ or less at 1 m apart |
| Vibration resistance | 6.86 m/s ${ }^{2}$ (0.7G) |
| Finishing color | Munsell N1.2 |
| Standard conformity | JEM 1487:2005 |
| Standard built-in parts | Pulse encoder (1024 P/R, +5 VDC, A, B, Z, U, V, W line driver output), one NTC thermistor (Two for 110 kW or above) and cooling fan |

### 2.3.2.3 External dimensions of dedicated motors

Shaft extension


## Figure $A$



Figure D


Figure B


Figure E



Note 1: Models of 110 kW output or above are exclusive to direct connection. For indirect connection, contact your Fuji Electric representative.
Note 2: Dimensional tolerance of rotary shaft height $C$ $\mathrm{C} \leq 250 \mathrm{~mm}$ : 0 to $-0.5 \mathrm{~mm}, \mathrm{C}>250 \mathrm{~mm}: 0$ to 1.0 mm

### 2.3.2.4 Exclusive cables for inverter connection



| Item | Specifications (Structure) |
| :---: | :---: |
| Connection example | *2 When the customer prepares the inverter connection cable, the shield (SS) of the PG shielded wire should be connected to CN15 at the motor side. For inverter side, no connection is required. |

Reference: Connectors and contact terminals recommended
The following specifications are recommended for customers who produce inverter connection cables.

| At the inverter side connector: $\begin{gathered}\text { 10320-52F0-008 } \\ \text { Sumitomo 3M Co., Ltd. }\end{gathered}$ | At the motor side connector contact terminal: JN1-22-22F-PKG100 <br> Japan Aviation Electronics Industry, Limited |
| :---: | :---: |
|  | Max. applicable wire size: AWG20 (Outer dia. of coated cable: $\varphi 1.5 \mathrm{~mm}$ or less) |
| At the motor side connector: JN2DW15SL (Straight plug connector) Japan Aviation Electronics Industry, Limited | At the motor side connector: JN2FW15SL1 (Angle plug connector) Japan Aviation Electronics Industry, Limited |
|  |  |

Note 1: The following specifications are recommended for PG shielded wires.

| Type | Braided, shielded wires Twisted-pair cable (Outer dia.: Approx. $\varphi 10$ ) |
| :--- | :--- |
| Number of cores | 14 or more |
| Dia. of lead | 0.2 to $0.3 \mathrm{~mm}^{2}$ |
| Outer dia. of coated cable | Max. $\varphi 1.5 \mathrm{~mm}$ |

Note 2: The PKG in contact terminal models denotes that 100 terminals are packed in bulk.
Note 3: Joint with contact terminals should be presoldered.

### 2.4 Connection diagrams and terminal functions

### 2.4.1 Connection diagrams

### 2.4.1.1 Standard stack

The connection example of the inverter (standard stack) is shown below.

（Note 1）For wiring protection，install the recommended circuit breaker（MCCB）or earth leakage breaker（ELCB）（with an overcurrent protection feature）on the input side（i．e．，the primary side）of the PWM converter or diode rectifier．Ensure that the circuit breaker capacity is equivalent to or lower than the recommended capacity．
（Note 2）Aside from the MCCB or the ELCB，install the recommended electromagnetic contactor（MC）as necessary as it will be used when disconnecting the power supply from the PWM converter or diode rectifier．Connect a surge absorber in parallel when installing a coil such as an MC or solenoid near the inverter．
（Note 3）To retain an alarm output signal issued on inverter＇s programmable output terminals by the protective function or to keep the keypad alive even if the main power has shut down，connect these terminals to the power supply lines．Without power supply to these terminals，the inverter can run．
（Note 4）Connect the fan power supply terminals to power source when capacity of inverter is above 90 kW ．
（Note 5）A grounding terminal for a motor．It is recommended that the motor be grounded via this terminal for suppressing inverter noise．
（Note 6）For wiring enclosed with $\begin{gathered}\sim \\ k-\lambda \\ k\end{gathered}$, use twisted or shielded wires．In principle，the shielded sheath of wires should be connected to ground．If the inverter is significantly affected by external induction noise，however， connection to $\mathrm{OV}(\lfloor M 】, 【 11 】, 【 T H C 】), ~ O V(I C M 】)$ may be effective to suppress the influence of noise． Keep the control circuit wiring away from the main circuit wiring as far as possible．（recommended： 10 cm or more）．When crossing the control circuit wiring with the main circuit wiring，set them at right angles．
（Note 7）The connection diagram shows factory default functions assigned to digital input terminals［X1］to［X9］， transistor output terminals［Y1］to［Y4］，relay contact output terminals［Y5A／C］，analog output terminal［AO1］to ［AO3］，and analog input terminals［Ai1］and［Ai2］．
（Note 8）Slide switches on the control printed circuit board（control PCB）．
（Note 9）The motor cooling fan voltage differs from motor to motor．Add a transformer as needed．

（Note 11）Use the auxiliary contact（manual reset）of the thermal relay to trip the MCCB or MC．
（Note 12）Jumper bars are mounted between safety terminals［EN1］／［EN2］and［PS］by factory default．To use the safety function，remove the jumper bars before connection of safety devices．
（Note 13）Diode rectifiers and PWM converter types are available for use as the inverter power supply（converter）． Additionally，selection of recommended peripherals matching the converter to be used is necessary．Refer to ＂Chapter 6 Converter System＂for details．
（Note 14）When used in combination with a PWM converter，be sure to connect the PWM converter and inverter auxiliary power input terminals（RO，TO）to the main power via contact b of the power supply electromagnetic contactor（MC1）．This is not necessary if used in combination with a diode rectifier．When using the product with a non－grounded power supply，it is necessary to install an insulated transformer．For more information， refer to＂6．3．15－（5）＂in Chapter 6.
（Note 15）Be sure to use the fuse（F1，F2）．Use the fuses on the $P(+)$ side for the 400 V series or on both the $P(+)$ and $N$ $(-)$ sides for the 690 V series．

### 2.4.1.2 Phase-specific stack

The following diagram shows the connection example of the phase-specific stack type, 630 to 800 kW (400V series) inverter. A single phase-specific stack consists of 3 units of the standard stack (4-frame size). Connections required in this case include stack-to-stack connections in addition to the connections described in "2.4.1.1 Standard stack". (The following example assumes that they are connected to a PWM converter.)

* Stack-to-stack connection cables (signal wires) are bundled with the product.

(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the connection diagram.
(Note 2) When used in combination with a PWM converter, be sure to connect the PWM converter and inverter auxiliary power input terminals (R0, T0) to the main power via contact b of the power supply electromagnetic contactor (52). This is not necessary if used in combination with a diode rectifier. When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#73 or \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Set the timer for 52T to 1 second.
(Note 6) Configure one of the inverter's terminals X1 to X9 for use by the external alarm (THR).
(Note 7) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.


### 2.4.2 Terminal functions

This section describes terminal functions of the inverter.

### 2.4.2.1 Terminal functions

| Symbol |  | Name | Functions |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { N } \\ & \text { U } \\ & \text { D } \\ & \text { N } \\ & \text { N } \end{aligned}$ | U, V, W | Inverter output terminal | Connects a three-phase motor. <br> For the stack type, one terminal connects to one phase (one stack). |
|  | P (+), N (-) | DC input terminal | To be used for connection to the DC link bus. Connect to the diode rectifier or PWM converter stack output terminals $\mathrm{P}(+)$ and $\mathrm{N}(-)$. |
|  | R0, T0 | Auxiliary control power input | Connects the same AC power lines as the main power input for a backup of the control circuit power supply. <br> For information on terminal ratings, refer to "4.5.3-(4) Control power auxiliary input terminals RO and TO" in Chapter 4. |
|  | R1, T1 | Auxiliary fan power input | To be used for an auxiliary power input to AC cooling fans in the inverter (90 kW or higher). No connection is required for a 75 kW or lower inverter. For information on terminal ratings, refer to "4.5.3-(5) Fan power auxiliary input terminals R1 and T1 (R3 and T3 on the converter side)" in Chapter 4. |
|  | $\begin{aligned} & \text { DCF1 } \\ & \text { DCF2 } \end{aligned}$ | Inputs for detection of fuse blown | Terminals for detecting a blowout of the DC fuse connected to the inverter main input power supply. <br> When the circuit between terminals [DCF1] and [DCF2] is OFF, the inverter detects the blowout of the DC fuse. <br> Remove the shorted piece and connect the DC fuse microswitch to use. |
| 은 응 흥 | - G | Grounding for inverter | Grounding terminal for inverter chassis. |
| $\begin{aligned} & \stackrel{\rightharpoonup}{\overrightarrow{0}} \\ & \stackrel{\rightharpoonup}{\bar{O}} \\ & \frac{0}{\sqrt{0}} \\ & \frac{c}{c} \end{aligned}$ | 13 | Power supply for potentiometer | Power supply for a speed command potentiometer (Variable resistor: 1 to $5 \mathrm{k} \Omega$ ) The potentiometer of $1 / 2 \mathrm{~W}$ rating or more should be connected. <br> Specifications: 10 VDC, 10 mA max. |
|  | 12 | Voltage input for speed setting | The speed is commanded according to the external analog voltage input. Specifications <br> - Reverse operation with $\pm$ signals: 0 to $\pm 10$ VDC/0 to maximum speed The maximum input is $\pm 15 \mathrm{VDC}$; however, the voltage out of the range of $\pm 10$ VDC is regarded as $\pm 10$ VDC. (Upper limit: $\pm 10$ VDC) <br> - Input impedance: $10 \mathrm{k} \Omega$ |
|  | $\begin{array}{\|l\|} \hline \mathrm{Ai} 1 \\ \mathrm{Ai} 2 \end{array}$ | Analog input 1 Analog input 2 | (1) Analog input voltage from external equipment. <br> Possible to assign various signal functions (Input signal off, Auxiliary speed setting 1, Torque limiter *), selected with Function codes E49 and E50 to these terminals. <br> (2) Only for terminal [Ai2], the input is switchable between voltage and current with the SW3 configuration. <br> (3) To use terminal [Ai2] for current input speed setting (N-REFC), turn SW3 to the I position, set F01 or C25 to "9" and set E50 to "26." <br> After that, check that the current input is normal on the I/O check screen*. <br> * For more information, refer to the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019). <br> Specifications <br> - Voltage input: 0 to $\pm 10 \mathrm{VDC}$, Input impedance: $10 \mathrm{k} \Omega$ The maximum input is $\pm 15 \mathrm{VDC}$; however, the voltage out of the range of $\pm 10$ VDC is regarded as $\pm 10$ VDC. (Upper limit: $\pm 10$ VDC) <br> - Current input (only on [Ai2]): Input impedance $250 \Omega$ The maximum input is 30 mADC ; however, the current out of the range of 20 mADC is regarded as 20 mADC . (Upper limit: 20 mADC ) |
|  | 11, M | Analog input common | Common for analog input signals ([12], [Ai1] and [Ai2]). <br> Isolated from other control circuit common terminals [CM], [CMY] and [PGM]. |




Figure 2.4.2-1: Circuit configuration using a relay contact
Using a programmable logic controller (PLC) to turn any of [FWD], [REV] and [X1] to [X9] ON or OFF

Figure 2.4.2-2 shows two examples of a circuit configuration using a programmable logic controller (PLC). In circuit (a), the slide switch SW1 is turned to SINK and in circuit (b), to SOURCE.
Circuit (a) uses an external power supply. When using this type of circuit, observe the following.

- Connect the + node of the external power supply (which should be isolated from the PLC's power) to terminal [PLC] of the inverter.
- Do not connect terminal [CM] of the inverter to the common terminal of the PLC.

(a) With the slide switch turned to SINK and an external power supply being used

(b) With the switch turned to SOURCE

Figure 2.4.2-2: Circuit configuration using a PLC
[4] For details about the slide switch configuration, refer to "2.4.2.2 Setting up the slide switches".

|  | Ao1 Ao2 Ao3 | Analog output 1 Analog output 2 Analog output 3 | Output of monitor signals with analog DC voltage. Various signals such as "Detected speed," "Speed setting," and "Torque current command" can be assigned to these terminals by setting Function codes E69 to E71. For more information, refer to " 4.3 Function code details" in Chapter 4 of the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019). <br> Specifications <br> - Voltage output: 0 to $\pm 10$ VDC, Connectable impedance: Min. $3 \mathrm{k} \Omega$ <br> - Gain adjustment range: 0 to $\pm 100$ times |
| :---: | :---: | :---: | :---: |
|  | M | Analog output Common terminals | Common terminals for analog output signals ([Ao1], [Ao2] and [Ao3]). Isolated from other control circuit common terminals [CM], [CMY] and [PGM]. |


|  | ymbol | Name | Functions |
| :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \mathrm{Y} 1 \\ & \mathrm{Y} 2 \\ & \mathrm{Y} 3 \\ & \mathrm{Y} 4 \end{aligned}$ | Transistor output 1 Transistor output 2 Transistor output 3 Transistor output 4 | Various signals such as "inverter running," "Speed valid," and "Speed agreement" can be assigned to these terminals by setting Function codes E15 to E18. <br> For more information, refer to "4.3 Function code details" in Chapter 4 of the separate volume "Unit Type Function Code Edition" (24A7-■-0019). <br> * It is possible to switch the operation mode for transistor output terminals [Y1]-[Y4] and [CMY] between "Active ON" (ON when the signal is output) and "Active OFF" (OFF when the signal is output). <br> Figure 2.4.2-3: Transistor output circuit <br> Note 1: When a transistor output drives a control relay, connect a surge-absorbing diode across relay's coil terminals. <br> Note 2: Through terminal [PLC], power can be supplied to the relay. Short-circuit between terminals [CMY] and [CM] in this case. <br> [Terminal PLC specifications] 24 VDC, Allowable voltage fluctuation range: 22 to 27 VDC, 100 mA max. |
|  | CMY | Transistor output common | Common terminal for transistor output signals. <br> Electrically isolated from terminals [CM], [11], [M], and [PGM]. |
| $\begin{aligned} & \stackrel{\rightharpoonup}{\partial} \\ & \stackrel{\rightharpoonup}{訁} \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{W}{L} \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { Y5A } \\ & \text { Y5C } \end{aligned}$ | General-purpose relay output | (1) The relay contact (1a) selects and outputs the same various signals as those from terminals [Y1] to [Y4]. <br> (2) It is possible to switch the operation mode for these terminals with Function code E28. <br> - When ON signal is issued, [Y5A]-[Y5C] is short-circuited (Excited: "Active ON"). <br> - When ON signal is issued, [Y5A]-[Y5C] is opened (Not excited: "Active OFF"). |
|  | $\begin{array}{\|l\|} \hline 30 A \\ 30 B \\ 30 C \end{array}$ | Alarm output (for any alarm) | (1) Outputs a contact signal (relay contact, 1C) when the protective function stops the inverter. <br> (2) It is possible to switch the operation mode for these terminals with Function code F36. <br> - When ON signal is issued, [30A]-[30C] is short-circuited (Excited: "Active ON"). <br> - When ON signal is issued, [30A]-[30C] is opened (Not excited: "Active OFF"). |
|  |  |  | [Contact output specification] <br> Contact rating: 250 VAC $0.3 \mathrm{~A} \cos \varphi=0.3,48$ VDC 0.5 A (resistance load) |

Note - The contact outputs (terminals Y5A/C, 30A/B/C) are mechanical contacts. Frequent ON/OFF operations cannot be permitted.
The guideline for the life of relay contacts is 200,000 times if turned ON/OFF at 1 second intervals at rated load. Signals turned ON/OFF at high frequency should be output from terminals Y1 to Y4.
Furthermore, even if using an AC power supply, the contact life may be shorter with loads for which the contact current direction is fixed (loads with half-wave rectifier circuit, etc., e.g., timers, power supply devices for motor electromagnetic brakes).
In cases such as this, instead of connecting the load directly to the contact output terminals, connect a control relay, etc. (separately installed) which satisfies load conditions to the contact output terminals, and then connect to the load via this relay.


### 2.4.2.2 Setting up the slide switches

Switching the slide switches (see Figure 2.4.2-4: Location of the slide switches on the control PCB) located on the PCB allows you to customize the operation mode of input/output terminals such as analog outputs.
To access the slide switches, remove the front cover so that you can see the control PCB. (Open also the keypad enclosure.)

1 For information on removing the front cover and opening/closing the keypad case, refer to "4.2.2.2 Procedure for removing and attaching the front cover" in Chapter 4.

Table2.4.2-1: Function of each slide switch


The following diagram shows the location of slide switches on the control PCB for the input/output terminal configuration.


Figure 2.4.2-4: Location of the slide switches on the control PCB

|  | SW1 | SW2 | SW3 | SW4 | SW5 | SW6 | SW7 <br> SW8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Factory default |  |  |  |  |  |  | $\square \square_{1}^{1}$ |
| - |  |  |  |  |  |  |  |

Note (1) Use a pointed tool (such as the tip of tweezers) to move the switch. Be careful not to touch other electronic components. Push the slider firmly to the edges as the connection is open when the slider is in the intermediate position. SW2 and SW5 are switches for the manufacturer, so please do not move the positions.
(2) When moving the switches, check that the direct intermediate circuit voltage between the $P(+)$ and $N(-)$ terminals of the major circuit has fallen to a safe voltage (+25 VDC or lower) using a tester after confirming that the LED monitor and the charge lamp have turned off and 10 minutes have elapsed from power off.

### 2.4.3 Multi-drive system connection diagrams

### 2.4.3.1 Direct parallel connection

In direct parallel connection, two or more inverter units drive one single-winding motor. Up to three inverter units can be connected in direct parallel connection.
For more information, refer to "9.4 Direct parallel connection system" in Chapter 9.

（Note 1）For wiring protection，install the converter－specific recommended circuit breaker（MCCB）or earth leakage breaker（ELCB）（with an overcurrent protection feature）on the input side（i．e．，the primary side）of the converter．Ensure that the circuit breaker capacity is equivalent to or lower than the recommended capacity．
（Note 2）Aside from the MCCB or the ELCB，install the converter－specific recommended electromagnetic contactor （MC）as necessary as it will be used when disconnecting the power supply from the converter．Connect a surge absorber in parallel when installing a coil such as an MC or solenoid near the inverter．
（Note 3）To retain an alarm output signal issued on inverter＇s programmable output terminals by the protective function or to keep the keypad alive even if the main power has shut down，connect these terminals to the power supply lines．Without power supply to these terminals，the inverter can run．
（Note 4）Connect to the fan power supply terminals for cases above 90 kW ．
（Note 5）A grounding terminal for a motor．It is recommended that the motor be grounded via this terminal for suppressing inverter noise．
（Note 6）For wiring enclosed with $\begin{gathered}\pi \\ k-\nu \\ -\nu\end{gathered}$ ，use twisted or shielded wires．In principle，the shielded sheath of wires should be connected to ground．If the inverter is significantly affected by external induction noise，however， connection to $\mathrm{OV}(\lfloor M \mathbf{I}$ ，【11】，【THC】）， OV （ICM】）may be effective to suppress the influence of noise． Keep the control circuit wiring away from the main circuit wiring as far as possible（recommended： 10 cm or more）．When crossing the control circuit wiring with the main circuit wiring，set them at right angles．
（Note 7）The connection diagram shows factory default functions assigned to digital input terminals［X1］to［X9］， transistor output terminals［Y1］to［Y4］，relay contact output terminals［Y5A／C］，analog output terminal［AO1］to ［AO3］，and analog input terminals［Ai1］and［Ai2］．
（Note 9）The motor cooling fan voltage differs from motor to motor．Add a transformer as needed．
（Note 10）©OV（IM】，【111，【THC】），OV（ICM】）are insulated inside the inverter unit．
（Note 11）Use the auxiliary contact（manual reset）of the thermal relay to trip the MCCB or MC．
（Note 13）Available converters include diode rectifiers and PWM converter types．Additionally，selection of recommended peripherals matching the converter to be used is necessary．Refer to＂Chapter 6 Converter System＂for details．
（Note 14）Direct parallel connection requires the optional high－speed serial communication support terminal block （OPC－VG1－TBSI）．The option comes with an optical cable（ 5 m ）．
If the optical cable in use is bent（at a curvature of 35 mm or smaller），an alarm（Inter－inverter communications

（Note 15）For the safety，configure the sequence circuit that causes all inverters running in direct parallel connection to coast to a stop（BX signal）when an inverter failure（heavy alarm）occurs．Do not assign BX signal via the communications link．
（Note 16）Configure the circuit that inputs a run command after the inverter ready－to－run signals on all inverters running in direct parallel connection are established．A run command and reset signal are valid only when they are entered to the master inverter．（There is no problem with them if entered via the communications link．）
（Note 17）Be sure to use the fuse（F）．Use the fuses on the $\mathrm{P}(+)$ side for the 400 V series or on both the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ sides for the 690V series．
（Note 18）When a motor is run in a direct parallel connection system，there is a restriction on the wiring length between the inverter and motor．
Note Refer to＂9．4．8 Wiring inductance＂and ensure that the wiring length between the inverter and motor is greater than the minimum wiring length．
（Note 19）When used in combination with a PWM converter，be sure to connect the PWM converter and inverter auxiliary power input terminals（ $\mathrm{RO}, \mathrm{TO}$ ）to the main power via contact $b$ of the power supply electromagnetic contactor（MC1）．This is not necessary if used in combination with a diode rectifier．When using the product with a non－grounded power supply，it is necessary to add an insulated transformer．
For more information，refer to item（5）in section＂6．3．15＂．

### 2.4.3.2 Multiwinding motor drive

Multiwinding motor drive system controls a special motor having more than one winding.
An inverter unit per motor winding is required. Generally, this system applies when VG7 or older inverter series are updated. (Vector control with a speed sensor is the only system which can be applied.)

（Note 1）For wiring protection，install the converter－specific recommended circuit breaker（MCCB）or earth leakage breaker（ELCB）（with an overcurrent protection feature）on the input side（i．e．，the primary side）of the converter．Ensure that the circuit breaker capacity is equivalent to or lower than the recommended capacity．
（Note 2）Aside from the MCCB or the ELCB，install the converter－specific recommended electromagnetic contactor （MC）as necessary as it will be used when disconnecting the power supply from the converter．Connect a surge absorber in parallel when installing a coil such as an MC or solenoid near the inverter．
（Note 3）To retain an alarm output signal issued on inverter＇s programmable output terminals by the protective function or to keep the keypad alive even if the main power has shut down，connect these terminals to the power supply lines．Without power supply to these terminals，the inverter can run．
（Note 4）Connect to the fan power supply terminals for cases above 90 kW ．
（Note 5）A grounding terminal for a motor．It is recommended that the motor be grounded via this terminal for suppressing inverter noise．
（Note 6）For wiring enclosed with be connected to ground．If the inverter is significantly affected by external induction noise，however， connection to $\mathrm{OV}(\lfloor M \mathbf{I}$ ，【11】，【THC】）， OV （ICM】）may be effective to suppress the influence of noise． Keep the control circuit wiring away from the main circuit wiring as far as possible（recommended： 10 cm or more）．When crossing the control circuit wiring with the main circuit wiring，set them at right angles．
（Note 7）The connection diagram shows factory default functions assigned to digital input terminals［X1］to［X9］， transistor output terminals［Y1］to［Y4］，relay contact output terminals［Y5A／C］，analog output terminal［AO1］to ［AO3］，and analog input terminals［Ai1］and［Ai2］．
（Note 9）The motor cooling fan voltage differs from motor to motor．Add a transformer as needed．
（Note 10）©（ IM】，【11】，【THC】），OV（ICM】）are insulated inside the inverter unit．
（Note 11）Use the auxiliary contact（manual reset）of the thermal relay to trip the MCCB or MC．
（Note 13）Available converters include diode rectifiers and PWM converter types．Additionally，selection of recommended peripherals matching the converter to be used is necessary．Refer to＂Chapter 6 Converter System＂for details．
（Note 14）Multiwinding motor drive requires the optional high－speed serial communication support terminal block （OPC－VG1－TBSI）．The option comes with an optical cable（ 5 m ）．
（Note 15）For the safety，configure the sequence circuit that causes all inverters driving a multiwinding motor to coast to a stop（ BX signal）when an inverter failure（heavy alarm）occurs．Do not assign BX signal via the communications link．
（Note 16）Configure the circuit that inputs a run command after the inverter ready－to－run signals on all inverters driving a multiwinding motor are established．A run command and reset signal are valid only when they are entered to the master inverter．（There is no problem with them if entered via the communications link．）
（Note 18）Be sure to use the fuse（F）．Use the fuses on the $\mathrm{P}(+)$ side for the 400 V series or on both the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ sides for the 690V series．
（Note 19）When used in combination with a PWM converter，be sure to connect the PWM converter and inverter auxiliary power input terminals（R0，T0）to the main power via contact b of the power supply electromagnetic contactor（MC1）．This is not necessary if used in combination with a diode rectifier．When using the product with a non－grounded power supply，it is necessary to add an insulated transformer．
For more information，refer to item（5）in section＂6．3．15＂．

### 2.5 External dimensions

### 2.5.1 List of the FRENIC-VG's external dimensions

## - 3-phase 400V series

| Standard stack capacity [kW] | Dimensions [mm] |  |  | Approx. mass [kg] | Figure | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | W | H | D |  |  |  |
| FRN30SVG1S-4 $\square$ | 226.2 | 740 | 406.3 | 30 | A |  |
| FRN37SVG1S-4 $\square$ |  |  |  |  |  |  |
| FRN45SVG1S-4 $\square$ |  |  |  |  |  |  |
| FRN55SVG1S-4 $\square$ |  | 880 |  | 37 | B |  |
| FRN75SVG1S-4 $\square$ |  |  |  |  |  |  |
| FRN90SVG1S-4 $\square$ |  |  |  | 45 |  |  |
| FRN110SVG1S-4■ |  |  |  |  |  |  |
| FRN132SVG1S-4■ |  | 1100 | 567.3 | 95 | C |  |
| FRN160SVG1S-4■ |  |  |  |  |  |  |
| FRN200SVG1S-4■ |  |  |  |  |  |  |
| FRN220SVG1S-4■ |  | 1400 |  | 125 | D |  |
| FRN250SVG1S-4■ |  |  |  | 135 |  |  |
| FRN280SVG1S-4■ |  |  |  |  |  |  |
| FRN315SVG1S-4■ |  |  |  |  |  |  |
| FRN630BVG1S-4■ |  |  |  | $135 \times 3$ | E | A set of three stacks constitutes a single inverter unit. |
| FRN710BVG1S-4■ |  |  |  |  |  |  |
| FRN800BVG1S-4■ |  |  |  |  |  |  |

- 3-phase 690 V series

| Standard stack capacity [kW] | Dimensions [mm] |  |  | Approx. mass [kg] | Figure | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | W | H | D |  |  |  |
| FRN90SVG1S-69 $\square$ | 226.2 | 880 | 406.3 | 45 | F |  |
| FRN110SVG1S-69■ |  |  |  |  |  |  |
| FRN132SVG1S-69■ |  | 1100 | 567.3 | 95 | C |  |
| FRN160SVG1S-69■ |  |  |  |  |  |  |
| FRN200SVG1S-69■ |  |  |  |  |  |  |
| FRN250SVG1S-69■ |  | 1400 |  | 135 | D |  |
| FRN280SVG1S-69■ |  |  |  |  |  |  |
| FRN315SVG1S-69■ |  |  |  |  |  |  |
| FRN355SVG1S-69■ |  |  |  |  |  |  |
| FRN400SVG1S-69■ |  |  |  |  |  |  |
| FRN450SVG1S-69■ |  |  |  |  |  |  |

### 2.5.1.1 Figure A (1-frame size: FRN30SVG1S-4 $\square$ to 45SVG1S-4 $\square$ )


[Unit: mm]

### 2.5.1.2 Figure B (2-frame size: FRN55SVG1S-4 $\square$ to 110SVG1S-4 $\square$ )


2.5.1.3 Figure C (3-frame size: FRN132SVG1S-4 $\square$ to 200SVG1S-4 $\square$, FRN132SVG1S-69 $\square$ to FRN200SVG1S-69■)

2.5.1.4 Figure D (4-frame size: FRN220SVG1S-4 $\square$ to 315SVG1S-4 $\square$, FRN250SVG1S-69 $\square$ to FRN450SVG1S-69 $\square$ )

2.5.1.5 Figure E (4-frame size: FRN630BVG1S-4 $\square$ to 800BVG1S-4 $\square$ )

2.5.1.6 Figure $F$ (2-frame size: FRN90SVG1S-69 $\square$ to 110SVG1S-69 $\square$ )

$4 \times \phi 18$ (Hanging hole)
[Unit: mm]

### 2.6 Generated loss

The following table shows inverter generated losses.
F26: Motor operating sound (carrier frequency) is $2[\mathrm{kHz}]$. (The carrier frequency is fixed at 2 kHz .)

| Power-based series | Type | Generated loss [W] |  |
| :---: | :---: | :---: | :---: |
|  |  | MD spec | LD spec |
| 3-phase 400V | FRN30SVG1S-4■ | 550 | 700 |
|  | FRN 37SVG1S-4 $\square$ | 700 | 850 |
|  | FRN 45SVG1S-4 $\square$ | 800 | 1000 |
|  | FRN55SVG1S-4■ | 1100 | 1450 |
|  | FRN75SVG1S-4■ | 1400 | 1600 |
|  | FRN90SVG1S-4■ | 1700 | 2000 |
|  | FRN110SVG1S-4 $\square$ | 2050 | 2400 |
|  | FRN132SVG1S-4 $\square$ | 2200 | 2650 |
|  | FRN160SVG1S-4 $\square$ | 2550 | 3100 |
|  | FRN200SVG1S-4 $\square$ | 3050 | 3350 |
|  | FRN220SVG1S-4 $\square$ | 3550 | 3950 |
|  | FRN250SVG1S-4 $\square$ | 3950 | 4350 |
|  | FRN280SVG1S-4 $\square$ | 4300 | 4750 |
|  | FRN315SVG1S-4 $\square$ | 4850 | 5350 |
|  | FRN 630BVG1S-4 $\square$ | 9300 | 10600 |
|  | FRN710BVG1S-4 $\square$ | 10350 | 11350 |
|  | FRN800BVG1S-4 $\square$ | 11400 | 14150 |
| 3-phase 690V | FRN90SVG1S-69■ | 1600 | 1950 |
|  | FRN110SVG1S-69■ | 2100 | 2400 |
|  | FRN132SVG1S-69 $\square$ | 2150 | 2500 |
|  | FRN160SVG1S-69■ | 2400 | 3050 |
|  | FRN200SVG1S-69■ | 3200 | 3500 |
|  | FRN250SVG1S-69■ | 4100 | 4500 |
|  | FRN280SVG1S-69■ | 4450 | 4950 |
|  | FRN315SVG1S-69■ | 4900 | 5400 |
|  | FRN355SVG1S-69■ | 3550 | 3950 |
|  | FRN400SVG1S-69■ | 4050 | 4500 |
|  | FRN450SVG1S-69■ | 4550 | - |

## FRENIC-

## Chapter 3 Transportation and Storage

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### 3.1 Transportation

This section explains the transportation and storage of the FRENIC-VG and converters.

### 3.1.1 Transportation in packed state

The packing form varies according to the type or order of the FRENIC-VG or converter.


Transportation in pile: Up to $\mathbf{3}$ packages can be loaded
<Vertical packing: Wood frame package>


Insertion positions of jaws (forks)

Transportation in pile: Not available

Figure 3.1-1: External appearance of package
Note 1) When you transport the package, place it on a pallet and hoist the pallet, or lift it using a fork lifter or a hand lifter, etc.

Note 2) Be sure not to transport the product by hooking wires to a crane as the product is stored in a cardboard or a wood frame. It will lead to the drop of the product.

### 3.1.2 Transportation in unpacked state

### 3.1.2.1 Transportation

This section explains the transportation of the unpacked product.
Be sure to transport the product in the state shown in Figure 3.1-2.


Figure 3.1-2: Transportation state for unpacked product

### 3.1.2.2 General caution

Before you start operating a crane, be sure to check the following:
(1) Use a crane with the sufficient capacity for the weight of the cabinet.
(2) Visually check that the hanging rings (eye bolts) are not loosened and/or cracked and that the screw sections are not bent and/or broken.
(3) Be sure to check the wires and ropes before using them. Do not use the wires and ropes listed below:
a) Those through which large current such as short-circuit current flowed
b) Those with external flaws such as spark marks and fire ball marks
c) Those of which wires are disconnected
d) Those which are significantly rusted
e) Those which are clearly abraded
f) Those of which the core steel is exposed or of which the twist is deformed
g) Those which are kinked (These wires and ropes are not acceptable even if they are repaired)
(4) If a wire comes into contact with any corner, cover the corner with a buffer material so that it will not be damaged or scratched.
(5) Upon loading and unloading, be sure not to suddenly move up and down the product. In addition, pay attention to the front and back, and left and right directions so that the product will not come into contact with any objects.
(6) During transportation, be careful not to drop and/or fall the product by vibration and at a curve.

### 3.1.2.3 Work procedure for lifting by crane

The work procedure to follow when you use a crane is explained below.

## Raising from the laying state

1-frame, 2 -frame sizes
When raising the unit from the horizontal position, attach wire ropes to two points on the FRENIC-VG's upper section and slowly pull up using the crane.

When pulling up, exercise caution as the bottom side may slide.

When raising the unit, face the front of the product and attach wire ropes to two points on the right side, as in the figure on the right.
(In the package, the right side of the product's front faces the top.)
 this direction.
(Same applies to 3-frame, 4-frame sizes)

## 3-frame, 4-frame sizes

When raising the unit from the horizontal position, place braces between the bar terminals and casters, and ensure that the unit is horizontal when mounted on the braces.

To ensure that the casters do not contact the ground, use braces with a height of 60 mm or higher. Next, attach wire ropes to two points on the FRENIC-VG's upper section and slowly pull up using the crane.

Note If the unit is stood up without using braces, a load will be applied to the casters, causing damage.

Furthermore, when standing the unit up, ensure that the bar terminals and casters do not contact the braces.
When pulling up, exercise caution as the bottom side may slide.
When raising the unit, face the front of the product and attach wire ropes to two points on the right side, as shown in the figure on the right.
(In the package, the right side of the product's front faces the top.)

## Lifting in the installed condition

Lift the FRENIC-VG as follows when it is installed on a cabinet.

## 1-frame, 2-frame sizes

Hook wires onto the front left and two rear right locations (viewed from the front) as shown on the right.

## 3-frame, 4 -frame sizes

Hook wires onto the front right and two rear right locations (viewed from the front) as shown on the right.


1-frame, 2-frame sizes


3-frame, 4-frame sizes

## Lifting in the horizontal condition

Transport the FRENIC-VG in its horizontal condition as follows.

## 1-frame, 2-frame sizes

Hook wires onto the three locations shown below.

## 3-frame, 4-frame sizes

Hook wires onto the four locations shown below.


1-frame, 2-frame sizes


3-frame, 4-frame sizes

### 3.1.3 Transportation after assembling the product into a cabinet

When you transport the FRENIC-VG, be extremely careful not to apply vibration and shock to it.
In the case of long distance transportation, do not transport the product using rollers, and be sure to transport it by lifting with a crane and the like.

### 3.1.3.1 Crane operation

When you transport the product using a crane or other heavy equipment, clear obstacles on the transportation route and follow the instructions given in "3.1.2.2 General caution".
(1) Figure 3.1-5 illustrates the methods of hooking wires. If there is only a single panel, use the method (a). Use the method (b) for 2 panels, and the method (c) for 3 panels.

(a) For single panel

(b) For 2 panels

(c) For 3 panels

Figure 3.1-5: How to hook wires
(2) As shown in Figure 3.1-5, hook a wire to each hanging ring. Be sure not to hook a single wire as shown in Figure 3.1-6. The hanging angle must be $60^{\circ}$ or less.
(3) Firstly, lift the product by approx. 30 mm to confirm the safety (the tension of wires and hanging angle, etc.) and verify that the cabinet is not tilted. Then, lift the product for transportation.
(4) When you lift down the cabinet, be sure to slowly lift it down in parallel with the floor.
(5) When anchors are attached, remove them before installation in principle. Such anchors as shown in Figure 3.1-8 can be removed after installation.


Figure 3.1-6: Incorrect hooking of wires


Figure 3.1-7: Tilt of cabinet (bad example)


Figure 3.1-8: Anchor

### 3.1.3.2 Transportation on rollers

When you transport the product on rollers, follow the procedure given below:
(1) Check the transportation route and clear obstacles.
(2) Give the workers clear instructions and signs for the work procedure and work method.
(3) In a place where the floor might get scratched, install protection plates in the traveling direction. As shown in Figure 3.1-9, protection plates must be placed as sprints or in the shape of "ハ".
(a) Bad example

Do not separate the plates.

(b) In the splint form

(c) In the shape of "ハ"


Figure 3.1-9: Layout of protection plates (protection of floor)
(4) Install rollers of which the diameter is approx. 50 mm and of which the length is 300 mm longer than the cabinet to the bottom of the cabinet, and slowly move the product following the instructions given below as checking the safety.
a) There must be always 3 or more rollers so that the cabinet will not tilt.
b) The rollers must protrude by 150 mm or more from the both ends of the cabinet during transportation.
c) Use a hammer to correct and cut rollers.
(5) When the traveling direction is changed, shift the protection plates little by little to the new direction as shown in Figure 3.1-11.


Figure 3.1-10: Transportation on rollers


Figure 3.1-11: Change of transportation direction

### 3.2 Check before use

Unpack the package and check the following:
An inverter and the following accessories are contained.
Accessories • Instruction manual

- CD-ROM (containing the FRENIC-VG User's Manual, FRENIC-VG Loader software (free version), and FRENIC-VG Loader Instruction Manual)

The inverter has not been damaged during transportation-there should be no dents or parts missing. The main and sub nameplates are attached to the inverter as shown in Figure 3.3-1 to -4. Check these nameplates to see that the inverter is exactly the type you ordered.

(a) Main Nameplate

## TYPE FRN30SVG1S-4J

SER.No. 28A456A0001BA
(b) Sub Nameplate

Figure 3.2-1: Nameplate

## TYPE: Inverter stack



The FRENIC-VG is available in two drive modes depending upon the inverter capacity: Medium Duty (MD) and Low Duty (LD) modes. Specifications in each mode are printed on the main nameplate.

Medium Duty: MD mode designed for medium duty load applications.
Overload capability: 150\% for 1 min. Continuous ratings = Capacity of inverters
Low Duty : LD mode designed for light duty load applications.
Overload capability: 110\% for 1 min. Continuous ratings = One rank or two ranks higher capacity of inverters
SOURCE : Input voltage, input current
OUTPUT : Number of output phases, rated output voltage, output frequency range
: Rated output capacity, rated output current, rated overload current
IP Code : IP protection level
SCCR : Short-circuit capacity
MASS Mass of the product in kilogram
SER.No. : Production number 28 A 456 A 0001 BA
232

C: Mark of conformity with European standards
: ML us usten : Mark of conformity with UL Standards and CSA Standards (cUL-listed for Canada)
: Mark of conformity with WEEE Directive

If you suspect the product is not working properly or if you have any questions about your product, contact your Fuji Electric representative.

### 3.3 External views

### 3.3.1 Overall external views

## ■ 3-phase 400 V series



Figure 3.3-1: FRN30-45SVG1S-4 $\square$ (Frame 1)


Figure 3.3-2: FRN55-110SVG1S-4 $\square$ (Frame 2)


Figure3.3-3: FRN132-200SVG1S-4 $\square$ (Frame 3)


Figure3.3-4: FRN220-315SVG1S-4 $\square$ (Frame 4)


Figure 3.3-5: FRN630-800BVG1S-4 $\square$ (Frame 4)

## 3-phase 690V series



Figure 3.3-6: FRN90-110SVG1S-69 $\square$ (Frame 2)


Figure 3.3-7: FRN132-200SVG1S-69 $\square$ (Frame 3)


Figure 3．3－8：FRN250－450SVG1S－69 $\square$（Frame 4）

## 3．3．2 Warning plate and warning label

| \．WARNING 公 |
| :---: |
| －RISK OF INJURY OR ELECTRIC SHOCK <br> －Refer to the instruction manual before installation and operation． <br> －Do not remove this cover while applying power． <br> －This cover can be removed after at least 10 min of power off and after the＂CHARGE＂lamp turns off． <br> －More than one live circuit．See instruction manual． <br> －Do not insert fingers or anything else into the inverter． <br> －Securely ground（earth）the equipment． <br> －High touch current． |
| \警告 |
| - 有可能引起受伤，触电 <br> - 安装运行之前请务必阅读操作说明书并遭照其指示 <br> - 通电中不要打开表面盖板 <br> - 断电 10 分钟以上，充电指示灯熄灭后才可打开表面盖板 <br> - 打开表盖时，要确认已经切断各路的辅助电源。（请参考说明书） <br> - 即使在安装了表面盖板时，也不要从缝隙间捅入手指或其他异物 <br> - 请正确接地 |
| ¢ 警告 |
| - けが，感電のおそれあり <br> - 据え付け運転時の前に，必ず取扱説明書を読んでその指示に従うこと。 <br> - 通電中は，表面力パーを開けないこと。 <br> - 表面カバーを開ける場合は，電源しや断後10分以上経過後チャーシランフカが消灯した のを碓認してから行うこと。 <br> －表面カバ一を開ける場合は，各補助電源もしゃ断していることを確認してから行うこと（取扱説明書を参照のこと）。 <br> －表面力バ一取付状態であっても，開口部より装置内部に指•異物等挿入しないこと。 －確実に接地をおこなうこと。 |
| Only type B of RCD is allowed． See manual for details． |



Figure 3．3－9：Warning plate and warning label

### 3.4 Environment for transportation / temporary storage

This section explains the environment for transportation and temporary storage after purchase.
Carefully note that the storage environment requirements differ depending on whether the product is stored temporarily or for a long time.

### 3.4.1 Transportation / temporary storage

Environment requirements for transportation and temporary storage are listed below.
Table 3.4-1: Transportation / temporary storage environment

| Item | Explanation | Avoid use in environments where abrupt changes in temperature <br> may cause condensation or freezing. |
| :--- | :--- | :--- |
| Storage temperature <br> (Note 1) | -25 to $+70^{\circ} \mathrm{C}$ |  |
| Relative humidity | 5 to $95 \%$ (Note 2) | Avoid exposure to dust, direct sunlight, corrosive gases, flammable gas, oil mist, steam, <br> water droplets and vibration. <br> Avoid exposure to excessive salt content. ( $0.01 \mathrm{mg} / \mathrm{cm}^{2}$ or less per year) |
| Atmosphere | 86 to 106 kPa (during storage) |  |
|  | 70 to 106 kPa (during transportation) |  |

(Note 1) Assuming comparatively short time storage, e.g., during transportation or the like.
(Note 2) Even if the humidity is within the specified requirements, avoid such places where the product will be subjected to sudden changes in temperature that will cause condensation or freeze to form.

## Points to note for temporary storage

(1) Do not leave the product directly on the floor.
(2) If the environment does not satisfy the specified requirements listed in Table 3.4-1, wrap the product in an airtight vinyl sheet or the like for storage.
(3) If the product is to be stored in a high-humidity environment, put a drying agent (such as silica gel) in the airtight package described in (2) above.

### 3.4.2 Long-term storage

You should store the product in the conditions given below if you do not use it for an extended period.
(1) The storage site must satisfy the requirements specified for temporary storage. However, for storage exceeding three months, the surrounding temperature range should be within the range from -10 to $30^{\circ} \mathrm{C}$. This is to prevent electrolytic capacitors in the product from deterioration.
(2) The package must be airtight to protect the product from moisture. Add a drying agent (such as silica gel) inside the package to maintain the relative humidity inside the package within $70 \%$.
(3) If the product has been installed to the equipment or cabinet at construction sites where it may be subjected to humidity, dust or dirt, then temporarily remove the product and store it in the environment specified in Table 3.4-1.

## Precautions for storage over 1 year

If the product has not been powered on for a long time, the property of the electrolytic capacitors may deteriorate. Power the product on once a year and keep the product powering on for 30 to 60 minutes. Do not connect the product to the load circuit (secondary side) or run it.
For details, see the "Long-Term Storage Manual" (SI47-1741■).

## Handling of drying agent

Drying agent type: Use Silica-Gel Type A Class 1.
Take out drying agent from the package and put it in a cloth bag. Clearly write "Drying Agent" on the bag and hang the bag above the control devices such as the electromagnetic switch and inverter using a cord. Hang the bag in a way that it does not contact the control devices. (If the control devices contact the bag over the long time, they will be rusted by moisture absorbed by the drying agent.)
Calculate the necessary quantity of the drying agent $\mathrm{W}[\mathrm{kg}]$ using the equation given below:

$$
W=N \bullet A \bullet M \quad[k g]
$$

N : The reference quantities of the drying agent is shown in the table below. These values are applicable when polyethylene film is used as a moisture-proof packing material.

| Relative humidity at <br> storage site | Reference quantity of drying <br> agent: $\mathrm{N}\left[\mathrm{kg} / \mathrm{m}^{2} \cdot\right.$ month] |
| :--- | :--- |
| $70 \% \mathrm{RH}$ or less | 0.05 |
| 71 to $90 \%$ RH | 0.25 |

A: Surface area of moisture-proof packing material [ $\mathrm{m}^{2}$ ]; internal area of control panel and operation panel
M : Effective period (in months) of the drying agent. It is recommended to put the drying agent for 6 months.

When you open the package after storage, be sure to remove the drying agent.
(If you power on the inverter as the drying agent is left inside, it might be melted.)

## FRENIC-VG

## Chapter 4 Installation and Wiring

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### 4.1 Precautions for installation

This section describes precautions about the installation environment, power supply system, and wiring of stack type inverters (FRENIC-VG and converters), and connections of peripheral equipment. Strictly observe the following precautions when handling stacks.

### 4.1.1 Installation environment

Install your stack type inverter in a location that complies with the installation environment requirements specified in "2.2.1 Installation environment and conformity with standards" in Chapter 2.
The product is basically designed to be installed in cabinets. It is recommended that they be installed in cabinets for safety reasons. To install the product in a special environment exceeding the specified range of specifications, it is necessary to design cabinets suitable for the environment, examine where stacks should be installed, and derate output.
(1) For further information, see "Chapter 12 Cabinet Construction" of this manual.

| Special environment | Possible problems | Examples of measures | Major applications |
| :---: | :---: | :---: | :---: |
| Corrosive gas, such as a sulfidizing gas | A corrosive gas, such as a sulfidizing gas, may cause the parts inside the stack type inverter to corrode, resulting in a malfunction. | Either of the following measures may be necessary: <br> - Mount the product in a cabinet of hermetic structure (IP6X level) or using an air purge mechanism. <br> - Place the product in a location free of the effect of such gases. | Paper manufacturing, sewage disposal, sludge treatment, tire manufacturing, gypsum manufacturing, metal processing, particular processes of textile manufacturing, etc. |
| Much conductive dust or foreign material (e.g. metal powder, cutting chips, carbon fiber, carbon dust) | If conductive dust or foreign material enters the product, it may cause a short circuit or another problem inside. | Either of the following measures may be necessary: <br> - Mount the product in a cabinet of hermetic structure. <br> - Place each product in a location free of the effect of conductive dust. | Wire drawing machines, general metal processing, extruding machines, printing machines, garbage incinerators, industrial waste treatment, etc. |
| Much fibrous dust or paper dust | Cooling efficiency may decrease due to the clogging of the cooling fin of the stack, or the electronic circuit may malfunction if fibrous dust or paper dust enters the product. | Any of the following measures against dust may be necessary. <br> - Adopt a cabinet of hermetic structure capable of shutting out dust. <br> - Adopt a cabinet design ensuring maintenance space for periodical cleaning of the cooling fin. <br> - Perform periodical maintenance. | Textile manufacturing, paper manufacturing, etc. |
| High humidity or much dew condensation | In an environment where a humidifier is installed to ensure the quality of workpieces or in an air-conditioned environment without a dehumidifying function, humidity may reach a high level or dew condensation may occur, resulting in a short circuit inside the product or an electronic circuit malfunction. | - Such a measure as the installation of a space heater inside the cabinet may be necessary. | Outdoor installation, film manufacturing lines, pumps, food processing, etc. |
| Vibration or shock exceeding the specified level | A shock produced when a carrier runs over a rail joint, or a vibration or shock exceeding the specified level caused by blasting at a construction site may cause damage to the structure of the product. | - Cushioning material or another vibration absorbing material may be required for the product installation area to ensure safety. | Installation on a carrier or self-propelled machine, ventilation at construction sites, pressing machines, etc. |
| Fumigation in export packaging | Halogen compounds, including methyl bromide used for fumigation, may corrode some parts inside the stack type inverter. | - When exporting the stack type inverter in a cabinet, pack it in fumigated wooden crates. <br> - When exporting the stack type inverter alone, use laminated veneer lumber (LVL). | Export to overseas countries |

### 4.1.2 Required ventilation

When installing the stack type inverter in a cabinet of IP20 or equivalent protection level, it is necessary to fulfill the air volume required by the stack type inverter in addition to the observance of the working temperature range. If the required air volume cannot be fulfilled, the FRENIC-VG or converter will generate unusual heat and cause an overheat protection alarm trip.
The tables below show the required air volume per stack for each of the FRENIC-VG inverter and converter models (or, for 630 kW and over, the required air volume per three stacks). Calculate the required air volume based on the number of stacks to be installed in a cabinet, and set ventilation.
[0] For further information, see "Chapter 12 Cabinet Construction".
Table 4.1.2-1: Required air volumes of the FRENIC-VG (inverters)

| Standard stack |  |  |  | Phase-specific stack |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Model (FRN) | Required air volume [ $\mathrm{m}^{3} / \mathrm{min}$ ] | Model (FRN) | Required air volume [ $\mathrm{m}^{3} / \mathrm{min}$ ] | Model (FRN) | Required air volume [ $\mathrm{m}^{3} / \mathrm{min}$ ] |
| 30SVG1S-4 $\square$ | 2.0 | 90SVG1S-69■ | 5.8 | 630BVG1S-4■ | 44.1 |
| 37SVG1S-4 $\square$ |  | 110SVG1S-69■ |  | 710BVG1S-4 $\square$ |  |
| 45SVG1S-4 $\square$ |  | 132SVG1S-69■ | 8.5 | 800BVG1S-4 $\square$ |  |
| 55SVG1S-4 $\square$ | 1.5 | 160SVG1S-69 $\square$ |  |  |  |
| 75SVG1S-4 $\square$ |  | 200SVG1S-69 $\square$ |  |  |  |
| 90SVG1S-4 $\square$ | 5.8 | 250SVG1S-69■ | 14.7 |  |  |
| 110SVG1S-4 $\square$ |  | 280SVG1S-69 $\square$ |  |  |  |
| 132SVG1S-4■ | 8.5 | 315SVG1S-69■ |  |  |  |
| 160SVG1S-4■ |  | 355SVG1S-69■ |  |  |  |
| 200SVG1S-4■ |  | 400SVG1S-69 $\square$ |  |  |  |
| 220SVG1S-4 $\square$ | 14.7 | 450SVG1S-69■ |  |  |  |
| 250SVG1S-4 $\square$ |  |  |  |  |  |
| 280SVG1S-4 $\square$ |  |  |  |  |  |
| 315SVG1S-4■ |  |  |  |  |  |

Table 4.1.2-2: Required air volumes of the converters

| Standard stack |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model (RHC) | volume <br> [ $\mathrm{m}^{3} / \mathrm{min}$ ] | Model (RHF/RHD) | volume [ $\mathrm{m}^{3} / \mathrm{min}$ ] | $\begin{gathered} \text { Model } \\ \text { (RHF/RHD) } \end{gathered}$ | volume <br> [ $\mathrm{m}^{3} / \mathrm{min}$ ] | Model (RHF/RHD) | volume [ $\mathrm{m}^{3} / \mathrm{min}$ ] |
| RHC132S-4D $\square$ | 8.5 | RHC132S-69D $\square$ | 8.5 | RHF160S-4D $\square$ | 14.7 | RHF160S-69D $\square$ | 14.7 |
| RHC160S-4D $\square$ |  | RHC160S-69D $\square$ |  | RHF220S-4D $\square$ |  | RHF220S-69D $\square$ |  |
| RHC200S-4D $\square$ |  | RHC200S-69D $\square$ |  | RHF280S-4D $\square$ |  | RHF280S-69D $\square$ |  |
| RHC220S-4D $\square$ | 14.7 | RHC250S-69D $\square$ | 14.7 | RHF355S-4D $\square$ |  | RHF355S-69D $\square$ |  |
| RHC280S-4D $\square$ |  | RHC280S-69D $\square$ |  | RHD200S-4D $\square$ | 8.5 | RHF450S-69D $\square$ |  |
| RHC315S-4D $\square$ |  | RHC315S-69D $\square$ |  | RHD315S-4D $\square$ | 14.7 | RHD220S-69D $\square$ |  |
|  |  | RHC355S-69D $\square$ |  |  |  | RHD450S-69D $\square$ |  |
|  |  | RHC400S-69D $\square$ |  |  |  |  |  |
|  |  | RHC450S-69D $\square$ |  |  |  |  |  |


| Phase-specific stack |  |
| :---: | :---: |
| Model (RHC) | volume <br> $\left[\mathrm{m}^{3} / \mathrm{min}\right]$ |
| RHC630B-4D $\square$ | 44.1 |
| RHC710B-4D $\square$ |  |
| RHC800B-4D $\square$ |  |

### 4.1.3 Installation direction and spacing to surroundings

The FRENIC-VG inverters and converters must be mounted only in the direction shown in Figure 4.1.3-1 (direction of the reading of the nameplate). For information on surrounding space, refer to Table 4.1.3-1 and Figure 4.1.3-2. Also, follow the space requirements shown in Table 4.1.3-1 when mounting stacks side by side.


Figure 4.1.3-1 : Mounting direction and peripheral space
Table 4.1.3-1: Surrounding space

|  |  | A | B | C | D | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Frame 1 | 10 | 10 | 300 | 350 | 50 |
|  | Frame 2 |  |  |  |  |  |
|  | Frame 3 |  |  |  |  | 20 |
|  | Frame 4 |  |  |  |  | 20 |
| Anoth | appliance | 20 | 20 | - | $\begin{gathered} \hline 350 \\ (100) \\ \hline \end{gathered}$ | 50 |

Table 4.1.3-2: Frame size and capacity

| Frame size | 400 V series | 690 V series |
| :---: | :---: | :---: |
| Frame 1 | 30 to 45 kW | - |
| Frame 2 | 55 to 110 kW | 90 to 110 kW |
| Frame 3 | 132 to 200 kW | 132 to 200 kW |
| Frame 4 | 220 to 315 kW <br> 630 to 800 kW | 250 to 450 kW | requirements

Note (1) Stacks cannot be mounted on top of each other.
(2) Only a DC fuse (fuse designated by Fuji Electric) can be mounted in space C (above the exhaust fan of the stack).
A general appliance capable of working at a temperature of up to $70^{\circ} \mathrm{C}$ can be mounted in this space. In this case, mount it so that it does not block the exhaust fan of the stack.
(3) The stack has an air intake in the lower area. Keep about $60 \%$ of the $350-\mathrm{mm}$ space in the lower area open. When installing an appliance in this space, keep a distance of at least 100 mm between it and the stack.


Figure 4.1.3-2: Spacing between phase-specific stacks (Frame 4: 630 to 800 kW )

Note (1) If space F exceeds 135 mm , the spacing between the stacks (U-phase, V-phase, and W-phase) is too large to connect the standard cable.
(2) When using direct parallel connection, connect the master and slave (or, for the phase-specific stack, $V$-phase) with the Optical fiber cable ( 5 m ). Therefore, the master and slave must be installed within the distance at which they can be connected
*The Optical fiber cable ( 5 m ) comes standard with the optional high-speed serial communication support terminal block (OPC-VG1-TBSI).

### 4.1.4 Stack derating by ambient temperature

In cases where the ambient temperature exceeds $40^{\circ} \mathrm{C}$, operation up to $55^{\circ} \mathrm{C}$ is possible if derating is considered. Carefully note that the derating curve differs depending on the product model.
Use the FRENIC-VG (inverter) 400 V series 30 to 75 kW and 630 to 800 kW , and all capacities of RHF (filter stack) $400 / 690 \mathrm{~V}$ series at ambient temperatures of up to $40^{\circ} \mathrm{C}$.

- FRENIC- VG (inverters)

| Standard stack |  |  |  | Phase-specific stack |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Model | Figure | Model | Figure | Model | Figure |
| FRN30SVG1S-4 $\square$ | (Not available) | FRN132SVG1S-4 $\square$ | A | FRN630BVG1S-4 $\square$ | (Not available) |
| FRN37SVG1S-4■ |  | FRN160SVG1S-4 $\square$ | B | FRN710BVG1S-4 $\square$ |  |
| FRN45SVG1S-4■ |  | FRN200SVG1S-4 $\square$ | D | FRN800BVG1S-4 $\square$ |  |
| FRN55SVG1S-4■ |  | FRN220SVG1S-4 $\square$ |  |  |  |
| FRN75SVG1S-4 $\square$ |  | FRN250SVG1S-4 $\square$ | A |  |  |
| FRN90SVG1S-4■ | D | FRN280SVG1S-4 $\square$ | B |  |  |
| FRN110SVG1S-4 $\square$ |  | FRN315SVG1S-4 $\square$ | D |  |  |
| FRN90SVG1S-69■ | C | FRN250SVG1S-69■ | E |  |  |
| FRN110SVG1S-69■ | E | FRN280SVG1S-69 $\square$ |  |  |  |
| FRN132SVG1S-69■ | C | FRN315SVG1S-69 $\square$ |  |  |  |
| FRN160SVG1S-69■ | D | FRN355SVG1S-69■ | B |  |  |
| FRN200SVG1S-69■ | E | FRN400SVG1S-69 $\square$ | C |  |  |
| - | - | FRN450SVG1S-69■ | D |  |  |

## - Converters

| Standard stack |  |  |  | Phase-specific stack |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Model | Figure | Model | Figure | Model | Figure |
| RHC132S-4D $\square$ | A | RHC220S-4D $\square$ | D | RHC630B-4D $\square$ | (Not available) |
| RHC160S-4D $\square$ | B | RHC280S-4D $\square$ | B | RHC710B-4D $\square$ |  |
| RHC200S-4D $\square$ | D | RHC315S-4D $\square$ | D | RHC800B-4D $\square$ |  |
| RHD200S-4D $\square$ | D | RHD315S-4D $\square$ | D |  |  |
| RHF160S-4D $\square$ |  | RHF280S-4D $\square$ |  |  |  |
| RHF220S-4D $\square$ | (Not available) | RHF355S-4D $\square$ | (Not available) |  |  |
| RHC132S-69D $\square$ | C | RHC250S-69D $\square$ | E |  |  |
| RHC160S-69D $\square$ | D | RHC280S-69D $\square$ |  |  |  |
| RHC200S-69D $\square$ | E | RHC315S-69D $\square$ |  |  |  |
| - | - | RHC355S-69D $\square$ | B |  |  |
|  |  | RHC400S-69D $\square$ | C |  |  |
|  |  | RHC450S-69D $\square$ | D |  |  |
| RHD220S-69D $\square$ | F | RHD450S-69D $\square$ | D |  |  |
| RHF160S-69D $\square$ | (Not available) | RHF280S-69D $\square$ | (Not available) |  |  |
| RHF220S-69D $\square$ |  | RHF355S-69D $\square$ |  |  |  |
| - | - | RHF450S-69D $\square$ |  |  |  |

Figure A


Figure C


Figure E


Figure $B$


Figure D


Figure $F$


Figure 4.1.4-1: Derating curve

### 4.2 Installation

### 4.2.1 Fixation points and terminal positions

### 4.2.1.1 Frame 1 and 2 size stacks (400V: $\mathbf{3 0}$ to $110 \mathrm{~kW}, 690 \mathrm{~V}$ : 90 to 110 kW )

## [1] Fixation points (common to Frame 1 and 2 sizes)

For Frame 1 and 2 sizes (400V series: 30 to 45 kW [Frame 1], 55 to 110 kW [Frame 2]. 690V series: 90 to 110 kW [Frame 2]), there are two supporting points for installation. When installing them in cabinets, securely fix them at these supporting points.
(1) For setting of the terminating resistor, refer to "4.2.2 Installing stacks in cabinets".
<Points of mounting>
(1) Fixing hole in the upper area of the back face ( $2 \times \varphi 10$ : M8 screw or stud bolt)
(2) Tapped hole for fixation in the lower area of the front face ( $2 \times \mathrm{M} 5-12$ (up to 25 ) when the recommended plate thickness of the attachment for fixation is 2.3 mm )


Figure 4.2.1-1: Fixation points for Frame 1 size ( 400 V : 30 to 45 kW )

When using the tapped holes for fixation in the front face to fix the stack, make attachments for fixation from sheet metal.

Provide an attachment for installation for each unit of the stack type inverter.


Figure 4.2.1-2: Attachment for fixing lower section (recommended)
<Dimensions for the attachment for fixing lower section>
The recommended dimensions of the attachment (front lower section) for fixing Frame 1 and 2 size ( 400 V : 30 to 110 kW , 690V: 90 to 110 kW ) stacks to the cabinet are shown below. This attachment should be used to fix the stacks individually.


Figure 4.2.1-3: Shape of attachment for fixing lower section
[2] Terminal positions and screw sizes (main circuit terminals)
■ Frame 1 size ( $400 \mathrm{~V}: 30$ to 45 kW ), models: FRN30SVG1S-4 $\square$ to FRN45SVG1S-4 $\square$
Unit: [mm] <Internal front view>
<Side face view: from the right side face>


DETAILS OFA


Figure 4.2.1-4: Terminal positions for Frame 1 size ( $400 \mathrm{~V}: 30$ to 45 kW )

Frame 2 size（ $400 \mathrm{~V}: 55$ to 110 kW ），models：FRN55SVG1S－4 $\square$ to FRN110SVG1S－4 $\square$
Unit：［mm］
＜Internal front view＞
＜Side face view：from the right side face＞


| A部詳細 |  | Fan power input terminal－ |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Terminal name | Terminal symbol | Screw size | Terminal tightening torque | Applicable crimped terminal size |
| Output terminal | U，V，W | M10 | $27 \mathrm{~N} \cdot \mathrm{~m}$ | R150－10／MAX |
| DC input terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |
| Grounding terminal | G |  |  |  |

Figure 4．2．1－5：Terminal positions for Frame 2 size（ 400 V ： 55 to 110 kW ）

Frame 2 size (690V:90 to 110 kW ), models: FRN90SVG1S-69 $\square$ to FRN110SVG1S-69 $\square$


| Terminal name | Terminal symbol | Screw size | Terminal tightening torque | Applicable crimped terminal size |
| :--- | :--- | :--- | :--- | :--- |
| Output terminal | U, V, W | M10 | $27 \mathrm{~N} \cdot \mathrm{~m}$ | R150-10/MAX |
| DC input terminal | P (+), N (-) |  |  |  |
| Grounding terminal | G |  |  |  |

Figure 4.2.1-6: Terminal positions for Frame 2 size (690V: 90 to 110 kW )

### 4.2.1.2 Frame 3 size ( 400 V : 132 to $200 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to $\mathbf{2 0 0} \mathrm{kW}$ )

## [1] Fixation points

For Frame 3 size ( 400 V series: 132 to 200 kW , 690 V series: 132 to 200 kW ), there are four supporting points for installation. When installing them in cabinets, securely fix them at these supporting points.

1 For setting of the terminating resistor, refer to "4.2.2 Installing stacks in cabinets".
<Points of mounting>
(1) Fixation plate provided in the upper area of the back face (with a set-in guide installed on the cabinet side)
(2) Fixation plate provided in the lower area of the back face (with a set-in guide installed on the cabinet side)
(3) Tapped hole for fixation in the upper area of the front face ( $2 \times \mathrm{M} 8-25$, when the recommended plate thickness of the attachment for fixation is 2.3 mm )
(4) Tapped hole for fixation in the lower area of the front face ( $2 \times \mathrm{M} 8-25$, when the recommended plate thickness of the attachment for fixation is 2.3 mm )


Figure 4.2.1-7: Fixation points for Frame 3 size (400V/690V: 132 to 200 kW )
When using the tapped holes for fixation in the front face to fix the stack, make attachments for fixation from sheet metal.
$\square$ Attachments for fixation of the same shape as the one shown in Figure 4.2.1-12: Attachment for fixing lower section (recommended) and Figure 4.2.1-13: Attachment for fixing upper section (recommended) can be used. (Refer to page 4-16.)

## [2] Terminal positions and screw sizes (main circuit terminals)

Frame 3 size ( $400 \mathrm{~V}: 132$ to 200 kW ), models: FRN132SVG1S-4 $\square$ to FRN200SVG1S-4 $\square$
<Internal front view>
<Side face view: from the right side face>


Note
To connect output terminals for Frame 3 size, use a relay bus bar provided on the cabinet side.
The relay bus bar should be fixed using an insulator.

| Terminal name | Terminal <br> symbol | Bolt size | Terminal <br> $\square$ tightening torque |
| :--- | :--- | :--- | :--- |
| Output terminal | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | M 12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | G |  |  |

Figure 4.2.1-8: Terminal positions for Frame 3 size (400V: 132 to 200 kW )

Frame 3 size (690V:132 to 200 kW ), models: FRN132SVG1S-69 $\square$ to FRN200SVG1S-69 $\square$


## Note

To connect output terminals for Frame 3 size, use a relay bus bar provided on the cabinet side.
The relay bus bar should be fixed using an insulator.

| Terminal name | Terminal <br> symbol | Bolt size | Terminal <br> $\square$ tightening torque |
| :--- | :--- | :--- | :--- |
| Output terminal | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | M 12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | G |  |  |

Figure 4.2.1-9: Terminal positions for Frame 3 size ( $690 \mathrm{~V}: 132$ to 200 kW )

### 4.2.1.3 Frame 4 size (400V: $\mathbf{2 2 0}$ to $\mathbf{8 0 0} \mathrm{kW}, 690 \mathrm{~V}$ : $\mathbf{2 5 0}$ to $\mathbf{4 5 0} \mathrm{kW}$ )

## [1] Fixation points

For Frame 4 size ( 400 V series: 220 to 800 kW , 690 V series: 250 to 450 kW ), there are four supporting points for installation. When installing them in cabinets, securely fix them at these supporting points.
[1] For setting of the terminating resistor, refer to "4.2.2 Installing stacks in cabinets".
<Points of mounting>
(1) Fixation plate provided in the upper area of the back face (with a set-in guide installed on the cabinet side)
(2) Fixation plate provided in the lower area of the back face (with a set-in guide installed on the cabinet side)
(3) Tapped hole for fixation in the upper area of the front face ( $2 \times \mathrm{M} 8-25$, when the recommended plate thickness of the attachment for fixation is 2.3 mm )
(4) Tapped hole for fixation in the lower area of the front face ( $2 \times \mathrm{M} 8-25$, when the recommended plate thickness of the attachment for fixation is 2.3 mm )


Figure 4.2.1-10: Fixation points for Frame 4 size ( 400 V : 220 to 315 kW, 690 V : 250 to 450 kW)


Figure 4.2.1-11: Fixation points for Frame 4 size ( 400 V : 630 to 800 kW )

When using the tapped holes for fixation in the front face to fix the stack, make attachments for fixation from sheet metal.


Figure 4.2.1-12: Attachment for fixing lower section (recommended)

## <Dimensions for the attachment for fixing lower section>

The recommended dimensions of the attachment (front lower section) for fixing Frame 3 and 4 size ( 400 V : 132 to 800 kW, 690V: 132 to 450 kW ) stacks to the cabinet are shown below. This attachment should be used to fix the stacks individually.


Figure 4.2.1-14: Attachment for fixing lower section

## <Dimensions for the attachment for fixing upper section>

The recommended dimensions of the attachment (front upper section) for fixing Frame 3 and 4 size ( 400 V : 132 to 800 kW, 690V: 132 to 450 kW ) stacks to the cabinet are shown below. Using this attachment, fix the stack type inverters together before putting them in the cabinet.



Recommended plate thickness: 2.3 mm

Figure 4.2.1-15: Attachment for fixing upper section
Note (1) This attachment should be applied to cabinets with width 800 and flat steel sheets bent to 45 degrees.
(2) For stack type inverters, your design should be based on the horizontal spacing (clearance) of 12 mm (assuming the use of a cabinet with a width of 800).
(3) A height of 35 mm is recommended for surfaces in contact with stack type inverters. If this recommended value is exceeded, the keyholes on the surface cover will be hidden, making cover removal impossible.

## <Position of the set-in guide hole for the back face lower fixation plate>

The following figure illustrates the position of the set-in guide hole for the attachment that supports the back face lower fixation plate for Frame 3 and 4 size ( 400 V : 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW ) stacks as well as the position of the screw clearance hole for stack type inverters.


Figure 4.2.1-16: Positions of the set-in guide hole for the back face lower fixation plate and the screw clearance hole for stack type inverters

Note (1) The figure above shows the dimensions for a single unit of stack type inverter.
(2) For stack type inverters, your design should be based on the horizontal spacing (clearance) of 12 mm (assuming the use of a cabinet with a width of 800).

## <Position of the set-in guide hole for the back face upper fixation plate>

■ Frame 3 size ( $\mathbf{4 0 0 \mathrm { V } : ~} 132$ to $200 \mathrm{~kW}, \mathbf{6 9 0 \mathrm { V }} \mathbf{1 3 2}$ to 200 kW )
The following figure illustrates the positions of the set-in guide hole for the back face upper fixation plate and the screw clearance hole for stack type inverters.


## - Frame $\mathbf{4}$ size ( $\mathbf{4 0 0 V}$ : $\mathbf{2 2 0}$ to $\mathbf{8 0 0} \mathrm{kW}, \mathbf{6 9 0 V}$ : $\mathbf{2 5 0}$ to $\mathbf{4 5 0} \mathbf{~ k W ) ~}$

The following figure illustrates the position of the set-in guide hole for the back face upper fixation plate.


Figure 4.2.1-17: Set-in guide hole for the back face upper fixation plate

Note (1) The figure above shows the dimensions for a single unit of stack type inverter.
(2) For stack type inverters, your design should be based on the horizontal spacing (clearance) of 12 mm (assuming the use of a cabinet with a width of 800).

## [2] Terminal positions and screw sizes (main circuit terminals)

Frame 4 size ( $400 \mathrm{~V}: 220$ to 315 kW ), models: FRN220SVG1S-4 $\square$ to FRN315SVG1S-4 $\square$



## Note

To connect output terminals for Frame 4 size, use a relay bus bar provided on the cabinet side.
The relay bus bar should be fixed using an insulator.

| Terminal name | Terminal <br> symbol | Bolt size | Terminal <br> tightening torque |
| :--- | :--- | :--- | :--- |
| Output terminal | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | M 12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | G |  |  |

Figure 4.2.1-18: Terminal positions for Frame 4 size (400V: 220 to 315 kW)

Frame 4 size (400V: 630 to 800 kW ), models: FRN630BVG1S-4 $\square$ to FRN800BVG1S-4 $\square$ (V-phase)


## Note

To connect output terminals for Frame 4 size, use a relay bus bar provided on the cabinet side.

| Terminal name | Terminal <br> symbol | Bolt size | Terminal <br> tightening torque |
| :--- | :--- | :--- | :--- |
| Output terminal | AC | M12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | G |  |  |

Figure 4.2.1-19: V-phase terminal positions for Frame 4 size (400V: 630 to 800 kW )

Frame 4 size（400V： 630 to 800 kW ），models：FRN630BVG1S－4 $\square$ to FRN800BVG1S－4 $\square$（U－and W－phases）
Unit：［mm］
＜Internal front view＞
＜Side face view：from the right side face＞


Select terminal screws that allow for a distance of 10 mm or greater to the chassis．

Note
To connect output terminals for Frame 4 size，use a relay bus bar provided on the cabinet side．

| Terminal <br> name | Terminal <br> symbol | Bolt size | Terminal <br> tightening torque |
| :--- | :--- | :--- | :--- |
| Output <br> terminal | AC | M 12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | ЭG |  |  |

## View from bottom

スタック底面から見る

Figure 4．2．1－20：U－and W－phase terminal positions for Frame 4 size（ 400 V ： 630 to 800 kW ）

Frame 4 size (690V: 250 to 450 kW ), models: FRN250SVG1S-69 $\square$ to FRN450SVG1S-69 $\square$


## Note

To connect output terminals for Frame 4 size, use a relay bus bar provided on the cabinet side.
The relay bus bar should be fixed using an insulator.

| Terminal <br> name | Terminal <br> symbol | Bolt size | Terminal <br> tightening torque |
| :--- | :--- | :--- | :--- |
| Output <br> terminal | $\mathrm{U}, \mathrm{V}, \mathrm{W}$ | M 12 | $48 \mathrm{~N} \cdot \mathrm{~m}$ |
| DC input <br> terminal | $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |
| Grounding <br> terminal | G |  |  |

Figure 4.2.1-21: Terminal positions for Frame 4 size ( 690 V : 250 to 450 kW )

### 4.2.2 Installing stacks in cabinets

### 4.2.2.1 Precautions

## (1) Circulation of exhaust air outside cabinets

Provide a cabinet adopting forced ventilation with an air intake in the lower area of the front door and an exhaust opening in the ceiling of the cabinet.
(Cabinet of IP20 or equivalent protection level)
Note that even if an exhaust opening is provided in the ceiling in the longitudinal direction as shown in Figure 4.2.2-1, most of the exhaust heat will be released from the front face when there is a wall or something behind the back face of the cabinet. If the exhaust area is small and exhaust heat is released only in the direction of the front face, exhaust air velocity will significantly increase.

On the other hand, air is introduced into the cabinet from the air intake, so that there is a possibility that it will be circulated through a route as shown in Figure 4.2.2-1.
To prevent exhaust heat released from the cabinet from being introduced through the air intake, consider the location of installation and increase the exhaust area of the exhaust opening.

If air is circuited through a route as shown in the right figure, the inside temperature of the cabinet may increase, and the stack may cause an overheat trip.
(2) Partition of side faces of cabinet

When installing stacks side by side and connecting cabinets, install a partition plate between cabinets as shown in Figure 4.2.2-2.

In partition plates, open only a hole for passing the PN bar provided in the upper area of the cabinets. (Maintain an insulation distance between the PN bars and steel panel of each cabinet.)
Note If no partition plate is installed between cabinets, exhaust air may circulate inside the cabinets and may not be completely released, which may result in an overheat trip of the stacks.
(3) Circulation of exhaust air released from stacks inside cabinets

When maintaining a horizontal spacing (clearance) of 10 mm or over between stacks contained in the same cabinet, install a circulation prevention plate in a position close to the upper area of the stacks to prevent the ingress of exhaust air released from the stacks into the clearance.


Figure 4.2.2-3: Example of installation of exhaust air circulation prevention plate
(4) Horizontal installation of stacks

Install stacks horizontally in cabinets in the direction shown in Figure 4.1.3-1 (on page 4-3).
If a stack is installed aslant, it may be distorted, or the casters may bend.
(5) Tightening torques

Tighten screws and bolts to the torques specified in Table 4.2.2-1.

If tightening torques are specified for the place or equipment, tighten them to the specified torques.
In addition, use screws and bolts in combination with a spring washer or flat washer.
Note (1) If the tightening torque applied to a conductive portion greatly deviates from the specified torque, the screw may become loose or the conductive portion will be separated, resulting in failure to maintain the normal contact state and unusual heat generation from the contact portion.

Table 4.2.2-1: Tightening torques

| Designation of <br> screw | Conductive <br> portion | Structure |
| :--- | :---: | :---: |
| M3 | $0.53 \pm 0.06$ | $0.7 \pm 0.08$ |
| M3.5 | $0.88 \pm 0.11$ | $1.2 \pm 0.14$ |
| M4 | $1.3 \pm 0.16$ | $1.8 \pm 0.21$ |
| M5 | $2.7 \pm 0.32$ | $3.5 \pm 0.42$ |
| M6 | $5 \pm 0.6$ | $5.8 \pm 0.7$ |
| M8 | $12 \pm 1.4$ | $13.5 \pm 1.6$ |
| M10 | $24 \pm 2.9$ | $27 \pm 3.2$ |
| M12 | $40 \pm 4.8$ | $48 \pm 5.8$ |
| M16 | $85 \pm 10.2$ | $118 \pm 14$ |

(2) Specified tightening torques are different between conductive portions (contact portion between bus bars or between a crimped terminal and an appliance terminal, etc.) and structures (steel panels and frames of cabinets, etc.).

### 4.2.2.2 Procedure for removing and attaching the front cover

(1) Loosen the screws fastening the front cover (four screws for Frame 1; six for Frame 2: eight for Frame 3: ten for Frame 4).
Potbelly-shaped holes are used for the points of mounting of the front cover and allow the front cover to be removed without unfastening the screws.
(2) When the front cover is not provided with a hand opening, hold the right and left ends of the front cover with both hands, and slide and remove it.
When the front cover is provided with a hand opening, lift the hand opening, and slide and remove the front cover.
(3) Attach the front cover by reversing the removal procedure.
(4) To make the control terminal on the control PCB visible, open the keypad case.

The keypad case opens and closes on the left side.


Figure 4.2.2-4: How to remove the front cover

### 4.2.2.3 Installing Frame 1 and 2 size stacks (400V: $\mathbf{3 0}$ to $\mathbf{1 1 0} \mathrm{kW}, 690 \mathrm{~V}: 90$ to 110 kW)

## (1) Installation procedure

To install in cabinets Frame 1 and 2 size stacks ( 400 V series: 30 to 45 kW [Frame 1], 55 to 110 kW [Frame 2]. 690V series: 90 to 110 kW [Frame 2]), use the following procedure:

1) Place a stack on the stack installation frame. Then, push both side faces of the stack (area below the center) to the specified position.
2) Fix the stack with screws at the points of fixation on the further side. (M8 bolt $x 2$ )
3) Using a fixation attachment, fix the stack with a screw (M5-12 to 25 ) at the point in the lower area of the front face.


Figure 4.2.2-5: How to fix Frame 1 and 2 size stacks (400V: 30 to $110 \mathrm{~kW}, 690 \mathrm{~V}$ : 90 to 110 kW ) in a cabinet

## Note

- Fix the stack in order of "points of fixation" (2), and (3) shown in the left figure.
- Carry out steps (3) mentioned above by making reference to (3) Description.


## (2) Removal procedure

Remove the stack by reversing the "(1) Installation procedure" above.
When drawing out the stack, remove the front cover of the stack, and hold the hand opening provided in the lower area.


Figure 4.2.2-6: Position of hand opening

Note (1) Frame 1 and 2 size (400V: 30 to $110 \mathrm{~kW}, 690 \mathrm{~V}$ : 90 to 110 kW ) stacks are not provided with casters, and the legs in the lower area of the stack rub against the cabinet when setting or drawing it out. If a painted steel panel is used on the cabinet side, the paint will come off from the rubbed area, and the area will get corroded. For this reason, it is advisable to use SUS panels or plated steel panels rather than painted steel panels. The legs of stacks that come into contact with cabinets use a plated steel panel (unpainted), and the cut face of the panel is chamfered so as not to cause damage to cabinets.
(2) Secure work space behind the back face to fix the stack at the points of fixation on the back face.
(3) Installing a quide for setting and drawing out stacks on the cabinet in advance ensures the smooth setting and draw-out of stacks.
(4) Create the fixation attachment on the front face of the stack according to the recommended dimensions. (See Figure 4.2.1-3 (on page 4-7).)
Design the cooling fan of the stack to be detached without removing this fixation attachment.
(5) The upper area of the stack is designed to attach a DC fuse. Lay out this area so that this DC fuse can be easily attached and detached.
(6) Do not fix the stack aslant.
(3) Description

1) Fixing the lower area of the front face of the stack (step 2 of "(1) Installation procedure").

Fix the lower area of the front face of each stack to be installed in a cabinet.
Temporarily fasten the fixation attachment to the stack and then to the frame of the cabinet. After the fixation attachment is temporarily fastened to the stack and the frame, securely tighten the temporarily fastened points of fixation.


Figure 4.2.2-7: Fixing the front face lower area for Frame 1 and 2 size stacks ( 400 V : 30 to $110 \mathrm{~kW}, 690 \mathrm{~V}$ : 90 to 110 kW )

### 4.2.2.4 Installing Frame 3 and 4 size stacks (400V: 132 to $\mathbf{8 0 0} \mathrm{kW}, 690 \mathrm{~V}$ : 132 to 450 kW)

To install in cabinets Frame 3 and 4 size stacks (400V series: 132 to 200 kW [Frame 3], 220 to 800 kW [Frame 4]. 690V series: 132 to 200 kW [Frame 3], 250 to 450 kW [Frame 4]), use the following procedure:
When installing stacks of these frame sizes, attach a bus bar terminal, which relays the main circuit terminal in the lower area of the stacks, in advance.

## (1) Installation procedure

Follow the procedure described below to install a stack in a cabinet.

1) Place a stack on the stack installation frame. Then, hold the hand opening, and push the stack until the fixation plate on the back face is fitted into the set-in guide.
2) Using a fixation attachment, fix the stack with a bolt (M8-16 bolt) at the point in the lower area of the front face.
3) Using a fixation attachment, fix the stack with a bolt (M8-16 bolt) at the point in the upper area of the front face.
Note Fix the stack in order of "points of fixation"
(2) and (3)
(3) shown in the figure below.

## (2) Removal procedure

Remove the stack by reversing "(1) Installation procedure" above. When drawing out the stack, remove the front cover of the stack, and hold the hand opening provided in the lower area.


Figure 4.2.2-8: How to fix Frame 3 and 4 size stacks ( 400 V : 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW ) in a cabinet

[^3]
## (3) Description

1) Guide rail

Caster outer perimeters for the respective inverter models are specified in the figures listed below. Install guide rails based on the specified perimeter according to the dimensions of the inverter used.

- 400 V series, 132 to $200 \mathrm{~kW} \Rightarrow$ Figure 4.2.1-8 (page 4-12)
- 690 V series, 132 to $200 \mathrm{~kW} \Rightarrow$ Figure 4.2.1-9 (page 4-13)
- 400 V series, 220 to $315 \mathrm{~kW} \Rightarrow$ Figure 4.2.1-18 (page 4-19)
- 400 V series, 630 to $800 \mathrm{~kW} \Rightarrow$ Figure 4.2.1-19 (page 4-20)
- 690 V series, 250 to $450 \mathrm{~kW} \Rightarrow$ Figure 4.2.1-21 (page 4-22)


Figure 4.2.2-9: Examples of guide rails
2) Fixation plate set-in guide on the back face of the stack

The relationship between the sizes of the holes in the set-in guide and the position of the stack fixation plate is shown in Figure 4.2.1-16 and Figure 4.2.1-17 (on pages 4-17 and 4-18). Note that size and the clearance are different between the upper and lower holes.
If it is possible to bend as the figure below, it is advisable to use a 2.3 -mm-thick steel sheet to manufacture a set-in guide. When bending a steel sheet only in the vertical direction to manufacture a set-in guide, use a 3.2-mm-thick steel sheet.
Punch holes in the set-in guide in the directions specified in the figures below.


Steel plate shape recommended when $\mathrm{t}=3.2 \mathrm{~mm}$


Figure 4.2.2-10: Overview of set-in guide for Frame 3 and 4 size stacks (400V: 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW )
3) Fixing the lower area of the front face of the stack (step 2 of "(1) Installation procedure")

Fix the lower area of the front face of each stack to be installed in a cabinet.
Temporarily fasten the fixation attachment to the stack and then to the frame of the cabinet.
After the fixation attachment is temporarily fastened to the stack and the frame, securely tighten the temporarily fastened points of fixation on the stack side.
Finally, pushing the stack in the direction of the back face, securely tighten temporarily fastened points of fixation on the cabinet side.


Figure 4.2.2-11: Fixing the front face lower area for Frame 3 and 4 size stacks (400V: 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW )
4) Fixing the upper area of the front face (step 3 of "(1) Installation procedure")

The upper areas of the front faces of stacks are designed to collectively fix the stacks to be installed with a fixation attachment.
Temporarily fasten the fixation attachment to the frame of the cabinet, and fix each stack. Finally, pushing the stack in the direction of the back face, securely tighten the temporarily fastened points on the frame side.
Note
Design this fixation attachment with a tolerance that presses it in the direction of the back face.


Figure 4.2.2-12: Fixing the front face lower area for Frame 3 and 4 size stacks
( 400 V : 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW )

### 4.2.2.5 Connecting output terminals of Frame 3 and 4 size stacks (400V: 132 to 800 kW, 690V: 132 to 450 kW)

In Frame 3 and 4 size stacks ( 400 V : 132 to 800 kW , 690 V : 132 to 450 kW ), connect a wire and etc. by connecting a relay copper bar to stack output terminal. This section describes relay copper bars.
Relay copper bars of the same shape are available for both Frame 3 and 4 size stacks.
Figure 4.2.2-13 shows the recommended size of a relay copper bar. Prepare a relay copper bar based on the figure, as well as an insulator for fastening this copper bar to the frame of the cabinet.
Note (1) Connect a relay copper bar before installing a stack.
(2) When removing stack type inverters, loosen the stack type output terminal bolts, lift and then pull out to prevent the output terminals interfering with the relay copper bar.

[Description of installation]


| Model | Voltage: *[V] | Model capacity: <br> \# [kW] | Relay copper bar size: $\mathrm{t}[\mathrm{mm}] \times \mathrm{b}[\mathrm{mm}]$ | Insulating support height: h [mm] |
| :---: | :---: | :---: | :---: | :---: |
| Inverters: <br> FRN*SVG1S-\# PWM converters: RHC*S-\#D Diode rectifiers: RHD*S-\#D | 400 | 132 to 200 | $5 \times 30$ | 27 to 31 |
|  |  | 220 to 315 | $10 \times 30$ | 26 to 30 |
|  |  | 630 to 800 | $10 \times 125$ |  |
|  | 690 | 132 to 220 | $5 \times 30$ | 27 to 31 |
|  |  | 250 to 450 | $10 \times 30$ | 26 to 30 |
| Filter stacks: <br> RHF*S-\#D | 400 | 160 to 220 | $5 \times 30$ | 34 to 38 |
|  |  | 280 to 355 | $10 \times 30$ | 33 to 37 |
|  | 690 | 160 to 220 | $5 \times 30$ | 34 to 38 |
|  |  | 280 to 450 | $10 \times 30$ | 33 to 37 |

Figure 4.2.2-13: Recommended size of a relay copper bar, insulating supports

Connect the relay copper bar and output wiring before installing the stack.


The clearance between the stack output terminal and the relay copper bar is 1 mm or greater. The stack output terminal is designed such that its vertical position can be adjusted.

Fix the stack to the cabinet and then make connections as shown below.
The stack is designed to be installable in a cabinet without modification.


Figure 4.2.2-14: Precautions when connecting a relay copper bar

### 4.2.3 Connecting DC bus bars

A stack has $D C$ bus bar connection terminals $P(+)$ and $N(-)$ in the upper area. By setting $D C$ bus bars in the upper area of the cabinet side, the $P(+)$ and $N(-)$ terminals can be easily connected.
[1] (1) For DC bus bars on the cabinet side, see "4.3 Basic configuration of cabinets".
(2) Select a bus bar size according to "4.4 Bus bars".

### 4.2.3.1 Connecting bus bars for Frame 1 to 3 size stacks (400V: $\mathbf{3 0}$ to 200 kW , 690V: 90 to 200 kW)

For Frame 1 to 3 size stacks ( 400 V : 30 to 200 kW, 690 V : 90 to 200 $k W)$, the $P(+)$ and $N(-)$ terminals are attached on the right side of the stack.
(Refer to Figure 4.2.1-1 (on page4-6) and Figure 4.2.1-7 (on page 4-11).)
Since nuts are welded to the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ terminals, position them so that the DC bus bars from the DC line will contact on the reverse side.
(Refer to Figure 4.2.3-1.)


Figure 4.2.3-1: Examples of DC bus bar connections for Frame 1 to 3 size stacks

### 4.2.3.2 Connecting bus bars for Frame 4 size ( 400 V : $\mathbf{2 2 0}$ to $\mathbf{8 0 0} \mathrm{kW}, \mathbf{6 9 0 V}$ : $\mathbf{2 5 0}$ to 450 kW)

For Frame 4 size stacks ( 400 V : 220 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 250 to 450 kW ), the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ terminals are attached on the front side of the stack. (Refer to Figure 4.2.1-10 (on page 4-14).) Since nuts are welded to the backside of these terminals, position them so that the DC bus bars from the DC line will contact on the front side. (Refer to Figure 4.2.3-2.)


Figure 4.2.3-2: Examples of DC bus bar connections for Frame 4 size ( 400 V : 220 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 250 to 450 kW )

### 4.3 Basic configuration of cabinets

The basic structure of a stack cabinet is designed to accommodate three stacks. Design the cabinet structure based on this basic structure.

### 4.3.1 Appearance of cabinets

The basic cabinet structure is as shown below.

## Cabinet specifications

(1) Ambient temperature
(2) IP protection level
(3) Maintenance and inspection
(4) Air intake
(5) Single swinging door
(6) Size
: -5 to $40^{\circ} \mathrm{C}$ (annual average temperature: $35^{\circ} \mathrm{C}$ ), temperature at inlet of stack: $40^{\circ} \mathrm{C}$ (maximum value)
: IP20
: Only access to the front face
: Provided with a dust collection filter (for coarse dust)
: Handle type. The door is fixed at three points - upper, lower, and central points.
: Overall length $=800 \times 2560 \times 630$
Body $=2200 \times 800 \times 600(+30)$, height of exhaust opening $=260$, channel base $=$ 100


Figure 4.3.1-1: Appearance of cabinet

### 4.3.2 Internal layouts of cabinets

This section shows the internal layouts of cabinets, assuming the case where stack type inverters are used in conjunction with peripheral equipment (DCF: DC fuse) and a ACL (radio noise reducing zero-phase reactor) connected on the output side.
As a DC bus (DC bus bar), Cux 100 (in two parallel rows) is adopted in consideration for connection of plural stacks and the low impedance of the PN bus.

### 4.3.2.1 Internal layout for Frame 1 size ( 400 V : $\mathbf{3 0}$ to $\mathbf{4 5} \mathrm{kW}$ )



Figure 4.3.2-1: Example of internal layout for Frame 1 size ( 400 V : 30 to 45 kW )

## Components

400 V series

| Specifications | Model: FRN_ |  | 30SVG1S-4■ | 37SVG1S-4 $\square$ | 45SVG1S-4■ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current | MD spec | 60 | 75 | 91 |
|  | [A] | LD spec | 75 | 91 | 112 |
| DC fuse | F1-F3 |  | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor |  | ACL1-3 | ACL-40B (x4) | ACL-40B (x4) | ACL-74B (x4) |
| External wire terminal Z1-Z3 |  |  | LT2E-080 (4pin) | LT2E-090 (4pin) | LT2E-150 (4pin) |

Note (1) The number of turns of the radio noise reducing zero-phase reactor (ACL) depends on the type and size of the wire to be used.
Thus, when this layout is applied, it is assumed that the wire is passed through the radio noise reducing zero-phase reactor only once.
(2) The external wire terminal block is selected based on the rated current of each inverter.
(Selection criteria: ambient temperature of $40^{\circ} \mathrm{C}$ and temperature rise of 30 K .)

### 4.3.2.2 Internal layout for Frame 2 size (400V: 55 to $110 \mathrm{~kW}, 690 \mathrm{~V}$ : 90 to 110 kW )



Figure 4.3.2-2: Internal layout for Frame 2 size (400V: 55 to $110 \mathrm{~kW}, 690 \mathrm{~V}: 90$ to 110 kW )

## Components

- 400 V series

| Specifications | Model: FRN |  | 75SVG1S-4■ | 90SVG1S-4■ | 110SVG1S-4 $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current <br> [A] | MD spec | 150 | 176 | 210 |
|  |  | LD spec | 176 | 210 | 253 |
| DC fuse F1-F3 |  |  | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor ACL1-3 |  |  | ACL-74B (x4) |  |  |
| External wire terminal $\mathrm{Z} 1-\mathrm{Z3}$ |  |  | LT2E-200 (4pin) | LT2E-300 (4pin) |  |

■ 690V series

| Specifications | Model: FRN |  | 90SVG1S-69■ | 110SVG1S-69 $\square$ |
| :---: | :---: | :---: | :---: | :---: |
|  | Rated current$[\mathrm{A}]$ | MD spec | 100 | 130 |
|  |  | LD spec | 130 | 140 |
| DC fuse F1-F3 |  |  | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |
| Zero-phase reactor ACL1-3 |  |  | - |  |
| External wire terminal Z1-Z3 |  |  | LT2E-150 (4pin) |  |

Note (1) The number of turns of the radio noise reducing zero-phase reactor (ACL) depends on the type and size of the wire to be used.
Thus, when this layout is applied, it is assumed that the wire is passed through the radio noise reducing zero-phase reactor only once.
(2) The external wire terminal block is selected based on the rated current of each inverter.
(Selection criteria: ambient temperature of $40^{\circ} \mathrm{C}$ and temperature rise of 30 K .)

### 4.3.2.3 Internal layout for Frame 3 size (400V: 132 to $200 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 200 kW)



Figure 4.3.2-3: Internal layout for Frame 3 size (400V: 132 to $200 \mathrm{~kW}, 690 \mathrm{~V}: 132$ to 200 kW )

## Components

400V series

| Specifications | Model: FRN |  | 132SVG1S-4 $\square$ | 160SVG1S-4 $\square$ | 200SVG1S-4■ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current$[\mathrm{A}]$ | MD spec | 253 | 304 | 377 |
|  |  | LD spec | 304 | 377 | 415 |
| DC fuse |  | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor |  | ACL1-3 | F200160PB (x4) |  |  |
| External wire terminal |  | Z1-Z3 | Cu5x30 (x3) |  |  |
|  |  | E | Cu6x25 |  |  |

690V series

| Specifications | Model: FRN |  | 132SVG1S-69 $\square$ | 160SVG1S-69 $\square$ | 200SVG1S-69 $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current [A] | MD spec | 140 | 161 | 216 |
|  |  | LD spec | 161 | 216 | 235 |
| DC fuse |  | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor |  | ACL1-3 | - |  |  |
| External wire terminal |  | Z1-Z3 | Cu3x30 (x3) |  |  |
|  |  | E | Cu6x25 |  |  |

Note (1) The number of turns of the radio noise reducing zero-phase reactor (ACL) depends on the type and size of the wire to be used. Thus, when this layout is applied, it is assumed that the wire is passed through the radio noise reducing zero-phase reactor only once.
(2) The external wire terminals are selected based on the rated current of each inverter. (Selection criteria: ambient temperature of $40^{\circ} \mathrm{C}$ and temperature rise of 30 K .)

### 4.3.2.4 Internal layout for Frame 4 size (400V: 220 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 250 to 450 kW)



Figure 4.3.2-4: Internal layout for Frame 4 size ( 400 V : 220 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 250 to 450 kW )

## Components

■ 400V series

| Specifications | Model: FRN |  | 220SVG1S-4 $\square$ | 250SVG1S-4 $\square$ | 280SVG1S-4 $\square$ | 315SVG1S-4 $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current$[\mathrm{A}]$ | MD spec | 415 | 468 | 520 | 585 |
|  |  | LD spec | 468 | 520 | 585 | 650 |
| DC fuse |  | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |  |
| Zero-phase reactor |  | ACL1-3 | F200160PB (x4) |  |  |  |
| External wire terminal |  | Z1-Z3 | Cu10x30 (x3) |  |  |  |
|  |  | E | Cu6x25 |  |  |  |


| Specifications | Model: FRN_ |  | 630BVG1S-4 $\square$ | 710BVG1S-4 $\square$ | 800BVG1S-4 $\square$ |
| :--- | :--- | :--- | :--- | :---: | :---: |
|  | Rated current <br> [A] | MD spec | 1170 | 1370 | 1480 |
|  | LD spec | 1370 | 1480 | 1850 |  |
| DC fuse | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |  |
| Zero-phase reactor | ACL1-3 | F200160PB (x4) |  |  |  |
| External wire terminal | Z1-Z3 | Cu10x125 (x3) |  |  |  |
|  | E | Cu6x25 |  |  |  |

## 690 V series

| Specifications | Model: FRN |  | 250SVG1S-69 $\square$ | 280SVG1S-69■ | 315SVG1S-69 $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current[A] | MD spec | 265 | 295 | 330 |
|  |  | LD spec | 295 | 330 | 365 |
| DC fuse |  | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor |  | ACL1-3 | - |  |  |
| External wire terminal |  | Z1-Z3 | Cu5x30 (x3) |  |  |
|  |  | E | Cu6x25 |  |  |


| Specifications | Model: FRN |  | 355SVG1S-69 $\square$ | 400SVG1S-69 $\square$ | 450SVG1S-69 $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rated current$[\mathrm{A}]$ | MD spec | 365 | 410 | 460 |
|  |  | LD spec | 410 | 460 | - |
| DC fuse |  | F1-F3 | Refer to "5.2.1.1 Fuses" in Chapter 5. |  |  |
| Zero-phase reactor |  | ACL1-3 | - |  |  |
| External wire terminal |  | Z1-Z3 | Cu5x30 (x3) |  |  |
|  |  | E | Cu6x25 |  |  |

Note (1) The number of turns of the radio noise reducing zero-phase reactor (ACL) depends on the type and size of the wire to be used.
Thus, when this layout is applied, it is assumed that the wire is passed through the radio noise reducing zero-phase reactor only once.
(2) The external wire terminals are selected based on the rated current of each inverter. (Selection criteria: ambient temperature of $40^{\circ} \mathrm{C}$ and temperature rise of 30 K .)

### 4.4 Bus bars

Use a bus bar to connect DC bus bar connection terminals $[P(+), N(-)]$ and output terminals ( $\mathrm{U}, \mathrm{V}, \mathrm{W}$ ). This section describes bus bars.

### 4.4.1 Materials and surface treatment of bus bars

Use bus bars made of any of the materials specified in JIS H3140 and subjected to any of the surface plating processes complying with JIS H0404.

| Material of bus bars | $:$ C1100BB | Copper (electric conductivity: $97 \%$ ) | $\ldots$ JIS H3140 |
| :--- | :--- | :--- | :--- |
|  | $:$ C1020BB |  |  |
| Surface plating | $:$ Ep-Cu/Sn3 | Tin plating (plating thickness: $3 \mu \mathrm{~m}$ ) | $\ldots$ JIS H0404 |
|  | $:$ Ep-Cu/Sn-Pb(5-10)3 | Tin lead alloy (plating thickness: $3 \mu \mathrm{~m}$ ) |  |

### 4.4.2 Connection of bus bars (sizes of holes in bus bars, drilling pitches)

According to the size of bus bar, the number of connection holes and the hole pitch are specified as shown in Table 4.4.2-2.

Connect bus bars in any of the patterns shown in Table 4.4.2-1. If bus bars of different widths are used, connect them based on the bus bar of the smaller width.

Table 4.4.2-1: Connection patterns of bus bars

|  | $\mathrm{a}=\mathrm{b}$ | $a<b$ | $a>b$ |
| :---: | :---: | :---: | :---: |
| Straight connection |  |  |  |
| L-branched connection |  |  |  |
| T-branched connection |  |  |  |

Table 4.4.2-2: Connection of bus bars (relatively narrow bus bars) and bolt holes and pitches

| Bus bar [mm] |  | Overlap dimension $\mathrm{A} \times \mathrm{B}[\mathrm{mm}]$ | Size of hole [mm] |  |  |  |  | Applicable bolt | Effective contact area [ $\mathrm{mm}^{2}$ ] | Application diagram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thickness | Width (B) |  | a | b | c | e | d |  |  |  |
| n0000000000 | 15 | $15 \times 15$ | - | - | - | - | 7 | M6 | 187 | ${ }^{\text {d }}$ |
|  | 20 | $20 \times 20$ |  |  |  |  | 10 | M8 | 322 | $\cdots{ }^{1}$ |
|  | 25 | $25 \times 25$ |  |  |  |  |  |  | 547 | $\sim$ |
|  | 30 | $30 \times 30$ | - | - | - | - | 12 | M10 | 787 |  |
|  | 40 | $40 \times 40$ |  |  |  |  | 15 | M12 | 1423 |  |
|  | 50 | $50 \times 50$ |  |  |  |  |  |  | 2323 | When the terminal of the mating appliance has two holes or when |
|  | 60 | $60 \times 60$ |  |  |  |  | 19 | M16 | 3317 | there is a possibility that the bus bar will rotate (slip out of position) because of the structure, two holes need drilled in the bus bar. |

Note (1) Secure an effective contact area equal to or larger than the appropriate value specified in the table above.
(2) Set the contact surface pressure at $5\left[\mathrm{~N} / \mathrm{mm}^{2}\right]$ or over.
(3) The bearing surface pressure of the bolt shall not exceed $50\left[\mathrm{~N} / \mathrm{mm}^{2}\right]$ in order to prevent creep.
(4) The stress of the bolt shall not exceed the yield point of $226 \mathrm{~N} / \mathrm{mm}^{2}$ (bolt made of 4T).
(5) These specifications apply to up to three bus bars connected in parallel.
(6) The effective contact area means the area of the contact portion calculated by subtracting the area of the bolt hole (d).

Table 4.4.2-3: Connection of bus bars (wide bus bars) and bolt holes and pitches


Note The precautions stated in Table 4.4.2-2 apply.

### 4.4.3 Connection methods and tightening torques

Connect bus bars using a bolt as shown in Figure 4.4.3-1. Use plural washer or belleville springs for bus bars that are connected in a frequently vibrating location or in which stress concentrates to prevent the bus bars from becoming loose.

In addition, comply with Table 4.2.2-1 "Tightening torques" (on page 4-24).

Note (1) It is recommended that belleville springs, spring washers, and
nuts be mounted on surfaces where they can be easily
checked after tightening.
(2) Use bolts and nuts plated with Ep-Fe, Zn5, or CM2.


Figure 4.4.3-1: Example of connection of bus bar

### 4.4.3.1 Rated current of Cu bus bars

Rated currents of bus bars are as shown in Table 4.4.3-1 (on page 4-43). However, if the ambient temperature of the cabinet is higher than $40^{\circ} \mathrm{C}$ and in some other cases, the derating of the current must be considered.

## [Current capacity of bus bars]

Bus bars are selected based on the assumption that the temperature is $70^{\circ} \mathrm{C}$ (ambient temperature $=40^{\circ} \mathrm{C}$ and temperature rise $=30 \mathrm{~K}$ ). If ambient temperature drops below $40^{\circ} \mathrm{C}$, the value of temperature rise increases. Consider a correction factor according to Figure 4.4.3-3.
In addition, the reduction rate of the supplied current depends on the layout of bus bars. When supplying a large current, plan the current by making reference to Figure 4.4.3-2.


Figure 4.4.3-3: Temperature correction factor


Figure 4.4.3-2: Derating in installation direction (reference)

Table 4.4.3-1: Rated currents of CU bus bars

| Dimensions (mm) |  | Cross sectional area [ $\mathrm{mm}^{2}$ ] |  | No parallel connection | YK | 2 parallel rows When equal to thickness |  | 3 parallel rows When equal to thickness |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thickness | Width |  | $\square$ |  |  |  |  |  |
|  |  |  | DC | AC (50/60Hz) | DC | AC (50/60Hz) | DC | AC (50/60Hz) |
| 3 | 15 | 45 | 180 | 180 |  |  |  |  |
|  | 20 | 65 | 225 | 225 |  |  |  |  |
|  | 25 | 75 | 275 | 275 |  |  |  |  |
|  | 30 | 90 | 320 | 320 |  |  |  |  |
| 4 | 25 | 100 | 325 | 325 |  |  |  |  |
|  | 30 | 120 | 380 | 375 |  |  |  |  |
|  | 40 | 160 | 485 | 480 |  |  |  |  |
| 5 | 25 | 125 | 370 | 365 |  |  |  |  |
|  | 30 | 150 | 430 | 425 |  |  |  |  |
|  | 40 | 200 | 550 | 540 |  |  |  |  |
|  | 50 | 250 | 660 | 650 |  |  |  |  |
|  | 60 | 300 | 780 | 860 |  |  |  |  |
|  | 75 | 375 | 950 | 930 | 1920 | 1790 |  |  |
| 6 | 25 | 150 | 410 | 410 |  |  |  |  |
|  | 30 | 180 | 480 | 470 |  |  |  |  |
|  | 40 | 240 | 610 | 600 |  |  |  |  |
|  | 50 | 300 | 730 | 720 |  |  |  |  |
|  | 60 | 360 | 860 | 840 |  |  |  |  |
|  | 75 | 450 | 1050 | 1010 | 2090 | 1910 |  |  |
|  | 80 | 480 | 1110 | 1070 | 2190 | 2000 |  |  |
|  | 100 | 600 | 1350 | 1280 | 2620 | 2330 | 3670 | 3060 |
| 8 | 25 | 200 | 500 | 490 |  |  |  |  |
|  | 30 | 240 | 570 | 560 |  |  |  |  |
|  | 40 | 320 | 720 | 700 |  |  |  |  |
|  | 50 | 400 | 860 | 840 |  |  |  |  |
|  | 60 | 480 | 1010 | 970 |  |  |  |  |
|  | 75 | 600 | 1220 | 1160 | 2390 | 2120 |  |  |
|  | 80 | 640 | 1290 | 1220 | 2510 | 2210 |  |  |
|  | 100 | 800 | 1580 | 1470 | 2990 | 2560 | 4230 | 3330 |
| 10 | 40 | 400 | 830 | 800 | 1730 | 1600 |  |  |
|  | 50 | 500 | 990 | 950 | 2010 | 1810 |  |  |
|  | 60 | 600 | 1150 | 1090 | 2280 | 2010 |  |  |
|  | 75 | 750 | 1390 | 1290 | 2680 | 2290 |  |  |
|  | 80 | 800 | 1460 | 1360 | 2810 | 2380 |  |  |
|  | 100 | 1000 | 1780 | 1620 | 3310 | 2730 | 4750 | 3490 |
|  | 125 | 1250 | 2150 | 1930 | 3930 | 3160 | 5570 | 3960 |
|  | 150 | 1500 | 2550 | 2260 | 4550 | 3590 | 6410 | 4450 |
| 12 | 125 | 1500 | 2390 | 2100 | 4290 | 3300 | 6140 | 4120 |
|  | 150 | 1800 | 2800 | 2430 | 4930 | 3700 | 7000 | 4590 |
| 15 | 100 | 1500 | 2110 | 1920 |  |  |  |  |
|  | 150 | 2250 | 3160 | 2660 | 5510 | 3870 | 7900 | 4790 |
|  | 175 | 2625 | 3550 | 2960 | 6080 | 4240 | 8660 | 5200 |
|  | 200 | 3000 | 4070 | 3350 | 6850 | 4680 | 9680 | 5700 |

Note (1) The selection conditions applied to this table are ambient temperature: $40^{\circ} \mathrm{C}$ and temperature rise: 30 K .
(2) The layout of bus bars is a vertical layout.
(3) The material of bus bars is one complying with "4.4.1 Materials and surface treatment of bus bars" (on page 4-40).

### 4.5 Main circuit wires

This section describes the wire sizes for the inverter main circuit section.
Depending on the wiring method for the main circuit section, noise may be applied to the control circuit system, and the system may malfunction.
(1) See Chapter 7 "EMC Compatible Peripherals" and Appendix 5 "Proficient way to use inverters (on preventing electric noise)" and Appendix 6 "Grounding as noise countermeasure and ground noise".

### 4.5.1 Wire selection criteria

Unless otherwise required by a special application, use the wire types listed below.

## <400V series>

- 600 V vinyl-insulated wire (IV wire)

This is an insulated wire with a rated voltage of 600 V and a maximum permissible temperature of $60^{\circ} \mathrm{C}$. It can be widely used for main circuits and control circuits inside cabinets or indoors.
However, this wire is low in flexibility and permissible current and is not suitable for large-capacity applications.

- 600 V class 2 vinyl wire or 600 V polyethylene-insulated wire (HIV wire)

This is an insulated wire with a rated current of 600 V and a maximum permissible temperature of $75^{\circ} \mathrm{C}$. It is superior in flexibility to IV wires of the same class and permits a large current to flow.
Thus, it is applicable to the main circuit sections inside cabinets or indoor.

- 600 V cross-linked polyethylene insulated wire (FSLC wire)

This is an insulated wire with a rated current of 600 V and a maximum permissible temperature of $90^{\circ} \mathrm{C}$. It is much superior in flexibility to IV wires of the same class and permits a large current to flow. Thus, it can be used not only for large-capacity applications but also for the reduction of the exclusive area of wires or the streamlining of work.
For your reference, Board Lex manufactured by Furukawa Electric Co., Ltd. is equivalent to this wire.

## <690V series>

Use wires rated at 1000 V or higher voltage. The maximum permissible temperature should be $70^{\circ} \mathrm{C}$ for PVC (polyvinyl chloride) or $90^{\circ} \mathrm{C}$ for XLPE (cross-linked polyethylene) or EP (ethylene-propylene rubber) according to IEC 60364-5-52: 2001(JIS C 60364-5-52: 2006).
(Examples of wires: NYY, NYCWY $\left(70^{\circ} \mathrm{C}\right)$ )

- IEC 60364-5-52 : 2001 Electrical installations of buildings - Part 5-52 : Selection and erection of electrical equipment - wiring systems
- JIS C 60364-5-52:2006 "Electrical installations of buildings -- Part 5-52: Selection and erection of electrical equipment -- Wiring systems"


### 4.5.1.1 Overcurrent protectors and protection coordination

Select a wire size that does not burn out with an overcurrent.

- PWM converter input/output side : Time until a molded case circuit breaker (MCCB) causes an overcurrent trip, or time until the overcurrent protection function of a PWM converter stack starts to work.
- Diode rectifier input/outputs side : Time until a molded case circuit breaker (MCCB) causes an overcurrent trip.
- Inverter output side : Time until the overcurrent trip function of an inverter starts to work.

Figure 4.5.1-1 shows the operating characteristic of an MCCB. The right side of this operating characteristic curve is the operating range, and the left side is the non-operating range. Judging from this curve, the wire showing the characteristic (3) is a proper wire. (The wires with the characteristics (1) and (2) are improper.)
(1) Continuous domain

To prevent the MCCB from operating after the current exceeds the permissible current (continuously supplied current) of the wire. The following relationship must be fulfilled:
Permissible current of wire [A] > Rated current of MCCB [A]
(2) Short-time domain

Note that the short-time domain may intersect with the permissible current characteristic of the wire at a point close to the point of intersection of the time delay trip and instantaneous trip characteristics of an MCCB (portion $\mathbb{A}$ a in Figure 4.5.1-1).
To make it easy to consider the short-time domain of IV wires, combinations of the rated currents of the MCCB and protectable wire sizes are shown in Table 4.5.1-1.
Consider FSLC wires based on the short-time characteristic shown in Figure 4.5.1-2 and the operating characteristic curve of the MCCB. For the operating characteristic curve of the MCCB, see the catalog for it or engineering documents.


Figure 4.5.1-1: Protection coordination between MCCB and wire

Table 4.5.1-1: Sizes of 600 V vinyl insulated wires (IV wires) protectable in short-time domain

|  | 15 | 20 | 30 | 40 | 50 | 60 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 | 300 | 350 | 400 | 500 | 600 | 700 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 38 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 150 |  |  |  |  |  | Dom |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 200 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 250 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 325 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Note (1) The short-time permissible temperature of the wire is set at $100^{\circ} \mathrm{C}$.
(2) Separately calculate an applicable wire size in case of a fault break.


Figure 4.5.1-2: Short-time characteristics of 600 V cross-linked polyethylene insulated wires (FSLCs)

Table 4.5.1-2: Short-time currents

| Wire size <br> $\square\left[\mathrm{mm}^{2}\right]$ | Short-time capacity $\left[\mathrm{kA}{ }^{2} \mathrm{~s}\right]$ |  |
| :---: | :---: | :---: |
| IV wire | FLSC wire |  |
| 2.0 | 0.054 | 0.079 |
| 3.5 | 0.165 | 0.242 |
| 5.5 | 0.408 | 0.597 |
| 8.0 | 0.863 | 1.262 |
| 14 | 2.64 | 3.865 |
| 22 | 6.53 | 9.544 |
| 38 | 19.47 | 28.47 |
| 60 | 48.55 | 71.0 |
| 100 | 135 | 197.2 |
| 150 | 303 | 443.7 |
| 200 | 539 | 788.8 |
| 250 | 843 | 1232.5 |
| 325 | 1425 | - |

Obtain the short circuit capacity of the wire from the catalogue for it or engineering documents. Calculate the total cutoff $I^{2} \cdot t$ of the MCCB at the time of short circuit current cutoff using the equation given below.
Total cutoff of MCCB at the time of short circuit current cutoff: $I^{2} t=I s^{2} \times t_{C B}\left[k A^{2} s\right]$

Is: Short circuit current passing through the MCCB, or the rated cutoff capacity [kA] of the MCCB when the short circuit current is unknown.
$t_{c B}$ : Operating time of the MCCB corresponding to the short circuit current, or the operating time [s] of the MCCB at the rated cutoff capacity when the short circuit current is unknown.

When the short-time characteristic curve of the wire is available, calculate the protectable time to the short circuit current and the operating time of the MCCB from this curve and the operating characteristic curve of the MCCB. The short circuit current passing through the wire and that passing through the MCCB are the same. Thus, compare the protectable time to the short circuit current of the wire with the operating time of the MCCB.
$\mathrm{tw}[\mathrm{s}]>\mathrm{t} C \mathrm{~B}[\mathrm{~s}]$
tw: Protectable time to the short circuit current of the wire
Use Table 4.5.1-2 for the short-time capacity of the wire.
Obtain the operating time of the MCCB from the catalogue for it or engineering documents.

### 4.5.1.2 Voltage drop

Since the wiring distance inside a cabinet is short, it is unlikely that any problem will occur even if the wire size is determined based on the permissible current. However, it is necessary to check for a voltage drop when considering wiring, including external cables. The wire size is determined by its electric resistance, not its permissible current, if the wiring distance is long.
Calculate a voltage drop using the equation given below.

$$
\begin{array}{cl}
\Delta V= & \frac{\sqrt{3} \times r \times \lambda \times I}{1000} \quad \ldots \quad \text { Equation 4.5.1-1 } \\
\Delta \mathrm{V} & : \text { Voltage drop }[\mathrm{V}] \\
r & : \begin{array}{l}
\text { Resistance value corresponding to the } \\
\\
\lambda
\end{array} \quad \begin{array}{l}
\text { conductor temperature }[\Omega / \mathrm{km}] \\
\mathrm{I}
\end{array} \\
\text { : } & \text { Passing distance }[\mathrm{m}] \\
\text { Parrent }[\mathrm{A}]
\end{array}
$$

Calculate the value of $r$ using the equation given below.
$r=K \cdot r 20$
K : Temperature correction factor
r20: Conductor resistance value at $20^{\circ} \mathrm{C}[\Omega]$


Figure 4.5.1-3: Temperature correction factor K

### 4.5.2 Recommended wire size

### 4.5.2.1 3-phase 400V series (MD spec)

Table 4.5.2-1: Recommended wire sizes (MD spec, ambient temperature: $40^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRNロ } \\ & \text { VG1S } \end{aligned}$ | DC bus bars P (+), N (-) |  |  |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  |  | $\begin{gathered} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {\left[\begin{array}{l}  \\ {[\mathrm{G}]} \\ {\left[\mathrm{mm}^{2}\right]} \end{array}\right.} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  |  | When diode rectifier is used |  |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |  |  |  |
|  |  | Permissibletemperature* ${ }^{*}\left[\mathrm{~mm}^{2}\right]$ |  |  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right.$ ] |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{D}} \\ & \text { Div } \\ & 0 \\ & 0 \end{aligned}$ |  | $\begin{gathered} \text { Permissible } \\ \text { temperature* }\left[\mathrm{mm}^{2}\right] \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \hline \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{gathered}$ |  |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 30 | 30S | 14 | 8 | 5.5 | 55 | 14 | 8 | 8 | 65 | t3×25 | 14 | 8 | 5.5 | - | 60 | 5.5 |
| 37 | 37 S |  | 14 | 8 | 68 | 22 | 14 | 14 | 80 | (75) | 22 | 14 | 8 |  | 75 | 8 |
| 45 | 45 S | 22 |  | 14 | 82 | 38 | 22 |  | 97 |  |  |  | 14 |  | 91 | 14 |
| 55 | 55S | 38 | 22 |  | 101 | 38 |  | 22 | 119 | t3×30 | 38 | 22 |  |  | 112 |  |
| 75 | 75 S | 60 | 38 | 22 | 137 | 60 | 38 | 38 | 162 | (90) | 60 | 38 | 38 |  | 150 | 22 |
| 90 | 90S |  |  | 38 | 164 | 100 | 60 |  | 195 |  |  | 60 |  |  | 176 |  |
| 110 | 110 S | 100 | 60 |  | 201 |  | 100 | 60 | 238 |  | 100 |  | 60 |  | 210 |  |
| 132 | 132S |  | 100 | 60 | 241 | 150 |  | 100 | 286 | $\begin{aligned} & \hline \mathrm{t} 4 \times 40 \\ & (160) \end{aligned}$ | 150 | 100 |  | $\begin{aligned} & \hline \mathrm{t} 5 \times 30 \\ & (150) \end{aligned}$ | 253 | 38 |
| 160 | 160S | 150 |  | 100 | 292 | 200 | 150 |  | 347 |  |  |  | 100 |  | 304 |  |
| 200 | 200 S | 200 | 150 |  | 365 | 250 | 200 | 150 | 433 |  | 200 | 150 |  |  | 377 | 60 |
| 220 | 220 S | 250 |  | 150 | 402 | 325 |  |  | 476 | $\begin{aligned} & \hline \mathrm{t} 8 \times 50 \\ & (400) \end{aligned}$ | 250 |  | 150 | $\begin{gathered} \hline \mathrm{t} 10 \\ \times 30 \\ (300) \end{gathered}$ | 415 |  |
| 250 | 250S | 325 | 200 |  | 457 | $2 \times 200$ | 250 | 200 | 541 |  | 325 | 200 |  |  | 468 |  |
| 280 | 280S |  | 250 | 200 | 512 |  | 325 | 250 | 606 |  |  | 250 | 200 |  | 520 |  |
| 315 | 315S | 2×200 |  |  | 576 | $2 \times 250$ |  |  | 682 |  | $2 \times 200$ |  |  |  | 585 |  |
| 630 | 630B | - | - | - | 1151 | - | - | - | 1365 | $\begin{aligned} & \hline \mathrm{t} 8 \times 50 \\ & (400) \end{aligned}$ | - | $3 \times 250$ | $2 \times 250$ | $\begin{array}{\|c} \hline \mathrm{t} 10 \\ \times 125 \\ (1250) \\ \hline \end{array}$ | 1170 | 150 |
| 710 | 710B | - | - | - | 1298 | - | - | - | 1538 |  | - | $4 \times 250$ | $2 \times 325$ |  | 1370 |  |
| 800 | 800B | - | - | - | 1462 | - | - | - | 1733 |  | - | $4 \times 325$ | $3 \times 325$ |  | 1480 |  |

*An "IV wire," a "600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.
Note (1) The current values of the DC bus bar were calculated on the assumption that the converter (PWM converter or diode rectifier) supply voltage was 400 V AC.
(2) The grounding wire is cited from the permissible short circuit current defined in internal wire regulations.
(3) When using wires of $150 \mathrm{~mm}^{2}$ or greater, use relay bus bars so that the wires can be connected. (The Frame 3 and 4 size inverters' output terminals are configured to connect wires by use of relay bus bars.)
(4) Use bus bars to connect to a DC line of 630 kW or greater. It is also recommended that the inverter output side be connected using a bus bar.

Table 4．5．2－2：Recommended wire sizes（MD spec，ambient temperature： $50^{\circ} \mathrm{C}$ ）

|  | $\begin{aligned} & \text { FRND } \\ & \text { VG1S } \end{aligned}$ | DC bus bars $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |  |  |  | Inverter output［U，V，W］ |  |  |  |  | $\begin{gathered} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {\left[\begin{array}{c}  \\ \mathrm{G}] \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{array}\right]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  |  | When diode rectifier is used |  |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |  |  |  |
|  |  | Permissible temperature ${ }^{*}\left[\mathrm{~mm}^{2}\right.$ ］ |  |  | $\begin{aligned} & \text { 若导 } \\ & \text { 苞 } \end{aligned}$ | Permissible temperature＊${ }^{\left[\mathrm{mm}^{2}\right]}$ |  |  |  |  | Permissible temperature＊$\left[\mathrm{mm}^{2}\right.$ ］ |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{gathered}$ |  |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 30 | 30 S | 22 | 8 | 5.5 | 55 | 22 | 14 | － | 60 | $\begin{gathered} \hline \mathrm{t} 3 \times 25 \\ (75) \end{gathered}$ | 22 | 14 | 8 | － | 60 | 5.5 |
| 37 | 37 S | 38 | 14 | 8 | 68 | 38 |  |  | 75 |  | 38 |  | 14 |  | 75 | 8 |
| 45 | 45S |  | 22 | 14 | 82 | 60 | 22 |  | 91 |  |  | 22 |  |  | 91 | 14 |
| 55 | 55 S | 60 |  |  | 101 |  | 38 |  | 112 | t3×30 | 60 | 38 | 22 |  | 112 |  |
| 75 | 75 S | 100 | 38 | 38 | 137 | 100 | 60 |  | 150 | （90） | 100 | 60 | 38 |  | 150 | 22 |
| 90 | 90S |  | 60 |  | 164 | 150 |  |  | 176 |  | 150 |  |  |  | 176 |  |
| 110 | 110S | 150 | 100 | 60 | 201 | 200 | 100 |  | 210 |  |  | 100 | 60 |  | 210 |  |
| 132 | 132 S | 200 |  |  | 241 | 250 | 150 | t5×30 | 253 | $\begin{aligned} & \hline \mathrm{t} 4 \times 40 \\ & (160) \end{aligned}$ | 200 |  | 100 | $\begin{aligned} & \hline \mathrm{t} 5 \times 30 \\ & (150) \end{aligned}$ | 253 | 38 |
| 160 | 160 S | 250 | 150 | 100 | 292 | 325 |  | （150） | 304 |  | 250 | 150 |  |  | 304 |  |
| 200 | 200S | 325 | 200 | 150 | 365 | $2 \times 200$ | 250 |  | 377 |  | 325 | 200 | 150 |  | 377 | 60 |
| 220 | 2205 | $2 \times 200$ |  |  | 402 | 2×250 |  | t10 | 415 | t8×50 | 2×200 |  |  | t10 | 415 |  |
| 250 | 250S | 2×250 | 250 | 200 | 457 | $2 \times 325$ | 325 | $\times 30$ | 468 | （400） | 2×250 | 250 |  | $\begin{gathered} \times 30 \\ (300) \end{gathered}$ | 468 |  |
| 280 | 280S |  | 325 |  | 512 |  | $\begin{gathered} 2 \times 20 \\ 0 \end{gathered}$ | （300） | 520 |  |  | 325 |  |  | 520 |  |
| 315 | 315S | $2 \times 325$ |  | 250 | 576 | $3 \times 325$ |  |  | 585 |  | $2 \times 325$ |  |  |  | 585 |  |
| 630 | 630B | － | － | － | 1151 | － | － | － | 1170 | $\begin{aligned} & \hline \mathrm{t} 8 \times 50 \\ & (400) \end{aligned}$ | － | $4 \times 250$ |  | $\begin{gathered} \mathrm{t} 10 \\ \times 125 \\ (1250) \end{gathered}$ | 1170 | 150 |
| 710 | 710B | － | － | － | 1298 | － | － | － | 1370 |  | － | $4 \times 325$ |  |  | 1370 |  |
| 800 | 800B | － | － | － | 1462 | － | － | － | 1480 |  | － | $5 \times 325$ |  |  | 1480 |  |

＊An＂IV wire，＂a＂600 V HIV insulated wire，＂and a＂ 600 V cross－linked polyethylene insulated wire＂were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$ ，and $90^{\circ} \mathrm{C}$ ，respectively，and the values represent aerial wiring．
Note（1）The current values of the DC bus bar were calculated on the assumption that the converter（PWM converter or diode rectifier）supply voltage was 400 V AC．
（2）The grounding wire is cited from the permissible short circuit current defined in internal wire regulations．
（3）When using wires of $150 \mathrm{~mm}^{2}$ or greater，use relay bus bars so that the wires can be connected．（The Frame 3 and 4 size inverters＇output terminals are configured to connect wires by use of relay bus bars．）
（4）Use bus bars to connect to a DC line of 630 kW or greater．It is also recommended that the inverter output side be connected using a bus bar．

### 4.5.2.2 3-phase 400V series (LD spec)

Table 4.5.2-3: Recommended wire sizes (LD spec, ambient temperature: $40^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRN } \square \\ & \text { VG1S } \end{aligned}$ | DC bus bars [ $\mathrm{P}(+), \mathrm{N}(-)]$ |  |  |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  |  | $\begin{gathered} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {\left[{ }_{\mathrm{EG}]}\right.} \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  |  | When diode rectifier is used |  |  |  | Bus <br> bar <br> size <br> [ $\mathrm{mm}^{2}$ ] |  |  |  |  |  |  |
|  |  | Permissible temperature ${ }^{*}\left[\mathrm{~mm}^{2}\right]$ |  |  | 䓂哥 | Permissible temperature* $\left[\mathrm{mm}^{2}\right]$ |  |  |  |  | Permissible temperature* $\left.{ }^{\text {[ }} \mathrm{mm}^{2}\right]$ |  |  | $\begin{gathered} \hline \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{D}} \\ & \stackrel{y}{\omega} \mathbb{~} \\ & \underset{0}{2} \end{aligned}$ |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 37 | 30S | 14 | 14 | 8 | 68 | 22 | 14 | 14 | 80 | $\begin{gathered} \hline \mathrm{t} 3 \times 25 \\ (75) \end{gathered}$ | 22 | 14 | 8 | - | 75 | 8 |
| 45 | 37S | 22 |  | 14 | 82 | 38 | 22 |  | 97 |  |  |  | 14 |  | 91 | 14 |
| 55 | 45S | 38 | 22 |  | 101 |  |  | 22 | 119 |  | 38 | 22 |  |  | 112 |  |
| 75 | 55S | 60 | 38 | 22 | 137 | 60 | 38 | 38 | 162 | $\mathrm{t} 3 \times 30$ | 60 | 38 | 38 |  | 150 | 22 |
| 90 | 75S |  |  | 38 | 164 | 100 | 60 |  | 195 | (90) |  | 60 |  |  | 176 |  |
| 110 | 90S | 100 | 60 |  | 201 |  | 100 | 60 | 238 |  | 100 |  | 60 |  | 210 |  |
| 132 | 110 S |  | 100 | 60 | 241 | 150 |  | 100 | 286 |  | 150 | 100 |  |  | 253 | 38 |
| 160 | 132S | 150 |  | 100 | 292 | 200 | 150 |  | 347 | $\begin{aligned} & \mathrm{t} 4 \times 40 \\ & (160) \end{aligned}$ |  |  | 100 | t5×30 | 304 |  |
| 200 | 160S | 200 | 150 |  | 365 | 250 | 200 | 150 | 433 |  | 200 | 150 |  | (150) | 377 | 60 |
| 220 | 2005 | 250 |  | 150 | 402 | 325 |  |  | 476 |  | 250 |  | 150 |  | 415 |  |
| 250 | 220 S | 325 | 200 |  | 457 |  | 250 | 200 | 541 | t8 $\times 50$ | 325 | 200 |  | t10 | 468 |  |
| 280 | 250S |  | 250 | 200 | 512 | $2 \times 200$ | 325 | 250 | 606 | (400) |  | 250 | 200 | $\begin{gathered} \times 30 \\ (300) \end{gathered}$ | 520 |  |
| 315 | 280S | 2×200 |  |  | 576 | $2 \times 250$ |  |  | 682 |  | $2 \times 200$ |  |  |  | 585 |  |
| 355 | 315S | 2×250 | 325 | 250 | 649 | $2 \times 325$ | 2x200 | 325 | 769 |  | 2×250 | 325 | 250 |  | 650 | 100 |
| 710 | 630B | - | - | - | 1151 | - | - | - | 1538 | $\begin{aligned} & \hline \mathrm{t} 8 \times 50 \\ & (400) \end{aligned}$ | - | 4×250 | $2 \times 325$ | $\begin{gathered} \mathrm{t} 10 \\ \times 125 \\ (1250) \end{gathered}$ | 1370 | 150 |
| 800 | 710B | - | - | - | 1298 | - | - | - | 1733 |  | - | $4 \times 325$ | $3 \times 325$ |  | 1480 |  |
| 1000 | 800B | - | - | - | 1462 | - | - | - | 2166 |  | - | $5 \times 325$ | $4 \times 325$ |  | 1850 | 2×150 |

Table 4.5.2-4: Recommended wire sizes (LD spec, ambient temperature: $50^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRN } \\ & \text { VG1S } \end{aligned}$ | DC bus bars [P (+), N (-)] |  |  |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  |  | $\begin{array}{\|c} \begin{array}{c} \text { Ground- } \\ \text { ing } \\ \text { terminal } \end{array} \\ {\left[\mathrm{E}^{2}\right]} \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  |  | When diode rectifier is used |  |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |  |  |  |
|  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right.$ ] |  |  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right]$ |  |  |  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right.$ ] |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{\omega}} \\ & \stackrel{y}{3} \mathbb{S} \\ & \hline \end{aligned}$ |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 37 | 30S | 38 | 14 | 8 | 68 | 38 | 14 | 14 | 80 | $\begin{gathered} \mathrm{t} 3 \times 25 \\ (75) \end{gathered}$ | 38 | 14 | 14 | - | 75 | 8 |
| 45 | 37S |  | 22 | 14 | 82 | 60 | 22 |  | 97 |  |  | 22 |  |  | 91 | 14 |
| 55 | 45S | 60 |  |  | 101 |  | 38 | 22 | 119 |  | 60 | 38 | 22 |  | 112 |  |
| 75 | 55S | 100 | 38 | 38 | 137 | 100 | 60 | 38 | 162 | $\left\lvert\, \begin{gathered} \mathrm{t} 3 \times 30 \\ (90) \end{gathered}\right.$ | 100 | 60 | 38 |  | 150 | 22 |
| 90 | 75S |  | 60 |  | 164 | 150 |  | 60 | 195 |  | 150 |  |  |  | 176 |  |
| 110 | 90S | 150 | 100 | 60 | 201 | 200 | 100 |  | 238 |  |  | 100 | 60 |  | 210 |  |
| 132 | 110S | 200 |  |  | 241 | 250 | 150 | 100 | 286 |  | 200 |  | 100 |  | 253 | 38 |
| 160 | 132S | 250 | 150 | 100 | 292 | 325 |  | 150 | 347 | t4×40 | 250 | 150 |  | $\begin{aligned} & t 5 \times 30 \\ & (150) \end{aligned}$ | 304 |  |
| 200 | 160S | 325 | 200 | 150 | 365 | $2 \times 200$ | 250 |  | 433 | (160) | 325 | 200 | 150 |  | 377 | 60 |
| 220 | 200S | $2 \times 200$ |  |  | 402 | $2 \times 250$ |  | 200 | 476 |  | $2 \times 200$ |  |  |  | 415 |  |
| 250 | 220S | 2×250 | 250 | 200 | 457 | $2 \times 325$ | 325 | 250 | 541 | $\begin{aligned} & t 8 \times 50 \\ & (400) \end{aligned}$ | $2 \times 250$ | 250 | 200 | $\begin{gathered} \mathrm{t} 10 \\ \times 30 \\ (300) \end{gathered}$ | 468 |  |
| 280 | 250S |  | 325 |  | 512 |  | 2×200 |  | 606 | (400) |  | 325 |  |  | 520 |  |
| 315 | 280S | $2 \times 325$ |  | 250 | 576 | $3 \times 325$ |  | 325 | 682 |  | $2 \times 325$ |  | 250 |  | 585 |  |
| 355 | 315S | $3 \times 325$ | $2 \times 200$ | 325 | 649 | $4 \times 325$ | 2×250 | $2 \times 200$ | 769 |  | $3 \times 325$ | $2 \times 200$ | 325 |  | 650 | 100 |
| 710 | 630B | - | $3 \times 325$ | $2 \times 325$ | 1151 | - | $5 \times 325$ | $4 \times 325$ | 1538 | t8×50 | - | $4 \times 325$ | $3 \times 325$ | t10 | 1370 | 150 |
| 800 | 710B | - | $4 \times 325$ | $3 \times 325$ | 1298 | - | - |  | 1733 | (400) | - | $5 \times 325$ | $4 \times 325$ | $\times 125$ | 1480 |  |
| 1000 | 800B | - | $5 \times 325$ | $4 \times 325$ | 1462 | - | - | - | 2166 |  | - | - | $5 \times 325$ | (1250) | 1850 | $2 \times 150$ |

*An "IV wire," a " 600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at
permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.
Note (1) The current values of the DC bus bar were calculated on the assumption that the converter (PWM converter or diode rectifier) supply voltage was 400 V AC.
(2) The grounding wire is cited from the permissible short circuit current defined in internal wire regulations.
(3) When using wires of $150 \mathrm{~mm}^{2}$ or greater, use relay bus bars so that the wires can be connected. (The Frame 3 and 4 size inverters' output terminals are configured to connect wires by use of relay bus bars.)
(4) Use bus bars to connect to a DC line of 630 kW or greater. It is also recommended that the inverter output side be connected using a bus bar.

### 4.5.2.3 3-phase 690V series (MD/LD spec)

Table 4.5.2-5: Recommended wire sizes (MD spec, ambient temperature: $40^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRN } \square \\ & \text { VG1S } \end{aligned}$ | DC bus bars [P(+), N (-)] |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  | $\begin{gathered} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {[\stackrel{B}{\mathrm{E}}]} \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  | When diode rectifier is used |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |  |  |
|  |  | Permissible temperature ${ }^{*}\left[\mathrm{~mm}^{2}\right]$ |  |  | $\begin{gathered} \text { Permissible } \\ \text { temperature* }\left[\mathrm{mm}^{2}\right] \end{gathered}$ |  |  |  | $\begin{gathered} \text { Permissible } \\ \text { temperature* }\left[\mathrm{mm}^{2}\right] \end{gathered}$ |  | Bus <br> bar <br> size <br> [ $\mathrm{mm}^{2}$ ] |  |  |
|  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 90 | 90S | 35 | 25 | 95 | 50 | 35 | 114 | t2×30 | 35 | 25 | - | 100 | 14 |
| 110 | 110S | 50 | 35 | 117 | 70 | 50 | 139 | (60) | 50 | 35 |  | 130 | 22 |
| 132 | 132S | 70 | 50 | 140 |  |  | 167 | t3×45 | 70 | 50 | t4×30 | 140 |  |
| 160 | 160S |  | 70 | 170 | 95 | 70 | 201 | (135) |  |  | (120) | 161 |  |
| 200 | 200S | 120 |  | 212 | 150 | 95 | 252 |  | 120 | 95 |  | 216 |  |
| 250 | 250S | $2 \times 70$ | $2 \times 50$ | 265 | $2 \times 95$ | $2 \times 70$ | 316 | t4×50 | $2 \times 70$ | $2 \times 50$ | t6×30 | 265 | 38 |
| 280 | 280S | 2×95 | $2 \times 70$ | 297 |  |  | 352 | (200) |  | $2 \times 70$ | (180) | 295 |  |
| 315 | 315S |  |  | 334 | $2 \times 120$ | $2 \times 95$ | 396 |  | $2 \times 95$ |  |  | 330 |  |
| 355 | 355S | $2 \times 120$ | $2 \times 95$ | 376 | $2 \times 150$ |  | 446 |  | $2 \times 120$ |  |  | 365 | 60 |
| 400 | 400S | $2 \times 150$ |  | 424 | $2 \times 185$ | $2 \times 120$ | 503 |  |  | $2 \times 95$ |  | 410 |  |
| 450 | 450S | $2 \times 185$ | $2 \times 150$ | 477 | $2 \times 240$ | $2 \times 150$ | 563 |  | $2 \times 150$ | $2 \times 120$ |  | 460 |  |

Table 4.5.2-6: Recommended wire sizes (LD spec, ambient temperature: $40^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRN } \square \\ & \text { VG1S } \end{aligned}$ | DC bus bars [P (+), N (-)] |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  | Grounding terminal [ $\left.{ }^{3} \mathrm{G}\right]$ <br> [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  | When diode rectifier is used |  |  | Bus <br> bar <br> size <br> [ $\mathrm{mm}^{2}$ ] |  |  |  |  |  |
|  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right.$ ] |  |  | Permissible temperature ${ }^{*}\left[\mathrm{~mm}^{2}\right]$ |  |  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right]$ |  | Bus <br> bar <br> size <br> [ $\mathrm{mm}^{2}$ ] | $\stackrel{\rightharpoonup}{\stackrel{\rightharpoonup}{\omega}} \underset{\substack{0 \\ 0}}{ }$ |  |
|  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 110 | 90S | 50 | 35 | 117 | 70 | 50 | 139 | t2×30 | 50 | 35 | - | 130 | 22 |
| 132 | 110S | 70 | 50 | 140 |  |  | 167 | t $3 \times 45$ | 70 | 50 |  | 140 |  |
| 160 | 132S |  | 70 | 170 | 95 | 70 | 201 | (135) |  |  | t4×30 | 161 |  |
| 200 | 160S | 120 |  | 212 | 150 | 95 | 252 | $\begin{aligned} & \mathrm{t} 4 \times 50 \\ & (200) \end{aligned}$ | 120 | 95 | (120) | 216 |  |
| 220 | 200S |  | 95 | 233 |  | 120 | 277 |  |  |  |  | 235 | 38 |
| 280 | 250S | $2 \times 95$ | $2 \times 70$ | 297 | $2 \times 95$ | $2 \times 70$ | 352 |  | $2 \times 70$ | $2 \times 70$ | t6×30 | 295 |  |
| 315 | 280S |  |  | 334 | $2 \times 120$ | $2 \times 95$ | 396 |  | $2 \times 95$ |  | (180) | 330 |  |
| 355 | 315S | $2 \times 120$ | $2 \times 95$ | 376 | $2 \times 150$ |  | 446 |  | 2×120 |  |  | 365 | 60 |
| 400 | 355S | $2 \times 150$ |  | 424 | $2 \times 185$ | $2 \times 120$ | 503 |  |  | $2 \times 95$ |  | 410 |  |
| 450 | 400S | $2 \times 185$ | $2 \times 150$ | 530 | $2 \times 240$ | $2 \times 150$ | 563 |  | $2 \times 150$ | $2 \times 120$ |  | 460 |  |

*A "PVC (polyvinyl chloride) wire" and an "XLPE (cross-linked polyethylene) wire" were used at permissible temperatures of $70^{\circ} \mathrm{C}$ and $90^{\circ} \mathrm{C}$, respectively, and the wire sizes were selected based on the permissible current under the following conditions. If the use conditions are different, select the wire sizes based on use conditions that comply with IEC 60364-5-52:2001(JIS C 60364-5-52:2006).
Ambient temperature: $40^{\circ} \mathrm{C}$, Multicore cable: 3 cores (conductor: copper), A single cable: aerial wiring, Two or more cables: electric duct wiring
Note (1) The current values of the DC bus bar were calculated on the assumption that the converter (PWM converter or diode rectifier) input voltage was $690 \vee$ AC.
(2) When using wires of $150 \mathrm{~mm}^{2}$ or greater, use relay bus bars so that the wires can be connected. (The frame 3 and 4 size inverters' output terminals are configured to connect wires by use of relay bus bars.)
(3) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

Table 4.5.2-7: Recommended wire size, domestic selection (MD spec., ambient temperature $40^{\circ} \mathrm{C}$ )

|  | FRN VG1S | DC bus bars [ $\mathrm{P}(+), \mathrm{N}(-)]$ |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  | $\left\{\begin{array}{c} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {[\ni \mathrm{G}]} \\ {\left[\mathrm{mm}^{2}\right]} \end{array}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  | When diode rectifier is used |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] |  |  |  |  |  |
|  |  | Permissible temperature ${ }^{*}$ [ $\mathrm{mm}^{2}$ ] |  |  | $\begin{gathered} \text { Permissible } \\ \text { temperature* }\left[\mathrm{mm}^{2}\right] \end{gathered}$ |  |  |  | Permissible temperature ${ }^{*}\left[\mathrm{~mm}^{2}\right]$ |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current [A] |  |
|  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 90 | 90S | 14 | 14 | 95 | 22 | 22 | 114 | t2×30 | 22 | 14 | - | 100 | 14 |
| 110 | 110 S | 22 | 22 | 117 | 38 |  | 139 | (60) | 38 | 22 |  | 130 | 22 |
| 132 | 132 S | 38 |  | 140 |  | 38 | 167 | t $3 \times 45$ |  |  | t4×30 | 140 |  |
| 160 | 160S |  | 38 | 170 | 60 |  | 201 | (135) |  | 38 | (120) | 161 |  |
| 200 | 200 S | 60 | 60 | 212 | 100 | 60 | 252 |  | 60 | 60 |  | 216 |  |
| 250 | 250S | 100 |  | 265 |  | 100 | 316 | t4×50 | 100 |  | t6×30 | 265 | 38 |
| 280 | 280S |  | 100 | 297 | 150 |  | 352 | (200) |  | 100 | (180) | 295 |  |
| 315 | 315S | 150 |  | 334 |  | 150 | 396 |  | 150 |  |  | 330 |  |
| 355 | 355S |  |  | 376 | 200 |  | 446 |  |  |  |  | 365 | 60 |
| 400 | 400S |  | 150 | 424 |  |  | 503 |  |  | 150 |  | 410 |  |
| 450 | 450S | 200 |  | 530 | 250 | 200 | 563 |  | 200 |  |  | 460 |  |

Table 4.5.2-8: Recommended wire size, domestic selection (LD spec., ambient temperature $40^{\circ} \mathrm{C}$ )

|  | $\begin{aligned} & \text { FRNロ } \\ & \text { VG1S } \end{aligned}$ | DC bus bars [ $\mathrm{P}(+), \mathrm{N}(-)]$ |  |  |  |  |  |  | Inverter output [U, V, W] |  |  |  | $\begin{gathered} \text { Ground- } \\ \text { ing } \\ \text { terminal } \\ {[\Xi \mathrm{G}]} \\ {\left[\mathrm{mm}^{2}\right]} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | When PWM converter is used |  |  | When diode rectifier is used |  |  | Bus <br> bar <br> size <br> [ $\mathrm{mm}^{2}$ ] |  |  |  |  |  |
|  |  | Permissible temperature* $\left[\mathrm{mm}^{2}\right]$ |  |  | $\begin{array}{\|c} \hline \text { Permissible } \\ \text { temperature }{ }^{*}\left[\mathrm{~mm}^{2}\right] \\ \hline \end{array}$ |  |  |  | $\begin{gathered} \text { Permissible } \\ \text { temperature }{ }^{*}\left[\mathrm{~mm}^{2}\right] \end{gathered}$ |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current <br> [A] |  |
|  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |
| 110 | 90S | 22 | 22 | 117 | 38 | 22 | 139 | t2×30 | 38 | 22 | - | 130 | 22 |
| 132 | 110 S | 38 |  | 140 |  | 38 | 167 | $\begin{aligned} & \hline \mathrm{t} 3 \times 45 \\ & (135) \\ & \hline \end{aligned}$ |  |  |  | 140 |  |
| 160 | 132 S |  | 38 | 170 | 60 |  | 201 |  |  | 38 | t4×30 | 161 |  |
| 200 | 160S | 60 | 60 | 212 | 100 | 60 | 252 | $\begin{aligned} & \hline \mathrm{t} 4 \times 50 \\ & (200) \end{aligned}$ | 60 | 60 | (120) | 216 |  |
| 220 | 200S |  |  | 233 |  |  | 277 |  | 100 |  |  | 235 | 38 |
| 280 | 250 S | 100 | 100 | 297 | 150 | 100 | 352 |  |  | 100 | $\begin{aligned} & \hline 6 \times 30 \\ & (180) \end{aligned}$ | 295 |  |
| 315 | 280 S | 150 |  | 334 |  | 150 | 396 |  | 150 |  |  | 330 |  |
| 355 | 315S |  |  | 376 | 200 |  | 446 |  |  |  |  | 365 | 60 |
| 400 | 355S |  | 150 | 424 |  |  | 503 |  |  | 150 |  | 410 |  |
| 450 | 400S | 200 |  | 530 | 250 | 200 | 563 |  | 200 |  |  | 460 |  |

*: The power supply voltage is 690 VAC.
Note (1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
(2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

### 4.5.3 Wiring of main circuit and grounding terminals

(1) Inverter output terminals U, V, and W and terminal eg for motor grounding

1) Connect the inverter output terminals $U, V$, and $W$ to the terminals $U, V$, and $W$ of the three-phase motor in the correct order of phases.
2) Connect the grounding wire of the output wires ( $\mathrm{U}, \mathrm{V}$, and W ) to the terminal ( $\because \mathrm{G}$ ) for grounding.

Note When multiple combinations of inverters and motors exist, do not use multicore cables for the purpose of handling the wiring together.


## (2) Terminal EG for inverter grounding

This is the grounding terminal provided with the chassis (case) of the inverter. Do not fail to connect the grounding terminal for safety and as a measure against noise. Technical standards concerning electrical equipment make it mandatory to perform grounding work of metallic frames for electrical appliances to prevent electric shock or fire.

Connect the grounding terminal on the power supply side as described below.

1) According to technical standards concerning electrical equipment, connect the grounding terminal to a grounding pole to which class C grounding work was applied.
2) Connect a thick grounding wire having a large surface area along as short a route as possible.
3) For 132 to 450 kW stacks, follow Figure 4.5.3-1 and Figure 4.5.3-2 on the connections to grounding terminals.

Table 4.5.3-1: Grounding of appliances according to technical standards concerning electrical equipment

| Type of grounding work | Grounding resistance |
| :--- | :--- |
| Class C grounding work | $10 \Omega$ or less |

Figure 4.5.3-1: Example of grounding wiring for Frame 3 size ( 132 to 200 kW )



Figure 4.5.3-2: Example of grounding wiring for Frame 4 size (220 to 450 kW )
(3) Inverter DC bus bar connection terminals/converter output terminals P (+), N (-)

The inverter uses DC (direct current) input and the converter uses DC (direct current) output terminals.
Bus bar connections are assumed, but when connecting by electric lines, keep the distance between the stacks to max. 2 m .
When connecting to the DC bus bar by wires, keep the distance to max. $\mathbf{2 m}$.


Figure 4.5.3-3: Restriction when connecting $\mathrm{P}(+)$ and $\mathrm{N}(-)$ terminals by electric lines
When using long electric lines, route the $P(+)$ and $N(-)$ lines together and do not route beside control circuits.
(Do not route the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ electric lines separately.)

## (4) Control power auxiliary input terminals R0 and T0

The inverter can operate even if the power is not supplied to the control power auxiliary input terminals. However, if the main power to the inverter is turned off, the control power will also be shut down, and output signals of the inverter and the keypad will be no longer displayed.
To retain an alarm output signal to be issued when the protective function operates or keep the keypad displayed even if the main power to the inverter is shut down, connect the power to the control power auxiliary input terminals. If a magnetic contactor ( MC ) is used on the input side of the inverter, connect the wire from the input (primary) side of the MC.
Terminal rating: 400 V series: 380 to $480 \mathrm{~V} \mathrm{AC}, 50 / 60 \mathrm{~Hz}$, maximum current 0.5 A
690 V series: 575 to $690 \mathrm{VAC}, 50 / 60 \mathrm{~Hz}$, maximum current 0.5 A


Figure 4.5.3-4: Connection of terminals R0 and T0

| Terminal name | Recommended wire size [mm ${ }^{2}$ ] |
| :---: | :---: |
| Control power auxiliary input terminals R0 and T0 | 2.0 |

Note If wires of a larger size than a recommended wire size are used, they may not be inserted into the control cable lead-in hole in the front cover depending on the number of wires.

When connecting the FRENIC-VG to a PWM converter by connecting the power to the control power auxiliary input terminals (R0 and TO) of the FRENIC-VG, insert an isolation transformer or the auxiliary $b$ contact of a magnetic contactor on the power supply side as shown in Figure 4.5.3-4.
When adding an isolation transformer, select the appropriate isolation transformer based on the sum of the required capacities of the FRENIC-VG and PWM converter, referring to the following tables:

## - Required transformer capacity for the inverter (FRENIC-VG)



- Required transformer capacity for the converter (RHC-D series)

| Model | 132S | 160S | 200S | 220 S | 250S | 280S | 315S | 355S | 400S | 450S | 500S | 630B | 710B | 800B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RHCD-4D $\square$ | 200VA |  |  |  | - | 200VA |  | - |  |  |  | 600VA |  |  |
| RHCD-69D $\square$ | 200VA |  |  | - | 200VA |  |  |  |  |  | - |  |  |  |

(5) Fan power auxiliary input terminals R1 and T1

400 V stacks with 90 kW or higher capacity and all 690 V stacks are equipped with fan power supply terminals, so connect them to AC power supply. Switch the fan power supply switching connectors "U1" and "U2" according to the power supply specifications.

## Terminal rating:

- 400 V series: $\quad 380$ to $440 \mathrm{VAC} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}$, Maximum current: 1.0 A
(For phase-specific stacks, the maximum current is 3 times larger than above.)
-690V series: $\quad 660$ to 690 VAC, $50 / 60 \mathrm{~Hz}$, maximum current 1.0 A
575 to $600 \mathrm{VAC}, 50 / 60 \mathrm{~Hz}$, maximum current 1.0 A
- Inverter (FRENIC-VG) - Rated capacity of terminals R1 and T1

| Model | 90 | 110 | 132 | 160 | 200 | 220 | 250 | 280 | 315 | 355 | 400 | 450 | 630 | 710 | 800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FRN $\square$ VG1S-4 $\square$ | 100 VA |  |  |  |  | 200 VA |  |  |  | - |  |  | 600 VA |  |  |
| FRN $\square$ VG1S-69 $\square$ | 100 VA |  |  |  |  | - | 200 VA |  |  |  |  |  | - |  |  |

## - Converter (RHC-D series) - Rated capacity of terminals R3 and T3

| Model | 132S | 160S | 200S | 220S | 250S | 280S | 315S | 355S | 400S | 450S | 500S | 630B | 710B | 800B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RHCD-4D $\square$ | 100VA |  |  | 200VA | - | 200VA |  | - |  |  |  | 600VA |  |  |
| RHCD-69D $\square$ | 100VA |  |  | - | 200VA |  |  |  |  |  | - |  |  |  |

Fan power supply switching connectors are located on "Auxiliary power supply printed circuit board" attached to the lower section of the stack.

- 400 V series ( 90 kW or higher)

- 690 V series (all capacities)


| Configuration | Applied <br> voltage | 400 V series: 398 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 430$ to <br> $480 \mathrm{~V} / 60 \mathrm{~Hz}$ <br> 690 V series: 660 to $690 \mathrm{~V}, 50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ <br> (Factory shipping state) |
| :--- | :--- | :--- |

Figure 4.5.3-5: Description of fan power supply switching connector


Figure 4.5.3-6: Connection of terminals R1 and T1

| Terminal name | Recommended wire size $\left[\mathrm{mm}^{2}\right]$ |
| :---: | :---: |
| Fan power auxiliary input terminals R1 and T1 | 2.0 |

Note - Terminals R1 and T1 are insulated from terminals R0, T0, P (+), and N(-). Thus, terminals R1 and T1 do not require an isolation transformer, unlike terminals R0 and T0.
When inserting an MCCB2 in terminals R1 and T1 as shown in Figure 4.5.3-6, assign the auxiliary a contact of this MCBB2 to the operation interlock circuit of the inverter. When the MCCB2 is turned off, the cooling fan of the inverter will not run even if the inverter is in operation, and the inverter will cause an overheat trip.

- If wires of a larger size than a recommended wire size are used, they may not be inserted into the control cable lead-in hole in the front cover depending on the number of wires.


### 4.6 Control circuit

### 4.6.1 Screw specifications and recommended wire sizes

Table 4.6.1-1 shows the screw specifications and wire sizes for the wiring of the control circuit.
The control circuit terminal block is common regardless of the inverter capacity.
Table 4.6.1-1: Screw specifications and recommended wire sizes

| Common terminal | Screw specifications |  | Recommended wire size $\left[\mathrm{mm}^{2}\right]$ |
| :---: | :---: | :---: | :---: |
|  | Screw size | Tightening torque $[\mathrm{N} \cdot \mathrm{m}]$ |  |
| Control circuit <br> terminal | M3 | 0.7 | 1.25 |

Note If wires of a larger size than a recommended wire size are used, they may not be inserted into the control cable lead-in hole in the front cover depending on the number of wires.

### 4.6.2 Control terminal layout

Figure 4.6.2-1 shows the control terminal layout.


Figure 4.6.2-1: Control terminal layout

### 4.6.3 Control wire routes

In general, there are three control circuit wiring routes.
(1) DCF disconnection detection circuit wiring route. (The control wire is led into the stack from the upper area of the front face.)
(2) Route through which the control wire is led into the stack from the left side of the front cover.
(3) Route through which the control wire is led into the stack from the right side of the front cover.

If the control wire routed inside the stack comes into contact with any of the electronic parts inside the stack, the wire may burn out.
A binding fixture is attached to the inside of the stack. Bind the wire at the binding fixture.


Figure 4.6.3-1: Control wire routes for Frame 1 size ( 400 V : 30 to 45 kW ) (example)

### 4.6.4 DCF disconnection detection circuit wiring route

Figure 4.6.4-1 shows the DCF disconnection detection circuit wiring route. On the PCB, aluminum electrolytic capacitors, high-voltage circuits, and heat sinks for cooling electronic parts are packaged.
If the wire comes into contact with any of these parts, the part may come off due to vibrations. For this reason, do not fail to fasten the wire using the binding band fixture. In addition, exercise care not to apply an excessive tension to the wire.


Figure 4.6.4-1: DCF disconnection detection circuit wiring route

### 4.6.5 Wiring between phase-specific stacks

After phase-specific stack inverters (FRN630BVG1S-4 $\square$ to FRN800BVG1S-4 $\square$ ) are installed, stack-to-stack wiring is required. To connect the stacks, use the wires that come with the product. For details, refer to Figure 4.6.5-1 to Figure 4.6.5-3.

- Applicable inverter models: FRN630BVG1S-4 $\square$ to FRN800BVG1S-4 $\square$
- Applicable PWM converter models; RHC630B-4D $\square$ to RHC800B-4D $\square$

*The inverter has U-, V-, and W-phases. The PWM converter has R-, S-, and T-phases.
Figure 4.6.5-1: Gate, fuse disconnection alarm, and inverter overheat protection wires connected between phase-specific stacks


Figure 4.6.5-2: Auxiliary power supply and CT (current detection) wires connected between phase-specific stacks
[Inverter]

[PWM converter]


Figure 4.6.5-3: Details of CT (portion A) wiring route between phase-specific stacks

### 4.7 Mounting and connecting the keypad

The keypad can be mounted in the following patterns:

- Attaching the keypad to the inverter body (state at the time of the delivery of the inverter)
- Mounting the keypad on the door of the cabinet and remote-operating it (Refer to 4.7.2.2 Mounting the keypad on the door of the cabinet.)
- Remote-operating the keypad in your hand


Figure 4.7.1-1: Example of installing keypad

### 4.7.1 Parts required for mounting and connecting the keypad

Use a keypad extension cable produced by Fuji Electric or a commercially available LAN cable (straight) to connect the keypad and the inverter. When mounting the keypad on the door of the cabinet, fix it with screws from the inside face of the door.
The parts required for mounting and connecting the keypad are not attached to the inverter. Prepare them yourself.

| Part name | Model | Remarks |
| :--- | :--- | :--- |
| Keypad extension cable *1 | CB-1S, CB-3S, CB-5S | Available in three different lengths: $5 \mathrm{~m}, 3 \mathrm{~m}, 1 \mathrm{~m}$. <br> The number in each model indicates the length of <br> the cable. |
| Keypad fixing screw | $\mathrm{M} 3 \times 12 * 2$ | Two fixing screws are required. |

*1 When using a commercially available LAN cable, select a straight cable (within 20 m ) for 10BASE-T/100BASE-TX complying with the category 5 specification of ANSI/TIA/EIA-568A of the U.S.
<Recommended LAN cables>
Manufacturer: Sanwa Supply Inc.
Model : KB-10T5-01K (1 m)
: KB-STP-01K (1 m) - Shielded cable (with improved noise resistance). Use this cable to make the inverter compliant with EMC Directives.
*2 When mounting the keypad on the cabinet, use fixing screws of proper length for the thickness of the steel panel. When the thickness of the steel panel is 1.2 to 2.3 mm : Use M3 $\times 12$ screws. (When the thickness of the steel panel is 1 mm , use M3 $\times 10$ screws.)

### 4.7.2 Installation procedure

After the wiring of the inverter is completed, mount the keypad according to the procedure described below. Before mounting the keypad, turn off the power to the inverter. The procedure described here proceeds on the assumption that the inverter used is a unit type, but is also applicable to stack type inverters.

### 4.7.2.1 How to mount and remove the keypad on/from the inverter

(1) Holding down the hook marked with an arrow shown in the figure below, pull the keypad toward you and remove it.


Figure 4.7.2-1: Removing the keypad
(2) Set the keypad on the latches shown in the figure below. Push the keypad in the direction of the terminal cover (arrow (1)) into the case of the inverter (arrow (2)).


Figure 4.7.2-2: Mounting the keypad

### 4.7.2.2 Mounting the keypad on the door of the cabinet

(1) Cut the door of the cabinet on which the keypad will be mounted to the panel cutting dimensions shown in "4.7.2.3 External dimensions of the keypad" below.
(2) Mount the keypad as shown in Figure 4.7.2-3.

- Use M3 x 12 screws (thickness of the door: 2.3 mm ).
- Tightening torque: $0.7 \mathrm{~N} \cdot \mathrm{~m}$
(3) Connect the RJ-45 connector of the keypad and the RJ-45 connector (modular jack) of the inverter using the keypad extension cable or a commercially available LAN cable (straight).
(Refer to Figure 4.7.2-4.)

The cable may get caught between the door and the cabinet and get damaged when the door opens or closes. Fasten the cable with a tying part, such as INSULOK. However, do not tie the cable more than necessary.


Figure 4.7.2-3: Mounting the keypad


Figure 4.7.2-4: Connecting the keypad and the inverter

### 4.7.2.3 External dimensions of the keypad

The outside dimensions of the keypad are shown in the figure below. When mounting the keypad on the door of the cabinet, cut the door to the dimensions specified in the figure.


### 4.8 Connecting FRENIC-VG Loader

To use the FRNIC-VG Loader software that runs on a personal computer, it can be connected in the two ways described below. Select either connection method according to the usage of the equipment.
(1) Using the USB connector (mini type B) on the front panel of the stack inverter, connect a personal computer and an inverter.
(2) Using the RS-485 communications ports of the inverter control terminal, connect a personal computer and multiple inverters (up to 31 inverters can be connected) in a multidrop configuration.
$\mathbb{\square}$ For more information on FRENIC-VG Loader, refer to "FRENIC-VG Loader Instruction Manual (INR-SI47-1588 (WPS-VG1-STR), INR-SI47-1616 (WPS-VG1-PCL))."

Note - The RJ-45 connector for keypad connection is designed exclusively for keypad communication. It cannot be connected for RS-485 communication or to FRENIC-VG Loader.

- Do not connect an inverter to the LAN port of the personal computer, an Ethernet hub, or a telephone line. The inverter or the unit to which the inverter is connected may get damaged.


### 4.8.1 Connecting a USB

A USB cable connection port (closed by a plastic cover) is provided on the right side of the keypad.
A USB connector appears from under the cable connection port cover. Insert a USB cable into the port.


Figure 4.8.1-1: Connecting a USB cable

- The connector below the USB connector is reserved for manufacturer use and cannot be used.
- A USB cable is not attached to inverters or the FRNIC-VG Loader software (CD-ROM). Prepare one yourself.


### 4.8.2 Using the RS-485 communications ports

### 4.8.2.1 Terminal specifications of the RS-485 communications ports

Connect the RS-485 communications ports to the terminals for RS-485 communication [DX+, DX-: half-duplex system (two-wire system)] on the control circuit terminal block. In addition, a terminating resistor is contained (for switching). Set it according to the connection configuration.


Figure 4.8.2-1: RS-485 terminals (part of control terminal block)

| Terminal symbol | Description | Remarks |
| :--- | :--- | :--- |
| DX- | RS-485 communication <br> data $(-)$ | $112-\Omega$ terminating resistor <br> contained Switch |
| DX+ | RS-485 communication <br> data $(+)$ | connection/disconnection by <br> operating the SW4*1. |

*1 For details of the SW4, see "2.4.2.2 Setting up the slide switches" in Chapter 2.
*2 There is no grounding terminal for shielding. Ground the shielded wire to the host unit.

### 4.8.2 2 RS-485 converter

Standard personal computers are not provided with an RS-485 communications port but are provided with an RS-232C or USB communications port.
To prevent this problem, use an RS-232C/RS-485 converter or USB/RS-485 converter. Note that the inverter will not properly function if a converter other than a recommended one that underwent a communication performance check is used.
Recommended converters (System Sacom Industry Corp.)

| Name | Model | Remarks |
| :--- | :--- | :--- |
| RS-232C/RS-485 converter | KS-485PTI |  |
| USB/RS-485 converter | USB-485I RJ45-T4P | A converter fixture (UTK-01) is available. |

[^4]
### 4.8.2.3 Cables

Use twisted-pair shielded cables of $0.5 \mathrm{~mm}^{2}$ ( 0.3 to $1.25 \mathrm{~mm}^{2}$ ) [AWG20 (AWG16 to AWG22)].

## Recommended cables

- AWM2789 cable for long-distance connection (Furukawa Electric Co., Ltd. standard specification: DTS5023) 2-pair product
- Cat. 5E-compatible cable (Cat. 5 cable provided with a shield) when using a LAN cable

Website of Furukawa Electric Co., Ltd.: http://www.furukawa.co.jp/
FRENIC-VG loader (personal computer)

## Converter



Figure 4.8.2-2: Connection diagram
Note - Maximum wiring length: 500 m (There is no restriction on the wiring distance between stations.)

- Provide the end unit with a terminating resistor. The recommended converters and inverters contain a terminating resistor. Set the terminating resistor to "Connect" using the appropriate selector switch or jumper switch.
- Even if FRENIC-VG Loader is not used, keep active the RS-485 communications line between the converter and the inverter. (If the converter is disconnected from the communications line, the communications line will serve as an antenna, and the converter will malfunction due to noise.)


### 4.8.3 Noise reduction

In some working environments, noise produced by an inverter may cause abnormal communication or malfunctions of the master's instrumentation units, converters, etc.
See Appendix 5 "Proficient way to use inverters (on electric noise)" in addition to this section.

| $\underline{\text { Isolated converter }}$ | $:$ Use a recommended converter. |
| :--- | :--- |
| Twisted-pair shielded wire | $:$ Use a recommended wire. |
| Change of grounding | : If an instrumentation unit and an inverter are grounded together, they may malfunction. <br> Prepare grounding exclusively for instrumentation units. Use a large-size wire for <br> grounding. |
| Reinforcement of converter | Noise may propagate through the power supply for an instrumentation unit. It is <br> recommended that an isolation transformer for power supply (TRAFY), noise cutting <br> transformer, or LC filter be used. |
| Addition of inductance | By slipping a ferrite core over the signal circuit or using an LC filter, add inductance to <br> the circuit to ensure high impedance against high-frequency noise. |



Slip the ferrite core over the circuit or wind it around the circuit twice or three times.

Figure 4.8.3-1: Example of setting of ferrite core
Filtering
: Form a low-pass filter (LPF) by connecting capacitors to signal input/output terminals in
parallel to prevent rigging or high-frequency noise.

## <Filtering effect>

Filtering is a method for separating normal signals from rigging resulting from signal reflection or normal mode noise. In general, rigging has a higher frequency than signals and can, therefore, be separated by an LPF.



Figure 4.8.3-2: Description of effect of filtering

Using an LC filter, ferrite core, or CR for filtering with a high damping rate for the communications line will make the waveform inactive and interrupt communication. (Communication error occurs.)
To continue communication with an inactive waveform, reduce the communication speed with H34 (communication speed setting function).

### 4.9 Dedicated lifter for stacks

### 4.9.1 Feature

(1) This is a dedicated lifter for transporting and replacing the FRENIC-VG series (stack type). It allows you to easily put a stack type inverter in the cabinet and take it out.
The lifter is available with the following products (stack type):

- FRENIC- VG series inverters (stack type)
- RHD-D series diode rectifiers
- RHC-D series PWM converters
- RHF-D series filter stacks
(2) The lifter pallet can be moved up and down (with a winching mechanism) and moved horizontally (with a ball screw mechanism) and can be easily aligned to the cabinet.
[Appearance]


Figure 4.9.1-1: Appearance of the lifter


Figure 4.9.1-2: Example of using the lifter
(3) The lifter can be easily installed by use of the lifter fixture (SA430288-01), which is designed to fix the cabinet and lifter pallet.
This fixture allows easy installation even if the cabinet front face has no space to put the tip of the lifter pallet.
Note

- The lifter can be used without the fixture.
- The fixture must be fastened on the cabinet side.
- The fixture should be prepared by you.
- Design the cabinet so that the fixture can be attached.


Figure 4.9.1-3: Example of using the lifter fixture

### 4.9.2 Specifications

| Item | Specifications |  |
| :---: | :---: | :---: |
| Model | LFT-VG1 | LFT-RHF450 |
| Maximum load weight | 250 [kg] (2450N) | 280 [kg] (2744N) |
| External dimensions [mm] | 702 (W) x 1254 (D) $\times 1450$ (H) |  |
| Lifting height [mm] | 0 to 800 |  |
| Move up/down | Hand-wound: winching mechanism |  |
| Move horizontally | Hand-wound: ball screw mechanism (rightward: 0 to 120 [mm], leftward: 0 to 120 [mm]) | Hand-wound: ball screw mechanism (rightward: 0 to 65 [mm], <br> leftward: 0 to 65 [mm]) |
| Anti-fall device | With an anti-fall device (protection in case of broken wire rope) |  |
| Front and rear wheels | Front wheels: 90-degree steerable Rear wheels: free type (with a stopper) |  |
| Approximate weight | 120 [kg] | 125 [kg] |
| Finishing color | 25-70B 5Y7/1, half-gloss |  |
| Ambient temperatures | -10 to $50^{\circ} \mathrm{C}$ |  |
| External dimensions | SA496984-01 | SA497688-01 |

### 4.9.3 Securing the Lifter

When using a lifter, a lifter securing fixture may be used.
The fixture should be prepared by you as needed.

### 4.9.3.1 Lifter securing fixture (for SA430288-01_ LFT-VG1)


Material: SPHC, t3.2
Plating: $\quad$ Specification JIS Ep-Fe/Zn8/CM2-F
To be post-plated.

Unit: mm

## ISOMETRIC DRAWING



(SAMB OF THB OPPOSITE)
based on the structural design of the cabinet.

### 4.9.3.2 Lifter securing fixture (for SA433892-01_ LFT-RHF45)



Material: SPHC, t3.2
Plating: Specification JIS Ep-Fe/Zn8/CM2-F To be post-plated.
 based on the structural design of the cabinet.

### 4.9.4 Lifter external dimensions

### 4.9.4.1 LFT-VG1 external dimensions



Wire rope


### 4.9.4.2 LFT-RHF450 external dimensions



## FRENIC-VG

## Chapter 5 Peripherals

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### 5.1 Precautions for use

Precautions for use including the selection and connectivity of inverter peripherals are described below.

### 5.1.1 Precautions in connecting main circuit peripherals

### 5.1.1.1 Fuses

Fuses have limited life. Fuji Electric recommends replacing these periodically. If the attachment of the fuse is inadequate, accidents can occur due to the impact of fuse melting, so fasten the fuse with the appropriate tightening torque.

### 5.1.1.2 Breakers/disconnectors (Molded Case Circuit Breaker: MCCB, Earth Leakage Circuit Breaker: ELCB)

An MCCB or ELCB cannot be used for the input (DC bus bar) and output sections of the inverter. (due to the characteristics of MCCB/ELCB)

- The output of the inverter has protective functions (overcurrent, ground fault, open phase, etc.), so no MCCB or ELCB is required. If an MCCB is used inevitably for the purpose of short protection, select a breaker with capacity which trips at a larger current than the rated inverter capacity. (An ELCB in particular cannot be used.) Protective coordination with the electric wire size should also be confirmed before the selection.
- To use as a disconnector, use the non-auto switch which detaches the overcurrent trip function.


### 5.1.1.3 Initial charging circuit

The common converter performs initial charging for the entire system at once. Refer to this chapter if initial charging circuit is to be inevitably implemented for each inverter. When the instructions in this chapter are not followed, peripherals may be adversely affected, resulting in damage in some cases.

### 5.1.1.4 Contactor (magnetic contactor)

For the contactor (electromagnetic contactor) attached to the DC bus bar and the output side, configure the sequence such that opening and closing operations are performed while the inverter is stopped (inverter output is cut off).

### 5.1.1.5 Motor overload protection

When connecting to and operating the motor on a $1: 1$ basis, use the electronic thermal function of the inverter. For the following cases, electronic thermal function cannot protect to maintain normal state, so attach thermistors (NTC / PTC) or thermal relays to the motor for protection.

- Applications where start and stop are frequent, where loading variation occurs frequently, and where very low speed operation is continuous.
- Motors other than the standard three phase motor is used (electronic thermal characteristics are different).

Do not use a thermal relay on the inverter's input (DC bus bar) side. The thermal relay will not function properly due to direct current voltage containing high frequency components.

### 5.1.2 Precautions for phase advancing capacitors

Do not attach phase advancing capacitors to the inverter output (secondary) side. When connected to inverter output, the phase advancing capacitors can burn and be damaged, or make the inverter trip from overcurrent due to the switching frequency of the inverter.

Attaching phase advancing capacitors to the power supply side does not improve the power factor because the inverter is capacitive.

When attaching the phase advancing capacitors to the power receiving side for other instruments, attach reactors which match the phase advancing capacitors.

### 5.1.3 Precautions for connecting control circuit instruments

## PG amplifier (isolation amplifier)

In facilities where PG (pulse generator) is attached to motors to control vectors with long distance wiring, the stray capacitance of the long wires distort PG waveforms, making normal speed detection impossible. In these cases, attach isolation amplifiers (PG amplifiers) for pulse detection.

When PG amplifiers are attached, PG cut off detection protection function is disabled. Enable the inverter's speed mismatch detection function and use it to replace the PG cut off detection protection function.

### 5.1.4 Precautions for using synchronous motors

Be careful of the following matters when using synchronous motors.
(1) When using motors other than Fuji's standard synchronous motor (GNF2), please contact Fuji Electric.
(2) One inverter cannot operate multiple synchronous motors.
(3) Synchronous motors cannot be operated using direct input from commercial power supplies.
(4) Synchronous motors become a generator and a voltage is induced on the motor terminals when they are rotated. Disconnectors and contactors may be attached on inverter outputs for maintenance checkups. Exercise caution on the following points, especially when using contactors.

## <Problem>

The following problems exist when using contactors (52-2) on inverter outputs and the instantaneous power failure restart mode.
(1) Tripping of inverter alarm, diode damage, and fuse (DCF) melting may occur.
(2) Welding, contact stain, and contact failure of the main contact points on contactor (52-2) may occur.

Synchronous motors become a generator (such as in the case of fans) when rotated from the load side, and the main circuit capacitors inside the inverter are charged via the inverter return flow diodes.

Even in the case when the inverter cuts off the gate from the inverter driven control state, the synchronous motors become a generator as in the above case, and charge the inverter.
Hence, when the synchronous motor is a generator, the voltage on the synchronous motor terminals is higher than the inverter intermediate voltage, and the contactor (52-2) is turned on, rush current flows in the route in Figure 5.1.4-1, causing the problems (1) and (2) above. (Similar phenomenon occurs when recovering from instantaneous power failure.)


Figure 5.1.4-1: Path of rush current
Problem does not exist if 52-2 is still ON, but rush current flows in this path when it turns from OFF to ON. (The larger the voltage difference between the motor terminal voltage and the inverter intermediate voltage, the larger the rush current.)

## <Countermeasure>

When driving synchronous motors, select instruments which can maintain open and close states for devices to be attached to the inverter output.
(1) Use of large switch (Non-auto switch of Fuji Electric's G-TWIN molded case circuit breaker series).
(2) Use of mechanical latches (e.g., systems which can turn contactors off only during alarms, such as SC-N**/VS) for the case of contactors.

### 5.2 Selection of peripherals

### 5.2.1 Main circuit

### 5.2.1.1 Fuses

To reduce secondary damage to other instruments in the event the inverter is damaged, install a fuse between the input (DC bus bar) and the inverter. The recommended connection for the 400 V series is on the P side (+ side), but N side (side) will provide the same protection without any problems.
For the 690V series, install fuses on both the P side (+ side) and N side (- side).
The FRENIC-VG contains fuse disconnection detection terminals, allowing detection of fuse disconnection. (Inverter alarm will trip.)
Purchase the microswitches for disconnection detection along with fuses.
Note Fuses other than those in the "Application list" below cannot be used.

## (1) Application list

Fuse manufacturer -
Eaton: http://www.eaton.com/


Table 5.2.1-1: Application list (400V series)


Note 1) Rated DC current is calculated using a diode rectifier and assuming that the received power voltage is 400 VAC 50 Hz .

Table 5.2.1-2: Application list (690V series)

| Voltage | Specifications | Motor rated capacity [kW] | Rated output [A] | Rated DC current [A] | Inverter type | Fuse |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Type | Quantity | Fig. | $\begin{gathered} \text { Generated } \\ \text { loss } \\ \text { [W] } \end{gathered}$ | Approx. mass [kg] |
| 690 V | MD | 90 | 100 | 117 | FRN90SVG1S-69■ | 170M3448-XA | 2 | B | 70 | 0.38 |
|  |  | 110 | 130 | 143 | FRN110SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 132 | 140 | 169 | FRN132SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 160 | 161 | 204 | FRN160SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 200 | 216 | 254 | FRN200SVG1S-69 $\square$ | 170M4445-XA | 2 | C | 85 | 0.58 |
|  |  | 250 | 265 | 315 | FRN250SVG1S-69 $\square$ | 170M6546-XA | 2 | E | 125 | 1.25 |
|  |  | 280 | 295 | 355 | FRN280SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 315 | 330 | 397 | FRN315SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 355 | 365 | 446 | FRN355SVG1S-69■ | 170M6547-XA | 2 |  | 130 |  |
|  |  | 400 | 410 | 501 | FRN400SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 450 | 460 | 561 | FRN450SVG1S-69 $\square$ |  |  |  |  |  |
|  | LD | 110 | 130 | 143 | FRN90SVG1S-69 $\square$ | 170M3448-XA | 2 | B | 70 | 0.38 |
|  |  | 132 | 140 | 169 | FRN110SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 160 | 161 | 204 | FRN132SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 200 | 216 | 254 | FRN160SVG1S-69■ |  |  |  |  |  |
|  |  | 220 | 235 | 277 | FRN200SVG1S-69 $\square$ | 170M4445-XA | 2 | C | 85 | 0.58 |
|  |  | 280 | 295 | 355 | FRN250SVG1S-69■ | 170M6546-XA | 2 | E | 125 | 1.25 |
|  |  | 315 | 330 | 397 | FRN280SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 355 | 365 | 446 | FRN315SVG1S-69 $\square$ |  |  |  |  |  |
|  |  | 400 | 410 | 501 | FRN355SVG1S-69 $\square$ | 170M6547-XA | 2 |  | 130 |  |
|  |  | 450 | 460 | 561 | FRN400SVG1S-69 $\square$ |  |  |  |  |  |

(2) Connection diagram


Figure 5.2.1-1: Fuse wire connection diagram

## (3) How to install a fuse



Figure 5.2.1-1 shows the connection diagram for the fuse and disconnection detection microswitch.
For the 400 V series, install a fuse to the P side (+ side). (* The N side (- side) will also provide the same protection.)
For the 690 V series, install fuses on both the P side (+ side) and N side (- side).
Connect microswitches to [DCF1, DCF2] terminals of the inverter. (These terminals support b contact output, and detect fuse disconnection when the contact is open.)

Figure 5.2.1-2 shows how to install a fuse. Install hexagon socket set screws into the fuse and fasten the bus bars with nuts.

Figure 5.2.1-2: Installing a fuse
(4) External dimensions

Table 5.2.1-3: Fuse external dimensions table

| Fig. | Dimensions (mm) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | D | E | F | G | H |
| A | 74 | 75 | 59 | 45 | M8 | 5 | $\varphi 17$ |
| B | 80 | 81 |  |  |  |  |  |
| C | 80 | 81 | 69 | 53 |  | 8 | $\varphi 20$ |
| D |  |  | 77 | 61 | M10 | 10 | ¢24 |
| E | 81 | 83 | 92 | 76 | M12 |  | $\varphi 30$ |
| F |  | 91 |  |  |  |  |  |
| G | - | 106.6 | 120 | 105 | M10 | 10 | $\varphi 56$ |

Note) Column H shows the fuse main circuit terminals.
Figure A-F


Figure G


Figure 5.2.1-3: Fuse external shape

## (5) Microswitch

## Type: 170H3027



Figure 5.2.1-5: Microswitch external shape


Figure 5.2.1-4: Microswitch contact structure

Install the microswitch to the fuse so that its tab terminals face down.
Press in the microswitch so that the claws for attaching the microswitch will hook onto the fuse body.

This red block protrudes if the fuse is disconnected. ( 3.5 mm )


Figure 5.2.1-6: Installing a microswitch

## 5．2．2 Disconnectors and molded case circuit breakers for wiring （MCCB）

This section describes disconnectors and molded case circuit breakers for wiring（hereinafter referred to as＂MCCBs＂） used in the inverter input／output circuit．
［Examples－Used to disconnect the inverter＇s input power supply from the converter before maintenance of the of use］ facilities
－Used to disconnect the inverter and motor from each other
When using an MCCB on the input（DC bus bar）and／or output side of the inverter，it is necessary to use a non－auto switch that excludes the overcurrent trip function．

## Inverter input side

The opening and closing of the disconnector or MCCB installed on the inverter input side should be performed after confirming that both the converter and inverter charge lamps are off．

## Inverter output side

Use of a non－auto switch is recommended when installing a disconnector or MCCB on the inverter output side．If MCCB is necessary for the purpose of short protection，use one that has larger capacity than the inverter rated capacity．In this case，also consider protective coordination with the electric wire．
＊Normally，protective coordination with the electric wire is achieved with the inverter＇s protective functions（overcurrent， ground fault，open phase，etc．）．However，if the user＇s facility standards require protective coordination with MCCBs as a rule，that rule should be followed．

## （1）Application list

Use the combinations in the following table．
Table 5．2．2－1：Application list

| $\begin{aligned} & \hline 0 \\ & \stackrel{\pi}{9} \\ & \hline \end{aligned}$ | Motor rating |  | Inverter type（FRN） |  | Diode rectifier |  | PWM converter |  | Inverter output side MCCB ${ }^{\text {² }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Capacity ［kW］ | Capacity ［kW］ | MD Spec | LD Spec | Input current ［Adc］${ }^{* 1}$ | MCCB ${ }^{2}$ | Input current ［Adc］${ }^{* 1}$ | MCCB ${ }^{2}$ |  |
| ট্ট | 30 | 60 | 30SVG1S－4■ | － | 65 | 400AF | 56.3 | 400AF | 400AF |
|  | 37 | 75 | 37SVG1S－4■ | 30SVG1S－4■ | 80 |  | 68.8 |  |  |
|  | 45 | 91 | 45SVG1S－4■ | 37SVG1S－4■ | 97 |  | 82.9 |  |  |
|  | 55 | 112 | 55SVG1S－4■ | 45SVG1S－4■ | 119 |  | 102 |  |  |
|  | 75 | 150 | 75SVG1S－4■ | 55SVG1S－4■ | 162 |  | 138 |  |  |
|  | 90 | 176 | 90SVG1S－4■ | 75SVG1S－4■ | 195 |  | 161 |  |  |
|  | 110 | 210 | 110SVG1S－4■ | 90SVG1S－4■ | 238 |  | 197 |  |  |
|  | 132 | 253 | 132SVG1S－4 $\square$ | 110SVG1S－4■ | 286 |  | 235 |  |  |
|  | 160 | 304 | 160SVG1S－4 $\square$ | 132SVG1S－4 $\square$ | 347 | 630AF | 285 |  |  |
|  | 200 | 377 | 200SVG1S－4■ | 160SVG1S－4 $\square$ | 433 |  | 355 | 630AF | 630AF |
|  | 220 | 415 | 220SVG1S－4 $\square$ | 200SVG1S－4 $\square$ | 476 |  | 386 |  |  |
|  | 250 | 468 | 250SVG1S－4 $\square$ | 220SVG1S－4 $\square$ | 541 | 800AF | 440 |  |  |
|  | 280 | 520 | 280SVG1S－4 $\square$ | 250SVG1S－4 $\square$ | 606 |  | 491 |  |  |
|  | 315 | 585 | 315SVG1S－4■ | 280SVG1S－4 $\square$ | 682 |  | 552 | 800AF | 800AF |
|  | 355 | 650 | － | 315SVG1S－4 $\square$ | 769 |  | 625 |  |  |
|  | 630 | 1170 | 630BVG1S－4 $\square$ | － | 1365 | － | 1102 | － | － |
|  | 710 | 1370 | 710BVG1S－4■ | 630BVG1S－4 $\square$ | 1538 | － | 1243 | － | － |
|  | 800 | 1480 | 800BVG1S－4 $\square$ | 710BVG1S－4 $\square$ | 1733 | － | 1400 | － | － |
|  | 1000 | 1850 | － | 800BVG1S－4 $\square$ | 2166 | － | 1750 | － | － |
| ৷⿱亠⿴囗口⿱日一 | 90 | 100 | 90SVG1S－69■ | － | 117 | － | 96 | － | － |
|  | 110 | 130 | 110SVG1S－69 $\square$ | 90SVG1S－69■ | 143 | － | 118 | － | － |
|  | 132 | 140 | 132SVG1S－69■ | 110SVG1S－69■ | 169 | － | 140 | － | － |
|  | 160 | 161 | 160SVG1S－69■ | 132SVG1S－69■ | 204 | － | 170 | － | － |
|  | 200 | 216 | 200SVG1S－69■ | 160SVG1S－69■ | 254 | － | 212 | － | － |
|  | 220 | 265 | － | 200SVG1S－69■ | 277 | － | 231 | － | － |
|  | 250 | 295 | 250SVG1S－69■ | － | 315 | － | 261 | － | － |
|  | 280 | 330 | 280SVG1S－69■ | 250SVG1S－69■ | 355 | － | 293 | － | － |
|  | 315 | 365 | 315SVG1S－69■ | 280SVG1S－69■ | 397 | － | 329 | － | － |
|  | 355 | 410 | 355SVG1S－69■ | 315SVG1S－69■ | 446 | － | 373 | － | － |
|  | 400 | 460 | 400SVG1S－69■ | 355SVG1S－69■ | 501 | － | 418 | － | － |
|  | 450 | 100 | 450SVG1S－69■ | 400SVG1S－69■ | 561 | － | 470 | － | － |

Note - Instruments in the table are products of Fuji Electric Co., Ltd. (http://www.fujielectric.co.jp/fcs/).
For information on available non-auto switch series, see the catalog of Fuji Electric's G-TWIN breakers for high-voltage DC circuits.
Refer to catalogs and information from Fuji Electric Co., Ltd. for external dimensions and installation methods.

- Columns marked with *1 show the inverter input current (DC) values when the individual converters are applied.
For the diode rectifiers, the diode rectifier input voltage is equivalent to $3 \varphi 400 \mathrm{VAC} 50 \mathrm{~Hz}$.
- For MCCBs with *2, it is recommended to use a non-auto switch.


## (2) Connection diagram

1) MCCBs on the inverter input side

When installing an MCCB (non-auto switch) on the DC bus bar, refer to the catalog of Fuji Electric's "breakers for high-voltage DC circuits". When operating an MCCB (non-auto switch), take the following precautions if applicable:
(1) When diode converters are used, always confirm that the input power supply is cut off before operating.
(2) When using PWM converters, always confirm that the input power supply is cut off and that both charge lamps for the inverter and converter are unlit before operating.
(3) Add the state where the inverter input side MCCB is closed (ON) as a turning-on interlock condition for the main power input MCCB.
2) MCCBs on the inverter output side


Figure 5.2.2-1: Example of an MCCB connected to the inverter output side

When connecting an MCCB (non-auto switch) on the inverter output side, wire it as shown in Figure 5.2.2-1. Take the following precautions if applicable:
(1) Operate the opening and closing of the MCCB when the inverter is suspended.
(2) Add the state where the inverter output side MCCB is closed (on) as a condition to start the inverter. In the connection shown in Figure 5.2.2-1, do not operate the MCCB while the inverter is running. Doing so would activate the inverter's protective functions.

### 5.2.2.1 Contactor (magnetic contactor)

This section describes the contactors (magnetic contactors) used in the inverter output circuits.
[Examples - Used to disconnect the inverter from the input power supply converter before facility maintenance, etc. of use]

- Used to disconnect the inverter and motor from each other
- Used to switch from commercial power supply operation to inverter-based operation

Perform the opening and closing of the contactor attached to the inverter output side while the inverter is suspended

## (i.e.. in free run state).

- Do not attach main circuit surge absorption units (Fuji Electric SZ-ZM $\square$, etc.) to the contactors.
- The inverter will be damaged if commercial power supply is connected to the inverter output side (secondary side). Interlock the commercial power supply side contactor and the inverter output side contactor to prevent simultaneous ON state.
- When using the instantaneous power failure restart function, connect the connection confirmation signal of the inverter output side contactor to the inverter's general purpose contact input terminal ( X terminal) and set the [IL: interlock function] for the X terminal.
[a] For more information, refer to Chapter 4 of the separate volume "Unit/Function Codes Edition" (24A7- $\square$-0019).


## (1) Application list

Use the combinations in the following table.
Table 5.2.2-2: Application list

| Voltage | Motor rating |  | Inverter type (FRN) |  | Inverter output side MC |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Capacity [kW] | Current (A) | MD Spec | LD Spec |  |
| 方 | 30 | 60 | 30SVG1S-4■ | - | SC-N2 |
|  | 37 | 75 | 37SVG1S-4■ | 30SVG1S-4■ | SC-N2S |
|  | 45 | 91 | 45SVG1S-4■ | 37SVG1S-4■ | SC-N3 |
|  | 55 | 112 | 55SVG1S-4■ | 45SVG1S-4■ | SC-N4 |
|  | 75 | 150 | 75SVG1S-4■ | 55SVG1S-4■ | SC-N5 |
|  | 90 | 176 | 90SVG1S-4■ | 75SVG1S-4■ | SC-N7 |
|  | 110 | 210 | 110SVG1S-4 $\square$ | 90SVG1S-4■ | SC-N8 |
|  | 132 | 253 | 132SVG1S-4■ | 110SVG1S-4■ |  |
|  | 160 | 304 | 160SVG1S-4■ | 132SVG1S-4■ | SC-N11 |
|  | 200 | 377 | 200SVG1S-4■ | 160SVG1S-4■ | SC-N12 |
|  | 220 | 415 | 220SVG1S-4■ | 200SVG1S-4■ |  |
|  | 250 | 468 | 250SVG1S-4■ | 220SVG1S-4■ | SC-N14 |
|  | 280 | 520 | 280SVG1S-4■ | 250SVG1S-4■ |  |
|  | 315 | 585 | 315SVG1S-4■ | 280SVG1S-4■ |  |
|  | 355 | 650 | - | 315SVG1S-4■ |  |
|  | 630 | 1170 | 630BVG1S-4■ | 吅 | 612CM ${ }^{* 1}$ |
|  | 710 | 1370 | 710BVG1S-4■ | 630BVG1S-4■ | 616CM ${ }^{*}$ |
|  | 800 | 1480 | 800BVG1S-4■ | 710BVG1S-4■ |  |
|  | 1000 | 1850 | - | 800BVG1S-4■ | - |
| ৪্ষ্ণ | 90 | 100 | 90SVG1S-69■ | - | SC-N3 |
|  | 110 | 130 | 110SVG1S-69■ | 90SVG1S-69■ | SC-N4 |
|  | 132 | 140 | 132SVG1S-69■ | 110SVG1S-69■ | SC-N5 |
|  | 160 | 161 | 160SVG1S-69] | 132SVG1S-69] | SC-N7 |
|  | 200 | 216 | 200SVG1S-69■ | 160SVG1S-69■ | SC-N8 |
|  | 220 | 235 | - | 200SVG1S-69■ |  |
|  | 250 | 265 | 250SVG1S-69■ | - | SC-N11 |
|  | 280 | 295 | 280SVG1S-69■ | 250SVG1S-69■ |  |
|  | 315 | 330 | 315SVG1S-69■ | 280SVG1S-69■ |  |
|  | 355 | 365 | 355SVG1S-69] | 315SVG1S-69] | SC-N12 |
|  | 400 | 410 | 400SVG1S-69■ | 355SVG1S-69■ |  |
|  | 450 | 460 | 450SVG1S-69■ | 400SVG1S-69■ | SC-N14 |

*1. Aichi Electric Works Co., Ltd.
Note Instruments in the table are products of Fuji Electric Co., Ltd. (http://www.fujielectric.co.jp/fcs/).
Refer to catalogs and information from Fuji Electric Co., Ltd. for external dimensions and installation methods.

### 5.2.2.2 Initial charging circuit

Inverters do not have a built-in initial charging circuit. If the system configuration requires an initial charging circuit, configure it using the steps described in this section.

## (1) Application list

Use the combinations in Table 5.2.2-3.
Table 5.2.2-3: Application list

| $\begin{aligned} & \mathscr{\otimes} \\ & \frac{\pi}{5} \\ & \hline \frac{1}{5} \end{aligned}$ | Inverter type | Diode rectifier |  |  |  |  |  | PWM converter |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MC type (73) |  | Charging resistor type (RO) | Quantity |  |
|  |  | MD Spec | LD Spec | MD Spec | LD Spec |  |  |  |
| 方 | FRN30SVG1S-4■ | 65 | 80 | SC-N1 | SC-N1 | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ | 1 | Contact <br> Fuji <br> Electric |
|  | FRN37SVG1S-4 $\square$ | 80 | 97 | SC-N1 | SC-N2 |  |  |  |
|  | FRN45SVG1S-4 $\square$ | 97 | 119 | SC-N2 | SC-N2 |  |  |  |
|  | FRN55SVG1S-4 $\square$ | 119 | 162 | SC-N2 | SC-N2S |  |  |  |
|  | FRN75SVG1S-4 $\square$ | 162 | 195 | SC-N2S | SC-N3 |  |  |  |
|  | FRN90SVG1S-4■ | 195 | 238 | SC-N3 | SC-N3 | $\begin{aligned} & \hline \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ |  |  |
|  | FRN110SVG1S-4■ | 238 | 286 | SC-N3 | SC-N4 |  |  |  |
|  | FRN132SVG1S-4■ | 286 | 347 | SC-N4 | SC-N5 | HF5C5504(80W$7.5 \Omega)$ | 3(Parallel) |  |
|  | FRN160SVG1S-4■ | 347 | 433 | SC-N5 | SC-N7 |  |  |  |
|  | FRN200SVG1S-4■ | 433 | 476 | SC-N7 | SC-N7 |  |  |  |
|  | FRN220SVG1S-4■ | 476 | 541 | SC-N7 | SC-N8 | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ | (Parallel) |  |
|  | FRN250SVG1S-4■ | 541 | 606 | SC-N8 | SC-N8 |  |  |  |
|  | FRN280SVG1S-4■ | 606 | 682 | SC-N8 | SC-N10 | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega \text { ) } \end{aligned}$ |  |  |
|  | FRN315SVG1S-4■ | 682 | 769 | SC-N10 | SC-N11 |  |  |  |
| ব্ষ্ণ | FRN90SVG1S-69■ | 117 | 143 | SC-N2 | SC-N2S | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ | $\begin{gathered} 2 \\ \text { (Series) } \end{gathered}$ |  |
|  | FRN110SVG1S-69■ | 143 | 169 | SC-N2S | SC-N2S |  |  |  |
|  | FRN132SVG1S-69] | 169 | 204 | SC-N2S | SC-N3 | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ | 4 (2 series, 2 parallel) <br> 2 parallel) |  |
|  | FRN160SVG1S-69■ | 204 | 254 | SC-N3 | SC-N4 |  |  |  |
|  | FRN200SVG1S-69] | 254 | 277 | SC-N4 | SC-N4 |  |  |  |
|  | FRN250SVG1S-69] | 315 | 355 | SC-N4 | SC-N5 | $\begin{aligned} & \text { HF5C5504(80W } \\ & 7.5 \Omega) \end{aligned}$ | 6 <br> (2 series, <br> 3 parallel) |  |
|  | FRN280SVG1S-69■ | 355 | 397 | SC-N5 | SC-N5 |  |  |  |
|  | FRN315SVG1S-69] | 397 | 446 | SC-N5 | SC-N7 |  |  |  |
|  | FRN355SVG1S-69■ | 446 | 501 | SC-N7 | SC-N8 |  |  |  |
|  | FRN400SVG1S-69■ | 501 | 561 | SC-N8 | SC-N8 |  |  |  |
|  | FRN450SVG1S-69■ | 561 | - | SC-N8 | - |  |  |  |

- Instruments in the table are products of Fuji Electric Co., Ltd. (http://www.fujielectric.co.jp/fcs/).

Refer to catalogs and information from Fuji Electric Co., Ltd. for external dimensions and installation methods.

- Regarding the column marked with *1, the input voltage is equivalent to $3 \varphi 400$ VAC 50 Hz when a diode rectifier is used.
- Contact your Fuji Electric representative for information on the 400 V series 630 to 800 kW models and the 690V series.
(2) Connection diagram, external dimensions of charging resistors


Figure 5.2.2-2: Example of connection of DC bus side disconnector


Figure 5.2.2-3: External dimensions of charging resistor
(1) Use a 3-phase parallel terminal board (SZ-SP $\square$ ), which is a contactor option, to connect the initial charging contactor (73).
(2) Install the main section of the charging resistor with approximately 10 mm spacing from other resistors, other instruments, and structural parts.
(3) When using multiple charging resistors, connect them in paralleI. IV2 $\mathrm{mm}^{2}$ is recommended for the relay wires.
(4) Contact your Fuji Electric representative for information on the charging resistor (R0) when configuring the system with PWM converters.
Depending on the system configuration, the configuration of the charging resistor may need to be reconsidered.
Note Use the charging circuit up to once an hour. Repeating initial charging too often may cause failures in the charging resistor.

### 5.2.2.3 Thermal relays

The inverter contains the electronic thermal function for motor protection. However, the electronic thermal function cannot detect an overload on individual motors when one inverter drives multiple motors. In this case, use thermal relays for overload protection of the motors.

## (1) Application list

The following is an application list of thermal relays for Fuji's standard motors. However, applications may differ from this table depending on use conditions. In conditions that require more than one minute of start-up time, the setup should be reconsidered. For the 690V series, selected appropriate thermal relays based on the rated current of the motor used.

Table 5.2.2-4: Application list


- Instruments in the table are products of Fuji Electric Co., Ltd. (http://www.fujielectric.co.jp/fcs/). Refer to catalogs and information from Fuji Electric Co., Ltd. for external dimensions and installation methods.
- The tripping characteristic curves for thermal relays differ between cold start and hot start. Configure after confirming the overload current and time of the motor at hot start. However, if starts/stops are frequent and the start-up current of the motor is large, the thermal relay may trip mistakenly. Consider the use depending on the mechanical application.


## (2) Precautions for use

## Ambient temperature compensation characteristics

Thermal relays regulate current referencing ambient temperature of $20^{\circ} \mathrm{C}$. The operating current varies by ambient temperature change, increasing current at low temperature and decreasing current at high temperature. The operating characteristic compensates for the deficiency.

Hence, the set point of the current may need to be adjusted depending on use conditions. When the operating temperature differs widely from $20^{\circ} \mathrm{C}$, use "Figure 5.2.2-4" as a rough guideline to calculate the set point current after compensation.


Figure 5.2.2-4: Operating temperature correction coefficient

[^5]
## Installation on the inverter output side

If thermal relay is selected according to the motor rated current, it may cause trip mistakenly. Reference the following to implement countermeasures.

## Principles for selection (example)

(1) Measure the current of the installed circuit with thermal relay, and select the rated current for the thermal relay. For current measurement, use a clamp meter (HIOKI made: 3284/200 A, 3285/2000 A equivalent products).
(2) Confirm that the current is within the motor's allowable heat characteristics.

## Countermeasures for mistaken trips

(1) Install an OFL filter (OFL- $\square \square-4 \mathrm{~A}$ ).
(2) Increase the set point value on the thermal relay adjustment dial.
(3) Install at a location distant from the inverter wiring (close to the motor).
(4) Attach a temperature sensor to the motor for motor temperature protection, without installing a thermal relay.

- Do not use delay type thermal relays or those above N10 type because they falsely trip more readily compared to standard types.
For protection of loads with long start times (loads with large inertia) and motors with large capacity (over 90 kW ), attach temperature sensors to motors to implement temperature protection.


## (3) Connection diagram

For large capacity motors, use instrument transformers (CT) and thermal relays in combination.
Refer to Figure 5.2.2-5.


Figure 5.2.2-5: Example of thermal relay connection with large current

### 5.2.2.4 Output transformer

Typical transformers cannot be connected to the inverter output side for the following reasons.
When transformers are needed, contact your Fuji Electric representative.
(1) Inverter output voltages contain direct current components accompanying slightly unbalanced IGBT switching. These direct current components cause bias magnetism.
(2) If the torque boost is set for increasing motor torque at low frequencies, the V/f ratio increases, resulting in higher magnetic flux density. This causes overexcitation of the transformer, causing magnetic saturation of the magnetic core and overheating.
(3) Because surge voltage accompanying IGBT switching occurs, enhancement of insulation matching surge voltage is necessary.

* Transformers (special) can be used only when the control method is V/f control. (Do not use a transformer when vector control is in use.)


### 5.2.2.5 Main circuit monitoring instrument

"6.2.12.9 Receiving power supply monitor" in Chapter 6 shows meters that can be attached to the inverter output side.
Refer to "6.2.12.9 Receiving power supply monitor" in Chapter 6.

### 5.3 Control circuit

### 5.3.1 Backup battery

When saving trace back memory or using calendar functions while the inverter is not powered, batteries are needed for memory storage. This inverter contains the battery in the standard package, so attach the battery when using the above features.

Table 5.3.1-1: Battery specifications
Units: [mm]

| Model | OPK-BP <br> * When battery runs out, purchase this model. |
| :--- | :--- |
| Battery voltage / <br> capacity | $3.6 \mathrm{~V}-1100 \mathrm{mAh}$ |
| Classification | Thionyl chloride lithium battery |
| Replacement cycle | 5 years (operating temp: $60^{\circ} \mathrm{C}$, inverter not <br> powered) |



Figure 5.3.1-1: External dimensions of the battery

### 5.3.1.1 Procedures for installing/replacing the battery

Battery installation steps are described below.
[1] For information on how to set the date/time, refer to Section 3.4. 4.12 in Chapter 3 of the separate volume "Unit/Function Codes Edition" (24A7-■-0019).

## (1) Remove the front cover.


(4) Attach the battery into the battery holder near the upper left side of the control circuit board.

(2) Open the keypad case and remove connectors CN5 and CN8 on the control print circuit board.
(3) Remove the keypad case.

Connectors CN5 and CN8 are located on the upper left side, viewed from the front side of the control print circuit board.

(5) Insert firmly the lead wire connector of the battery into connector CN7 on the control print circuit board.


Figure 5.3.1-2: Battery replacement steps

### 5.3.1.2 Overseas and aerial transportation of battery (lithium metal battery)

Exercise caution on the following items when transporting the battery (lithium metal battery) by itself, by packaging it with other instruments, or by embedding it into instruments.
(1) Transportation of lithium metal battery by embedding it into instruments When transporting control boards with more than five inverters containing batteries, attach a label as shown in Figure 5.3.1-3 and prepare transportation documents.
(2) Transportation of lithium metal battery by packaging it with instruments
Attach a label as shown in Figure 5.3.1-3 and prepare a certificate of conformance to drop test in the transportation material.
For air transport, the number of batteries which can be bundled is limited to two additional to the number required for instrument operation.


Figure 5.3.1-3: Label to attach to package exterior

### 5.3.2 PG amplifier (insulating converter)

When the motor speed cannot be normally detected due to distorted PG waveforms resulting from the long wiring to the pulse generator (PG) for motor speed detection, use a PG amplifier that corrects and amplifies PG waveforms.

### 5.3.2.1 Recommended pulse amplifier model

- SHP-115150 (FAITH product)
- SHC-215150 (FAITH product)

The only difference between the above products is in the control power supply specifications of the PG amplifier.
PG voltage of the standard vector motor type is 15 V .
Contact your Fuji Electric representative when purchasing these products.

## Type number nomenclature

SHP-


### 5.3.2.2 External dimensions



Figure 5.3.2-1: External dimensions of the PG amplifier

- Steel closed box (IP20 equivalent)
- Paint color: Cream color (Munsell 5Y7/1)
- Approx. mass: 1 kg
- Position approx. 10 mm away from instruments such as control relays and structural parts. Also, position more than 100 mm away from the main circuit instruments and wiring.


### 5.3.2.3 Specifications and terminal description

## (1) Specifications



Specifications marked with * in the table are determined by the model.

## (2) Terminal description

| Terminal <br> No. |  |
| :---: | :--- |
| 1 | N.C |
| 2 | N.C |
| 3 | A-phase input (+ side) |
| 4 | A-phase input (- side, common side) |
| 5 | B-phase input (+ side) |
| 6 | B-phase input (- side, common side) |
| 7 | PG power supply (+ side) |
| 8 | PG power supply (common side) |
| 9 | -5 V terminal |
| 11 | A-phase output (- side, common side) |
| 12 | A-phase output (+ side) |
| 13 | B-phase output (- side, common side) |
| 14 | B-phase output (+ side) |
| 15 | External power supply (+ side) |
| 16 | External power supply (- side, common side) |
| 17 | Earthing terminal |
| 18 | AC power supply input |
| 19 |  |

### 5.3.2.4 Precautions for connection and specifications

## (1) Connection diagram

Connect the wiring as shown in Figure 5.3.2-2.

(1) Connect the grounding terminal of the PG amplifier to the same ground connection as the inverter. (Connect to the common ground bus when housed inside a cabinet.)
(2) For the pulse signals, use shielded lines between the motor and the PG amplifier, and between the PG amplifier and the inverter.

- Inside cabinet: MVVS-3 over $0.3 \mathrm{~mm}^{2}$ core
- Outside cabinet: CVVS-4 over $2 \mathrm{~mm}^{2}$ core
(3) Connect the shield of the shield line between the motor and PG amplifier to the SS (E) terminal dedicated for motor signals.

Figure 5.3.2-2: Connection diagram

## (2) Precautions for use

When the PG amplifier is used, "PG cut off" detection ( unavailable because the connection to the inverter's terminal "PGP" is lost. Therefore, configure to use the speed mismatch alarm function [E45] instead of the PG cut off function in the function code setup.

[1] For information on how to set the date/time, refer to Section 3.4. 4.12 in Chapter 3 of the separate volume "Unit/Function Codes Edition" (24A7- $\square$-0019)For information on how to set the date/time, refer to "Chapter 4 Control and Operation" of the separate volume "Unit/Function Codes Edition" (24A7-■-0019).

### 5.4 Inverter options

This section contains an overview of control options and the restrictions on installation in inverters.
$\mathbb{1}$ For information on how to set the date/time, refer to Section 3.4. 4.12 in Chapter 3 of the separate volume "Unit/Function Codes Edition" (24A7-J-0019)For information on how to set the date/time, refer to "Chapter 6 Control Options" of the separate volume "Unit/Function Codes Edition" (24A7-J-0019).

### 5.4.1 Option list

| Category | Name | Type | Switch functions using SW | Specifications |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Analog card (for A port only) | Synchronous interface | OPC-VG1-SN |  | Synchronous interface circuit for dancer control |  |
|  | Aio extension card | OPC-VG1-AIO |  | Ai 2 points + Ao 2 points extension card |  |
|  | Di interface card | OPC-VG1-DI | OPC-VG1-DIA OPC-VG1-DIB | 16 bit Di binary or BCD 4 speed command, torque current command setup. (Setting must be switched port is used) | gits + sign used for mmand, torque <br> epending on which |
|  | Dio extension card | OPC-VG1-DIO | OPC-VG1-DIOA | Function selection Di x 4bit Do x 8bits extension | + function selection |
|  |  |  | OPC-VG1-DIOB | UPAC I/O extension Di x | bits + Do $\times 10$ bits |
|  | T link interface card | OPC | -VG1-TL | T link interface card |  |
|  | CC-Link interface card | OPC | VG1-CCL | This interface card suppo | CC-Link |
|  |  |  | OPC-VG1-PG (SD) |  |  |
| Digital 8 bit (for |  |  | OPC-VG1-PG (LD) | signals) (500 kHz) |  |
| A or B port only) |  |  | OPC-VG1-PG (PR) | Used for motor speed, | eed, position |
|  |  |  | OPC-VG1-PG (PD) | command, and position | ion. |
|  | PG interface card |  | OPC-VG1-PGo (SD) | Open collector type enc | terface (A, B, Z |
|  |  | OPC-VG1-PGo | OPC-VG1-PGo (LD) | signals) ( 100 kHz ) |  |
|  |  | OPCVG1-PGo | OPC-VG1-PGo (PR) | Used for motor speed, lin | peed, position |
|  |  |  | OPC-VG1-PGo (PD) | command, and position | on. |
|  |  | OPC-V | VG1-SPGT | 17 bit high resolution AB | oder interface |
|  | PMPG interface card for driving synchronous | OPC- | G1-PMPG | Supports +5 V line driver output | A, B, position of magnetic pole |
|  |  | OPC-V | G1-PMPGo | Supports open collector output | (max. 4 bits) |
| Field bus interface card | PROFIBUS-DP interface card | OPC-V | G1-PDP (*1) | PROFIBUS-DP interface |  |
| (for C port only) | DeviceNet interface card | OPC-V | G1-DEV (*2) | DeviceNet interface card |  |
|  | SX bus interface card | OPC | -VG1-SX | SX bus interface card |  |
|  | E-SX bus interface card | OPC- | VG1-ESX | E-SX bus interface card |  |
| Digital 16 bit (for <br> D port only) | User Programmable Application Card | OPC-VG | 1-UPAC (*1) | Used for inverter control fro software created by the us | customized |
|  | PROFINET-IRT interface card | OPC-VG | 1-PNET (*3) | Supports PROFINET-RT | d IRT |
| Safety card (for E port only) | Functional safety card | OPC-VG | 1-SAFE (*1) | Functional safety standard | ompatible card |
| Control circuit terminal (for $F$ port only) | High speed serial communication supported terminal board | OPC-V | G1-TBSI (*1) | Used for multiplexed syste multi-winding motor driving systems | s such as and direct parallel |
| Loader |  | WPS | VG1-STR | CD-ROM (free) for Window |  |
| Loader | Inverter support loader | WPS | VG1-PCL | CD-ROM (paid version) fo | Windows |

(*1) Available when the ROM version is $\mathrm{H} 1 / 20021$ or later.
(*2) Available when the ROM version is $\mathrm{H} 1 / 20030$ or later.
(*3) Available with FRENIC-VG types with PROFINET support (i.e., type numbers that end with "PN").

### 5.4.2 Restrictions on mounting control option cards and others

### 5.4.2.1 Mountable ports

Control options are restricted by function on the ports which can be mounted (attachment section). Refer to Table 5.4.2-1 Option mounting port and Figure 5.4.2-1 Option mounting locations.

Table 5.4.2-1: Option mounting port

| CN | Port | Category | Pattern 1 | Pattern 2 | Pattern 3 |
| :---: | :---: | :--- | :---: | :---: | :---: |
| 3 | A | Digital 8bit, analog card | 1 | 1 | 1 |
| 2 | B | Digital 8bit | 1 | 0 | 0 |
| 6 | C | Field bus interface card | 0 | 0 | 1 |
| 10 | D | Digital 16bit | 1 | 1 | 0 |
| 16 | E | Safety card | 0 | 1 | 1 |
| 1 | F | Control circuit terminal | 1 | 1 | 1 |



Figure 5.4.2-1: Option mounting locations

## 5．4．2．2 Restrictions when mounting control options

Some combinations of control option digital cards（ 8 bit and 16 bit）cannot be mounted together，due to their functions． Construct the system in accordance with Table 5．4．2－2＂Control options which can be mounted together＂．

Table 5．4．2－2：Control options which can be mounted together
OK：Can be mounted together NG：Cannot be mounted together

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline $$
\begin{aligned}
& \text { Model } \\
& \text { OPC-VG1 } \\
& \text {-■ดロロ }
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{S} \\
& \mathrm{~N}
\end{aligned}
$$ \&  \& $$
\begin{gathered}
\text { D } \\
\text { I }
\end{gathered}
$$ \& $$
\begin{aligned}
& \text { D } \\
& \text { I }
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{T} \\
& \mathrm{~L}
\end{aligned}
$$ \& $$
\begin{aligned}
& \text { C } \\
& \text { C } \\
& \text { L }
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{P} \\
& \mathrm{G} \\
& \mathrm{l} \\
& \mathrm{P} \\
& \mathrm{G} \\
& \mathrm{o}
\end{aligned}
$$ \& $P$
$M$
$P$
P
G
l
P
M
P
G
O \& $$
\begin{aligned}
& \mathrm{S} \\
& \mathrm{P} \\
& \mathrm{G} \\
& \mathrm{~T}
\end{aligned}
$$ \& $$
\begin{array}{|c}
\hline \mathrm{T} \\
\mathrm{~B} \\
\mathrm{~S} \\
\mathrm{I} \\
\\
\\
\hline 7 \\
\hline
\end{array}
$$ \& $$
\begin{aligned}
& \mathrm{S} \\
& \mathrm{X}
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{E} \\
& \mathrm{~S} \\
& \mathrm{X}
\end{aligned}
$$ \& $$
\begin{aligned}
& \text { U } \\
& \text { P } \\
& \text { A } \\
& \text { C }
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{P} \\
& \mathrm{~N} \\
& \mathrm{E} \\
& \mathrm{~T}
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{P} \\
& \mathrm{D} \\
& \mathrm{P}
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{D} \\
& \mathrm{E} \\
& \mathrm{~V}
\end{aligned}
$$ \& $$
\begin{aligned}
& \mathrm{S} \\
& \mathrm{~A} \\
& \mathrm{~F} \\
& \mathrm{E}
\end{aligned}
$$ \& T
B
S
1

＊8 <br>
\hline SN \& NG \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline AIO \& NG \& NG \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline DI＊1 \& OK \& OK \& OK \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline DIO＊1 \& OK \& OK \& OK \& OK \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline TL \& OK \& OK \& OK \& OK \& NG \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline CCL \& OK \& OK \& OK \& OK \& NG \& NG \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PG／PGo＊1＊2 \& OK \& OK \& OK \& OK \& OK \& OK \& ＊3 \& \& \& \& \& \& \& \& \& \& \& <br>
\hline PMPG／PMPGo＊4 \& OK \& OK \& OK \& OK \& OK \& OK \& ＊3 \& NG \& \& \& \& \& \& \& \& \& \& <br>
\hline SPGT＊5 \& ＊6 \& ＊6 \& OK \& OK \& OK \& OK \& NG \& NG \& NG \& \& \& \& \& \& \& \& \& <br>
\hline TBSI ${ }^{\text {＊}}$ \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& NG \& \& \& \& \& \& \& \& <br>
\hline SX \& OK \& OK \& OK \& OK \& OK \& NG \& OK \& OK \& OK \& NG \& NG \& \& \& \& \& \& \& <br>
\hline ESX \& OK \& OK \& OK \& OK \& NG \& NG \& OK \& OK \& OK \& NG \& NG \& NG \& \& \& \& \& \& <br>
\hline UPAC \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& NG \& NG \& NG \& \& \& \& \& <br>
\hline PNET \& OK \& OK \& OK \& OK \& NG \& NG \& OK \& OK \& OK \& NG \& NG \& NG \& NG \& NG \& \& \& \& <br>
\hline PDP \& OK \& OK \& OK \& OK \& NG \& NG \& OK \& OK \& OK \& NG \& NG \& NG \& NG \& NG \& NG \& \& \& <br>
\hline DEV \& OK \& OK \& OK \& OK \& NG \& NG \& OK \& OK \& OK \& NG \& NG \& NG \& NG \& NG \& NG \& NG \& \& <br>
\hline SAFE \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& NG \& <br>
\hline TBSI＊8 \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& OK \& NG \& OK \& OK \& OK \& OK \& OK \& OK \& ＊6 \& NG <br>
\hline
\end{tabular}

As shown above，certain combinations of communication related option cards（such as the OPC－VG1－TL and the OPC－VG1－CCL）cannot be mounted together．An attempt to mount such cards together will result in an operation procedure alarm（に，にーム）．
＊1 The use method for OPC－VG1－DI，DIO，PG，and PGo can be selected by the setup of the SW on the print board． Two cards of OPC－VG1－DI，DIO，PG，and PGo each can be mounted，but an operation procedure alarm（I，－－1）will be activated if the setup of the 2 cards determining the use method becomes identical．
＊2 When using the OPC－VG1－PG for motor speed detection，inputs from main control print circuit board terminals（PA and PB ）are not available．
＊3 When two cards of OPC－VG1－PG／PGo and／or OPC－VG1－PMPG／PMPGo are mounted，the following restrictions apply：

|  | VG1－PG／PGo（SD） <br> VG1－PMPG／PMPGo | VG1－PG／PGo（LD） | VG1－PG／PGo（PR） | VG1－PG／PGo（PD） |
| :--- | :---: | :---: | :---: | :---: |
| VG1－PG／PGo（SD） | NG |  |  |  |
| VG1－PMPG／PMPGo | OK | NG |  |  |
| VG1－PG／PGo（LD） | OK | NG | NG |  |
| VG1－PG／PGo（PR） | OK | NG | NG | NG |
| VG1－PG／PGo（PD） |  |  |  |  |

＊4 When OPC－VG1－PMPG is attached，the available terminals change depending on the control method selected． When the vector control with speed sensor for induction motor is selected，terminals（PA and PB）of the main control print circuit board are available．
When the vector control with speed sensor for synchronous motor is selected，OPC－VG1－PMPG is available．
＊5 The OPC－VG1－SPGT can only be mounted on B port．
＊6 When this combination is needed，contact your Fuji Electric representative．
＊7 Restrictions when TBSI is used in as a part of SIU system．
＊8 Restrictions when TBSI is used for multi－winding motor drive or direct parallel system．

## FRENIC-

## Chapter 6 Converter System

## (Diode Rectifier, PWM Converter, Filter Stack, Braking System)

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### 6.1 Multi-converter system

A converter that converts AC power to DC power is separately required to use the FRENIC-VG stack type inverters. For this purpose, two versions of stack type converts (i.e., diode rectifiers and PWM converters) are available to support your system configuration needs.
A converter may also be connected to more than one inverter via DC bus bars, to conserve energy more efficiently by transferring regenerative energy of the inverter, while reducing the capacity of the converter at the same time.
In addition, unit type PWM converters (RHC-C series) are also available for use in combination with the FRENIC-VG stack type inverters.
This chapter describes two different versions of stack type converters (i.e., diode rectifiers and PWM converters), filter stacks (RHF-D series), and braking systems (braking unit + braking resistor).

| Converter type | Description | Max. output capacity ${ }^{* 1}$ |
| :---: | :---: | :---: |
| Diode rectifier <br> Stack type <br> RHD-D series | - AC power is converted to DC power by diode rectifier, which is then supplied to inverter. <br> - Supply of high capacity power is enabled by parallel connection. <br> - Equipped with DC reactor for input power factor improvement (reduction of the harmonic currents). On the other hand, reduction of harmonic currents generated by 12 -pulse rectifier is also made possible by installing a power transformer. <br> - By connecting a braking unit and a braking resistor (DBR), it may also be made to convert regenerative energy from motor (electric power energy) to thermal energy, for processing of regenerative energy. | 400V series <br> - 1450 kW (MD spec) <br> - 1640 kW (LD spec) <br> 690V series <br> - 2000 kW (MD spec) |
| High-efficiency <br> power <br> regeneration <br> PWM converter <br> Stack type <br> RHC-D series <br> Unit type <br> RHC-C series | - IGBT is driven by PWM control to convert AC power to DC power, which is then supplied to inverter. <br> - Supply of high capacity power is enabled by parallel connection. <br> - Use of PWM control makes it possible to greatly reduce the harmonic current of the AC power supply. <br> (The power factor is controlled at approximately "1".) <br> - The regenerative energy is returned to the AC power. The regenerative energy is applicable to a large load. | RHC-D series (Transformer parallel system) 400V series <br> - 2400 kW (MD spec) <br> - 3000 kW (LD spec) <br> 690V series <br> - 1200 kW <br> (MD, LD spec) |
| Filter stack <br> Stack type <br> RHF-D series <br> *Dedicated to use with the RHC-D*2 | - This filter stack is dedicated to use with the RHC-D series high-efficiency power regeneration PWM converters. <br> - All peripherals (filter, booster, charging circuits, etc.) required to run a PWM converter are packaged in a single unit. <br> - It is possible to save wiring work and installation space for peripherals. <br> - Built on the same stack design and shape as inverters and PWM converters, these products effectively help reduce the panel size. | (10) Refer to Section 6.4.) |
| Braking system (braking unit) (braking resistor) | - These products provide a braking system that consumes regenerative energy from a motor as thermal energy by use of a resistor. (thus achieving high braking performance). <br> - Braking unit: BU $\square \square \square-4 \mathrm{C}$ <br> Standard rating at duty cycle of $10 \%$ ED. Can be increased to duty cycle of $30 \%$ ED Max. by installing the optional fan unit (BU-F). <br> - Braking resistor: DB $\square \square \mathrm{V}-\square \square$ <br> Two standard types are available: duty cycle 10\%ED and 20\%ED. | (떼 Refer to Section 6.5.) |

*1 The Max. output capacity values are based on the assumption that the respective converters are connected in parallel. The number of connectable units varies depending on the converter.
*2 Cannot be used with unit type PWM converters (RHC-C series).

### 6.2 Diode rectifiers (RHD-D series)

### 6.2.1 Features

## - Converter type

Diode rectifier converts AC power to DC power, and then supplies DC power to inverter.

Diode rectification circuit converts AC power to DC power.


Substantial applicable capacity
A high capacity system can be constructed by connecting diode rectifiers in parallel.
(12-phase rectification + parallel connection (using 6 units of diode rectifiers))

- 400 V series: 1450 kW (MD spec) or 1640 kW (LD spec) (at supply voltage of 400 V )
- 690 V series: 2000 kW (MD spec) (at supply voltage of 690 V )
<Example of constructing a high capacity system>
RFI: Diode rectifier
$\mathrm{I}:$ Inverter
$\mathrm{TBSI}:$ Optical communication card (optional)
Power
supply

Note To connect multiple diode rectifiers in parallel (so that all of them have the same output), ensure that they all have the same capacity.

## Reduction of harmonic currents

The RHD-D series diode rectifiers are equipped with a built-in DC reactor for reduction of the harmonic currents. Further reduction of harmonic currents is made possible by creating a 12-phase rectification system in combination with a power transformer, when connecting more than one unit in parallel.

## Braking device

A discharging resistor braking device (that consists of a braking unit and braking resistor) is available an externally mounted option. You can select the capacity based on the required regenerative energy amount, thereby constructing a compact system.

### 6.2.2 Standard specifications

### 6.2.2.1 3-phase 400V series

| Model |  |  |  | RHD200S-4D $\square$ | RHD315S-4D $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 0 \\ & \stackrel{\otimes}{0} \\ & \dot{N} \\ & 0 \\ & \sum \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{訁} \\ & \frac{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity [kW] *1 |  | 227 | 353 |
|  |  | Nominal applied inverter/motor capacity *1 |  | 200 | 315 |
|  |  | Overload rating |  | 150\% of the continuous rating for 1 minute |  |
|  |  | Voltage |  | 513 to 679 VDC (variable according to input voltage and load) |  |
|  | Max. connection capacity [kW] ${ }^{* 1 * 2}$ |  |  | 600 | 945 |
|  | Min. connection capacity [kW] ${ }^{\text {¹ }}$ |  |  | 110 | 180 |
|  | Required power supply capacity [kVA] |  |  | 248 | 388 |
| $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{3} \\ & \stackrel{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity [kW]*1 |  | 247 | 400 |
|  |  | Nominal applied inverter/motor capacity * 1 |  | 220 | 355 |
|  |  | Overload rating |  | 110\% of the continuous rating for 1 minute |  |
|  |  | Voltage |  | 513 to 679 VDC (variable according to input voltage and load) |  |
|  | Max. connection capacity [kW] ${ }^{* 1 * 2}$ |  |  | 600 | 1065 |
|  | Min. connection capacity [kW] ${ }^{\text {*1 }}$ |  |  | 110 | 180 |
|  | Required power supply capacity [kVA] |  |  | 271 | 435 |
|  | Main power supply <br> Number of phases, voltage, and frequency |  |  | 3-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}$ |  |
|  | Fan power supply auxiliary input Number of phases, voltage, and frequency |  | 400 V input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 3}$ |  |
|  |  |  | 200 V input | Single-phase, 200 to $220 \mathrm{~V} / 50 \mathrm{~Hz}, 200$ to $230 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{*}$ |  |
|  | Allowable fluctuation |  |  | Voltage: +10 to -15\% (inter-phase unbalance rate: within $2 \%{ }^{* 5}$ ) Frequency wave number: $+5 \%$ to $-5 \%$ |  |
| Approx. mass [kg] |  |  |  | 125 | 160 |
| Enclosure |  |  |  | IP00 |  |
| Common Specifications |  |  |  | RaRefer to "2.2.1 Installation environment and conformity with standards" in Chapter 2. |  |

*1 Reduction of capacity is required for supply voltage under 400 V . Reduction of capacity is also required when multiple units are connected.
*2 Due to the restriction of the initial charging circuit, this is the total capacity of inverters that can be connected. However, the capacity of inverters that can be run at the same time is limited to the continuous capacity. This shows the total capacity of inverters that can be connected. However, the capacity of inverters that can be run in driving mode at the same time is the continuous capacity.
*3 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$ power supply, switching of converter internal terminals (U1, U2) is required.
*4 200 V power supply can also be used. For details, refer to "6.2.4 Terminal functions".
*5 Interphaseunbalance rate(\%) $=\frac{\text { Max. voltage[V] - Min. voltage[V] }}{3 \text { - phase average voltage }} \times 67$

### 6.2.2.2 3-phase 690V series

| Model |  |  |  | RHD220S-69D $\square$ | RHD450S-69D |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ©0 } \\ & \stackrel{N}{0} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { H } \\ & \text { 弟 } \\ & 0 \end{aligned}$ | Continuous capacity [kW] ${ }^{\text {¹ }}$ |  | 252 | 504 |
|  |  | Nominal applied inverter/motor capacity ${ }^{*}$ |  | 220 | 450 |
|  |  | Overload rating |  | 150\% of the continuous rating for 1 minute |  |
|  |  | Voltage |  | 776 to 1091 VDC (variable according to input voltage and load) |  |
|  | Max. connection capacity [kW] *1 *2 |  |  | 660 | 1350 |
|  | Min. connection capacity [kW] ${ }^{* 1}$ |  |  | 132 | 250 |
|  | Required power supply capacity [kVA] |  |  | 270 | 549 |
| $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & 0 \\ & 0 \end{aligned}$ | Continuous capacity [kW] ${ }^{+1}$ |  |  | 280 | - |
|  | $\begin{aligned} & \frac{1}{3} \\ & \frac{2}{3} \\ & \frac{1}{0} \end{aligned}$ | Nominal applied inverter/motor capacity ${ }^{*}$ |  | 250 | - |
|  |  | Overload rating |  | 110\% of the continuous rating for 1 minute |  |
|  |  | Voltage |  | 776 to 1091 VDC (variable according to input voltage and load) |  |
|  | Max. connection capacity [kW] ${ }^{* 1}$ *2 |  |  | 750 | - |
|  | Min. connection capacity [kW] ${ }^{\text {* }}$ |  |  | 132 | - |
|  | Required power supply capacity [kVA] |  |  | 308 | - |
|  | Main power supply <br> Number of phases, voltage, and frequency |  |  | 3-phase, 575 to $690 \mathrm{~V} / 50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ |  |
|  | Fan power supply auxiliary input Number of phases, voltage, and frequency |  | 690 V input | Single-phase, 660 to 690 V, $50 \mathrm{~Hz} / 60 \mathrm{~Hz}, 575$ to $600 \mathrm{~V}, 50 \mathrm{~Hz} / 60$ $\mathrm{Hz}^{* 3}$ |  |
|  |  |  | 200 V input | Single-phase, 200 to $220 \mathrm{~V} / 50 \mathrm{~Hz}, 200$ to $230 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{*} 4$ |  |
|  | Allowable fluctuation |  |  | Voltage: +10 to -15\% (inter-phase unbalance rate: within $2 \%{ }^{* 5}$ ) Frequency wave number: $+5 \%$ to $-5 \%$ |  |
| Approx. mass [kg] |  |  |  | 125 | 160 |
| Enclosure |  |  |  | IP00 |  |
| Common Specifications |  |  |  | $\square$ Refer to "2.2.1 Installation environment and conformity with standards" in Chapter 2. |  |

*1 This specification applies when the supply voltage is 690 V . Reduction of capacity is required for supply voltage under 690 V . Reduction of capacity is also required when multiple units are connected.
*2 Due to the restriction of the initial charging circuit, this is the total capacity of inverters that can be connected. However, the capacity of inverters that can be run at the same time is limited to the continuous capacity. This shows the total capacity of inverters that can be connected. However, the capacity of inverters that can be run in driving mode at the same time is the continuous capacity.
*3 For 690 V series 575 to $600 \mathrm{~V}, 50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ power supply, switching of converter internal terminals (U1, U2) is required.
*4 200 V power supply can also be used. For details, refer to "6.2.4 Terminal functions".
*5 Interphaseunbalance rate $(\%)=\frac{\text { Max. voltage[V] - Min. voltage[V] }}{3 \text { - phase average voltage }} \times 67$

### 6.2.3 Basic connection diagrams

### 6.2.3.1 When a diode rectifier and an inverter are connected on a $1: 1$ basis



Figure 6.2.3-1: Basic connection diagram (when a diode rectifier and an inverter are connected on a 1:1 basis)
Note 1) Construct a sequence in which the "Coast to a stop" command is input to the inverter until the initial charging of the diode rectifier is completed. Assign the "Coast to a stop" command (BX) to one of the inverter's terminals X1 to X9. Use function code E14 to configure the b-contact input so that input occurs on the b-contact. In this connection configuration, the motor will be in "coast to a stop" state when an instantaneous power failure occurs. Therefore, when using the circuit for purposes such as vertical transportation, provide an external interlock circuit.
Note 2) The overheat signal of the diode rectifier is output. Make sure to connect one of the inverter's terminals X1 to X9 to external alarm (THR). Use function code E14 to configure the b-contact input so that input occurs on the b-contact.
Note 3) When using microswitches for AC fuse disconnection detection, assign external alarm (THR) to one of the inverter's terminals X1 to X9, and connect all of the microswitches in series. Use function code E14 to configure the b-contact input so that input occurs on the b-contact.
Note 4) When inputting 200 VAC as the fan power supply, remove jumper wires from between terminals R11 and R12 and from between terminals T11 and T12, and then connect the input to terminals R12 and T12.
Note 5) The control signal and drive power supply for the charging circuit contactor (73) can be input from the outside. To do so, make the wiring as illustrated in Figure 6.2.3-2. Additionally, contactors 73A and 73C can also be used for the external sequence circuit.
Note 6) When connecting multiple diode rectifiers, use the electromagnetic contactor for power supply (52) at the same time. Furthermore, connect overheat signal outputs (1, 2), charging circuit operation signals (ONA, ONB, ONC), and AC fuse blow detection microswitch output in series between each stack.
Note 7) For the 400 V series, connect "Fdc" (fuse) to either the $P(+)$ side or $N(-)$ side.
For the 690V series, connect "Fdc" (fuse) to both the $\mathrm{P}(+)$ and $\mathrm{N}(-)$ sides.
(Use two microswitches and connect them in series.)

## WARNING

- Be sure to assign the inverter digital input terminal (X1 to X9) to the external alarm (THR), and to connect the diode rectifier overheat signal outputs $(1,2)$.
- Be sure to stop the inverter when the overheat signal is output.


## Risk of fire, accident



Figure 6.2.3-2: Control signal connection for the charging circuit contactor (73)

### 6.2.3.2 When connecting multiple diode rectifiers



Figure 6.2.3-3: Basic connection diagram (with two diode rectifiers connected in parallel)

* When connecting multiple diode rectifiers, use the electromagnetic contactor for power supply (52) at the same time. Furthermore, connect overheat signal outputs (1, 2), charging circuit operation signals (ONA, ONC), and AC fuse blow detection microswitch output in series between each stack.


### 6.2.4 Terminal functions

| Terminal symbol |  | Name | Specifications |
| :---: | :---: | :---: | :---: |
|  | L1/R, L2/S, L3/T | Main power input | Connect to a 3-phase power supply. |
|  | P (+), N (-) | Converter output | Connect to inverter power input terminals $\mathrm{P}(+)$ and $\mathrm{N}(-)$. |
|  | E(G) | Converter grounding | Grounding terminal for the chassis (case) of the diode rectifier. |
|  | R1, T1 | Fan power input (400V series: when 400 V is input) ( 690 V series: when 690 V is input) | To be used as supply input of AC cooling fan of inside the diode rectifier. Internal switching connector needs to be changed to meet supply voltage. <br> Refer to "4.5.3 (5) Fan power auxiliary input terminals R1 and T1" in Chapter 4. |
|  | $\begin{aligned} & \text { R11, R12 } \\ & \text { T11, T12 *1 } \end{aligned}$ | Fan power input (when 200 V is input) | To be used when inputting 200 VAC as the power to the AC cooling fan inside the diode rectifier. <br> When inputting 200 VAC as the fan power supply, remove jumper wires from between terminals R11 and R12 and from between terminals T11 and T12, and then connect the input to terminals R12 and T12. |
|  | $\begin{aligned} & 73 R \\ & 73 T \end{aligned}$ | Power supply for charging circuit | Driving supply of charging circuit contactor. Not to be used as power supply for an external circuit. |
|  | U1, U2 *2 | Supply voltage switching terminal | Change the terminal connection depending on the power supply connected to the fan power input terminals. <br> (Refer to Figure 6.2.4-2.) |
|  | $\begin{aligned} & 73-1 \\ & 73-2 \end{aligned}$ | Charging circuit contactor Control input | Control signal input for charging circuit contactor Control signal may also be input externally.* ${ }^{3}$ <br> <Coil rated capacity> <br> - 400V series <br> At power on ... $200 \mathrm{~V} / 50 \mathrm{~Hz}: 390 \mathrm{VA}, 220 \mathrm{~V} / 60 \mathrm{~Hz}: 460 \mathrm{VA}$ <br> At power hold ... $200 \mathrm{~V} / 50 \mathrm{~Hz}$ : 28.6 VA, $220 \mathrm{~V} / 60 \mathrm{~Hz}: 28.8 \mathrm{VA}$ <br> - 690V series <br> At power on ... $200 \mathrm{~V} / 50 \mathrm{~Hz}: 470 \mathrm{VA}, 220 \mathrm{~V} / 60 \mathrm{~Hz}: 500 \mathrm{VA}$ <br> At power hold ... $200 \mathrm{~V} / 50 \mathrm{~Hz}: 40.0 \mathrm{VA}, 220 \mathrm{~V} / 60 \mathrm{~Hz}: 39.0 \mathrm{VA}$ |
| $\begin{aligned} & \frac{\infty}{0} \\ & \stackrel{\rightharpoonup}{0} \\ & 0 \\ & \stackrel{0}{0} \\ & \frac{0}{3} \\ & 0 \end{aligned}$ | $\begin{aligned} & 73 A^{* 4} \\ & 73 C \end{aligned}$ | Control signal output for charging circuit | Control signal for charging circuit Contact rating: 250 VAC $0.5 \mathrm{~A} \cos \varphi=0.3,30$ VDC 0.5 A |
|  | ONA ONC | Charging circuit operation signal | Auxiliary contact output for charging circuit contactor To be used as signal for operational check of charging circuit. Contact rating: 24 VDC 3 A * Min. working voltage/current: 5 VDC 3 mA |
|  | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | Overheat signal output | Signal is output when internal parts of diode rectifier are overheated. Contact rating: 24 VDC (max. 27 V ), max. $0.3 \mathrm{~A} / \mathrm{max}$. 6 W <br> * Min. usage voltage, current: $1 \mathrm{VDC}, 0.1 \mathrm{~mA}$ |

*1 Terminals R11, R12, T11, and T12 are 200 V power terminals and their withstand voltage is 2000 VAC for 1 minute.
*2 Terminals U1 and U2 can be switched as shown in Figure 6.2.4-2.
*3 Refer to Figure 6.2.3-2 for connection method.
Contactor should be powered after completion of initial charging. Do not open contactor while inverter is in operation. This poses a risk of damaging the initial charging circuit.
*4 Refer to Figure 6.2.4-1 for timing chart of output signal, and DC PN voltage at signal output.


Figure 6.2.4-1: 73A-73C signal timing chart

## WARNING

- Be sure to assign the inverter digital input terminal (X1 to X9) to the external alarm (THR), and to connect the diode rectifier overheat signal outputs $(1,2)$.
- Be sure to stop the inverter when the overheat signal is output.

Risk of fire, accident


Figure 6.2.4-2: Supply voltage switching terminals

### 6.2.5 Check before use

Unpack the package and check the following:
Check that you have properly received the product main unit and the following accessories.
Accessories Instruction manual
Check that the inverter has not been damaged during transportation-there should be no dents or parts missing. The main and sub nameplates are attached to the main unit. The main nameplate is located on the front face of the main unit (as shown in Figure 6.2.6-2 and Figure 6.2.6-3). Check these main nameplates to see that the inverter is exactly the type you ordered.

(a) Main Nameplate

## TYPE RHD200S-4DJ

 SER.No. 28A456A0004BA(b) Sub Nameplate

Figure 6.2.5-1: Nameplate
TYPE: Diode rectifier (RHD-D)


The diode rectifier may be used by selecting either MD spec/LD spec, depending on the applicable load. Specifications in each mode are printed on the nameplate.

| Medium Duty $:$ | MD spec: designed for medium duty overload applications. Overload current rating: $150 \%$ for 1 min., Continuous |
| :--- | :--- |
| rating capacity = Capacity of inverters |  |

If you suspect the product is not working properly or if you have any questions about your product, contact your Fuji Electric representative.
[1] Refer to Chapter 3 "Transportation and Storage of Stack" for information on transportation and long-term storage of diode rectifiers.
(1) Refer to Chapter 4 "Installation and Wiring" for information on installation of diode rectifiers. For information on the main circuit wire sizes, refer to "6.2.13 Recommended wire size".

띠 For more details, refer to the Instruction Manual. (400V: INR-SI47-1786, 690V: INR-SI47-1852)

### 6.2.6 External views

### 6.2.6.1 Warning label and falling warning label

| ■RISK OF INJURY OR ELECTRIC SHOCK |
| :--- |
| •Refer to the instruction manual before installation and operation. |
| - Do not remove any cover while applying power and at least 10 min |
| after disconnecting power. |
| - More than one live circuit. See instruction manual. |
| - Do not insert fingers or anything else into the inverter. |
| - Securely ground (earth) the equipment. |
| •High touch current. |



Figure 6.2.6-1: Warning label and falling warning label

### 6.2.6.2 Appearance



Figure 6.2.6-2: Frame 3 size (RHD200S-4D $\square$, RHD220S-69D $\square$ )


Figure 6.2.6-3: Frame 4 size (RHD315S-4D $\square$, RHD450S-69D $\square$ )

### 6.2.7 External dimensions

### 6.2.7.1 List of external dimensions - RHD-D series (stack type)

Unit: [mm]

| Power-based <br> series | Model | Figure | W | H | D | Approx. mass <br> $[\mathrm{kg}]$ | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RHD200S-4D $\square$ | A | 226.2 | 1100 | 565 | 125 | Frame 3 size |
|  | RHD315S-4D $\square$ | B | 226.2 | 1400 | 565 | 160 | Frame 4 size |
| 690V | RHD220S-69D $\square$ | A | 226.2 | 1100 | 565 | 125 | Frame 3 size |
|  | RHD450S-69D $\square$ | B | 226.2 | 1400 | 565 | 160 | Frame 4 size |

### 6.2.7.2 External dimensions

(1) Figure A (Frame 3 size: RHD200S-4D $\square$, RHD220S-69D $\square$ )

(2) Figure B (Frame 4 size: RHD315S-4D $\square$, RHD450S-69D $\square$ )


## 6．2．8 Terminal positions

## 6．2．8．1 Main circuit terminals



View from bottom底面から見る

Figure 6．2．8－1：Frame 3 size（RHD200S－4D $\square$ ，RHD220S－69D $\square$ ）

Select terminal screws that allow for a distance of 10 mm or greater to the chassis.


### 6.2.8.2 Control circuit terminal



Figure 6.2.8-3: Control terminal layout

### 6.2.8.3 Switch 1

400V series
690V series


Do not change Switch 1 from the factory default.
Note Make sure that Switch 1 is set to the factory default before turning on the power.

|  | Setting of Switch 1 |
| :--- | :---: |
| 400 V series | 400 V |
| 690 V series | 690 V |

### 6.2.9 Multi-unit connection (capacity expansion)

A high capacity system can be constructed by connecting diode rectifiers (RHD-D) in parallel.
There are two methods of capacity expansion: parallel connection and 12-phase rectification.

| Parallel connection method | 12-phase rectification method |
| :---: | :---: |
| Up to three diode rectifiers can be connected in parallel to the same power supply system. | Up to six diode rectifiers (two sets of three rectifiers connected in parallel) by use of a 12-phase rectification transformer. <br> Connect an AC reactor (ACR) to the secondary side of the 12-phase rectification transformer. |
| <Nominal applied inverter/motor capacity> <br> - 400 V series: (at supply voltage of 400 V ) 850 kW for MD spec or 950 kW for LD spec <br> - 690 V series: (at supply voltage of 690 V ) 1200 kW for MD spec | <Nominal applied inverter/motor capacity> <br> - 400 V series: (at supply voltage of 400 V ) 1450 kW for MD spec or 1640 kW for LD spec <br> - 690 V series: (at supply voltage of 690 V ) 2000 kW for MD spec |
|  |  |

Figure 6.2.9-2: 12-phase rectification and parallel connection
Figure 6.2.9-1: 3 units connected in parallel
(Note 1) To connect multiple diode rectifiers so that all of them have the same output, ensure that they all have the same capacity.
(Note 2) The maximum applied capacity is calculated on the assumption that the capacity reduction compensation factor based on the supply voltage is $100 \%$. For information on how to accurately calculate the capacity based on the use conditions, refer to "6.2.9.1 Parallel connection method" to "6.2.9.4 Example of calculating the nominal applied inverter/motor capacity".

### 6.2.9.1 Parallel connection method

## (1) Output capacity reduction

Up to three diode rectifiers (RHD-D) can be connected in parallel. Parallel connection requires reduction of the output capacity. Use the reduction rates shown in Table 6.2.9-1, calculate and consider the output capacity.
(The reduction rates shown apply to the 400 V series at supply voltage of 400 V and to the 690 V series at supply voltage of 690 V .)

Table 6.2.9-1: Output capacity reduction rates for the parallel connection method

| Number of sets connected in parallel | Output capacity reduction rate |
| :---: | :---: |
| 2 parallel sets | $92[\%]$ |
| 3 parallel sets | $92[\%]$ |

## (2) Precautions for connecting rectifiers

1) Ensure that all the diode rectifiers (RHD-D) have the same wiring length (portion A) from the power supply to their input terminal.
2) Ensure that all the diode rectifiers (RHD-D) have the same wiring length (portion B) from their output terminal to the DC bus bar.
3) The wiring length for portion $C$ should be within 500 mm . Also, the wiring length for portion C 1 should be equal to that for portion C 2 .


Figure 6.2.9-3: Precautions for parallel connection

### 6.2.9.2 12-phase rectification method

## (1) Output capacity reduction

Output capacity reduction (applicable to the 400 V series at supply voltage of 400 V and to the 690 V series at supply voltage of 690 V )
Up to six diode rectifiers (RHD-D) can be connected by use of a 12-phase rectification transformer in combination with parallel connection. Whether or not combined with parallel connection, 12-phase rectification requires reduction of the output capacity. Use the reduction rates shown in Table 6.2.9-2, and calculate and consider the output capacity. (The reduction rates shown apply to the 400 V series at supply voltage of 400 V and to the 690 V series at supply voltage of 690 V .)

Table 6.2.9-2: Output capacity reduction rates for the 12-phase rectification method

| Configuration | 400 V series | 690 V series |
| :---: | :---: | :---: |
| 12-phase rectification | $87 \%$ | $77 \%$ |
| 12-phase rectification combined with parallel connection | $77 \%$ | $70 \%$ |

## (2) Precautions for connecting rectifiers

Ensure that the 12-phase rectification transformer meets the specifications in Table 6.2.9-3.
Table 6.2.9-3: 12-phase rectification transformer specifications

| Characteristics | 400 V <br> Series | 690 V <br> Series |
| :---: | :---: | :---: |
| No-load voltage difference (voltage <br> transformation ratio) between $\Delta$ and Y | 1.5 V or <br> lower | 3.0 V or <br> lower |
| $\% \mathrm{X}$ | $4 \%$ or higher |  |
| Unbalance rate between $\Delta$ and $\mathrm{Y}(\% \mathrm{X})$ | $10 \%$ or lower |  |
| $\% \mathrm{R}$ | $1 \%$ or higher |  |
| Unbalance rate between $\Delta$ and $\mathrm{Y}(\% \mathrm{R})$ | $10 \%$ or lower |  |


$\left(^{*}\right)$ If the supply voltage includes 5 th and/or 7 th order components, a reactor is required on the secondary side of the 12-phase rectification transformer.
This reactor must have an inductance equivalent to $10 \%$ or higher of the required power capacity of the diode rectifiers.
In addition, the variation in inductance must not exceed 10\%.

### 6.2.9.3 Capacity reduction compensation based on the supply voltage

When capacity reduction is required for parallel connection and/or 12-phase rectification, the reduction rate can be mitigated based on the supply voltage. To calculate the compensation factor based on the supply voltage, use the formula given below.

However, if (reduction rate) $x$ (compensation factor) is higher than $100 \%$, use $100 \%$ as the upper limit.

$$
\text { Compensation factor }(\%)=\frac{\text { Supply voltage [V] }}{400[\mathrm{~V}]}
$$

(*) Even when the supply voltage is lower than 400 V , use the formula above to reduce the capacity (in the case of the 400 V series).

### 6.2.9.4 Example of calculating the nominal applied inverter/motor capacity

The nominal applied inverter/motor capacity can be calculated using the formula below.
Nominal applied inverter/motor capacity[kW]
$=($ Stack capacity $[\mathrm{kW}]) \times$ (number of units) $\times$ (parallel connectiondegressionrate [12-phase rectification reductionrate]) x (supply voltage compensation factor)

|  | Conditions | Parallel connection reduction rate | 12-phase rectification reduction rate | Supply voltage compensation factor | Nominal applied inverter/motor capacity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\underset{1}{\text { Example }}$ | Supply voltage $: 440 \mathrm{~V}$ <br> Stacks used $:$ RHD315-4D (MD) x <br>  6 units <br> Connection method $: 3$ parallel sets x <br>  12 -phase rectification | 77\% |  | $\begin{gathered} 110 \% \\ (440 \mathrm{~V} / 400 \mathrm{~V}) \end{gathered}$ | $\begin{gathered} 1600 \mathrm{~kW} \text { (MD) } \\ (315 \times 6 \times 77 \% \times 110 \%) \end{gathered}$ |
| $\begin{gathered} \text { Example } \\ 2 \end{gathered}$ | Supply voltage $: 480 \mathrm{~V}$ <br> Stacks used $:$ RHD200-4D(MD) x <br>  2 units <br> Connection method $: 12$-phase rectification | - | 87\% | $\begin{gathered} 120 \% \\ (480 \mathrm{~V} / 400 \mathrm{~V}) \end{gathered}$ | 400 kW (MD) ( $200 \times 2 \times 100 \%$ ) (Note 1) |
| $\begin{gathered} \text { Example } \\ 3 \end{gathered}$ | Supply voltage $: 380 \mathrm{~V}$ <br> Stacks used $:$ RHD315-4D (LD) x <br>  3 units <br> Connection method $: 3$ parallel sets | 92\% | - | $\begin{gathered} 95 \% \\ (380 \mathrm{~V} / 400 \mathrm{~V}) \end{gathered}$ | $\begin{gathered} 930 \mathrm{~kW} \text { (LD) } \\ (355 \times 3 \times 92 \% \times 95 \%) \end{gathered}$ |

(Note 1) $87 \% \times 120 \%=104.4 \%$. Hence, use $100 \%$, the upper limit.

### 6.2.10 System configuration examples

| No. | System configuration diagram (Symbols in diagram) <br> RFI: Diode rectifier <br> I: Inverter, TBSI: Optical communication card (optional) | Diode rectifier configured system |  | Inverter configured system |  | Remarks* <br> - Applied inverter/motor capacity <br> - Precautions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity expansion method | Number of connected units | Capacity expansion method | Number of connected units |  |
| 1 |  | - | 1 | - | Multiple | [Applied capacity] <400V series> <br> - MD: up to 315 kW <br> - LD: up to 355 kW <690V series> |
| 2 |  | - | 1 | Direct parallel <br> Multiwinding driving | 3 (Max) $\begin{gathered} 6 \\ (\mathrm{Max}) \end{gathered}$ | kW |
| 3 |  | Parallel connection | $2$ | - | Multiple | When used without connecting (sharing) each RFI output. <br> [Applied capacity] <400V series> <br> - MD: up to 315 kW <br> - LD: up to 355 kW <690V series> <br> - MD: up to 450 kW |
| 4 |  | Parallel connection | 2 | - | Multiple | When used by connecting (sharing) each RFI output. <br> [Applied capacity] <400V series> <br> - MD: up to 579 kW <br> - LD: up to 653 kW <br> <690V series> <br> - MD: up to 828 kW |

* The nominal applied inverter/motor capacity is calculated on the assumption that the capacity reduction compensation based on the supply voltage is $100 \%$. For information on how to accurately calculate the capacity based on the use conditions, refer to "6.2.9.1 Parallel connection method" to "6.2.9.4 Example of calculating the nominal applied inverter/motor capacity".
(Note 1) To connect multiple diode rectifiers so that all of them have the same output, ensure that they all have the same capacity.
(Note 2) When using direct parallel connection and multi-winding driving systems, ensure that all the inverters have the same capacity.

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \multirow[b]{2}{*}{No} \& \multirow[t]{2}{*}{\begin{tabular}{l}
System configuration diagram \\
(Symbols in diagram) \\
RFI: Diode rectifier \\
I: Inverter, TBSI: Optical communication card (optional)
\end{tabular}} \& \multicolumn{2}{|l|}{Diode rectifier configured system} \& \multicolumn{2}{|l|}{Inverter configured system} \& \multirow[t]{2}{*}{\begin{tabular}{l}
Remarks* \\
- Applied inverter/motor capacity \\
- Precautions
\end{tabular}} \\
\hline \& \& Capacity expansion method \& Number of connected units \& Capacity expansion method \& Number of connected units \& \\
\hline 5 \&  \& Parallel connection \& 3 \& - \& Multiple \& \begin{tabular}{l}
When used by connecting (sharing) each RFI output. \\
[Applied capacity] <400V series> \\
- MD: up to 869 kW \\
- LD: up to 979 kW <690V series> \\
- MD: up to 1240 kW
\end{tabular} \\
\hline 6 \&  \& Parallel connection \& 2

3 \& Multiwinding driving \& \[
$$
\begin{gathered}
6 \\
(\operatorname{Max})
\end{gathered}
$$

\] \& | [Applied capacity] When using 3 units of RFI <400V series> |
| :--- |
| - MD: up to 945 kW |
| - LD: up to 1065 kW <690V series> |
| - MD: up to 1350 kW | <br>


\hline 7 \&  \& Parallel connection \& 2 \& | Direct parallel |
| :--- |
| Multiwinding driving | \& \[

$$
\begin{gathered}
3 \\
(M a x)
\end{gathered}
$$
\]

\[
$$
\begin{gathered}
6 \\
(\mathrm{Max})
\end{gathered}
$$

\] \& | [Applied capacity] <400V series> |
| :--- |
| - MD: up to 579 kW |
| - LD: up to 653 kW |
| <690V series> |
| - MD: up to 828 kW | <br>


\hline 8 \&  \& Parallel connection \& 3 \& | Direct parallel |
| :--- |
| Multiwinding driving | \& | 3 $(\mathrm{Max})$ |
| :--- |
| (Max) $\begin{gathered} 6 \\ (\mathrm{Max}) \end{gathered}$ | \& | [Applied capacity] <400V series> |
| :--- |
| - MD: up to 869 kW |
| - LD: up to 979 kW <690V series> |
| - MD: up to 1240 kW | <br>

\hline
\end{tabular}

* The nominal applied inverter/motor capacity is calculated on the assumption that the capacity reduction compensation based on the supply voltage is $100 \%$. For information on how to accurately calculate the capacity based on the use conditions, refer to "6.2.9.1 Parallel connection method" to "6.2.9.4 Example of calculating the nominal applied inverter/motor capacity".
(Note 1) To connect multiple diode rectifiers so that all of them have the same output, ensure that they all have the same capacity.
(Note 2) When using direct parallel connection and multi-winding driving systems, ensure that all the inverters have the same capacity.

| No | System configuration diagram <br> (Symbols in diagram) <br> RFI: Diode rectifier <br> I: Inverter, TBSI: Optical communication card (optional) | Diode rectifier configured system |  | Inverter configured system |  | Remarks* <br> - Applied inverter/motor capacity <br> - Precautions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Capacity expansion method | Number of connected units | Capacity expansion method | Number of connected units |  |
| 9 |  | 12-phase rectification | 2 | Multiwinding driving | $\begin{gathered} 6 \\ \text { (Max) } \end{gathered}$ | [Applied capacity] <400V series> <br> - MD: up to 548 kW <br> - LD: up to 617 kW <690V series> <br> - MD: up to 783 kW |
| 10 |  | 12-phase rectification | 2 | Direct parallel <br> Multiwinding driving | 3 $(\mathrm{Max})$ <br> (Max) <br> 6 $(\mathrm{Max})$ | [Applied capacity] <400V series> <br> - MD: up to 548 kW <br> - LD: up to 617 kW <690V series> <br> - MD: up to 783 kW |
| 11 |  | 12-phase rectification | 4 | Direct parallel <br> Multiwinding driving | 3 $(\mathrm{Max})$ <br> 6 $(\mathrm{Max})$ | [Applied capacity] When using 3 units of RFI <400V series> <br> - MD: up to 970 kW <br> - LD: up to 1093 kW <690V series> <br> - MD: up to 1386 kW |
| 12 |  | 12-phase rectification | 6 | Direct parallel <br> Multiwinding driving | $\begin{gathered} 3 \\ (\operatorname{Max}) \\ \\ \hline \\ \\ 6 \\ (M a x) \end{gathered}$ | [Applied capacity] <400V series> <br> - MD: up to 1450 kW <br> - LD: up to 1640 kW <690V series> <br> - MD: up to 2000 kW |

* The nominal applied inverter/motor capacity is calculated on the assumption that the capacity reduction compensation based on the supply voltage is $100 \%$. For information on how to accurately calculate the capacity based on the use conditions, refer to "6.2.9.1 Parallel connection method" to "6.2.9.4 Example of calculating the nominal applied inverter/motor capacity".
(Note 1) To connect multiple diode rectifiers so that all of them have the same output, ensure that they all have the same capacity.
(Note 2) When using direct parallel connection and multi-winding driving systems, ensure that all the inverters have the same capacity.


### 6.2.11 Generated loss

The Table 6.2.11-1 shows diode rectifier generated losses.
Table 6.2.11-1: Diode rectifier generated losses

| Power-based <br> series | Model |  | Generated loss [W] |  |
| :---: | :--- | :---: | :---: | :---: |
|  |  | MD spec mode | LD spec mode |  |
| 400 V | RHD200S-4D $\square$ | 1650 | 1900 |  |
|  | RHD315S-4D $\square$ | 2550 | 3250 |  |
| 690 V | RHD220S-69 D $\square$ | 1200 | 1450 |  |
|  | RHD450S-69D $\square$ | 2450 | - |  |

### 6.2.12 Peripherals

### 6.2.12.1 AC fuse for diode rectifier

This is an AC fuse used for protecting a diode rectifier.
Use the inverter's fuse disconnection detection terminals to implement the detection of fuse disconnection. Purchase microswitches along with fuses.

* Fuse other than the types listed in "Application table" may not be used.



## (1) Application table

Fuse manufacturer: Eaton website: http://www.eaton.com/
*This product can be also purchased from Fuji Electric.
Table 6.2.12-1: Application table

| Voltage | Specifications | Nominal applied motor capacity [kW] | Diode rectifier model | AC Fuse |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Model | Fig. | Generated loss [W] | Approx. mass [kg] |
| 400 V | MD | 200 | RHD200S-4D $\square$ | 170M6547 | E | 130 | 1.25 |
|  |  | 315 | RHD315S-4D $\square$ | 170M6500 | F | 145 |  |
|  | LD | 220 | RHD200S-4D $\square$ | 170M6547 | E | 130 | 1.25 |
|  |  | 355 | RHD315S-4D $\square$ | 170M6500 | F | 145 |  |
| 690 V | MD | 220 | RHD220S-69D $\square$ | 170M6497 | F | 130 | 1.25 |
|  |  | 450 | RHD450S-69D $\square$ | 170M6501 | F | 150 |  |
|  | LD | 250 | RHD220S-69D $\square$ | 170M6497 | F | 130 | 1.25 |

## (2) External dimensions

For information on fuse external dimensions and installation steps, refer to "5.2.1.1 Fuses" in Chapter 5.

## (3) Microswitch

Model: 170 H 3027 * For details, refer to "5.2.1.1 Fuses" in Chapter 5.
(4) Connection diagram


Use the relay sequence shown in Figure 6.2.12-1
When using multiple inverters, abnormality signals for the microswitches and diode rectifiers (CNV1) associated with the AC fuses (ACF1 to ACF3) should be input to the relay ( 30 CNV ).
Connect this relay contact (30CNV) to one of terminals X1 to X9 on each inverter.

Assign "Coast to a stop" (BX) or external alarm (THR) to the inverter side.

If you choose to assign BX , make this a self-holding circuit (to be cancelled by reset PBS, etc.) as necessary.

Figure 6.2.12-1: Fuse wire connection diagram

### 6.2.12.2 $A C$ reactor (ACR: alternate current reactor)

An AC reactor is used for the purpose of preventing load allocation of diode rectifiers from becoming unbalanced when connected in parallel. It is also used when the supply voltage is unstable (extreme inter-phase voltage unbalance).

## (1) Applied example

When there are thyristor-driven loads or when phase-advancing capacitors are turned ON or OFF in the same power supply system


Figure 6.2.12-2: Description of receiving power supply

When the inter-phase unbalance rate of the inverter power supply exceeds $2 \%$
Interphaseunbalance rate $(\%)=\frac{\text { Max. voltage }(\mathrm{V})-\text { Min. voltage }(\mathrm{V})}{3-\text { phase average voltage }(\mathrm{V})} \times 67$

When connecting diode rectifiers in parallel


Figure 6.2.12-3: Configuration with two converters

Note 1) The diode rectifier and AC reactor used should be of the identical type.
Note 2) The contactor and AC reactor may be arranged in the opposite order of arrangement shown in this diagram.
Note 3) The wiring from MCCB to diode rectifiers (CNV1, CNV2) should be made the same length whenever possible.

## (2) AC reactor specifications



Figure 6.2.12-4: $A C$ reactor ( ACL ) and connection example

Table 6.2.12-2: List of AC reactor specifications

| Power supply system | Reactor model | Rated current [A] | Reactance [m $\Omega /$ phase] |  | Winding resistance [ $\mathrm{m} \Omega$ ] | $\begin{gathered} \text { Generated } \\ \text { loss } \\ {[\mathrm{W}]} \end{gathered}$ | Approx. mass [kg] | Dimensions |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 50 \\ & \mathrm{~Hz} \end{aligned}$ | $\begin{aligned} & 60 \\ & \mathrm{~Hz} \end{aligned}$ |  |  |  | Figure | W | W1 | D | D1 | D2 | G | H | J |
| 400 V | ACR4-110 | 250 | 16.7 | 20 | 0.523 | 60.3 | 24 | A | 250 | 100 | 136 | 105 | 202 | $\begin{gathered} \hline \text { M8 } \\ (9.5 \times 18) \end{gathered}$ | 245 | M12 |
|  | ACR4-132 | 270 | 20.8 | 25 | 0.741 | 119 | 32 |  | 250 | 100 | 146 | 115 | 207 | $\begin{gathered} \text { M8 } \\ (10 \times 16) \end{gathered}$ | 250 | M12 |
|  | ACR4-220 | 561 | 10 | 12 | 0.236 | 107 | 40 |  | 320 | 120 | 150 | 110 | 240 | $\begin{gathered} \text { M10 } \\ (12 \times 20) \\ \hline \end{gathered}$ | 300 | M12 |
|  | ACR4-280 | 825 | 6.67 | 8 | 0.144 | 108 | 52 |  | 380 | 130 | 150 | 110 | 260 | $\begin{gathered} \text { M10 } \\ (12 \times 20) \\ \hline \end{gathered}$ | 300 | M12 |
|  | ACR4-355 | 825 | 6.67 | 8 | 0.144 | 245 | 52 |  | 380 | 130 | 150 | 110 | 260 | $\begin{gathered} \text { M10 } \\ (12 \times 20) \end{gathered}$ | 300 | M12 |
|  | ACR4-450 | 950 | 6.67 | 8 | 0.136 | 473 | 95 | B | 460 | 155 | 290 | 230 | 200 | $\begin{array}{r} \text { M12 } \\ (\varphi 15) \\ \hline \end{array}$ | 490 | $4 \times \mathrm{M} 12$ |
|  | ACR4-530 | 1100 | 5.75 | 6.9 | 0.0824 | 340 | 100 | C | 480 | 155 | 420 | 370 |  | $\begin{gathered} \text { M12 } \\ (15 \times 25) \\ \hline \end{gathered}$ | 380 | $4 \times \mathrm{M} 12$ |
|  | ACR4-630 | 1300 | 4.87 | 5.84 | 0.0713 | 422 | 110 |  | 510 | 170 | 420 | 370 | - | $\begin{gathered} \text { M12 } \\ (15 \times 25) \\ \hline \end{gathered}$ | 390 | $4 \times \mathrm{M} 12$ |

Note 1) Generated losses listed in the above table are calculated under the conditions shown below.

- The power supply is 3 -phase $400 \mathrm{VAC}, 50 \mathrm{~Hz}$ and the inter-phase voltage unbalance ratio is $0 \%$.
- The power supply capacity is " 500 kVA " or "a capacity 10 times larger than the rated capacity of the inverter", whichever is larger.
- For the load motor, a 4-pole standard motor is used at full load (100\%).

Note 2) For information on AC reactors other than listed above, refer to "8.5.4 AC reactor (ACR)" in Chapter 8 of the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019).

## <Common>

Withstand voltage: 2500 VAC for 1 min. (Insulation class: Class H)
Insulation resistance: $100 \mathrm{M} \Omega$ (1000 V-Megger)
Ambient temperature: -20 to $50^{\circ} \mathrm{C}$
Humidity: 90\% Rh or less
Indoor altitude 1000 m or less
<External dimensions>

Figure A


Figure B


Figure C


Figure 6.2.12-5: External dimensions of AC reactor ( ACL )

### 6.2.12.3 Use of molded case circuit breakers (MCCBs)

A molded case circuit breaker (MCCB) protects the main circuit terminals (L1/R, L2/S, L3/T) of a converter (inverter) and is mainly used to protect the wiring from overload and short-circuiting to prevent a secondary accident after breakage of an inverter.

The degree of inverter protection generally depends on the overcurrent and overload protection functions built in the inverter.
[1] Equipment selection list for each converter model

- Diode rectifiers: Refer to "6.2.12.6 List of equipment (MCCB and MC)"
- PWM converters: Refer to "6.3.12.3 Input power supply circuit (MCCB, ELCB)".
- The modeled case circuit breakers (MCCBs) used for converters (including diode rectifiers and PWM converters) should be those for general wiring.
- Motor protection breakers may not be used for converters and inverters because they are rated to meet conditions for full-voltage starting.


## (1) Overcurrent tripping method

The overcurrent tripping devices should be a thermal-electromagnetic type, full electromagnetic type, or electronic type with higher harmonics prevention measures taken (RMS value detection method).

Table 6.2.12-3: Comparison of current tripping operations

| Comparison item | Thermal-electromagnetic type | Full electromagnetic type | Electronic type |
| :---: | :---: | :---: | :---: |
| Effect of ambient temperature | A bimetal is used. A bimetal has the property that changes the shape by the temperature. <br> Therefore, the effect of the temperature is not large, but the temperature may affect the internal components, causing the rated current to change. <br> * When the overcurrent relay is equipped with an ambient temperature compensation device, the rated current rarely changes. | The rated current does not change. However, as the viscosity of the silicon oil in the dash pod changes, the operation time changes. | A current detection circuit detects the conduction current. The temperature drift of the electronic device exists, but it does not affect greatly. |
| Effect of mounting posture | The impact is small. (Almost non-change.) | Since the weight of the plunger in the dash pod affects the operation, the operation current value changes depending on the mounting posture. | The impact is small. (Almost non-change.) |

## (2) Rated voltage

The rated voltages stated in the catalog or technical reference of the MCCB are the applicable maximum voltages.

## (3) Rated current

1) An appropriate MCCB should be selected that does not operate (trip) by either the input current or overload current during motor operation and protects the wires reliably. The MCCB operation characteristic curve shown in Figure 6.2.12-6 becomes the boundary line. The right portion shows that the MCCB operates while the left portion shows that it does not operate. Therefore, select an appropriate MCCB so that the right position shows the allowable current of the wire along the MCCB operation characteristic curve while the left portion shows the current during converter/inverter operation.


Figure 6.2.12-6: How to select the rated current of molded case circuit breaker (MCCB)
2) The rated current stated in the catalog or technical reference of the MCCB shows the value at an operating temperature of $40^{\circ} \mathrm{C}$. When storing the MCCB in a cabinet, the temperature coefficient (which should be reduced to 0.85 to 0.95 during operation depending on the MCCB) should be taken into consideration according to the set temperature inside the cabinet.

Rated current when using INV $=$ Rated current of $\mathrm{MCCB} \times \frac{1}{\text { Temperatue correctioncoefficient }(0.85 \text { to } 0.95)}$

## (4) Rated breaking current

Select an appropriate MCCB with the ability to break the short-circuit current. This is called full capacity breaking method.
In addition to this method, a cascade breaking method is also available that breaks the short-circuit current in cooperation with the breaker of the power supply if the breaking capacity of the MCCB for the inverter is insufficient. (However, there are restrictions on the combinations of breakers and protectors.)

When the short-circuit current value is unknown, calculate it while referring to the references shown below:

- Fuji auto breaker technical reference (EH150■)
- Technical description catalog "Short-circuit current calculation method (CY002)."

The value of the MCCB output terminal should be used as the short-circuit current value that becomes the reference.

If the short-circuit current is calculated with the value of the converter input terminal, the calculated value becomes small when the wiring is long since the impedance of the wire is taken into consideration. As a result, the breaking capacity becomes insufficient if a short-circuit accident occurs in the main circuit terminal of the MCCB.
(Refer to Figure 6.2.12-7.)


Figure 6.2.12-7: Accident point and short-circuit current

## (5) Selective tripping coordination

This selective tripping coordination means a relationship where only the breaker on the power supply side closest to the accident point operates and upstream breakers do not operate. This relationship needs to be established in both the overload and short-circuit areas. The selective tripping coordination is used when the reliable power supply is required for the power supply system with an important load.
For example, if a short-circuit accident occurs at point $X$ in Figure 6.2.12-7, the short-circuit current flows to the MCCB-1 and MCCB-3.
If the MCCB-1 is tripped by this short-circuit current, a power failure also occurs in the load of the MCCB-2. Therefore, to satisfy the selective tripping coordination, it is necessary to combine the MCCBs so that the tripping operation of the MCCB-3 is completed before the MCCB-1 operates in all ranges of the overcurrent protective area. (Refer to Figure 6.2.12-8.)


Figure 6.2.12-8: Selective tripping coordination
Table 6.2.12-4: List of Fuji Electric's MCCB (G-TWIN series) models: extracted from G-TWIN catalog (EH130■)

| Series/Applications <br> Specifications |  |  | Standard |  |  |  |  |  |  |  |  |  |  |  | Global <br> Momentary fixing type for general wiring (5) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | For general wiring |  | For motor protection | For primary side of transformer | Momentary breaking type |  | Non-auto switch (1) | With earth leakage alarm | With ZCT | With single-phase 3-wire neutral line open-phase protection (2) | Class 2 heat resistant type (3) | Distribution panel module (4) |  |
|  |  |  | Momentary fixed type | Momentary adjustable type |  |  | Momentary fixed type | Momentary adjustable type |  |  |  |  |  |  |  |
| Frame <br> (A) | Basic name | $\begin{aligned} & \begin{array}{l} \text { Rated braking } \\ \text { capacity } \\ \text { Icu[kA) } \end{array} \\ & \text { AC230V/ } \\ & \text { AC440V (JIS) } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 | BW32 | 2.5/1.5 | BW32AAG |  | BW32AAM |  |  |  |  |  |  |  |  | BW32AFC |  |
|  |  | 5/2.5 | BW32SAG |  | BW32SAM | BW32SAT | BW32SAQ |  | BW32SAS |  |  |  |  |  |  |
| 50 | BW50 | 2.5/1.5 | BW50AAG |  |  |  |  |  |  |  |  |  |  | BW50AFC |  |
|  |  | 5/2.5 | BW50EAG |  | BW50EAM | BW50EAT |  |  |  | BW50EAL |  | BW50EAN | BW50EAH |  |  |
|  |  | 10/7.5 | BW50SAG |  | BW50SAM | BW50SAT | BW50SAQ |  | BW50SAS |  |  |  | BW5OSAH |  |  |
|  |  | 25/10 | BW50RAG |  | BW50RAM |  |  |  |  |  |  |  |  |  | BW50RAGU |
|  |  | 125/65 | BW50HAG |  |  |  |  |  |  |  |  |  |  |  |  |
| 63 | BW63 | 5/2.5 | BW63EAG |  | BW63EAM |  | BW63EAQ |  |  |  |  |  |  |  |  |
|  |  | 10/7.5 | BW63SAG |  | BW63SAM |  | BW63SAO |  | BW63SAS |  |  |  |  |  |  |
|  |  | 25/10 | BW63RAG |  |  |  |  |  |  |  |  |  |  |  |  |
| 100 | BW100 | 5/1.5 | BW100AAG |  |  |  |  |  |  |  |  |  |  | BW100AFC |  |
|  |  | 25/10 | BW100EAG |  | BWIOOEAM | BWIOOEAT |  |  | BWIOOEAS | BWI00EAL |  | BWIOOEAN | BW100EAH |  | BW100EAGU |
| 125 | BW125 | 50/30 | BW125JAG |  | BW125JAM | BW125JAT | BW125JAQ |  | BWI25JAS | BW125JAL | BW125JAZ |  |  |  | BWI25JAGU |
|  |  | 100/50 | BW125RAG |  | BW125RAM |  | BW125AAQ |  | BWI25RAS | BW125RAL | BW125RAZ. |  |  |  | BWI25RAGU |
|  |  | 125/65 | BW125HAG |  |  |  |  |  |  |  |  |  |  |  |  |
| 250 | BW250 | 36/18 | BW250EAG |  | BW250EAM | BW250EAT |  |  | BW250EAS | BW250EAL |  | BW250EAN | BW250EAH |  | BW250EAGU |
|  |  | 50/30 | BW250JAG |  | BW250JAM |  | BW250JAQ |  |  | BW250JAL | BW250JAZ |  |  |  | BW250JAGU |
|  |  | 100/50 | BW250RAG |  | BW250RAM | BW250RAT | BW250RAQ |  | BW250RAS | BW250RAL | BW250RAZ |  |  |  | BW250RAGU |
|  |  | 125/65 | BW250HAG |  |  |  |  |  |  |  |  |  |  |  |  |
| 400 | BW400 | 50/30 | BW400EAG | BW400EAA |  | BW400EAT |  |  | BW400EAS | BW400EAL |  | BW400EAN | BW400EAH |  | BW400EAGU |
|  |  | 85/36 | BW400SAG | BW400SAA |  |  |  |  |  | BW400SAL | BW400SAZ |  |  |  | BW4OOSAGU |
|  |  | 100/50 | BW400PAG | BW400RAA |  | BW400RAT | BW400RAQ | BW400RAB | BW400RAS | BW400RAL | BW400RAZ |  |  |  | BW400RAGU |
|  |  | 125/70 | BW400HAG | BW 400 HAA |  |  | BW400HAQ | BW400HAB |  |  |  |  |  |  | BW400HAGU |
| 630 | BW630 | 50/36 | BW630EAG | BW630EAA |  | BW630EAT |  |  | BW630EAS | BW630EAL |  |  |  |  |  |
|  |  | 100/50 | BW630RAG | BW630RAA |  | BW630RAT | BW630RAQ | BW630RAB | BW630RAS | BW630RAL | BW630RAZ |  |  |  | BW630RAGU |
|  |  | 125/70 | BW630HAG | BW630HAA |  |  | BW630HAQ | BW630HAB |  |  |  |  |  |  | BW630HAGU |
| 800 | BW800 | 50/36 | BWBOOEAG | BW800EAA |  |  |  |  | BW800EAS | BW800EAL |  |  |  |  |  |
|  |  | 100/50 | BW800RAG | BW800RAA |  |  | BW800PAQ | BW800RAB | BWBOORAS | BW800RAL | BWBOORAZ |  |  |  | BW800RAGU |
|  |  | 125/70 | BW800HAG | BW800HAA |  |  | BW800HAQ | BW800HAB |  |  |  |  |  |  | BW800HAGU |

[^6]
### 6.2.12.4 Use of earth leakage circuit breakers (ELCBs)

To protect work personnel from an electric shock, prevent fire caused by earth leakage, or maintain the electric facilities, an earth leakage circuit breaker (ELCB) should be used instead of an MCCB to prevent such accidents. When using an ELCB with a converter or an inverter, the ELCB may function by the leakage current caused by high frequency switching operations.
(1) - The overcurrent protective function of an ELCB is the same as an MCCB. Refer to "6.2.12.3 Use of molded case circuit breakers (MCCBs)".

- For information on the equipment used for each diode rectifier model, refer to "6.2.12.6 List of equipment (MCCB and MC)".


## (1) Rated current sensitivity

As a rule, to aim at prevention of electric shock accidents, a product with high sensitivity and high-speed operation should be used. To aim at prevention of fire caused by earth leakage or damage to the unit, a product with medium sensitivity can be used. Additionally, the sensing time may need to be changed according to the wiring distance or motor capacity.
When the current sensitivity to be used is defined in a legally controlled place (an ELCB with high sensitivity and high-speed operation is used), investigate whether or not unnecessary operation is performed by continuous leakage current. In other cases, determine an appropriate ELCB in the manner shown below.

Table 6.2.12-5: Examples of current sensitivity selection standards

| Current sensitivity |  | Operating conditions |
| :---: | :---: | :---: |
|  | 15 mA | Place where the risk of an electric shock accident is very high (moistened place, etc.) Place where a human body needs to be protected even when touching any electrically live line. Movable or transportable grounding wire may be cut. However, when the ELCB has a large capacity, it may malfunction. <br> Unit installation work is difficult. ( 15 mA : Refer to Article 28 of the Electrical Equipment Technical Standards.) |
|  | 30 mA |  |
|  | 100 mA | Protection from an electric shock accident caused by earth leakage in a circuit where units are installed securely. <br> (For details about unit grounding resistance, refer to Table 6.2.12-8.) <br> Protection from fire caused by earth leakage <br> When the high sensitivity type ELCB is used, it malfunctions. |
|  | 200 mA |  |
|  | 500 mA |  |
|  | 1000 mA |  |
|  | 3000 mA |  |

## (2) Operation time and grounding resistance

According to Article 19 of the Electrical Equipment Technical Standards, the grounding resistance is relaxed as shown in "Table 6.2.12-6" when an earth leakage circuit breaker (ELCB) is connected. Additionally, when the grounding resistance of the grounding work for prevention of electric shock accident conforms to Table 6.2.12-8 and the operation time is 0.1 sec. or less (high-speed type), an ELCB with medium sensitivity can be used according to the relationship with allowable human body contact voltage (Table 6.2.12-7).

Table 6.2.12-6: Grounding and the grounding resistance of electrical equipment according to Electrical Equipment Technical Standards


Table 6.2.12-7: Allowable contact voltage

| (From low-voltage protective circuit guideline) |  |  | ELCB <br> current sensitivity [mA] | Grounding resistance [ $\Omega$ ] |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Class | Contact status | Allowable contact voltage |  | Moistened or other place | Other |
| Class 1 | Most part of human body is in the water. | 2.5 V or lower |  | with a high risk of an | places |
| Class 2 | Human body is moistened significantly. Metallic electric machine unit is always in contact with a part of human body from the structural aspect. | 25 V or lower |  | electric shock. |  |
|  |  |  | 30 | 500 | 500 |
|  |  |  | 50 | 500 | 500 |
| Class 3 | In cases other than classes 1 and 2 , the risk is high when the contact voltage is applied in the normal human body status. | 50 V or lower | 75 | 333 | 500 |
|  |  |  | 100 | 250 | 500 |
|  |  |  | 150 | 166 | 333 |
| Class 4 | In cases other than classes 1 and 2 , the risk is low even when the contact voltage is applied in the normal human body status. <br> There is no risk to apply any contact voltage. | No limit. | 200 | 125 | 250 |
|  |  |  | 300 | 83 | 166 |
|  |  |  | 500 | 50 | 100 |
|  |  |  | 1,000 | 25 | 50 |

## (3) Continuous leakage current

When an earth leakage circuit breaker (ELCB) is connected to the inverter input side, the inverter output side also becomes the protective area as illustrated in Figure 6.2.12-9.
Therefore, the high-frequency charging/discharging current that flows through the wiring on the inverter output side or static capacitance to the earth of the motor becomes the continuous leakage current. This may cause the ELCB to operate.


Figure 6.2.12-9: Leakage current transmission route
The level of the leakage current that flows the ELCB may vary depending on the power supply transformer (and also depending on the transformer grounding). The following summarizes the leakage current calculation methods.

Table 6.2.12-9: Grounding method and continuous leakage current

| Kind of system |  | Leakage current to the static capacitance to the earth (overview) |
| :---: | :---: | :---: |
|  |  | When the static capacitance to the earth of each phase of the electric circuit is balanced, the following Equation is established in the steady status ${\underset{C}{C}}_{\&}^{\&}{\underset{C R}{C}}_{\&}^{\mathcal{F}_{C S}^{\&}}+\mathcal{K}_{C T}^{\&}=0$ <br> and no leakage current flows. <br> Actually, the distribution line of each phase does not have the same conditions or the contacts become uneven when the switch is turned ON or OFF. This may cause the leakage current to flow through the static capacitance to the earth of a specific phase. <br> Therefore, the zero phase current of the leakage current that flows through the static capacitance to the earth for at least one phase needs to be taken into consideration. $I_{\Delta n} \geqq 10 \times 2 \pi f \times\left(C_{1}+C_{2}\right) \times V_{C} \quad \cdots \cdots \cdots \cdots \cdot . \text { Equation 6.2.12-1 }$ |
|  |  | The leakage current flows through the static capacitance to the earth of a phase other than the grounding phase. $\mathcal{A}_{C}^{\&}=\mathbb{F}_{C R}^{\&}+\&_{C T}^{k}$ <br> The vector of each leakage current is illustrated in the figure on the right. $I_{\Delta n} \geqq 10 \times \sqrt{3} \times 2 \pi f \times\left(C_{1}+C_{2}\right) \times V_{C} \quad \cdots \cdots \cdots \cdots \text { Equation 6.2.12-2 }$ |

Table 6.2.12-10


Figure 6.2.12-10: Leakage current model diagram

Leakage current (3- $\phi 200 \mathrm{VAC}, 60 \mathrm{~Hz}$ ) per km when the CV wires are used in wiring through the metal conduit pipes (tightly in contact with the grounding).

| Wire size <br> $\left[\mathrm{mm}^{2}\right]$ | Static capacitance <br> $[\mathrm{uF}]$ | Leakage current <br> $[\mathrm{mA}]$ |
| :---: | :---: | :---: |
| 5.5 | 0.250 | 33 |
| 8 | 0.276 | 36 |
| 14 | 0.341 | 45 |
| 22 | 0.353 | 46 |
| 38 | 0.450 | 59 |
| 60 | 0.457 | 60 |
| 100 | 0.444 | 57 |
| 150 | 0.531 | 68 |
| 200 | 0.496 | 65 |
| 250 | 0.547 | 71 |
| 315 | 0.616 | 80 |

As the rated current sensitivity is summarized as described above, it can be investigated and calculated from the contents. Actually, it is very difficult to calculate the leakage current according to the inverter or motor grounding method, or cables to be used, etc.
Therefore, Fuji Electric summarizes the relationship between the rated current sensitivity and wiring distance on the output side in Table 6.2.12-11 from the data based on the actual machine test with an inverter and a motor combined.

## (4) ELCB installation place

Install the ELCB on the converter input side (primary side: L1/R, L2/S, L3/T). Since the voltage and frequency on the converter output side or inverter output side (secondary side) do not meet the ELCB specifications, the ELCB does not operate correctly. (Do not use.) Normal operation may not be attained by installing an ELCB on the input side of each converter when more than one converter is connected in parallel to the same supply system. (Refer to Figure 6.2.12-11.)


Figure 6.2.12-11: ELCB installation place

## (5) Settings on the inverter side

An appropriate ELCB is selected under conditions that the inverter carrier frequency is 1 kHz or more and that the operation frequency is 60 Hz or less. When the carrier frequency is set to a level less than 1 kHz , it is greatly redundant by the fundamental current. So, the safety factor that is twice larger than the normal level should be used.

## (6) Applicable category of rated current sensitivity of ELCB

Table 6.2.12-11: Applicable category of rated current sensitivity of ELCB

| Power-based series | Standard application motor (kW) | Wiring distance/current sensitivity |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 10 m | 30 m | 50 m | 100 m | 200 m | 300 m |
| ৪̀ | 3.7 |  |  |  |  |  |  |
|  | 5.5 |  |  |  |  |  |  |
|  | 7.5 | 30 mA |  |  |  |  |  |
|  | 11 |  |  | 100 mA |  |  |  |
|  | 15 |  |  |  |  |  |  |
|  | 18.5 |  |  |  |  |  |  |
|  | 22 |  |  |  | 200 mA |  |  |
|  | 30 |  |  |  |  |  |  |
|  | 37 |  |  |  |  |  |  |
|  | 45 |  |  |  |  | 500 mA |  |
|  | 55 |  |  |  |  |  |  |
|  | 75 |  |  |  |  |  |  |
|  | 90 |  |  |  |  |  |  |
|  | 110 |  |  |  |  |  |  |
|  | 132 |  |  |  |  |  | 1000 mA |
|  | 160 |  |  |  |  |  |  |
|  | 200 |  |  |  |  |  |  |
|  | 220 |  |  |  |  |  |  |
|  | 250 |  |  |  |  |  |  |
|  | 280 |  |  |  |  |  |  |
|  | 315 |  |  |  |  |  |  |
|  | 355 |  |  |  |  |  | 3000 mA |
|  | 400 |  |  |  |  |  | (Special) |
|  | 450 |  |  |  |  |  |  |
|  | 500 |  |  |  |  |  |  |
|  | 630 |  |  |  |  |  |  |
|  | 710 |  |  |  |  |  |  |

Note (1) The list above is obtained when Fuji Electric's earth leakage circuit breaker or earth leakage relay applies to the test setup.
(2) The rated current of the standard application motor is the numeric values for Fuji Electric's standard motor (4-pole, $400 \mathrm{VAC}, 50 \mathrm{~Hz}$ ).
(3) The power supply grounding is calculated when the neutral point grounding is performed with 400 V class Y-connection.
(4) The values listed above are calculated based on the static capacitance to the earth when 3-core 600 V cross linked-polyethylene-insulated wire (CV wire) is used in a wiring through metal conduit pipes (tightly in contact with the grounding). When the wire has a static capacitance to the earth smaller than that of the CV wire, the wiring distance can be made longer in reverse proportion to the decrease ratio of the static capacitance to the earth.
(5) The values listed above are calculated with the metal conduit pipe wiring (tightly in contact with the grounding). When the static capacitance to the earth is small by separating the wire from the grounding, the wiring distance can be made longer.
(6) The wiring distance is the total distance from the inverter to the motor. Therefore, when multiple motors are connected to one inverter, the wiring length becomes the total wiring length.
$\lambda_{M}=\lambda_{1}+\lambda_{2}+\lambda_{3}+\lambda_{4}$
$\lambda_{M}$ : Total wiring length


## (7) Enhanced model for inverter

Fuji Electric's G-TWIN series earth leakage circuit breaker (ELCB) standard models are designed to be applied to inverter circuits. However, when the static capacitance to the earth is large due to the wiring length or noise filter, the leakage current becomes large and the ELCBs do not function correctly.
To suppress this unnecessary operation, an enhanced model for inverters is available that provides an earth leakage detection circuit improved in terms of frequency characteristics.
(In particular, a grounding capacitor with a large static capacitance is used for the noise filter.)
When placing an order, specify "-01065" at the end of the model.

The enhanced model for inverters can detect a ground fault on the secondary side of the inverter at an operation frequency of 120 Hz or less.
However, Fuji Electric's inverters are equipped with the ground fault detection and output phase loss protective functions.
Additionally, when using the Y -connection neutral point grounding method, the current sensitivity becomes dull in response to a ground fault on the secondary side of the inverter. For this reason, the protective grounding of the load (class C and D grounding) should be $10 \Omega$ or less.


Figure 6.2.12-12: Frequency characteristics of the enhanced model for inverters

Table 6.2.12-12: List of Fuji Electric's ELCB (G-TWIN series) models - extracted from G-TWIN Catalog (EH130 $\square$ )

| Series/Applications <br> Specifications |  |  | Standard |  |  |  | Global <br> Momentary fixing type for general wiring (2) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | For general wiring Momentary fixed type | For motor protection | With single-phase 3-wire neutral line open-phase protection (1) | For resistance welding machine |  |
| Frame <br> (A) | Basic name | Rated braking capactiy IculkA] AC230V/ AC440V (JIS) |  |  |  |  |  |
| 32 | EW32 | 2.5/. | EW32AAG |  |  |  |  |
|  |  | 2.5/1.5 | EW32EAG | EW32EAM |  |  |  |
|  |  | 5/2.5 | EW32SAG | EW32SÄM |  |  |  |
| 50 | EW50 | 2.5/. | EW50AAG |  |  |  |  |
|  |  | 5/2.5 | EW50EAG | EWSOEAM | EW50EAN |  |  |
|  |  | 10/7.5 | EW50SĀ̆ | EW50̈S̈ÄM |  |  |  |
|  |  | 25/10 | EW50RAG |  |  |  | EW50RAGU |
|  |  | 125/65 | EW5OHAG |  |  |  |  |
| 63 | EW63 | 5/2.5 | EW63EAG | EW63EAM |  |  |  |
|  |  | 10/7.5 | EW63SAG | EW63SAMM |  |  |  |
|  |  | 25/10 | EW63RAG |  |  |  |  |
| 100 | EW100 | 5/. | EW100AAG |  |  |  |  |
|  |  | 25/10 | EW100EAG | EW100EAM | EWW100EĀN |  | EWWióEAGÜ |
| 125 | EW125 | 50/30 | EW125JAG | EW125JAM |  |  | EW125JAGU |
|  |  | 100/50 | EW125RAG | EW125RAM |  |  | EW125RAGU |
|  |  | 125/65 | EW125HAG |  |  |  |  |
| 250 | EW250 | 36/18 | EW250EAG | EW250EAM | EW250EAN |  |  |
|  |  | 50/30 | EW250JAG | EW250JAM |  |  | EW250JAGU |
|  |  | 100/50 | EW250RAG | EW250RAM |  | EW250RAW | EW250RAGU |
|  |  | 125/65 | EW250HAG |  | EW400EAIN |  |  |
| 400 | EW400 | 50/30 | EW400EAG |  |  |  | EW400SAGU |
|  |  | 85/36 | EW400SAG |  |  | EW400RAW | EW400AAGU |
|  |  | 100/50 | EW400RAG |  |  |  | EW400HAGU |
|  |  | 125/70 | EW400HAG |  |  |  |  |
| 630 | EW630 | 50/36 | EW630EAG |  |  |  | EW630RAGU |
|  |  | 100/50 | EW630RAG |  |  |  |  |
|  |  | 125/70 | EW630HAG |  |  |  |  |
| 800 | EW800 | 50/36 | EW800EAG |  |  |  |  |
|  |  | 100/50 | EW800RAG |  |  |  |  |
|  |  | 125/70 | EW800HAG |  |  |  |  |

(Note 1) The product is dedicated to the single-phase 3-wire circuit. Icu at 100 VAC/ 200 VAC becomes as follows. EW50EAN: 50 kA, BW100EAN: 25 kA ,
BW250EAN: 35 kA , EW400EAN: 50 kA
(Note 2) For details about UL ratings, refer to the list of specifications (page 34).
Table 6.2.12-13: List of Fuij Electric's ELCB (G-TWIN series) current sensitivities

| Specifications | Rated current sensitivity $[\mathrm{mA}]$ |
| :--- | :--- |
| High-speed type | 15 |
|  | 30 |
|  | 50 (EW50RAG-3P and EW100EAGU-3P only) |
|  | 100 |
|  | $100 / 200$ or 100/200/500 setting can be switched. |
| Time delay type | $100 / 200 / 500$ setting can be switched. (EW100EA D only) |
| High-speed/time <br> delay type | $100 / 200 / 500 / 1000$ setting can be switched. |

Some models provide the ability to switch different current sensitivity and operating time settings although available only in particular frame sizes.

## [1] Refer to the G-TWIN Catalog

(EH130■).

## (8) Ground fault protection coordination

As the period of time from detection of a ground fault to the operation of the ELCB is shorter, the earth leakage protection characteristics become more excellent. However, it is necessary to consider the ground fault protection coordination in the same manner as the selective tripping coordination for the overcurrent protection.
The ground fault protection coordination performs the selective tripping coordination between the upstream (power supply side) and downstream (load side) ground fault protection devices. If a ground fault accident occurs on the downstream side, only this ground fault device is tripped and the upstream ELCBs do not operate.
For example, even though ELCB-1 and ELCB-2 with different rated current sensitivity and the same operation time are used as illustrated in" Figure 6.2.12-13", both ELCBs may operate if a ground fault accident exceeding 500 mA occurs.
(Shaded portion $\square$ in the figure.)
When a model with a slow operation time (time delay type) is applied to the upstream ELCB-1, the coordination can be established. Therefore, the ground fault protection coordination needs a combination of ELCBs with not only different rated current sensitivity, but also different operation time.


Figure 6．2．12－13：Ground fault protection coordination of earth leakage circuit breaker（ELCB）
（9）Model applicable to different voltage
Fuji Electric＇s standard earth leakage circuit breaker can be used for a circuit with a voltage of up to 440 V ．If the circuit voltage exceeds this level，use a special voltage earth leakage circuit breaker．When placing an order，specify＂－C5＂at the end of the model．

Table 6．2．12－14：Fuji Electric＇s ELCB（G－TWIN series）models applicable to different voltage－extracted from G－TWIN Catalog（EH130 $\square$ ）

| Model |  |  | EWI25JMG | EW125RAG | EW250EAG | EW250，4G | EW250P4G | EW400EAG | EW400SAG | EW400PAG | EW400HAG | EVESOEAG | EmbSorat | EW630HAG | Embooeag | Ewboopag | EW800HAG |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of poles |  |  | 3P．4P | 3P，4P | 3P | 3P．4P | 3P，4P | 3 P | 3 P | 3P，4P | 3P，4P | 3 P | 3 P | 3 P | 3 P | 3P | 3 P |
| Rated operation AC voltage（V） |  |  | 380.500 |  | 230－500 |  |  | 230－500 |  |  |  | 230．500 |  |  | 230．500 |  |  |
| Operable AC voltage range（V） |  |  | 160－550 |  | 160.550 |  |  | 160．550 |  |  |  | 160－550 |  |  | 160.550 |  |  |
| Rated impulse withstand voltage Ulimp（V） |  |  | 6 |  | 6 |  |  | 6 |  |  |  | 6 |  |  | 6 |  |  |
| Rated current lo（A） |  |  | $\begin{aligned} & 15.20,30,40,50, \\ & 60.75,100,125 \end{aligned}$ |  | $\begin{aligned} & 125,150,160,175, \\ & 200,225,250 \end{aligned}$ |  |  | 250，300，350，400 |  |  |  | 500，600，630 |  |  | 700，800 |  |  |
| Rated frequency（Hz） |  |  | 50．60 |  | 50－60 |  |  | 50．60 |  |  |  | 50.60 |  |  | 50.60 |  |  |
| Rated current sensitivity（mA） |  |  | 30，100／200／500／1000切笪 |  | 30．100／200／500／1000切格 |  |  | 30，100／200／500／1000ヶヶ澘 |  |  |  | 100／200／500／1000切贸 |  |  | 100／200／500／1000切蟑 |  |  |
| Ratedbrakingcapacity （kA） | IEC60947．2 <br> JIS C8201－2－2 <br> Ann1 2 <br> lcu／los | AC500V | 8／4 | 10／5 | 5／3 | 8／4 | 10／5 | 18／9 | 20／10 | 36／18 | 42／21 | 20／10 | 36／18 | 42／21 | 20／10 | 36／18 | 42／21 |
|  |  | AC440V | 30／15 | 50／25 | 18／9 | 30／15 | 50／25 | 30／15 | 36／18 | 50／25 | 70／35 | 36／18 | 50／25 | 70／35 | 36／18 | 50／25 | 70／35 |
|  |  | AC380V | 30／15 | 50／25 | 18／9 | 30／15 | 50／25 | 30／15 | 36／18 | 50／25 | 70／35 | 36／18 | 50／25 | 70／35 | 36／18 | 50／25 | 70／35 |
|  |  | AC230V | － | － | 36／18 | 50／25 | 100／50 | 50／25 | 85／43 | 100／50 | 125／63 | 50／25 | 100／50 | 125／63 | 50／25 | 100／50 | 125／63 |


| Model |  |  | EW125JAGU | EW125RAGU | EW250JAGU | EW250RAGU | EW400SAGU | EW400RAGU | EW400HAGU |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number of poles |  |  | 3P | 3 P | 3P | 3P | 3 P | 3P | 3P |
| Rated operation voltage |  | IEC | 380－500 |  | 230－500 |  | 230．500 |  |  |
|  |  | UL | 240－480 |  | 240－480 |  | $240-480$ |  |  |
| Operable AC voltage range |  |  | 160.550 |  | 160．550 |  | 160.550 |  |  |
| Rated impulse withstand voltage Uimp（kV） |  |  | 6 |  | 6 |  | 6 |  |  |
| Rated current lo（A） |  |  | 15，20，30，40，50，60，75，100，125 |  | 125，150，160，175．200，225，250 |  | 250，300，350．400 |  |  |
| Rated frequency（Hz） |  |  | 50．60 |  | 50．60 |  | 50．60 |  |  |
| Rated current sensitivity（mA） |  |  | 30．100／200／500／1000切新 |  | 30，100／200／500／1000切復 |  | 30．100／200／500／1000切楼 |  |  |
| Rated braking （kA） | IEC60947－2 JIS C8201－2－2 Ann1 2 low／lcs | AC500V | 15／8 | 36／18 | 18／9 | 36／18 | 20／10 | 36／18 | 42／21 |
|  |  | AC440V | 30／15 | 50／25 | 30／15 | 50／25 | 36／18 | 50／25 | 70／35 |
|  |  | AC380V | 30／15 | 50／25 | 30／15 | 50／25 | 36／18 | 50／25 | 70／35 |
|  |  | AC230V | － | － | 50／25 | 100／50 | 85／43 | 100／50 | 125／63 |
|  | $\begin{array}{\|l\|} \hline \text { UL.489 } \\ \text { CAN } / \text { CSA C22.2 No. } 5 \\ \hline \end{array}$ | 480 V | 30 | 50 | 30 | 50 | 35 | 50 | 65 |
|  |  | 240 V | 50 | 100 | 50 | 100 | 50 | 100 | 100 |

### 6.2.12.5 Use of electromagnetic contactor for power supply circuit

An electromagnetic contactor (MC) to be installed on the input side of the converter is used for the purposes shown below.

- The inverter is separated from the power supply by operation of the converter or inverter protective function or external signal
- The stop command cannot be input due to circuit trouble and the emergency stop needs to be activated.
- The inverter needs to be separated from the power supply if molded case circuit breaker (MCCB) connected to the power supply side cannot be turned OFF when starting the maintenance and inspection work of the inverter. (In this case, it is recommended to add an interlock mechanism, such as manual switch to the operation circuit of the MC.)

Note Do not turn ON or OFF the electromagnetic contactor on the input side (primary side) frequently. Doing so may cause an inverter failure (faulty wiring may occur in the charging circuit). When it is necessary to frequently turn ON or OFF the electromagnetic contactor, do not exceed the frequency of once per 30 minutes. To maintain an inverter service life of 10 years or longer, turn ON or OFF the electromagnetic contactor once per hour.
If it is required to start or stop the operation frequently, perform this operation using the "FWD" or "REV" signal


| Voltage | Nominal applied motor capacity [kW] | Diode rectifier model | Specifications | MCCB, ELCB | MC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 400 V | 200 | RHD200S-4D $\square$ | MD | 500AT | SC-N12 |
|  | 315 | RHD315S-4D $\square$ |  | 700AT | SC-N14 |
|  | 220 | RHD200S-4D $\square$ | LD | 500AT | SC-N12 |
|  | 355 | RHD315S-4D $\square$ |  | 800AT | SC-N14 |
| 690 V | 220 | RHD220S-69D $\square$ | MD | 300AT | SC-N11 |
|  | 450 | RHD450S-69D $\square$ |  | 600AT | SC-N14 |
|  | 250 | RHD220S-69D $\square$ | LD | 350AT | SC-N11 |

Note (1) Install the MCCB or ELCB on the input side of the converter.
(2) This table selects an appropriate MCCB or ELCB under conditions that the temperature inside the cabinet is $50^{\circ} \mathrm{C}$ or less. Select installation environment conditions by considering the correction coefficient $(0.85$ to 0.93 ) according to the ambient temperature conditions. To select a specific model, consider the short-circuit breaking capacity of the equipment.
(3) When selecting an electromagnetic contactor (MC), it is assumed that the wire type to be connected is HIV wire (allowable temperature is $75^{\circ} \mathrm{C}$ ). When using other wires, select an electromagnetic contactor (MC) again by considering the terminal block size and wire size.
(4) To prevent any consequential accident if the converter is broken, use an appropriate MCCB or ELCB with the rated current shown in the table above.
Do not use any MCCB or ELCB with a rated current larger than the required level.

### 6.2.12.7 Use of earth leakage detector (earth leakage relay)

This section describes an earth leakage relay that eliminates the breaking performance of the earth leakage circuit breaker and contains an earth leakage detection function.
The following shows recommended earth leakage relays (Fuji Electric).


| RRD |
| :--- | :--- |
| type | | This earth leakage relay has the same frequency characteristics of the |
| :--- |
| leakage current as the standard type of Fuji Electric's ELCB. |
| There are two types of ZCTs available: the through type and the bus bar |
| integrated type. An earth leakage of up to approx. 3000 A can be detected. |
| Additionally, the high-speed type and the time delay type are also provided. |
| Rated current sensitivitySwitching is possible. (100/200 mA, 200/500 <br> mA, $500 / 1000 \mathrm{~mA})$ |
| Rated non-operation current : Rated current sensitivity x $50 \%$ or switching is |
| possible. |



Figure 6.2.12-14: Basic circuit configuration diagram

Note (1) For details about specifications, refer to Fuji Electric's earth leakage relay catalog.
(2) Place the main unit 10 cm or more far from the power system (particularly, large current system) equipment or wires. If the main unit is put close to such equipment, the external magnetic field may adversely affect it.
(3) When necessary, pass or connect the neutral wires in the circuit. However, do not pass or connect the class C or D grounding wire.
(4) The signal cable between the relay and ZCT [Z1 and Z2 terminals] should be a twist pair cable with a cross-sectional area of 0.3 to $2 \mathrm{~mm}^{2}$ and its length is 10 m or less.
(5) Make the wiring of the signal cable 10 cm or more far from other power cables [control power supply and test circuit (T1 and T2 terminals), etc.].

### 6.2.12.8 Power supply transformer (power receiving transformer)

When specifying a power supply transformer capacity on the input side, required power supply capacity of the converter (diode rectifier or PWM converter) and voltage drop when the power is turned ON should be taken into consideration.

## (1) Transformer capacity

The following shows a simple calculation method to calculate the transformer capacity from the required power supply capacity of the converter. However, when determining the transformer capacity, the calculated value should be multiplied by the safety ratio. Additionally, when the power supply to the control circuit is supplied from this transformer, the power supply capacity of the control circuit should be also added.


Figure 6.2.12-15: Circuit configuration

## (2) Voltage drop

When the wiring distance to the load is short like transformer to be installed inside the cabinet, the voltage drop can be calculated simply from the percent impedance of the transformer.

When the power is turned ON, the charging (rush) current flows into the smoothing capacitor of the converter and the voltage largely drops in the transient status.
However, for this voltage drop, an initial charging circuit is normally provided in the converter to suppress the rush current. Additionally, this rush current is set to a level that is the rated current of the inverter or less.
When large capacity equipment is installed in the converter, inverter, or other AC power supply system, the voltage drop must be taken into consideration when selecting a transformer.

$$
\begin{array}{llll}
\Delta V=\% Z_{t} \times \frac{n \times P_{1}}{P_{T}}[\%] \cdots & \text { Equation 6.2.12-5 } & \Delta \mathrm{V} & \text { : Voltage drop in transient status [V] } \\
& & \% \mathrm{Z}_{\top} & : \text { Percent impedance of transformer [\%] } \\
& & \mathrm{n}^{2} & \text { : Current magnification in transient status } \\
& & \mathrm{P}_{1} & \text { : Required power supply capacity of inverter [kVA] } \\
& & \mathrm{P}_{\mathrm{T}} & \text { : Capacity of transformer to be used [kVA] }
\end{array}
$$

The current magnification $(\mathrm{n})$ in the transient status is set to a value 4 times larger than the inverter input current I . Actually, the current magnification may become 20 times larger than the inverter input current I1. However, since this symptom occurs within a short time (several ms), there are normally no problems.

This transient voltage drop that occurs when the power is turned ON does not adversely affect the inverter itself, but it affects the unit connected to the same power supply transformer as the inverter. To avoid the effects on such units, the following relationship must be satisfied.

Allowable lower limit voltage of unit $[\mathrm{V}]<\mathrm{Vn} \cdots$ Equation 6.2.12-6 • Vn: Transformer output voltage in transient

$$
V n<V o \times \frac{1-\Delta V}{100}[V] \cdots
$$

status [V]
Equation 6.2.12-7 • Vo: Transformer voltage in no-load status [V]

If this $\% Z_{T}$ is pointed out as a problem, this is solved when the $\%_{T}$ is made larger than the calculated transformer capacity value. Additionally, a transformer with $\% Z_{\text {T }}$ specified is prepared to solve the problem, but this transformer may become a special product.

The $\% Z_{T}$ of the general transformer has the trend shown below.

- $\% Z_{T}$ is small in the oil transformer.
- $\% Z_{T}$ is large in the molded transformer.

When the transformer is commonly used by other power load, select an appropriate transformer by considering the operating conditions, such as system impedance and load.
If the power supply voltage decreases to a level lower than the allowable lower limit voltage of the inverter, the inverter does not operate correctly and the protective function may operate. In particular, when starting a large capacity motor, a large voltage drop occurs by the start current.


Figure 6.2.12-16: Secondary fluctuation of transformer

## (3) Other items

1) In the V-connection transformer, since the inter-phase balance of the power supply impedance is not balanced when viewed from the converter, the unbalance of the input current of each phase becomes large. So, use a 3-phase transformer for the power supply transformer.
2) When a three-winding transformer with a phase difference between the secondary (delta connection) and tertiary (star connection) windings is used to drive multiple inverters, the harmonic current on the primary side is reduced. Note that the harmonic current of the secondary and tertiary windings is not reduced. To reduce the second and tertiary harmonic currents, connect the DC reactor (DCR).
(This reduces the harmonic current close to the fundamental wave current components.)
3) To ensure the safety and prevent noise propagation, use a two-winding type or three-winding type transformer with the grounding terminal. When noise resistance or surge resistance is required, use a static shield type transformer.
<Reference: Fuji Electric's molded transformer: Extracted from catalog TC76-7V.>

<Reference: Fuji Electric's molded transformer: Extracted from catalog TC76-7V.>

| $\square$ Model (Series) | KT-CT type KS-CS type KF-CF type CH-EH type LC type |
| :---: | :---: |
| $\square$ Heat resistant class | Standard Class B Class F Class H |
| - Number of phases | Single-phase 3-phase Scott connection |
| - Frequency (Hz) | 5060 50/60 |
| - Rated capacity (kVA) |  |
| - Primary voltage | 21042033006600110002200033000 |
|  | Standard $\pm$ 2.5, 5.0\% tap |
|  | Standard $1 . \triangle$ |
| ■Secondary voltage V | R210-105 210420 ( 50 Hz ) 440 (60 Hz) 33006600 |
|  | Standard ^ ¢¢(With neutral point) $\triangle$ Delta connection Delta transformer |
| $\square$ Cooling | Standard Natural cooling Wind cooling |
| - Wheels | Provided None |
| $\square$ Accessories (options) | Contact prevention plate Dial thermometer Protective case |
| $\square$ Order quantity |  |
| $\square$ Desired delivery time |  |
| Other remarks |  |
| Operating environment | The operating environment conforms to the following normal conditions defined in JEC-2200. <br> If the operating environment is other than that shown below, specify it separately. |

Describe desired specifications or enclose a desired specification by a circle in the table. $\square$ shows absolutely required items.
Note: The guarantee of this product covers only the purchased product and delivered single product. Consequential damages (damages or losses of machine and equipment and losses of profits) resulting from the malfunction are expected from the guarantee.
<Reference: Fuji Electric's oil transformer: Extracted from catalog TC77g.>
Standard specification series products


Note 1) Transformer with specifications other than those described above can also be manufactured. Contact Fuji Electric separately. 2) Tap-less transformer is also manufactured.

### 6.2.12.9 Receiving power supply monitor

(1) Transformer for instrument (VT)

- Converter stack input side

General VT for $50 / 60 \mathrm{~Hz}$ can be used.

## Inverter output side

The output voltage waveform of the inverter is a square wave (rectangular wave).
The output waveform on the secondary side of the transformer for instrument (VT) is a pulse shape distorted waveform. The voltage cannot be measured correctly and the iron core of the VT is saturated magnetically, possibly causing burning. Additionally, when the inverter is operated at a low speed, the frequency becomes low and the voltage becomes close to the DC voltage. In this case, the VT may be burnt.

Therefore, the VT should not be connected to the output side of the inverter.

Table 6.2.12-16: Fuji Electric's coil molded transformer

| Model | CD32 $\square-\mathrm{O} 1$ | CD34 $\square-\mathrm{O} 1$ | CD36口-O1 |
| :--- | :---: | :---: | :---: |
| Rating | $220 / 110 \mathrm{~V}, 440 / 110 \mathrm{~V}$ |  |  |
| Rated load | 15 VA | 50 VA | 100 VA |
| Accuracy class | $1.0 \cdot 1 \mathrm{P}$ | $3.0 \cdot 3 \mathrm{P}$ | $1.0 \cdot 1 \mathrm{P}$ |
| Rated frequency | $50 / 60 \mathrm{~Hz}$ |  |  |
| Withstand voltage | 220 V product: $2 \mathrm{kV}, 440 \mathrm{~V}$ product: 4 kV |  |  |

$\square: F$ (Primary side with fuse), N (without fuse)
O: 2 or 4 (Rated primary voltage specifications)

## (2) Current transformer for instrument (CT)

## - Converter stack input side

General CT for $50 / 60 \mathrm{~Hz}$ can be used. However, since harmonic components are included, a larger rated load is taken.

## - Inverter output side

As a current including a large amount of high frequency and harmonic components may flow, the iron core loss increases. An allowance 10 times larger than the rated load should be given.

CT rated load [VA] $\geq 10 \times$ (rated load of instrument + wire load) [VA]
The wire load should be calculated from Figure 6.2.12-17.

$$
P \lambda=r \times \lambda \times \frac{I}{1000}[V A] \cdots \cdots \cdots \cdots \quad \text { Equation 6.2.12-8 }
$$

$P \lambda$ : Wire load [VA]
$r \quad:$ Resistance value of wire $[\Omega / \mathrm{km}]$
$\lambda$ : Wiring distance of wire (round trip distance) $[\mathrm{m}]$
I : Rated secondary current of CT [A]
Note Do not open the secondary side of the CT.
If the secondary side is open while the primary current flows, a high voltage is produced to flow the secondary current according to the CT ratio.
Therefore, the insulation of the secondary winding is broken to produce a short-circuit, possibly resulting in burning.


Figure 6.2.12-17: Wire load of circuit

Table 6.2.12-17: Fuji Electric's molded current transformer

| Product name | Round window through type |  |  | With primary winding |  |  | Square window through type |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model | CC3L1 | CC3L2 | CC3L3 | CC3P1 | CC3P2 | CC3P3 | CC3M2 | CC3M3 |
| Rated primary current | 10 to 750 A |  |  | 5 to 50 A |  |  | 150 to 750 A 200 to $6,000 \mathrm{~A}$ |  |
| Rated secondary current | 5 A or 1 A |  |  |  |  |  |  |  |
| Rated load | 5 VA | 15 VA | 40 VA | 5 VA | 15 VA | 40 VA | 15 VA | 40 VA |
| Rated overcurrent strength | 40 |  |  |  |  |  |  |  |
| Max. voltage | 1,150 V |  |  |  |  |  |  |  |
| Error class | 1.0 class |  |  |  |  |  |  |  |
| Rated frequency | $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |
| Insulation method | Double-molding (*1) |  |  |  |  |  |  |  |

(*1) Epoxy molding is used to insulate a rated primary current of 5,000 or $6,000 \mathrm{~A}$.

## (3) Voltmeter

## ■ Converter input side

The waveform is distorted by the effect of the harmonic. However, since the commercial power supply is measured, "a moving-iron type" or "rectifier type voltmeter" should be used.

## - Inverter output side

The output voltage including high-frequency components is measured. "A rectifier type voltmeter" should be used that indicates a value close to the r.m.s. value of the fundamental wave.

## (4) Ammeter

## Converter input side

Since the harmonic current with a high peak value called "rabbit's ear" is measured, "a moving-iron type" or "r.m.s. value response type (RMS type)" should be used that indicates the general r.m.s. value including harmonic components.

## Inverter output side

A current with the harmonic components superimposed on the fundamental wave current is measured. The current cannot be measured accurately in all frequency areas. The following models can be used conditionally.
Area of 20 Hz or more: Moving-iron type, rectifier type, r.m.s. value rectifier type,

> : R.m.s. value response type (RMS type)

## (5) Frequency meter and wattmeter (watt-hour meter)

## Inverter output side

 General purpose analog output terminal of the inverter should be used.As a value ranging from 0 to $10 \mathrm{VDC}(4-20 \mathrm{~mA} \mathrm{DC})$ is output, a meter with the scale plate used for the DC voltmeter should be used.

Fuji Electric Technica's analog meter

- Panel meter

| Product name | Model | Operation principle | Inverter |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Primary side | Secondary side |
| AC ammeter | FS- $\square$ type | Moving-core type | $\bigcirc$ | $\begin{aligned} & \triangle \text { (Note) } \\ & 1,2 \\ & \hline \end{aligned}$ |
| AC voltmeter | FS- $\square$ type | Moving-core type | $\bigcirc$ | $\times$ |
| AC ammeter | FR- $\square$ type | Rectifier type | $\times$ | $\triangle$ (Note) 1 |
| AC voltmeter | FR- $\square$ type | Rectifier type | $\bigcirc$ | $\times$ |
| Single-phase wattmeter | FR- $\square$ W1 type | Converter type | O | $\times$ |
| Single-phase 3-wire wattmeter | FR- $\square$ W2 type | Converter type | O | $\times$ |
| 3-phase wattmeter | FR- $\square$ W3 type | Converter type | $\bigcirc$ | $\times$ |
| 3-phase reactive power meter | FR- $\square$ V3 type | Converter type | O | $\times$ |
| 3-phase balanced power factor meter | FR- $\square$ FP3 type | Converter type | $\times$ | $\times$ |
| 3-phase unbalanced power factor meter | FR- $\square$ PFU type | Converter type | $\times$ | $\times$ |
| Frequency meter | FR- $\square$ F type | Converter type | $\bigcirc$ | $\times$ |




Figure 6.2.12-18: Current waveform

| Product name | Model | Operation principle | Inverter |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Primary side | Secondary side |
| AC ammeter | SWR- $\square$ type | RMS value rectifier type | $\times$ | $\triangle$ (Note) 1 |
| AC voltmeter | SWR- $\square$ type | RMS value rectifier type | O | $\times$ |
| AC ammeter | SWRA- $\square$ type | RMS value response type | O | $\triangle$ (Note) 1 |
| AC voltmeter | SWRA- $\square$ type | RMS value response type | O | $\times$ |
| Single-phase wattmeter | SWC- $\square$ type | Converter type | $\bigcirc$ | $\times$ |
| Single-phase 3-wire wattmeter | SWC1- $\square$ type | Converter type | $\bigcirc$ | $\times$ |
| 3-phase wattmeter | SWC2- $\square$ type | Converter type | $\bigcirc$ | $\times$ |
| 3-phase 4-wire wattmeter | SWC3- $\square$ type | Converter type | O | $\times$ |
| 3-phase reactive power meter | SWC2- $\square$ type | Converter type | O | $\times$ |
| 3-phase 4-wire reactive power meter | SWC3- $\square$ type | Converter type | O | $\times$ |
| 3-phase balanced power factor meter | SWA1- $\square$ type | Converter type | $\times$ | $\times$ |
| 3-phase unbalanced power factor meter | SWA2- $\square$ type | Converter type | $\times$ | $\times$ |
| 3-phase 4-wire power factor meter | SWA4- $\square$ type | Converter type | $\times$ | $\times$ |
| Frequency meter | SWP1- $\square$ type | Converter type | 0 | $\times$ |

## Note Carefully check the following on the inverter output side.

(1) When the operation frequency is less than 20 Hz , the indication may fluctuate.
(2) When the inverter is operated at a carrier frequency of 5 kHz or more, overcurrent loss produced in the metallic part inside the moving-iron type instrument increases, possibly causing burning.
(3) When monitoring in a low speed area, it is recommended to use the analog output of the inverter stack.

## (6) Multi-meter

The following introduces multi-meters that monitor the electric power in the input power supply system of the converter. Two kinds of multi-meters are recommended as multi-meters to be mounted in the cabinet. Investigate an appropriate multi-meter suitable for the purpose.

## PPMC $\square \square \square \square$ - $\square$ (Fuji Electric)



## Features

- This multi-meter is compact and lightweight with front panel dimensions of $48 \times 96 \mathrm{~mm}$ and easy to install on individual equipment or power distribution panel.
- The current input signal is intended for the general purpose CT (secondary side, $1 \mathrm{~A}, 5 \mathrm{~A}$ ). An appropriate selection suitable for the application can be made.
- The RS485 interface can be built-in. Communication/function software: Dedicated data collection software is available.
- Data for an extended period of time can be recorded into a SD card. The data stored in the SD card can be loaded onto the personal computer and can be edited using Excel.

UM03-ARA3 $\square$ (F-MPC04S series products: Fuji Electric FA Components \& Systems)


## Features

- This multi-meter is compact and lightweight with front panel dimensions of $48 \times 96 \mathrm{~mm}$ and easy to install on individual equipment or power distribution panel.
- Dedicated CT is used. When monitoring a large capacity, this can be made in a combination with general purpose CT.
- The RS-485 is built-in as standard function. The same communication cable as the F-MPC series product can be used.
- A wide variety of output functions suitable for preventive maintenance can be selected.

Power alarm/current pre-alarm output (provided as standard), electric energy pulse signal (provided as standard), earth leakage alarm, earth leakage pre-alarm output (model with leakage current measurement function only)

- The rush current of the welding machine, etc. can be measured.

All cycles of the voltage and current are sampled at a high speed to perform the calculation.
Monitor measurable items

| Measurement contents | PPMC | UM03 |  |
| :--- | :--- | :--- | :--- |
| Voltage | $\bigcirc$ | $O$ |  |
| Current | $\bigcirc$ | $O$ | Remarks |
| Harmonic current | $\times$ | $O^{* 1}$ |  |
| Leakage current | $\times$ | $O^{* 2}$ |  |
| Active power | $\bigcirc$ | $O$ |  |
| Reactive power | $\bigcirc$ | $O$ |  |
| Power factor | $\bigcirc$ | $O$ |  |
| Electric energy | $O$ | $O$ |  |
| Reactive energy | $O$ | $O$ |  |
| Frequency | $O$ | $O$ |  |

*1 The total harmonic current of only R/T phase can be measured. The total of 3rd, 5th, and 7th harmonic currents is measured.
*2. The measurement is possible only when the model is specified.
[1] For details, refer to relevant catalog or technical reference.

### 6.2.13 Recommended wire size

The wire size of the main circuit is calculated based on the Equation below.
$I_{A C}=\frac{P_{M}}{\sqrt{3} \times \operatorname{Vin} \times \cos \vartheta \times \eta_{C N V} \times \eta_{I N V} \times \eta_{M}}$
[A] $\cdots$ Equation 6.2.13-1
$I_{D C}=\sqrt{\frac{3}{2}} \times I_{A C}[A]$
Equation 6.2.13-2

Note The structure from the converter output to the DC bus bar should be designed to cover it with the bus bar.

Additionally, when using the wire, the wiring length must be $\underline{\mathbf{2} \mathbf{m}}$ or less.

- IAC : Converter input current [A]
- IDC : Converter output current [A]
- Pm : Motor capacity [kW]
- Vin : Converter input voltage [A]
- $\cos \theta$ : Input power factor
- $\eta$ cnv : Converter efficiency
- $\eta \mathrm{inv}$ : Inverter efficiency
- $\eta \mathrm{M}$ : Motor efficiency


### 6.2.13.1 3-phase 400V series

(1) Ambient temperature: $40^{\circ} \mathrm{C}$

| Nominal applied motor capacity [kW] | RHD $\square$-4D $\square$ | Specifications | Main input: L1/R, L2/S, L3/T |  |  |  |  | Output: P(+), N(-) |  |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Control wire $\left[\mathrm{mm}^{2}\right]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Wire size (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] |  | Wire size (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{0}} \\ & \stackrel{D}{0} \\ & \frac{0}{3} \\ & 0 \end{aligned}$ |  |  |
|  |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 200 | 200S |  | 200 | 150 | 100 | t5x30 | 357 | 250 | 200 | 150 | t4x40 | 421 | 38 | 1.25 |
| 315 | 315S |  | 2x200 | 250 | 200 | t10x30 | 559 | 2x250 | 325 | 250 | t8x50 | 654 | 60 |  |
| 220 | 200S |  | 250 | 150 | 150 | t5x30 | 390 | 325 | 200 | 150 | t4x40 | 458 | 60 | 1.25 |
| 355 | 315S |  | 2x200 | 325 | 250 | t10x30 | 628 | 2x325 | 2x200 | 325 | t8x50 | 741 | 100 |  |

(2) Ambient temperature: $50^{\circ} \mathrm{C}$

| Nominal applied motor capacity [kW] | RHD $\square$-4D $\square$ | Specifications | Main input: L1/R, L2/S, L3/T |  |  |  |  | Output: P(+), N(-) |  |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Control wire [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Wire size (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | $\begin{aligned} & \stackrel{\rightharpoonup}{\omega} \\ & \stackrel{y}{\omega} \\ & \hline \end{aligned}$ | Wire size (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | $\begin{aligned} & \stackrel{\rightharpoonup}{\omega} \\ & \stackrel{\delta}{0} \\ & \stackrel{0}{0} \end{aligned}$ |  |  |
|  |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 200 | 200S |  | 325 | 150 | 150 | t5x30 | 357 | 2x200 | 250 | 150 | t4x40 | 421 | 38 | 1.25 |
| 315 | 315S |  | - | 325 | 250 | t10x30 | 559 | - | 2x200 | 325 | t8x50 | 654 | 60 |  |
| 220 | 200S |  | 2x200 | 200 | 150 | t5x30 | 390 | 2x250 | 250 | 200 | t4x40 | 458 | 38 | 1.25 |
| 355 | 315S |  | 2x325 | 2x200 | 250 | t10x30 | 628 | - | 2x250 | 2x200 | t8x50 | 741 | 60 |  |

The power supply voltage is 400 VAC.
(Note 1) An "IV wire," a " 600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.
(Note 2) The grounding wire is cited from the permissible short circuit current defined in internal wire regulations.

### 6.2.13.2 3-phase 690V series

(1) Ambient temperature: $40^{\circ} \mathrm{C}$ (IEC standard)

| Nominal applied motor capacity [kW] | $\left\lvert\, \begin{gathered} \text { RHD } \square \\ -69 D \square \end{gathered}\right.$ | Specifications | Main input: L1/R, L2/S, L3/T |  |  |  | Output: P(+), N(-) |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] | $\left[\begin{array}{c} \text { Control } \\ \text { wire } \\ {\left[\mathrm{mm}^{2}\right]} \end{array}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Wire size (Permissible temperature) (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] |  | Wire size (Permissible temperature) (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] |  |  |  |
|  |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $70^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 220 | 220 S | MD | 120 | 95 | t5x30 | 226 | 150 | 120 | t4x40 | 277 | 22 | 1.25 |
| 450 | 450S |  | 2x150 | 2×120 | t10x30 | 460 | 2x240 | 2×150 | t8x50 | 561 | 38 |  |
| 250 | 220 S | LD | 150 | 95 | t5x30 | 258 | 185 | 150 | t4x40 | 315 | 60 |  |

The power supply voltage is 690 VAC.
(Note 1) A "PVC (polyvinyl chloride) wire" and an "XLPE (cross-linked polyethylene) wire" were used at permissible temperatures of $70^{\circ} \mathrm{C}$ and $90^{\circ} \mathrm{C}$, respectively, and the wire sizes were selected based on the permissible current under the following conditions. If the use conditions are different, select the wire sizes based on use conditions that comply with IEC 60364-5-52:2001(JIS C 60364-5-52:2006).
Ambient temperature: $40^{\circ} \mathrm{C}$, Multicore cable: 3 cores (conductor: copper), A single cable: aerial wiring, Two or more cables: electric duct wiring
(Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

## (2) Ambient temperature: $40^{\circ} \mathrm{C}$ (domestic selection)

| Nominal applied motor capacity [kW] | $\begin{aligned} & \text { RHD } \square \\ & -69 D \square \end{aligned}$ | Specifi cations | Main input: L1/R, L2/S, L3/T |  |  |  | Output: P(+), N(-) |  |  |  | Grounding wire [mm²] | Control wire [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Wire size (Permissible temperature) (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{\omega}} \\ & \stackrel{y y}{心} \\ & 0 \\ & \hline \end{aligned}$ | Wire size (Permissible temperature) (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] |  |  |  |
|  |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 220 | 220S | MD | 60 | 60 | t5x30 | 226 | 100 | 60 | t4x40 | 277 | 22 | 1.25 |
| 450 | 450S |  | 200 | 150 | t10x30 | 460 | 200 | 150 | t8x50 | 561 | 60 |  |
| 250 | 220S | LD | 100 | 60 | t5x30 | 258 | 100 | 100 | t4x40 | 315 | 38 |  |

The power supply voltage is 690 VAC.
(Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
(Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

### 6.3 High-efficiency power regeneration PWM converter

### 6.3.1 Features

## - Compliant with the harmonic wave

 suppression guidelinesThe current on the power supply side is converted into the sine waveform by the PWM control to greatly reduce the harmonic current. When this converter is combined with the inverter, the conversion coefficient Ki stated in "Japanese Guideline for Suppressing Harmonics by Customers Receiving High Voltage or Special High Voltage" issued by the Agency for Natural

Comparison of input current waveforms
 Resources and Energy of the Ministry of Economy, Trade, and Industry is handled as zero (0) (no harmonic is produced).

## - Power supply equipment capacity can be reduced.

Since the current with the same phase as the power supply phase voltage is flowed by the power factor control, the operation with a power factor of almost "1" can be made.
Therefore, the power supply transformer capacity can be reduced or the unit can be made compact when compared to the standard type inverter.

## Braking performance is improved significantly.

All of the regenerative energy generated by highly frequent acceleration and deceleration operations or the lift are returned to the power supply side. This ensures the energy saving.
Additionally, as the current waveform of the regenerative energy also becomes the sine waveform, this does not cause any trouble in the power supply system. The following describes the regenerative performance.

Unit type - Continuous regenerative rating : 100\%

- Regenerative rating for 1 min . : $150 \%$ (CT spec)
: 120\% (VT spec)
Stack type - Continuous regenerative rating : 100\%
- Regenerative rating for 1 min . : $150 \%$ (MD spec)
: 110\% (LD spec)

Allowable regenerative electric power


Protective and maintenance functions are enhanced.
(1) Use of trace back (option) function makes it possible to easily analyze the cause of the alarm trip.
(2) The past alarm contents (memory for past ten alarms) can be checked using the segment LED.
(3) If a momentary power failure occurs, the gate is shut down and the operation is immediately restarted after the power has been recovered.
(4) A warning signal, such as overload, fin overheat, or service life is used to give an alarm before the converter is tripped.

## - Network functions are enhanced

This PWM converter can be connected to Fuji Electric's network systems, such as SX bus, T-Link, CC-Link (optional). The RS-485 is provided as standard. (Unit type: RHC-C only)

## Applicable capacity are enhanced

(1) Two models, unit type (RHC-C) and stack type (RHC-D), are available. An appropriate model for the system can be selected.
(2) Use of high-speed serial card (OPC-VG7-SI $\square$ ) (optional) makes it possible to perform the parallel operation of the PWM converters. As the power supply transformer is used for the input power supply, up to six parallel operations can be performed.

- Transformer-less parallel system: 3-parallel operation (stack type 400 V ) $\Rightarrow$ MD spec: 2400 kW , LD spec: 3000 kW)
- Insulated parallel system with a transformer: 6-parallel operation (stack type 400 V ) $\Rightarrow$ MD spec: 4800 kW , LD spec: 6000 kW )

Note Use of the transformer-less parallel system with the unit type (RHC-C) requires the product dedicated to transformer-less parallel systems (RHC $\square-4 C R$ ) as well as the optical link option card for parallel systems (OPC-VG7-SIR).

This section is focused on the RHC-D series (stack type) PWM converters.
For more information on the stack and unit types, refer to the separate volume instruction manual.
©al For details on the unit type, refer to the RHC-C Instruction Manual (INR-HF51746c).
For details on the stack type, refer to the RHC-D Instruction Manual (INR-SI47-1722).

### 6.3.2 Standard specifications

The standard specifications described here include those for the RHC-C series (unit type) as well.

### 6.3.2.1 3-phase 400V series (RHC-C: unit type)

|  |  | Item | Standard specifications |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model |  |  | RHC $\square$-4C |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 280 | 315 | 355 | 400 | 500 | 630 |  |
|  | Applicable inverter capacity (kW) |  | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 280 | 315 | 355 | 400 | 500 | 630 |  |
|  | $\begin{aligned} & \frac{7}{2} \\ & \frac{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity (kW) | 36 | 44 | 53 | 65 | 88 | 103 | 126 | 150 | 182 | 227 | 247 | 314 | 353 | 400 | 448 | 560 | 705 |  |
|  |  | Overload rating | 150\% of the continuous rating for 1 minute |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Voltage | 640 to 710 VDC (variable according to input power voltage) *1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Required power supply capacity (kVA) |  | 38 | 47 | 57 | 70 | 93 | 111 | 136 | 161 | 196 | 244 | 267 | 341 | 383 | 433 | 488 | 610 | 762 |  |
|  | Carrier frequency *2 |  | Standard 15 kHz |  |  |  | Standard 10 kHz |  |  |  |  |  |  |  |  |  |  | Standard 6 kHz |  |  |
| $\begin{aligned} & \text { © } \\ & \stackrel{\circ}{5} \\ & \stackrel{5}{5} \end{aligned}$ | Applicable inverter capacity (kW) |  | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 | 200 | 220 | 280 | 315 | 355 | 400 | 500 |  |  |  |
|  | $\begin{aligned} & \stackrel{\rightharpoonup}{2} \\ & \frac{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity (kW) | 44 | 53 | 65 | 88 | 103 | 126 | 150 | 182 | 227 | 247 | 314 | 353 | 400 | 448 | 560 |  |  |  |
|  |  | Overload rating | 120\% of the continuous rating for 1 minute |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Voltage | 640 to 710 VDC (variable according to input power voltage) *1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Required power supply capacity (kVA) |  | 47 | 57 | 70 | 93 | 111 | 136 | 161 | 196 | 244 | 267 | 341 | 383 | 433 | 488 | 610 |  |  |  |
|  | Carrier frequency *2 |  | Standard 10 kHz |  |  |  | Standard 6 kHz |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Number of phases, voltage, and frequency Allowable voltage and frequency fluctuation |  | 3-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $460 \mathrm{~V} / 60 \mathrm{~Hz}$ *3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Voltage: -15 to $+10 \%$, Frequency; $\pm 5 \%$, Voltage unbalance ratio; $2 \%$ or less *4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

*1 When the power supply voltage is $400 \mathrm{~V}, 440 \mathrm{~V}$, and 460 V , the output voltage is approx. $640 \mathrm{VDC}, 686 \mathrm{VDC}$ and 710 VDC, respectively.
*2 When the OPC-VG7-SIR is installed (to provide a transformer-less parallel system), the carrier frequency is automatically set to 5 kHz .
*3 When the power supply voltage is 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, the tap switching inside the PWM converter is required.
When the power supply voltage is less than 400 V , the capacity needs to be reduced.
*4 Inter-phase unbalance rate [\%] = (Max. voltage [V] - Min. voltage [V])/3-phase average voltage $\times 67$

### 6.3.2.2 3-phase 400V/690V series (RHC-D: stack type)

| Item |  |  | Standard specifications |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model |  |  | RHCDS-4D $\square$ |  |  |  |  |  | RHCDB-4D ${ }^{\text {*1 }}$ |  |  | RHCDS-69D $\square$ |  |  |  |  |  |  |  |  |
|  |  |  | 132 | 160 | 200 | 220 | 280 | 315 | 630 | 710 | 800 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 | 450 |
|  | App cap | licable inverter acity (kW) | 132 | 160 | 200 | 220 | 280 | 315 | 630 | 710 | 800 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 | 450 |
|  | $\begin{aligned} & \frac{7}{3} \\ & \frac{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity (kW) | 150 | 182 | 227 | 247 | 314 | 353 | 705 | 795 | 896 | 150 | 182 | 227 | 280 | 314 | 353 | 400 | 448 | 504 |
|  |  | Overload rating | 150\% of the continuous rating for 1 minute |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Voltage | 640 to 710 VDC (variable according to input power voltage) *2 |  |  |  |  |  |  |  |  | 895 to 1073 VDC (variable according to input power voltage) *3 |  |  |  |  |  |  |  |  |
|  | Required power supply capacity (kVA) |  | 161 | 196 | 244 | 267 | 341 | 383 | 762 | 858 | 967 | 161 | 196 | 244 | 304 | 341 | 383 | 433 | 488 | 549 |
|  | Carrier frequency *3 |  | 5 kHz |  |  |  |  |  | 5 kHz |  |  | 5 kHz |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \otimes \\ & \hline 0 \\ & \hline \\ & \hline \\ & \hline \end{aligned}$ | App <br> cap | licable inverter acity (kW) | 160 | 200 | 220 | - | 315 | 355 | 710 | 800 | 1000 | 132 | 160 | 200 | 250 | 280 | 315 | 355 | 400 |  |
|  | $\begin{aligned} & \frac{7}{3} \\ & \frac{2}{3} \\ & 0 \end{aligned}$ | Continuous capacity (kW) | 182 | 227 | 247 | - | 353 | 400 | 795 | 896 | 1120 | 160 | 200 | 220 | 280 | 315 | 355 | 400 | 450 |  |
|  |  | Overload rating | 110\% of the continuous rating for 1 minute |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Voltage | 640 to 710 VDC (variable according to input power voltage) *2 |  |  |  |  |  |  |  |  | 895 to 1073 VDC (variable according to input power voltage) *3 |  |  |  |  |  |  |  |  |
|  | Required power supply capacity (kVA) |  | 196 | 244 | 267 | - | 383 | 433 | 858 | 967 | 1210 | 196 | 245 | 267 | 341 | 383 | 433 | 488 | 549 |  |
|  | Carrier frequency *3 |  |  |  |  |  |  |  |  |  |  | 5 kHz |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \bar{\omega} \\ & \sum_{0}^{0} \\ & \hline \end{aligned}$ | Number of phases, voltage, and frequency |  | 3-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $460 \mathrm{~V} / 60 \mathrm{~Hz}$ *5 |  |  |  |  |  |  |  |  |  |  | 3-phase, 3-wire type, 660 to 690 V, $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ <br> 3-phase, 3-wire type, 575 to 600 V , $50 \mathrm{~Hz} / 60 \mathrm{~Hz}$ * 6 |  |  |  |  |  |  |
| 은 | Allowable voltage and frequency fluctuation |  | Voltage: -15 to +10\%, Frequency; $\pm 5 \%$, Voltage unbalance ratio; $2 \%$ or less *7 |  |  |  |  |  |  |  |  |  |  | Voltage: -15 to $+10 \%$, Frequency; $\pm 5 \%$, Voltage unbalance ratio; 2\% or less *7 |  |  |  |  |  |  |

*1 The RHC $\square \mathrm{B}-4 \mathrm{D}$ consists of three stacks per set.
*2 When the power supply voltage is $400 \mathrm{~V}, 440 \mathrm{~V}$, and 460 V , the output voltage is approx. $640 \mathrm{VDC}, 686 \mathrm{VDC}$ and 710 VDC, respectively.
*3 The output voltage is 895 VDC when the power supply voltage is 575 V , and 1073 VDC when the power supply voltage is 690 V .
*4 When the OPC-VG7-SIR is installed (to provide a transformer-less parallel system), the carrier frequency is automatically set to 2.5 kHz .
*5 When the power supply voltage is 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$, the tap switching inside the PWM converter is required.
When the power supply voltage is less than 400 V , the capacity needs to be reduced.
*6 The tap inside the converter must be switched when the power supply voltage is 575 to $600 \mathrm{~V} / 50 \mathrm{~Hz}$ or 575 to 600 $\mathrm{V} / 60 \mathrm{~Hz}$.
The capacity must be reduced when the power supply voltage is less than 690 V .
*7 Inter-phase unbalance rate [\%] = (Max. voltage [V] - Min. voltage [V])/3-phase average voltage $\times 67$

### 6.3.3 Common specifications

| Item |  | Specifications |
| :---: | :---: | :---: |
| $\begin{aligned} & \text { 흐 } \\ & \text { రర } \end{aligned}$ | Control method | AVR constant control with DC ACR minor |
|  | Start/stop operation | Starts the rectification when the power is turned ON after connection. <br> Starts boosting when it receives the run signal (RUN-CM short-circuit or run command from the communication). After that, the converter is ready to run. |
|  | Running status signal | Running, power running, regenerative operation, ready-to-run, alarm output (for any alarm), etc. |
|  | Overload rating switching | Unit type CT spec: $150 \%$ of overload rating for 1 min . VT spec: $120 \%$ of overload rating for 1 min. <br> Stack type <br> Either rating is selected. (CT spec is fixed when the capacity is 500 kW or more.) <br> MD spec: $150 \%$ of overload rating for $1 \mathrm{~min} ., ~ L D ~ s p e c: ~$ <br>  <br>  <br> Either rating is selected. |
|  | Carrier frequency | Unit type: 5 kHz to 15 kHz (The setting range may vary depending on the capacity.) Stack type: Fixed at 5 kHz *1 |
|  | Input power factor | 0.99 or more (at full load) *2 |
|  | Input harmonic current | Conversion coefficient Ki can be set to zero ( 0 ) according to the harmonics suppressing guideline by METI. |
|  | Restart after momentary power failure | Shuts down the gate when the voltage level reaches the under-voltage level if a momentary power failure occurs, and the PWM converter is automatically restarted after the power recovers. |
|  | Power limiting control | Controls the power to the preset limit value or less. |
| $\begin{aligned} & \frac{\widehat{ㅁ}}{0} \\ & \stackrel{0}{01} \end{aligned}$ | Alarm display (protective functions) | Refer to "Table 6.3.10-1 List of alarm displays and protective operations". |
|  | Alarm history | Saves and displays the alarm history data for past ten alarms. Saves and displays the detailed contents of the trip cause for past one alarm. |
|  | Monitor | Displays the input power, input current in RMS, input voltage in RMS, DC intermediate current, and power supply frequency. |
|  | Load factor | Allows the user to measure the load factor with the keypad. |
|  | Display language | Allows the user to specify or refer to function codes in any of the three languages: Japanese, English, and Chinese. |
|  | Charging lamp | Lights up when the main circuit capacitor is charged. For the stack type, it lights up when only the auxiliary control power input is active. |
| Structure/environment |  | $\square$ Unit type: Refer to the RHC-C Instruction Manual (INR-HF51746c). <br> $\mathbb{1}$ Stack type: Refer to "2.2.1 Installation environment and conformity with standards" in Chapter 2. |

*1 When the OPC-VG7-SIR is installed (to provide a transformer-less parallel system), the carrier frequency is automatically set to 2.5 kHz .
*2 When the power supply voltage is 420 V ( 400 V series) or higher, or 630 V or higher ( 690 V series), and the operating load is $50 \%$ or higher, the power factor for the power supply drops to approx. 0.95 (only during regenerative operation).

### 6.3.4 Control options

Control options shown below can be used for the PWM converter.
$\begin{array}{l|l|l|l}\hline \text { Category } & \text { Model } & \text { Name } & \text { Specifications } \\
\hline \text { Analog card } & \text { OPC-VG7-AIO } & \text { Aio extension card } & \text { Extension card for analog signal output x 2 points } \\
\hline \begin{array}{l}\text { Digital card } \\
\text { (Applicable to 8-bit } \\
\text { bus.) }\end{array} & \text { OPC-VG7-DIO } & \text { Dio extension card } & \begin{array}{l}\text { Extension card for digital output (Y terminal) x 8 points } \\
\text { This card is used when DIOA is set. }\end{array} \\$\cline { 2 - 4 } \& OPC-VG7-TL \& T link interface card \& For Fuji Electric's private link: T-Link communication <br>
\cline { 2 - 4 } \& OPC-VG7-CCL \& CC-Link interface card \& For CC-Link communication <br>
\cline { 2 - 4 } \& OPC-VG7-SI \& $\begin{array}{l}\text { Optical link card for parallel } \\
\text { system }\end{array} & \begin{array}{l}\text { For converter parallel operation (for insulated parallel system } \\
\text { with a transformer) }\end{array} \\$\cline { 2 - 4 } \& OPC-VG7-SIR \& \(\left.$$
\begin{array}{l}\text { Optical link card for parallel } \\
\text { system }\end{array}
$$ \& $$
\begin{array}{l}\text { For converter parallel operation (for transformer-less parallel } \\
\text { system) } \\
\text { The special version (RHC } \square-4 C R) ~ i s ~ r e q u i r e d ~ w h e n ~ t h i s ~\end{array}
$$ <br>
system is applied to the unit type (RHC-C). (The stack type <br>

can be used with the standard type.)\end{array}\right]\)| SX bus interface card |
| :--- |
| Digital card <br> (Applicable to <br> 16-bit bus.) |

Allowable option combinations

| Category | Max. number of mountable cards |  |  |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Analog card | 1 | 1 | 0 | 0 | Analog (1 card) + digital ( 1 card) or digital ( 2 cards) (It is impossible to mount the TL and CCL at the same time.) |
| Digital card (Applicable to 8-bit bus.) | 1 | - | 2 | 2 |  |
| Digital card (Applicable to 16-bit bus.) | - | 1 | 0 | 1 | It is possible to mount this card and the TL or SI $\square$ at the same time. It is impossible to mount this card and the CCL at the same time. |

Note Take great care since there are restrictions on mounting of option card.
凹】 For more information, refer to the RHC-C instruction manual (INR-HF51746c) and the RHC-D Instruction Manual (INR-SI47-1722).

|  | AIO | TR | DIO | TL | CCL | SI | SIR | SX | PDP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AIO | NG |  |  |  |  |  |  |  |  |
| TR | OK | NG |  |  |  |  |  |  |  |
| DIO | OK | OK | NG |  |  |  |  |  |  |
| TL | OK | OK | OK | NG |  |  |  |  |  |
| CCL | OK | OK | OK | NG | NG |  |  |  |  |
| SI | OK | OK | OK | OK | OK | NG | NG |  |  |
| SIR | OK | OK | OK | OK | OK | NG | NG |  |  |
| SX | OK | OK | OK | OK | NG | OK | OK | NG |  |
| PDP | OK | OK | OK | NG | NG | OK | OK | NG | NG |

### 6.3.5 Check before use

Unpack the package and check the following:
Check that you have properly received the product main unit and the following accessories.

## Accessories Instruction manual

The inverter has not been damaged during transportation-there should be no dents or parts missing. The main and sub nameplates are attached to the main unit. The main nameplate is located on the front face of the main unit (as shown in Figure 6.3.6-2 and Figure 6.3.6-3). Check these main nameplates to see that the inverter is exactly the type you ordered.

(a) Main Nameplate

## TYPE RHC132S-4DJ

SER.No. 28A456A0002BA
(b) Sub Nameplate

Figure 6.3.5-1: Nameplate
TYPE: PWM converter (RHC-D)


The PWM converter (RHC-D) is available in two drive modes depending upon the applied load: Medium Duty (MD) spec and Low Duty (LD) spec modes.
Specifications in each spec are printed on the nameplate.


If you suspect the product is not working properly or if you have any questions about your product, contact your Fuji Electric representative.
1 Refer to Chapter 3 "Transportation and Storage of Stack" for information on transportation and long-term storage of PWM converters.
[1] Refer to Chapter 4 "Installation and Wiring" for information on installation of PWM converters.
For information on the main circuit wire sizes, refer to "6.3.15.2 Wire size".

### 6.3.6 External views

### 6.3.6.1 Warning label and falling warning label




Figure 6.3.6-1: Warning label and falling warning label

### 6.3.6.2 Appearance



Figure 6.3.6-2: Frame 3 size (RHC132S to RHC200S-4D $\square$ )



Figure 6.3.6-4: Frame 3 size (RHC132S to RHC200S-69D $\square$ )


Figure 6.3.6-5: Frame 4 size (RHC250S to RHC450S-69D口)

For phase-specific stacks, the keypad can be installed to the S-phase stack only.


Figure 6.3.6-6: Frame 4 size (RHC630B to RHC800B-4D $\square$ )

### 6.3.7 Terminal functions

|  | Terminal symbol | Terminal name | Specifications |
| :---: | :---: | :---: | :---: |
|  | L1/R, L2/S, L3/T | Main power input | Connect to 3-phase power supply via dedicated reactor, etc. |
|  | $\mathrm{P}(+), \mathrm{N}(-)$ | Converter output | Connect to inverter power input terminals $\mathrm{P}(+)$ and $\mathrm{N}(-)$. |
|  | $\mathrm{E}(\mathrm{G})$ | Earthing terminal | Grounding terminal for the chassis (case) of the PWM converter. |
|  | R0, T0 | Auxiliary control power input | Connect to the backup terminal of the power supply for the control power supply and the same power supply system as the main power input. <br> For information on terminal ratings, refer to "4.5.3 (4) Auxiliary control power input and fan power input". |
|  | R1, S1, T1 | For voltage detection Synchronous power supply input | Voltage detection terminals used to control the inside of the PWM converter. These terminals are connected to the power supply sides of the dedicated filter. |
| $\begin{aligned} & \text { 추 } \\ & \text { 를 } \end{aligned}$ | R2, T2 | Control monitor input | (400V series) <br> Connection terminal for AC fuse disconnection detection. <br> No connection is required when the filter stack (RHF-D) is used. (690V series) <br> There are no R2 or T2 terminals. |
| $\stackrel{\cdot}{\bar{\omega}}$ | R3,T3 | Fan power input | (400V series) <br> Connection terminals for the AC cooling fan inside the stack. Connect these terminals to the same power supply system as the main power input. Jumper wires are connected between R1 and R3 and between T1 and T3 when the product is shipped from the factory. Remove the jumper wires and wire these terminals independently when the fan power supply is used individually. For information on how to connect the terminals, refer to the PWM converter (RHC-D) instruction manual. For information on terminal ratings, refer to "6.3.15.1-(5) Auxiliary control power input (RO, TO) and fan power input (CNV: R3, T3 INV: R1, T1)". <br> (690V series) <br> There are no R3 or T3 short-circuit wires. <br> If using a separate fan power supply, switch the tap inside the converter, and connect the fan power supply to the R3 and T3 terminals. Refer to the PWM converter (RHC-D) instruction manual for information on the connection method. |


| ¿ <br> 0 <br> 0 <br> 0 <br> 0 | Terminal symbol | Terminal name | Specifications |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | [RUN] | Start/stop command | When the portion between the RUN and CM is turned ON, the converter performs boosting. The converter stops when this portion is turned OFF. |  |  |  |  |  |
|  | [RST] | Alarm reset command | If an alarm stop occurs, remove the cause of the alarm. When the portion between the RST and CM is turned ON, the protective function in operation is cancelled to restore the operation. |  |  |  |  |  |
|  | [X1] | Digital input | The following function can be assigned to terminal X1. <br> 0: External alarm [THR], 1: Current limit cancellation [LMT-CCL], <br> 2: 73 answer back [73ANS], 3: Current limit switching [I-LIM], <br> 4: Option DI [OPT-DI] |  |  |  |  |  |
| $\stackrel{0}{0}$ | [CM] | Digital input common | Common terminal for the digital input signals |  |  |  |  |  |
| \% | [PLC] | PLC signal power | Connect the PLC output signal power supply. (Rated voltage 24 V ( 22 to 27 V) DC) |  |  |  |  |  |
| $\stackrel{\text { ㄹㅡㅡ }}{\text { - }}$ |  |  |  | Item |  | min. | typ. | max. |
|  |  |  |  | Operating voltage | ON level | 0 V | - | 2 V |
|  |  |  |  | - | OFF level | 22 V | 22 V | 27 V |
|  |  |  |  | Operating current in | ON state | - | 3.2 mA | 4.5 mA |
|  |  |  |  | Allowable leak cur | the OFF state | - | - | 0.5 mA |
|  | $\begin{aligned} & \text { [DCF1] } \\ & {[\mathrm{DCF} 2]} \end{aligned}$ | Input for DC fuse disconnection detection | This terminal is intended to connect the microswitch for DC fuse blow detection in the case the converter output is protected with a DC fuse. It supports the b-contact output. <br> 24 VDC 12 mA Typ |  |  |  |  |  |



[^7]
### 6.3.8 Communication specifications

| Item |  |
| :--- | :--- |
| General communication <br> specifications | Specifications <br> Run information, running status, function code monitor function (polling), RUN, RST, <br> and X1 can be controlled (selected). (* Function codes other than "S" codes cannot <br> be written.) |
| Network <br> (option) | T link |
|  | SX bus |
|  | Option to be used: OPC-VG7-TL <br> Performs the T link communication with the T link module of the MICREX-F or <br> MICREX-SX. |
| CC-Link | Option to be used: OPC-VG7-SX <br> Performs the SX bus connection with the MICREX-SX. |
| Option to be used: OPC-VG7-CCL <br> Performs the connection with the CC link master unit. |  |
| (option) communication * | Option to be used: OPC-VG7-SI, OPC-VG7-SIR <br> Use of this option makes it possible to perform the load allocation control of the parallel <br> multiplex system. |

### 6.3.9 Basic connection diagrams

### 6.3.9.1 List of basic connection diagrams

How to wire the filter circuits and sequence units differs depending on the inverter used in conjunction with the PWM converter capacity. From Table 6.3.9-1, select the appropriate basic connection diagram.

Table 6.3.9-1: List of basic connection diagrams for PWM converters (RHC-D series)

|  | Filter circuit | PWM converter *2 |  | Inverter | Recommended ${ }^{\text {3 }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Specifi- <br> cations | Model |  |  |
| 1 | Configuration of peripherals *1 | MD | RHC132S-4D $\square$ to RHC220S-4D $\square$ | Stack type |  |
|  |  | LD | RHC132S-4D $\square$ to RHC200S-4D $\square$ |  |  |
| 2 | Configuration of peripherals *1 | MD | RHC280S-4D $\square$ to RHC315S-4D $\square$ | Stack type |  |
|  |  | LD | RHC280S-4D $\square$ to RHC315S-4D $\square$ |  |  |
| 3 | Configuration of peripherals *1 | MD | RHC630B-4D $\square$ to RHC800B-4D $\square$ | Stack type | $\bigcirc$ |
|  |  | LD | RHC630B-4D $\square$ to RHC800B-4D $\square$ |  |  |
| 4 | Filter stack (RHF-D series) <br> RHF160S-4D $\square$ to RHF355S-4D $\square$ | MD | RHC132S-4D $\square$ to RHC315S-4D $\square$ | Stack type | $\bigcirc$ |
|  |  | LD | RHC132S-4D $\square$ to RHC315S-4D $\square$ |  |  |
|  | RHF160S-69D $\square$ to RHF450S-69D $\square$ | MD | $\begin{aligned} & \text { RHC132S-69D } \square \text { to } \\ & \text { RHC450S-69D } \\ & \hline \end{aligned}$ |  |  |
|  |  | LD | $\begin{aligned} & \text { RHC132S-69D } \square \text { to } \\ & \text { RHC400S-69D } \end{aligned}$ |  |  |

*1 The peripherals are those shown in "6.3.12.2 List of peripherals with no filter stack used".
*2 A single unit of PWM converter is used.
*3 This means recommended basic connections.
RHC630B-4D $\square$ to RHC800B-4D $\square$
Configuration with peripherals is recommended.
RHC132S-4D $\square$ to RHC315S-4D $\square$
RHC132S-69D $\square$ to RHC450S-69D $\square$
Use of filter stack is recommended. When using a single PWM converter or using an insulated parallel system with a transformer (where multiple PWM converters are run in parallel), the filter circuit can be configured with peripherals. This is not possible, however, when using a transformer-less parallel system (where multiple PWM converters are run in parallel). Use a filter stack when using a transformer-less parallel system.

### 6.3.9.2 Basic connection diagram 1

## - RHC132S-4D $\square$ to RHC220S-4D $\square$ (MD spec)

## - RHC132S-4D $\square$ to RHC200S-4D $\square$ (LD spec)


(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the connection diagram.
(Note 2) Be sure to connect the PWM converter and inverter auxiliary power input terminals (R0, T0) to the main power via contact $b$ of the charging circuit electromagnetic contactor (73) or power supply electromagnetic contactor (52). When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#73 or \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Configure one of the inverter's terminals X 1 to X 9 for use by the external alarm (THR).
(Note 6) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.

### 6.3.9.3 Basic connection diagram 2

## $\square$ RHC280S-4D $\square$ to RHC315S-4D $\square$ (MD spec)

■ RHC280S-4D $\square$ to RHC315S-4D $\square$ (LD spec)

(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the connection diagram.
(Note 2) Be sure to connect the PWM converter and inverter auxiliary power input terminals ( $\mathrm{RO}, \mathrm{TO}$ ) to the main power via contact b of the power supply electromagnetic contactor (52). When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Set the timer for 52T to 1 second.
(Note 6) Configure one of the inverter's terminals X1 to X9 for use by the external alarm (THR).
(Note 7) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.

### 6.3.9.4 Basic connection diagram 3

$\square$ RHC630B-4D $\square$ to RHC800B-4D $\square$ (MD spec)

- RHC630B-4D $\square$ to RHC800B-4D $\square$ (LD spec)

(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the connection diagram.
(Note 2) Be sure to connect the PWM converter and inverter auxiliary power input terminals ( $\mathrm{RO}, \mathrm{TO}$ ) to the main power via contact $b$ of the power supply electromagnetic contactor (52). When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Set the timer for 52 T to 1 second.
(Note 6) Configure one of the inverter's terminals X 1 to X 9 for use by the external alarm (THR).
(Note 7) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.


### 6.3.9.5 Basic connection diagram 4

$\square$ RHC132S-4D $\square$ to RHC315S-4D $\square$ (MD spec)
■ RHC132S-4D $\square$ to RHC315S-4D $\square$ (LD spec)

- RHC132S-69D $\square$ to RHC450S-69D $\square$ (MD spec)

■ RHC132S-69D $\square$ to RHC400S-69D $\square$ (LD spec)

(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the connection diagram.
(Note 2) Be sure to connect the PWM converter and inverter auxiliary power input terminals (R0, T0) to the main power via contact $b$ of the power supply electromagnetic contactor (52). When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Set the timer for 52 T to 1 second.
When using microswitches for AC fuse disconnection detection, assign external alarm (THR) to the PWM converter's terminal X1, and connect all of the microswitches in series.
(Note 6) Be sure to assign the PWM converter digital input terminal (X1) to the external alarm (THR), and to connect the filter stack overheat signal outputs (1, 2). Set contact b input with function code E14 to input with contact b. Furthermore, connect the microswitch for AC fuse blow detection to the digital input terminal (X1) in series with all microswitches and the overheat signal outputs (1, 2).
(Note 7) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.
(Note 8) When inputting 200 VAC as the fan power supply, remove jumper wires from between terminals R11 and R12 and from between terminals T11 and T12, and then connect the input to terminals R12 and T12. Note that these terminals are dedicated to the internal fan power supply. Do not use them for any other purposes.
(Note 9) Be sure to set the timer for 73 T to 5 seconds.
(Note 10) For the 400 V series, connect "Fdc (fuse)" to the $\mathrm{P}(+)$ side. No "Fdc (fuse)" is required at the $\mathrm{N}(-)$ side. For the 690 V series, connect "Fdc (fuse)" to the $P(+)$ side and $N(-)$ side.
Furthermore, use two microswitches and connect them in series.
(Note 11) With the 690V series, there are no R3 or T3 short-circuit wires.

## WARNING

- Be sure to assign the PWM converter digital input terminal (X1) to the external alarm (THR), and to connect the filter stack overheat signal outputs (1, 2).
- Be sure to stop the PWM converter and inverter when the overheat signal is output. Furthermore, shut off electromagnetic contactors 52 and 73.


## Risk of fire, accident

### 6.3.10 Protective functions

If an error occurs in the PWM converter, the protective function operates to immediately stop (trip) the PWM converter and display the alarm code on the keypad. If the protective function operates, check and remove the cause, and then replace any defective parts. When a reset command is input after that, the operation of the protective function is cancelled, and then the converter operation can be restarted.
For details about alarm contents, refer to Table 6.3.10-1.

### 6.3.10.1 List of alarm codes

Table 6.3.10-1: List of alarm displays and protective operations

| Alarm name | Display | Operation contents |
| :--- | :---: | :--- |
| AC fuse blown | ACF | Operates if the external AC fuse of PWM converter is blown due to short-circuiting or <br> breakage of internal circuits. |
| AC overcurrent | AOC | Operates if the momentary value of the AC current exceeds the overcurrent detection <br> level due to short-circuiting or ground fault of the power supply circuit. |
| AC insufficient | ALV | Operates if the AC power supply voltage drops to the insufficient voltage detection <br> level or less during PWM converter operation. <br> No alarm is output when "F02: Restart Mode after Momentary Power Failure (Mode <br> selection)" is set to "1" (Restart). <br> AC insufficient voltage detection level (400V system: 176 Vrms, $690 V$ series: 350 <br> Vrms) |
| AC input current |  |  |
| error |  |  |$\quad$| ACE |
| :--- | | Operates if the deviation between the PWM converter current command value and |
| :--- |
| input AC power supply detection value exceeds the input current error detection level. |
| No alarm is output when "F02: Restart Mode after Momentary Power Failure (Mode |
| selection)" is set to "1" (Restart). |


| Alarm name | Display | Operation contents |
| :--- | :---: | :--- |
| Charging circuit <br> error | PbF | This function operates when "73 answer back" [73ANS] is selected in the X1 function <br> selection. <br> The function also operates if X1 is not input (electromagnetic contactor for charging <br> circuit bypass is closed) within 0.5 sec. after the charging circuit control output [73A] <br> signal of the PWM converter has operated. <br> The alarm is reset by switching the X1 function selection or powering ON again <br> (power ON reset). |
| Cooling fin <br> overheat | OH1 | Operates if the temperature around the cooling fins that cool the semiconductor <br> elements of the main circuit increases due to cooling fan stop. |
| External alarm | OH2 | Performs the PWM converter alarm stop operation by the external signal input (THR). |
| Overheat inside <br> converter | OH3 | Operates if the temperature around the control PCB increases due to poor ventilation <br> inside the PWM converter. |
| Converter overload | OLU | Operates if the AC power supply current exceeds the overload level shown in Figure <br> $6.3 .10-1$. <br> MD mode: 150\%/60 sec. <br> LD mode: $110 \% / 60$ sec. |
| Memory error | Er1 | Operates if an error occurs in the memory, such as a data write error. |
| Keypad <br> communication <br> error | Er2 | Operates if the keypad transmission error occurs. |

(1) MD mode

(2) LD mode


Figure 6.3.10-1: Overload trip time

### 6.3.10.2 Troubleshooting

(1) If the protective function operates [PWM converter main unit]


## (3) DC fuse blown (dCF)



Short-circuit failure may occur inside the converter. Contact Fuji Electric.

(5) Insufficient voltage (ALV, dLV)

(6) Overheat inside converter ( OH 3 ), cooling fin overheat (OH1), IPM error (IPE)

(7) Converter overload (OLU)

(8) Memory error (Er1), CPU error (Er3)

(9) Input open-phase (LPV)

(10) A/D converter error (Er8)

(11) Synchronous power supply frequency error (FrE)


## (12) Touch panel communication error (Er2)


(13) External alarm (OH2)

(14) Charging circuit error (PbF)

(15) AC input current error (ACE)


## (2) If the protective function operates [Network option: Network error (Er4)]

<T-Link: OPC-VG7-TL>
The T-Link option provides two kinds of alarms, light alarm and heavy alarm, according to the failure level.

| Item | Light alarm | Heavy alarm |  |
| :---: | :---: | :---: | :---: |
| Cause | - Noise is applied to the communication line. <br> - Address is duplicated. (Setting mistake of RSW 1 and 2) | - Communication line is disconnected. <br> Power to MICREX (PLC) is shut down (OFF). | T-Link option hardware is faulty (breakage or defect). |
| Reset method | Resolve the cause of the alarm (automatic resolution by restoring the communication), and give the reset command (reset from the keypad, [RST], or communication). |  | Remove the cause of the hardware failure and reset the power supply (power ON reset). |
| Failure state control | Alarm may occur only when the run command is sent from the T-Link. Momentary Er4 alarm Alarm can be controlled with function codes H 02 and H 03 . |  |  |

<SX bus: OPC-VG7-SX>
The SX bus option provides two kinds of alarms, light alarm and heavy alarm, according to the failure level.

| Item | Light alarm | Heavy alarm 1 | Heavy alarm 2 |
| :---: | :---: | :---: | :---: |
| Cause | Communication data error due to noise application to the communication line. | - All master units are failed. <br> - Disconnection is detected. <br> - SX bus power supply is shut down. | - Option hardware failure <br> - Option mounting failure |
| Reset method | Resolve the cause of the alarm restoring the communication), (reset from the keypad, [RST], | (automatic resolution by and give the reset command or communication). | Remove the cause of the hardware failure and reset the power supply (power ON reset). |
| Failure state control | Alarm may occur only when the run command is sent from the $S X$ bus. Momentary Er4 alarm Alarm can be controlled with function codes H 02 and H03. |  |  |
| Keypad display (Communication error code) | 1 | 2 | 3 |

Note (1) If any heavy alarm 1 occurs, reset also the power supply to the MICREX-SX (power ON reset) depending on the CPU status.
(2) The communication error code of a light alarm or heavy alarm can be checked on the Maintenance Information Communication Status screen on the keypad. To display the Communication Status screen, press the PRG key on the Operation Mode screen to change to the Menu screen, use the $\boldsymbol{\lambda}$ or $\boldsymbol{V}$ key to move the arrow mark at
 the left end of the screen to " 5 . Maintenance", and then press the FUNC/DATA key.
After that, press the $\mathbf{V}$ key three times to display the following screen.
<CC-Link: OPC-VG7-CCL>
The CC-Link option provides two kinds of alarms, light alarm and heavy alarm, according to the error level.

| Item | Light alarm (operation in the case of communication <br> line error) | Heavy alarm (operation in the case of option <br> error) |
| :--- | :--- | :--- |
| Cause | - Master unit is failed. <br> - Disconnection is detected. <br> Communication data error (Noise is applied to <br> the communication line.) | - Option hardware error <br> - Option mounting failure |
| Reset method | After the cause of the alarm has been removed <br> (automatic release by resetting communication), <br> give the reset. | Remove the cause of the hardware failure <br> and reset the power supply (power ON reset). |
| Alarm output <br> control | Error is detected only in the CC-Link operation <br> mode. <br> Alarm output method if an error is detected can <br> be controlled with function codes H02 and H03. | Momentary Er4 alarm |
| Communication <br> error code | 01 | 02 |

(3) If the protective function operates [Parallel system: OPC-VG7-SI/OPC-VG7-SIR is used.]

## 1) Parallel system alarm display

If an alarm occurs in the master or slave (PWM converter) unit (protective function operates) during parallel system operation, all units enter the alarm mode and the operations of all converters stop.
At the same time, the alarm code showing the cause of the alarm No. 1 is displayed on the LED displays of the keypads of all units. According to this alarm code display, a unit in which the alarm occurred can be judged.
Additionally, even when multiple alarms occur at the same time, the cause of only alarm No. 1 is displayed as alarm caused by other station. Furthermore, the alarm history display is the normal alarm display.



Alarm occurs in its own station (Alarm trip caused by its own station)

## 2) Link error among converter links (Erb)

If the optical cable has any faulty wiring or the connector drops during PWM converter operation, the protective function operates by the link error among converters (Erb). (All stacks operate at the same time.) When the PWM converter alarm output is used as external alarm conditions of the inverter, the inverter is tripped by the alarm and stops in the coast-to-a-stop mode.
Even when the reset command (any of the keypad, terminal block, and communication system, etc.) is input without the cause of the alarm reset, the alarm state cannot be cancelled. Be sure to investigate the cause of the alarm, and then reset it.

## <Troubleshooting "Erb">

If the "Erb" alarm occurs, the following causes may be considered. Check the causes.

- The optical cable is not connected or inserted into the connector completely. $\rightarrow$ Insert the cable securely into the optical connector.
- The optical cable is bundled or bent with a bending radius of 35 mm or less. $\rightarrow$ Bend the optical cable to a specified level.
- The connection plugs of the optical cable do not meet the connector colors (gray and blue) of the PCB. $\rightarrow$ Match the connector colors on the cable side with those on the PCB side.
- The optical cable connection is not formed as a loop. $\rightarrow$ Be sure to loop back the signal from the master.


## 3) Operation procedure error (Er6)

If the station number of this optical communication option is set incorrectly or if the same communication option card is installed in the inverter, the protective function operates.
This function provides preventive measures so that unstable operation caused by illegal operation is not performed.

## <Troubleshooting "Er6">

- The optical link option hardware station number SW1 setting is set to 6 or more.
- The optical link option hardware number SW1 setting is higher than H13 "Number of parallel system slave stations". $\rightarrow$ Make the setting correctly.
- Two optical link options are installed. $\boldsymbol{\rightarrow}$ Install only one optical link option.


## 4) Reset process

All stations are reset at the same time by the reset command of the master (slave) unit under conditions that the cause of the alarm is reset.

|  | Master alarm status | Slave alarm status | Reset target |
| :--- | :---: | :---: | :---: |
| Reset command from master unit | Valid | Valid | All units |
| Reset command from slave unit | Valid | Valid | All units |

## (4) Ready-to-run of PWM converter is not completed.

The PWM converter outputs the ready-to-run signal [RDY] that is the inverter operation condition after the run command [RUN] has been input.
The following describes the troubleshooting if the ready-to-run completion signal is not output after the run command has been input.


### 6.3.11 List of function codes

Table 6.3.11-1: List of function codes

|  | Function code |  |  | Data range | Min. unit | Unit | Factory default value |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. |  |  |  |  |  |  |  |
| 000.0000000 | F00 | Data protection |  | 0 to 1 | 1 | - | 0 |  |
|  | F01 | Harmonic filter selection |  | 0 to 1 |  |  | 0 |  |
|  | F02 | Restart after momentary power failure (operation selection) |  | 0 to 1 |  |  | 0 |  |
|  | F03 | Current rating switching |  | 0 to 1 |  |  | 0 |  |
|  | F04 | LED monitor (display selection) |  | 0 to 5 |  |  | 0 |  |
|  | F05 | LCD monitor (display selection) |  | 0 to 2 |  |  | 2 |  |
|  | F06 | LCD monitor (language selection) |  | 0 to 2 |  |  | 0 |  |
|  | F07 | LCD monitor (contrast adjustment) |  | 0 to 10 |  |  | 5 |  |
|  | F08 | Carrier frequency |  | 5 |  |  | 5 |  |
|  | E01 | X1 function selection |  | 0 to 4 | 1 | - | 4 |  |
|  | E02 | Y1 function selection |  | 0 to 14 | 1 | - | 0 |  |
|  | E03 | Y2 function selection |  |  |  |  | 2 |  |
|  | E04 | Y3 function selection |  |  |  |  | 3 |  |
|  | E05 | Y5 function selection |  |  |  |  | 1 |  |
|  | E06 | Y11 function selection | OPC-VG7-DIO option function | 0 to 14 | 1 | - | 0 |  |
|  | E07 | Y12 function selection |  |  |  |  | 0 |  |
|  | E08 | Y13 function selection |  |  |  |  | 0 |  |
|  | E09 | Y14 function selection |  |  |  |  | 0 |  |
|  | E10 | Y15 function selection |  |  |  |  | 0 |  |
|  | E11 | Y16 function selection |  |  |  |  | 0 |  |
|  | E12 | Y17 function selection |  |  |  |  | 0 |  |
|  | E13 | Y18 function selection |  |  |  |  | 0 |  |
|  | E14 | I/O function normally open/closed |  | 0000 to 007F |  |  | 0000 |  |
|  | E15 | RHC overload warning level |  | 50 to 105\% | 1 | \% | 80 |  |
|  | E16 | Cooling fan ON/OFF control |  | 0 to 1 | 1 | - | 0 |  |
|  | E17 | Output during current limiting (hysteresis width) |  | 0 to 30\% | 1 | \% | 10 |  |
|  | E18 | AO1 function selection |  | 0 to 10 | 1 | - | 1 |  |
|  | E19 | AO4 function selection | OPC-VG7-AIO option function |  |  |  | 0 |  |
|  | E20 | AO5 function selection |  |  |  |  | 0 |  |
|  | E21 | AO1 gain setting |  | $-100.00 \text { to } 100.00$ <br> (multiplication) | 0.01 | (multipli- <br> cation) | 1.00 |  |
|  | E22 | AO4 gain setting | OPC-VG7-AIO option function |  |  |  | 1.00 |  |
|  | E23 | AO5 gain setting |  |  |  |  | 1.00 |  |
|  | E24 | AO1 bias setting |  | -100.0 to 100.0\% | 0.1 | \% | 0.0 |  |
|  | E25 | AO4 bias setting | OPC-VG7-AIO option function |  |  |  | 0.0 |  |
|  | E26 | AO5 bias setting |  |  |  |  | 0.0 |  |
|  | E27 | AO1-5 filter setting |  | 0.000 to 0.500 s | 0.001 | S | 0.010 |  |

Note (1) The settings of the functions in the shaded portions in the list can be changed during operation. Other functions should be set after the operation has been stopped.

|  | Function code |  |  | Data range | Min. unit | Unit | Factory default value |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. | Name |  |  |  |  |  |  |
|  | H01 | Station address | Built-in RS-485 function | 0 to 255 | 1 | - | 1 |  |
|  | H02 | Operation selection in case of error | Communication option common function | 0 to 3 | 1 | - | 3 |  |
|  | H03 | Timer operation time |  | 0.01 to 20.00s | 0.01 | S | 2.00 |  |
|  | H04 | Transmission speed | Built-in RS-485 function | 0 to 4 | 1 | - | 2 |  |
|  | H05 | Data length selection |  | 0 to 1 |  |  | 0 |  |
|  | H06 | Parity bit selection |  | 0 to 2 |  |  | 0 |  |
|  | H07 | Stop bit selection |  | 0 to 1 |  |  | 0 |  |
|  | H08 | Communication faulty wiring time |  | 0.0 to 60.0s | 0.1 | S | 60.0 |  |
|  | H09 | Response interval time |  | 0.00 to 1.00 s | 0.01 | S | 0.05 |  |
|  | H10 | Protocol selection |  | 0 to 3 | 1 | - | 0 |  |
|  | H11 | TL transmission format | OPC-VG7-TL function | 0 to 1 | 1 | - | 0 |  |
|  | H12 | Parallel system | OPC-VG7-SI $\square$ function | 0 to 1 |  |  | 0 |  |
|  | H13 | Number of parallel system slave stations |  | 1 to 5 |  |  | 1 |  |
|  | H14 | Alarm data deletion |  | 0 to 1 |  |  | 0 |  |
|  | H15 | Power supply current limit (drive 1) |  | 0 to 150\% | 1 | \% | 150 |  |
|  | H16 | Power supply current limit (drive 2) |  |  |  |  | 150 |  |
|  | H17 | Power supply current limit (braking 1) |  | -150 to 0\% |  |  | -150 |  |
|  | H18 | Power supply current limit (braking 2) |  |  |  |  | -150 |  |
|  | H19 | Current limit warning (level) |  | -150 to 150\% |  |  | 100 |  |
|  | H20 | Current limit warning (timer) |  | 0 to 60s | 1 | s | 0 |  |
|  | U01 | Reserved for particular manufacturers. | OPC-VG7-SX option function | -32768 to 32767 | 1 | - | 0 |  |
|  | U02 | SX bus station number monitor |  | -32768 to 32767 | 1 | - | 0 |  |
|  | U03 | DC fan alarm cancellation |  | 0000 to FFFF | 1 | - | 0000 |  |
|  | U04 | AVR control response |  | -32768 to 32767 | 1 | - | 0 |  |
|  | U05 | DC voltage commend value selection |  | -32768 to 32767 | 1 | - | 0 |  |
|  | U06 | Reserved for particular manufacturers. |  | -32768 to 32767 | 1 | - | 0 |  |
|  | U07 | Reserved for particular manufacturers. |  | -32768 to 32767 |  |  | 0 |  |
|  | U08 | Reserved for particular manufacturers. |  | -32768 to 32767 |  |  | 0 |  |
|  | U09 | Reserved for particular manufacturers. |  | -32768 to 32767 |  |  | 0 |  |
|  | U10 | Reserved for particular manufacturers. |  | -32768 to 32767 |  |  | 0 |  |

Note (1) U01 and U06 to U10 are function codes that are reserved for the manufacturer. Do not change them from the factory default values.
(2) U codes to be displayed on the keypad are USER P1 to USER P10.
(3) The settings of the functions in the shaded portions in the list can be changed during operation. Other functions should be set after the operation has been stopped.

## 6．3．12 Configuration of peripherals

## 6．3．12．1 Configuration for the RHF－D series filter stacks

（1）In the case of MD

|  | PWM converter model | Filter stack |  | MCCB／ELCB rated current ［A］ | Electro－ magnetic contactor |  | AC Fuse |  | Microswitch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model | 2 2 N N 0 |  | Model | 公 | Model | （ | 形式 | ？ |
|  | RHC132S－4D $\square$ | RHF160S－4D $\square$ | 1 | 300 | SC－N8 | 1 | 170M5446 | 3 | 170H3027 | 3 |
|  | RHC160S－4D $\square$ | RHF160S－4D $\square$ | 1 | 350 | SC－N11 | 1 | 170M6546 | 3 |  |  |
|  | RHC200S－4D $\square$ | RHF220S－4D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC220S－4D $\square$ | RHF220S－4D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC280S－4D $\square$ | RHF280S－4D $\square$ | 1 | 600 | SC－N14 | 1 | 170M6499 | 3 |  |  |
|  | RHC315S－4D $\square$ | RHF355S－4D $\square$ | 1 | 700 | SC－N14 | 1 | 170M6500 | 3 |  |  |
|  | RHC132S－69D $\square$ | RHF160S－69D $\square$ | 1 | 175 | SC－N6 | 1 | 70M5447 | 3 |  |  |
|  | RHC160S－69D $\square$ | RHF160S－69D $\square$ | 1 | 200 | SC－N7 | 1 | 70M5447 | 3 |  |  |
|  | RHC200S－69D $\square$ | RHF220S－69D $\square$ | 1 | 250 | SC－N8 | 1 | 170M5448 | 3 |  |  |
|  | RHC250S－69D $\square$ | RHF280S－69D $\square$ | 1 | 300 | SC－N8 | 1 | 170M6548 | 3 |  |  |
|  | RHC280S－69D $\square$ | RHF280S－69D $\square$ | 1 | 350 | SC－N11 | 1 |  |  |  |  |
|  | RHC315S－69D | RHF355S－69D $\square$ | 1 | 400 | SC－N11 | 1 |  |  |  |  |
|  | RHC355S－69D $\square$ | RHF355S－69D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6500 | 3 |  |  |
|  | RHC400S－69D | RHF450S－69D $\square$ | 1 | 500 | SC－N12 | 1 |  |  |  |  |
|  | RHC450S－69D $\square$ | RHF450S－69D $\square$ | 1 | 600 | SC－N14 | 1 |  |  |  |  |

＊For information on peripherals for RHC630B to 800B－4DJ，refer to＂6．3．12．2 List of peripherals with no filter stack used＂．
（2）In the case of LD

|  | PWM converter model | Filter stack |  | MCCB／ELCB rated current <br> ［A］ | Electro－ magnetic contactor |  | AC Fuse |  | Microswitch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model |  |  | Model | 年 | Model | （1） | Model | 2 |
|  | RHC132S－4D $\square$ | RHF160S－4D $\square$ | 1 | 350 | SC－N11 | 1 | 170M5446 | 3 | 170H3027 | 3 |
|  | RHC160S－4D $\square$ | RHF220S－4D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6546 | 3 |  |  |
|  | RHC200S－4D $\square$ | RHF220S－4D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC280S－4D $\square$ | RHF355S－4D $\square$ | 1 | 700 | SC－N14 | 1 | 170M6499 | 3 |  |  |
|  | RHC315S－4D $\square$ | RHF355S－4D $\square$ | 1 | 800 | SC－N14 | 1 | 170M6500 | 3 |  |  |
|  | RHC132S－69D $\square$ | RHF160S－69D $\square$ | 1 | 200 | SC－N7 | 1 | 170M5447 | 3 |  |  |
|  | RHC160S－69D $\square$ | RHF220S－69D $\square$ | 1 | 250 | SC－N8 | 1 |  |  |  |  |
|  | RHC200S－69D $\square$ | RHF220S－69D $\square$ | 1 | 300 | SC－N8 | 1 | 170M5448 | 3 |  |  |
|  | RHC250S－69D $\square$ | RHF280S－69D $\square$ | 1 | 350 | SC－N11 | 1 | 170M6548 | 3 |  |  |
|  | RHC280S－69D $\square$ | RHF355S－69D $\square$ | 1 | 400 | SC－N11 | 1 |  |  |  |  |
|  | RHC315S－69D $\square$ | RHF355S－69D $\square$ | 1 | 500 | SC－N12 | 1 |  |  |  |  |
|  | RHC355S－69D $\square$ | RHF450S－69D $\square$ | 1 | 500 | SC－N12 | 1 | 170M6500 | 3 |  |  |
|  | RHC400S－69D $\square$ | RHF450S－69D $\square$ | 1 | 600 | SC－N14 | 1 |  |  |  |  |

[^8]Note The "MCCB (ELCB) rated current" column shows the recommended rated current values at panel temperatures $50^{\circ} \mathrm{C}$ or lower.

* Since the ambient temperature is $40^{\circ} \mathrm{C}$, the installation environment standards for MCCBs or ELCBs have been selected taking into account the correction coefficient depending on the temperature conditions ( 0.90 for 800AF or lower; 0.85 for 1000AF or higher). To select a specific model, consider the short-circuit breaking capacity of the equipment.
[1] Refer to "6.2.12.3 Use of molded case circuit breakers (MCCBs)" and "6.2.12.4 Use of earth leakage circuit breakers (ELCBs)".


### 6.3.12.2 List of peripherals with no filter stack used

When configuring a transformer-less parallel system with RHC132S-4D $\square$ to RHC315S-4D $\square$, use the RHF-D series filter stacks to implement an input filter. You cannot implement a filter circuit by use of peripherals.
(1) In the case of MD

|  | RHC-D model | Charging circuit contactor |  | Main contactor |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (73) | $\begin{aligned} & \text { ? } \\ & \text { N } \\ & \text { N } \\ & 0 \end{aligned}$ | (52) | त त N O O |  |  |  |  |  |  |
| 132 | RHC132S-4D $\square$ | SC-N8 | 1 | SC-N8 | 1 |  |  |  |  |  |  |
| 160 | RHC160S-4D $\square$ | SC-N11 | 1 | SC-N11 | 1 |  |  |  |  |  |  |
| 200 | RHC200S-4D $\square$ | SC-N12 | 1 | SC-N12 | 1 |  |  |  |  |  |  |
| 220 | RHC220S-4D $\square$ |  |  |  |  |  |  |  |  |  |  |
| 280 | RHC280S-4D $\square$ | SC-N3 | 1 | SC-N14 | 1 |  |  |  |  |  |  |
| 315 | RHC315S-4D $\square$ |  |  |  |  |  |  |  |  |  |  |
| 630 | RHC630B-4D $\square$ |  |  | SC-N12 | 3 |  |  |  |  |  |  |
| 710 | RHC710B-4D $\square$ | SC-N4 | 1 |  |  |  |  |  |  |  |  |
| 800 | RHC800B-4D $\square$ |  |  | SC-N14 | 3 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | RHC-D model | Pressurizing reactor (Lr) |  | Resistor for filter (Rf) |  | Reactor for filter (Lf) |  | Capacitor for filter (Cf) | \# | Contactor for filter circuit (6F) |  |
| 132 | RHC132S-4D $\square$ | LR4-160C | 1 | RF4-160C | 1 | LFC4-160C | 1 | CF4-160C | 1 | - | - |
| 160 | RHC160S-4D $\square$ |  |  |  |  |  |  |  |  |  |  |
| 200 | RHC200S-4D $\square$ | LR4-220C | 1 | RF4-220C | 1 | LFC4-220C | 1 | CF4-220C | 1 |  |  |
| 220 | RHC220S-4D $\square$ |  |  |  |  |  |  |  |  |  |  |
| 280 | RHC280S-4D $\square$ | LR4-280C | 1 | RF4-280C | 1 | LFC4-280C | 1 | CF4-280C | 1 | SC-N4 | 1 |
| 315 | RHC315S-4D $\square$ | LR4-315C | 1 | RF4-315C | 1 | LFC4-315C | 1 | CF4-315C | 1 |  |  |
| 630 | RHC630B-4D $\square$ | LR4-630C | 1 | RF4-630C | 1 | LFC4-630C | 1 | CF4-630C *1 | 1 | SC-N7 *2 | 1 |
| 710 | RHC710B-4D $\square$ | LR4-710C | 1 | RF4-710C | 1 | LFC4-710C | 1 | CF4-710C *1 | 1 | SC-N8 | 1 |
| 800 | RHC800B-4D $\square$ | LR4-800C | 1 | RF4-800C | 1 | LFC4-800C | 1 | CF4-800C *1 | 1 |  |  |

*1 Two units of capacitors of the identical type will be delivered when an order is made for any of CF4-630C to CF4-800C for quantity $=$ " 1 ".
*2 When you apply OPC-VG7-SIR and use it in a transformer-less parallel system, change "(6F)" to "SC-N8".

## (2) In the case of LD

|  | RHC-D model | Charging circuit contactor |  | Main contactor |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (73) |  | (52) |  |  |  |  |  |  |  |
| 160 | RHC132S-4D | SC-N11 | 1 | SC-N11 | 1 |  |  |  |  |  |  |
| 200 | RHC160S-4D $\square$ | SC-N12 | 1 |  |  |  |  |  |  |  |  |
| 220 | RHC200S-4D $\square$ |  |  | SC-N12 | 1 |  |  |  |  |  |  |
| 315 | RHC280S-4D $\square$ | SC-N3 | 1 | SC-N14 | 1 |  |  |  |  |  |  |
| 355 | RHC315S-4D $\square$ |  |  |  |  |  |  |  |  |  |  |
| 710 | RHC630B-4D $\square$ | SC-N4 | 1 | SC-N12 | 3 |  |  |  |  |  |  |
| 800 | RHC710B-4D $\square$ |  |  | SC-N14 | 3 |  |  |  |  |  |  |
| 1000 | RHC800B-4D $\square$ |  |  | SC-N16 | 3 |  |  |  |  |  |  |
|  | RHC-D model | Pressurizing reactor (Lr) |  | Resistor for filter (Rf) | $\begin{gathered} \text { 空 } \\ \stackrel{\rightharpoonup}{T} \\ \text { OU } \end{gathered}$ | Reactor for filter (Lf) | $\begin{aligned} & \text { ? } \\ & \stackrel{\rightharpoonup}{2} \\ & \tilde{0} \\ & 0 \end{aligned}$ | Capacitor for filter (Cf) |  | Contactor for filter circuit (6F) | 2 L In O |
| 160 | RHC132S-4D | LR4-160C | 1 | RF4-160C | 1 | LFC4-160C | 1 | CF4-160C | 1 | - | - |
| 200 | RHC160S-4D $\square$ | LR4-220C | 1 | RF4-220C | 1 | LFC4-220C | 1 | CF4-220C |  |  |  |
| 220 | RHC200S-4D $\square$ |  |  |  |  |  |  |  | 1 |  |  |
| 315 | RHC280S-4D $\square$ | LR4-315C | 1 | RF4-315C | 1 | LFC4-315C | 1 | CF4-315C | 1 | SC-N4 | 1 |
| 355 | RHC315S-4D $\square$ | LR4-355C | 1 | RF4-355C | 1 | LFC4-355C | 1 | CF4-355C *1 | 1 |  |  |
| 710 | RHC630B-4D $\square$ | LR4-710C | 1 | RF4-710C | 1 | LFC4-710C | 1 | CF4-710C *1 | 1 | SC-N8 | 1 |
| 800 | RHC710B-4D $\square$ | LR4-800C | 1 | RF4-800C | 1 | LFC4-800C | 1 | CF4-800C *1 | 1 |  |  |
| 1000 | RHC800B-4D $\square$ | LR4-1000C | 1 | RF4-1000C | 1 | LFC4-1000C | 1 | CF4-1000C *1 | 1 | SC-N11/SF | 1 |

*1 Two units of capacitors of the identical type will be delivered when an order is made for any of CF4-630C to CF4-800C for quantity $=$ " 1 ".
Three units of capacitors of the identical type will be delivered when an order is made for any of CF4-1000C for quantity = "1".

### 6.3.12.3 Input power supply circuit (MCCB, ELCB)

| PWM converter (400V series) |  |  |  |
| :---: | :---: | :---: | :---: |
| Applicable <br> capacity [kW] | MD spec | LD spec | MCCB/ELCB rated current [A] |
| 132 | RHC132S-4D $\square$ | - | 300 |
| 160 | RHC160S-4D $\square$ | RHC132S-4D $\square$ | 350 |
| 200 | RHC200S-4D $\square$ | RHC160S-4D $\square$ | 500 |
| 220 | RHC220S-4D $\square$ | RHC200S-4D $\square$ | 500 |
| 280 | RHC280S-4D $\square$ | - | 600 |
| 315 | RHC315S-4D $\square$ | - | RHC280S-4D $\square$ |
| 355 | $R H C 630 B-4 D \square$ | $R H C 315 S-4 D \square$ | 700 |
| 630 | $R H C 710 B-4 D \square$ | - | 800 |
| 710 | $R H C 800 B-4 D \square$ | $R H C 630 B-4 D \square$ | 1400 |
| 800 | - | $R H C 800 B-4 D \square$ | 1600 |
| 1000 |  |  | 1800 |

The "MCCB (ELCB) rated current" column shows the recommended rated current values at panel temperatures $50^{\circ} \mathrm{C}$ or lower.

* Since the ambient temperature is $40^{\circ} \mathrm{C}$, the installation environment standards for MCCBs or ELCBs have been selected taking into account the correction coefficient depending on the temperature conditions ( 0.90 for 800 AF or lower; 0.85 for 1000AF or higher). To select a specific model, consider the short-circuit breaking capacity of the equipment.
[1] Refer to "6.2.12.3 Use of molded case circuit breakers (MCCBs)" and "6.2.12.4 Use of earth leakage circuit breakers (ELCBs)".


### 6.3.13 Parallel system (capacity expansion)

A "parallel system" means that multiple PWM converters are connected in parallel to increase the total capacity of the converters. For example, when three 200 kW PWM converters are driven in parallel, this converter parallel system can produce an output power up to 600 kW or equivalent.
Controlling a parallel system requires the use of the optical link option card for parallel systems (OPC-VG7-SIR) so that each individual converter can be controlled in terms of synchronous behavior and load current balancing.
A parallel system is characterized by the following:
(1) If a PWM converter failure occurs during parallel operation of two PWM converters and one converter stops, the reduced capacity operation with the other remaining converter can be made (single converter operation).
(2) There are two kinds of parallel systems: transformer-less connection and transformer insulation connection. Select a desired system.

Note To connect PWM converters in parallel (so that all of them have the same output voltage), ensure that they all have the same capacity.

### 6.3.13.1 Transformer-less parallel system

In this system, the input to each PWM converter is not insulated by a transformer or the like and the PWM converters are connected to the same power supply system.

- Unit type is a dedicated product.
(RHC $\square-4 C R$ * Standard equipment for the OPC-VG7-SIR)
- The OPC-VG7-SIR (option) allows the use of the stack type.

Table 6.3.13-1: Transformer-less parallel system control specifications

| Item | Specifications |  |
| :--- | :--- | :---: |
|  | Unit | Stack |
| Applicable converter | CT spec only | MD spec, LD spec |
| Max. number of <br> converters connected <br> in parallel | 3 units (Master: 1 unit, Slave: 2 units) |  |
| Output voltage | Fixed at 710 VDC |  |
| Carrier frequency | 5 kHz |  |
| Input power supply ${ }^{* 1}$ | 3-phase 380 to $440 \mathrm{~V} \mathrm{50/60} \mathrm{~Hz}$ |  |
| Input power factor | Approx. $0.94(30 \%$ or more load) |  |

*1 When the input power supply voltage is less than 400 V , the capacity needs to be reduced.


Figure 6.3.13-1: Transformer-less parallel system connection diagram

### 6.3.13.2 Transformer insulation type parallel system

This system insulates the input to the PWM converter by use of a transformer.

Use the OPC-VG7-SI optical link option card.
Table 6.3.13-2: Transformer insulation type parallel system control specifications

| Item | Specifications |  |
| :--- | :--- | :---: |
|  | Unit | Stack |
| Applicable converter | CT spec, VT <br> spec | MD spec, LD spec |
| Max. number of <br> converters connected <br> in parallel | 6 units (Master: 1 unit, Slave: 5 units) |  |
| Output voltage | 640 to 710 VDC |  |
| Carrier frequency | Same as rating <br> specifications. | 5 kHz |
| Input power supply *1 | 400 V series: <br> $3-$ phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}$, <br> 380 to $460 \mathrm{~V} / 60 \mathrm{~Hz}$ |  |
| Input power factor | Approx. $0.99\left(100 \%\right.$ or more load) ${ }^{* 2}$ |  |



DC bus (INV-DC input)
Figure 6.3.13-2: Transformer insulation type parallel system connection diagram

### 6.3.13.3 Parallel system common specifications

Table 6.3.13-3: Specifications common to both "transformer-less" and "transformer insulation type" parallel systems

| Item |  | Specifications |
| :---: | :---: | :---: |
| Parallel control method |  | AVR constant control with DC ACR minor |
| Input harmonic current |  | Conversion coefficient Ki can be set to zero (0) according to the harmonics suppressing guideline by METI. |
| Restart after momentary power failure |  | When a momentary power failure occurs, the gate is shut off at the insufficient voltage level, and the converter resumes operation automatically following recovery. |
| Control function |  | A part of the slave unit functions is restricted. *1 |
|  | Data transmission method | Asynchronous serial communication through plastic optical fiber (loop-back method) |
|  | Transmission rate | 1 Mbps |
|  | Error check method | Parity, framing, overrun, BCC, or time-out monitor |
|  | Max. optical cable length (Transmission distance) | $20 \mathrm{~m}\left(0\right.$ to $\left.70^{\circ} \mathrm{C}\right)$ - If the wiring length exceeds 20 m , the communication cannot be guaranteed due to transmission loss. <br> * Optical cable supplied with OPC-VG7-SI $\square$ as standard: 5 m ( 10 m or 15 m cable should be ordered separately.) |
|  | Erb alarm process (Erb: Link error) | All PWM converters in the parallel system are stopped when an alarm output (30A/B/C) is received. *2 |
|  | Process if protective function operates | All PWM converters in the parallel system are stopped when an alarm output (30A/B/C) is received. ${ }^{* 2}$ <br> When 30A/B/C is operated, all the PWM converters should be forcibly stopped via an external sequence to ensure the safety. |
|  | Protective function reset process | When a reset command is sent to a desired PWM converter connected through the optical link option card, all the other PWM converter are also reset at the same time (when the cause of the alarm is removed). |

*1 The function code setting is restricted as follows.
The master can be set in the same manner as the standard product except for carrier frequency setting (F08). However, the slave functions are restricted.

凹】 For details, refer to the instruction manuals listed below.

$$
\begin{array}{ll}
\text { • RHC-C series } & \text { Optical link option for parallel system (OPC-VG7-SI): INR-HF52179 } \\
\text { • RHC-C series } & \text { Optical link option for transformer-less parallel system (OPC-VG7-SIR): INR-HF51998 } \\
\text { - RHC-D series } & \text { High-efficiency power regeneration PWM converter (stack type): INR-SI47-1722 }
\end{array}
$$

*2 For more information on the any alarm protective operation for all the converters in parallel system:
@ Refer to "(3) If the protective function operates [Parallel system: OPC-VG7-SI/OPC-VG7-SIR is used.]" in "6.3.10.2 Troubleshooting".

## (1) Optical fiber cable connection

The optical fiber cable plug colors at both ends are Table 6.3.13-4: Connectors on the optical link option card different from each other (gray and blue).
Connect each optical fiber cable to the same-colored connector on the optical link option card. The connection is performed so that the entire connection is looped.

| Part number | Name | Color | Overview |
| :--- | :--- | :--- | :--- |
| T-1528 | TX | Gray | Transmitter (optical <br> communication send) |
| R-2528 | RX | Blue | Receiver (optical <br> communication receive) |



Figure 6.3.13-3: Example of optical fiber cable connections

Table 6.3.13-5: Max. absolute rating of plastic fiber cable

| Item | Mini <br> mum | Maxi <br> mum | Unit | Remarks |
| :--- | :--- | :--- | :--- | :--- |
| Storage temperature <br> range | -40 | +75 | ${ }^{\circ} \mathrm{C}$ |  |
| Tension |  | 50 | N | 30 min. or less |
| Short-time bending <br> radius | 10 | - | mm | Operation stops within 1 hr . and "Erb" alarm is given. |
| Long-time bending <br> radius | 35 | - | mm | If the cable is bent to a radius of 35 mm or less for a long time, "Erb" <br> alarm may be given. <br> Be sure to keep that the bending radius is 35 mm or more. |
| Tensile strength (long <br> time) | - | 1 | N |  |
| Flexibility | - | 1000 | times | Bent $90^{\circ}$ on 10 mm-mandrel (mandrel, spindle). |
| Impact | - | 0.5 | kg | Impact test shall conform to MIL-1678, Method2030, Procefurel. |

### 6.3.13.4 Configuration table for transformer-less parallel system

You can implement a redundant system with a greater capacity by connecting two or three converters that have the same capacity in parallel.
Table 6.3.13-6 to Table 6.3.13-8 provides a list of typical combinations but other configurations are also possible.
Table 6.3.13-6: Example of combinations in a transformer-less parallel system
(in the case of the 400 V series in the MD spec mode)

| Connected system | Single unit |  |  | Phase-specific |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| Capacity (kW) | Applicable converter | Applicable converter | Number of units | Applicable converter | Applicable converter | Number of units |
| 132 | RHC132S-4D $\square$ |  |  |  |  |  |
| 160 | RHC160S-4D $\square$ |  |  |  |  |  |
| 200 | RHC200S-4D $\square$ |  |  |  |  |  |
| 220 | RHC220S-4D $\square$ |  |  |  |  |  |
| 280 | RHC280S-4D $\square$ |  |  |  |  |  |
| 315 | RHC315S-4D $\square$ |  |  |  |  |  |
| 355 |  | RHC200S-4D $\square$ | 2 |  |  |  |
| 400 |  | RHC200S-4D $\square$ | 2 |  |  |  |
| 500 |  | RHC280S-4D $\square$ | 2 |  |  |  |
| 630 |  | RHC315S-4D $\square$ | 2 | RHC630B-4D $\square$ |  |  |
| 710 |  | RHC280S-4D $\square$ | 3 | RHC710B-4D $\square$ |  |  |
| 800 |  | RHC280S-4D $\square$ | 3 | RHC800B-4D $\square$ |  |  |
| 1000 |  |  |  |  | RHC630B-4D $\square$ | 2 |
| 1200 |  |  |  |  | RHC630B-4D $\square$ | 2 |
| 1500 |  |  |  |  | RHC800B-4D $\square$ | 2 |
| 1800 |  |  |  |  | RHC630B-4D $\square$ | 3 |
| 2000 |  |  |  |  | RHC710B-4D $\square$ | 3 |
| 2400 |  |  |  |  | RHC800B-4D $\square$ | 3 |

[^9]Table 6.3.13-7: Example of combinations in a transformer-less parallel system (in the case of the 400 V series in the LD spec mode)

| Connected system | Single unit |  |  | Phase-specific |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| Capacity (kW) | Applicable converter | Applicable converter | Number of units | Applicable converter | Applicable converter | Number of units |
| 160 | RHC132S-4D $\square$ |  |  |  |  |  |
| 200 | RHC160S-4D $\square$ |  |  |  |  |  |
| 220 | RHC200S-4D $\square$ |  |  |  |  |  |
| 280 |  |  |  |  |  |  |
| 315 | RHC280S-4D $\square$ |  |  |  |  |  |
| 355 | RHC315S-4D $\square$ |  |  |  |  |  |
| 400 |  | RHC160S-4D $\square$ | 2 |  |  |  |
| 500 |  | RHC280S-4D $\square$ | 2 |  |  |  |
| 630 |  | RHC280S-4D $\square$ | 2 |  |  |  |
| 710 |  | RHC315S-4D $\square$ | 2 | RHC630B-4D $\square$ |  |  |
| 800 |  | RHC280S-4D $\square$ | 3 | RHC710B-4D $\square$ |  |  |
| 1000 |  | RHC315S-4D $\square$ | 3 | RHC800B-4D $\square$ |  |  |
| 1200 |  |  |  |  | RHC630B-4D $\square$ | 2 |
| 1500 |  |  |  |  | RHC710B-4D $\square$ | 2 |
| 1800 |  |  |  |  | RHC800B-4D $\square$ | 2 |
| 2000 |  |  |  |  | RHC800B-4D $\square$ | 2 |
| 2400 |  |  |  |  | RHC710B-4D $\square$ | 3 |
| 3000 |  |  |  |  | RHC800B-4D $\square$ | 3 |

*1 Requires the option OPC-VG7-SIR.
*2 To connect PWM converters in parallel (so that all of them have the same output), ensure that they all have the same capacity.

Table 6.3.13-8 Example of combinations in a transformer-less parallel system (in the case of the 690V series)

| Connected system | MD spec |  |  | LD spec |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| Capacity (kW) | Applicable converter | Applicable converter | Number of units | Applicable converter | Applicable converter | Number of units |
| 132 | RHC132S-69D $\square$ |  |  | - | - | - |
| 160 | RHC160S-69D $\square$ |  |  | RHC132S-69D $\square$ |  |  |
| 200 | RHC200S-69D $\square$ |  |  | RHC160S-69D $\square$ |  |  |
| 250 | RHC250S-69D $\square$ |  |  | RHC200S-69D $\square$ |  |  |
| 280 | RHC280S-69D $\square$ |  |  | RHC250S-69D $\square$ |  |  |
| 315 | RHC315S-69D $\square$ |  |  | RHC280S-69D $\square$ |  |  |
| 355 | RHC355S-69D $\square$ |  |  | RHC315S-69D $\square$ |  |  |
| 400 | RHC400S-69D $\square$ |  |  | RHC355S-69D $\square$ |  |  |
| 450 | RHC450S-69D $\square$ |  |  | RHC400S-69D $\square$ |  |  |
| 500 |  | RHC250S-69D $\square$ | 2 |  | RHC250S-69D $\square$ | 2 |
| 630 |  | RHC315S-69D $\square$ | 2 |  | RHC280S-69D $\square$ | 2 |
| 710 |  | RHC355S-69D $\square$ | 2 |  | RHC315S-69D $\square$ | 2 |
| 800 |  | RHC400S-69D $\square$ | 2 |  | RHC355S-69D $\square$ | 2 |
| 1000 |  | RHC355S-69D $\square$ | 3 |  | RHC315S-69D $\square$ | 3 |
| 1200 |  | RHC400S-69D $\square$ | 3 |  | RHC355S-69D $\square$ | 3 |
| 1350 |  | RHC450S-69D $\square$ | 3 |  | RHC400S-69D $\square$ | 3 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

*1 Requires the option OPC-VG7-SIR.
*2 To connect PWM converters in parallel (so that all of them have the same output), ensure that they all have the same capacity.

### 6.3.13.5 Parallel system connection diagram



Figure 6.3.13-4: Parallel system connection diagram


Figure 6.3.13-5: Converter run command sequence (1)
(4) The alarms of all PWM converters (units) can be simultaneously reset by inputting the [RST] signal from any unit. When switched to the single unit system, only the unit that inputs the [RST] signal is to be reset.
(5) When using the parallel/single unit system switching function, assign [OPT-DI] to the contact input of X1. Configure a sequence circuit where the [OPT-DI] signal is input and the run command bypasses the alarm circuits other than those for the single unit operation unit and inputs to only the single unit operation unit when switching to the single unit system.
(6) Input the run and stop commands to both the master and slave units.
(7) The run and stop commands are the same as the standard model.


Figure 6.3.13-6: Converter run command sequence (2)

### 6.3.13.6 Charging circuit in parallel system

When only one charging circuit is used for the parallel system or when the PWM converter has the reduced unit (single unit) operation mode, select an appropriate charging circuit (charging resistor and electromagnetic contactor) based on the capacity calculated using Equation 6.3.13-1

- Calculate the total capacity of the PWM converters and inverters connected to the DC bus bar (PN)
- After that, the total capacity is multiplied by " $1 / 2$ ". Select the appropriate charging resistor ( R 0 ) and electromagnetic contactor (73) from the appropriate PWM converter capacity stated in "6.3.12.2 List of peripherals with no filter stack used" according to the calculated capacity.

$$
P_{(C H G)}=\frac{1}{2} \times \sum\left(P_{C N V}+P_{I N V}\right) \cdots \text { Equation 6.3.13-1 }
$$



Figure 6.3.13-7: Parallel system configuration (such as configured by one charging circuit)

### 6.3.14 System configuration examples

| No | System configuration diagram <br> (Symbols in diagram) <br> F: Filter circuit or filter stack (RHF-D) <br> C: PWM converter (RHC-C,RHC-D) <br> I: Inverter, TBSI, SI, SIR: Optical communication card | System configuration | Filter stack (RHF-D) application *1 | Filter circuit (peripheral equipment) application |
| :---: | :---: | :---: | :---: | :---: |
| 1 |  | $\odot$ Applicable <br> C: Up to 6 units I: Up to 6 parallel sets | Applicable | Unit type (RHC-C) <br> - Applicable <br> Stack type (RHC-D) <br> - RHC132S to 315S-4D $\Rightarrow$ X Not applicable ( ${ }^{*}$ ) <br> - RHC630B to 800B-4D $\Rightarrow$ - Applicable |
| 2 |  | X Not applicable (For direct parallel connection, use No.3.) | - | - |
| 3 |  | $\odot$ Applicable C: Up to 6 parallel sets I: Up to 3 parallel sets | Applicable |  |
| 4 |  | $\odot$ Applicable C: Up to 6 units I: Up to 6 parallel sets | Applicable | - RHC630B to 800B-4D $\Rightarrow \odot$ Applicable |
| 5 |  | X Not applicable (To ensure that all the PWM converters have the same output, use No.7.) | - | - |
| 6 |  | X Not applicable (To ensure that all the PWM converters have the same output, use No.8.) | - | - |

*1 The filter stacks (RHF-D) are dedicated to the use with stack type PWM converters (RHC-D). It cannot be used with unit type PWM converters (RHC-C).
*2 There are restrictions on the use of a filter circuit (peripheral equipment) with stack type PWM converters (RHC-D). Refer to "6.3.12.2 List of peripherals with no filter stack used".
(Note 1) When using any of the above in direct parallel connection and multi-winding driving systems, ensure that all the inverters have the same capacity.
(Note 2) When a single PWM converter is used to drive multiple inverters, ensure that the PWM converter capacity is equal to or greater than the inverter capacity (total).
(Note 3) When a motor is run in a direct parallel connection system, there is a restriction on the wiring length of motor. Refer to "9.4.8 Wiring inductance" in Chapter 9.
(Note 4) Be sure to turn ON the main power to all the PWM converters at once.

| No | System configuration diagram <br> (Symbols in diagram) <br> F: Filter circuit or filter stack (RHF-D) <br> C: PWM converter (RHC-C,RHC-D) <br> I: Inverter, TBSI, SI, SIR: Optical communication card | System configuration | Filter stack <br> (RHF-D) <br> application ${ }^{* 1}$ | Filter circuit (peripheral equipment) application |
| :---: | :---: | :---: | :---: | :---: |
| 7 |  | $\odot$ Applicable C: Up to 3 parallel sets I: Up to 6 parallel sets | Applicable | Unit type (RHC-C) <br> - Applicable <br> Stack type (RHC-D) <br> - RHC132S to 315S-4D <br> $\Rightarrow$ X Not applicable ${ }^{*}{ }^{2}$ ) <br> - RHC630B to 800B-4D $\Rightarrow$ - Applicable |
| 8 |  | $\odot$ Applicable C: Up to 3 parallel sets I: Up to 3 parallel sets | Applicable | Unit type (RHC-C) <br> - Applicable <br> Stack type (RHC-D) <br> - RHC132S to 315S-4D $\underset{(2)}{\Rightarrow}$ Not applicable ${ }^{*}{ }^{2}$ ) |
| 9 |  | - Applicable I: Up to 6 parallel sets | Applicable | - RHC630B to 800B-4D $\Rightarrow$ Applicable |
| 10 |  | $\odot$ Applicable I: Up to 3 parallel sets | Applicable |  |

*1 The filter stacks (RHF-D) are dedicated to the use with stack type PWM converters (RHC-D). It cannot be used with unit type PWM converters (RHC-C).
*2 There are restrictions on the use of a filter circuit (peripheral equipment) with stack type PWM converters (RHC-D). Refer to "6.3.12.2 List of peripherals with no filter stack used".
(Note 1) When using any of the above in direct parallel connection and multi-winding driving systems, ensure that all the inverters have the same capacity.
(Note 2) When a single PWM converter is used to drive multiple inverters, ensure that the PWM converter capacity is equal to or greater than the inverter capacity (total).
(Note 3) When a motor is run in a direct parallel connection system, there is a restriction on the wiring length of motor. Refer to "9.4.8 Wiring inductance" in Chapter 9.
(Note 4) Be sure to turn ON the main power to all the PWM converters at once.
Note To connect PWM converters in parallel (so that all of them have the same output), ensure that they all have the same capacity.

### 6.3.15 Wiring

### 6.3.15.1 Precautions on wiring

## (1) Main circuit (L1/R, L2/S, L3/T)

## When installing filter stacks (RHF-D series)

The main circuit's power supply terminals L1/R, L2/S, and L3/T should be connected to the filter stack's terminals U1, V1, and W1.

## When not installing filter stacks (RHF-D series)

The main circuit's power supply terminals L1/R, L2/S, and L3/T should be connected to the power supply through the charging circuits (R0, 73), pressurizing reactor (Lr), filter circuits (Lf/Rf/Cf), contactor for power supply (MC), and molded case circuit breaker (MCCB).
Install the charging circuit box, if applicable, between the power supply terminals ( $\mathrm{L} 1 / \mathrm{R}, \mathrm{L} 2 / \mathrm{S}, \mathrm{L} 3 / \mathrm{T}$ ) and the electromagnetic contactor for the charging circuit. Do not connect any other device (such as a zero-phase reactor) between the charging circuit box and any of $L 1 / R, L 2 / S, L 3 / T, R 2$, and $T 2$.

The wirings of the filter circuit, pressurizing reactor, and charging circuit should be connected as illustrated in Figure 6.3.15-1.
The same circuit configuration is also used for the capacity range that uses the charging box. Additionally, an MCCB or electromagnetic contactor (MC) should be used to ensure that the main circuit can be separated from the power supply system when the protective function of the PWM converter or inverter operates (alarm trip)


Figure 6.3.15-1: Main input circuit of PWM converter for some reason.

Note (1) If the wiring is connected incorrectly, the PWM converter does not operate correctly, possibly causing damage to each unit.
(2) The pressurizing slightly generates electromagnetic sound due to high frequency current flowing through it.
If this electromagnetic sound is undesirable, store the boosting reactor into the cabinet.

## 1) Capacitor for filter

The wiring length between the filter capacitor and filter reactor must be 5 m or less.

Note The effect of the filter may decrease due to the effect of the wiring inductance.

The filter resistor generates the heat during PWM converter operation. Even when the inverter stops, the PWM converter performs the constant power factor control as the PWM converter operates.
The surface temperature of this resistor may reach approx. $100^{\circ} \mathrm{C}$. So, it is recommended to install the filter resistor on the cabinet ceiling (cabinet exterior).
( Refer to "12.5.2 Principles in designing layout in cabinets" in Chapter 12.)
When storing the filter resistor into the cabinet, heat radiation measures must be investigated sufficiently. (Investigate a structure where the heat of the filter resistor does not adversely affect units stored inside the cabinet.)

## (2) Main circuit ( $\mathbf{P}(+), \mathrm{N}(-))$

Connect the converter output terminals $(\mathrm{P}(+), \mathrm{N}(-))$ to the inverter DC input terminals $(\mathrm{P}(+), \mathrm{N}(-))$. Bus bar connections are assumed. When connecting by wire, ensure that the distance between the stacks (i.e., between the PWM converter and inverter) is within 2 meters.
Similarly, when connecting wires to a branch line or terminal of the DC bus bar, ensure that the wiring length is within 2 meters and that the wires are in close contact (or twisted).


Figure 6.3.15-3: Connecting P and N terminals by wires


Figure 6.3.15-4: Connecting P and N terminals by bus bars

## (3) Grounding

To ensure the safety and take noise prevention measures, be sure to ground the grounding terminals $\boldsymbol{\theta}$ of the PWM converter and inverter. In the Electrical Equipment Technical Standards, it is instructed to perform the grounding to the metallic frame of the electrical equipment so as to prevent accidents, such as electric shock or fire.
To connect the terminal, follow the steps below.

1) Connect to grounding electrodes on which class C grounding work ( 400 V series) or class A grounding work ( 690 V series) has been carried out in accordance with the Electrical Equipment Technical Standards.
2) Connect a thick wire to the grounding terminal with a short distance and connect the grounding terminal to the grounding pole dedicated to the inverter system.
For details, refer to "6.3.15.2 Wire size".

## (4) Control Circuit

## 1) $R 1, S 1$, and $T 1$ terminals

Since the R1, S1, and T1 terminals are intended to input the reference signal of the converter, connect a filter reactor (Lf) without waveform distortion to the power supply side. The wiring length must be 5 m or less.
2) Digital input terminals (RUN, X1, RST, PLC, CM)
(1) The digital input terminals are turned ON or OFF by the CM terminal.
On the other hand, when the digital input terminals are turned ON or OFF by the open collector output of the programmable controller (PLC) using the external power supply, they may malfunction due to round-about leakage circuit.
In this case, use the PLC terminal to make the connection as illustrated in Figure 6.3.15-6.
(2) When inputting using the relay contact, use a contact (high contact reliability) that does not cause any contact fault. Example: Fuji Electric's control relay HH54PW


Figure 6.3.15-5: Connection of voltage detection terminal


Figure 6.3.15-6: Prevention of round-about leakage by external power supply


Figure 6.3.15-7: Amplification of the contact capacity and the number of contacts

These are control output signals for the charging circuit. Wire these signals, referring to the basic connection diagram.

## 6) Charging circuit drive input (RHF-D series filter stacks) (73-1, 73-2)

These are control input signals for the charging circuit. Wire these signals, referring to the basic connection diagram.

## 7) Sequence circuit

The breaker on the power supply side may trip depending on the failure contents of the PWM converter stack. In the standard circuit configuration, the sequence circuit is connected from the secondary side of the MCCB to the auxiliary power supply circuit. So, the auxiliary power supply is also shut down.
In this case, the failure status is not retained. As the breaker is turned ON next, and the contactor is turned ON, the damage inside the converter may expand. To prevent expansion of damage, it is recommended to retain the alarm signal of the PWM converter using the keep relay.
Additionally, a configuration needs to be investigated that stops the operation of the converter by taking the safety into consideration if the protective function on the inverter stack side operates (alarm trip).



Figure 6.3.15-8: Example of sequence configuration

## (5) Auxiliary control power input (R0, T0) and fan power input (CNV: R3, T3 INV: R1, T1)

The wiring to the "R0, T0" "R1, T1" and "R3, T3" terminals may vary depending on the applicable inverter/PWM converter. As described in the group shown in
Table 6.3.15-1, perform the wiring according to the applicable inverter/PWM converter.
Groups D and E apply to the configuration that connects the stack type inverter and PWM converter stack. This section describes group $E$.

Table 6.3.15-1: Wiring to R0 and T0 terminals

| Group | Applicable inverter/converter | Wiring to R0 and T0 Terminals |
| :---: | :--- | :--- |
| A | FRN22G11S- $\square$ or less, FRN22P11S- $\square$ or less <br> FRN15VG7S- $\square$ or less <br> FRN500BVG7S-4DC to FRN800BVG7S-4DC <br> FRN30G1S-2 or less, FRN55G1S-4 or less <br> FRN37F1S-2 or less, FRN45F1S-4 or less | Insert the "b" contact of the contactor (52 or 73) to the <br> wiring to R0, T0. |
| B | FRN30G11S- $\square$ or more, FRN30P11S- $\square$ or more <br> FRN18.5VG7S- $\square$ or more | Switch "CN RXTX" inside the inverter. <br> (For details, refer to the instruction manual for the <br> inverter. $)$ |
| C | FRN37G1S-2 or more, FRN75G1S-4 or more <br> FRN45F1S-2 or more, FRN55F1S-4 or more | Insert the "b" contact of the isolation transformer or <br> contactor (52 or 73) to the wiring to R0, T0. |
| D | INV: FRN30SVG1S-4 to FRN75SVG1S-4 | Insert the "b" contact of the isolation transformer or <br> contactor (52 or 73) to the wiring to R0, T0. |
| E | INV:FRN90SVG1S-4 or more <br> FRN: <br> FRN90SVG1S-69 or more | RHC132S-4D or more <br> RHC132S-69D or more |

Table 6.3.15-2: Wiring to CNV terminals R3 and T3 and to INV terminals R1 and T1

| Group | Applicable inverter | Wiring to the "R1, T1" and "R3, T3" terminals |
| :---: | :---: | :---: |
| C | FRN37G1S-2 or more, FRN75G1S-4 or more FRN45F1S-2 or more, FRN55F1S-4 or more | Switch "CN R"/"CN W" inside the inverter. (For details, refer to the instruction manual for the inverter.) |
| D | INV: FRN30SVG1S-4 to FRN75SVG1S-4 | No fan power supply is needed. Since the fan to be used is a DC fan, the power is supplied from the power supply inside each stack. |
| E | INV: FRN90SVG1S-4 or more FRN90SVG1S-69 or more <br> CNV: RHC132S-4D or more RHC132S-69D or more | The wiring is needed. <br> - Switch the "U1, U2" connector switch in each stack according to the power voltage specifications. <br> [1] Refer to "4.5.3 Wiring of main circuit and grounding terminals" in Chapter 4. |

Even when the power supply is not input to the auxiliary control power input (R0, TO) terminals, the PWM converter or inverter can be operated. However, if the main power is turned off, the control power will also be shut down, and output signals of the PWM converter and inverter and the keypad will be no longer displayed. To retain an alarm output signal to be issued when the protective function operates or keep the keypad displayed even if the main power is shut down, connect the DC power supply to the auxiliary control power input terminals.
[R0 and T0 terminal ratings]

- 400 V series: 380 to $480 \mathrm{VAC}, 50 / 60 \mathrm{~Hz}$, maximum current: 0.5 A
-690V series: 575 to $690 \mathrm{VAC}, 50 / 60 \mathrm{~Hz}$, maximum current: 0.5 A
When adding an isolation transformer, select the appropriate isolation transformer based on the sum of the required capacities of the inverter and PWM converter, referring to the following tables:
- Required transformer capacity for the inverter (FRENIC-VG)

- Required transformer capacity for the converter (RHC-D series)

| Model | 132S | 160S | 200S | 220S | 250S | 280S | 315S | 355S | 400S | 450S | 500S | 630B | 710B | 800B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RHC $\square$-4D $\square$ | 200VA |  |  |  | - | 200VA |  | - |  |  |  | 600VA |  |  |
| RHCD-69D $\square$ | 200VA |  |  | - | 200VA |  |  |  |  |  | - |  |  |  |

[CNV: R3 and T3 terminal ratings, INV: R1 and T1 terminal ratings]

- 400 V series: 380 to $440 \mathrm{VAC} / 50 \mathrm{~Hz}, 380$ to $480 \mathrm{VAC} / 60 \mathrm{~Hz}$, Maximum current: 1.0 A
(For phase-specific stacks, the maximum current is 3 times larger than above.)
-690V series: 660 to 690 VAC, $50 / 60 \mathrm{~Hz}$, maximum current 1.0 A
575 to $600 \mathrm{VAC}, 50 / 60 \mathrm{~Hz}$, maximum current 1.0 A
■ Inverter (FRENIC-VG) - Rated capacity of terminals R1 and T1

| Model | 90S | 110S | 132S | 160S | 200S | 220S | 250S | 280S | 315S | 355S | 400S | 450S | 630B | 710B | 800B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FRN $\square$ VG1S-4 $\square$ | 100 VA |  |  |  |  | 200 VA |  |  |  | - |  |  | 600 VA |  |  |
| FRN $\square$ VG1S-69■ | 100 VA |  |  |  |  | - | 200 VA |  |  |  |  |  | - |  |  |

## - Converter (RHC-D series) - Rated capacity of terminals R3 and T3

| Model | 132S | 160S | 200S | 220S | 250S | 280S | 315S | 355S | 400S | 450S | 500S | 630B | 710B | 800B |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RHCD-4D $\square$ | 100VA |  |  | 200VA | - | 200VA |  | - |  |  |  | 600VA |  |  |
| RHCD-69D $\square$ | 100VA |  |  | - | 200VA |  |  |  |  |  | - |  |  |  |

## If the fan power input is the same as the main power supply

PWM converters and inverters contain internal parts (such as the AC fan) that operate on the AC power. Therefore, "R3 and T3" terminals of a PWM converter and "R1 and T1" terminals of an inverter must be supplied with AC power.
Note that the PWM converters or inverters belonging to group D do not need this fan power supply.
 terminals" in Chapter 4.
Figure 6.3.15-9: Example of connections when supplying fan power from the same system as main power supply
$\qquad$ 1

Figure 6.3.15-9 shows that the fan power supply is supplied at the same time when the PWM converter becomes ready to run.
There is no problem even when the connection is made from the primary side of the same MC as the synchronous power supply detection. In this case, if the fan ON/OFF control function setting of the PWM converter or inverter is set to the factory default ("disabled"), you can operate the fan by just turning ON the MCCB.
From view points of the energy saving and fan service life, it is recommended to change the function or construct the circuit as illustrated in the Figure.

Note
If the fan power supply switching connector is set incorrectly, the cooling fan does not operate at correct RPM and required air volume cannot be obtained. As a result, the overheat ( OH 1 ) or overload (OU1) protective function of the converter or inverter may operate (alarm trip).

## Cautions on application to non-grounding system power supply

If a ground fault accident occurs on the inverter output side when the power receiving voltage system of the PWM converter is not grounded, a round-about leakage circuit may be constructed through the grounding. If this round-about leakage circuit is constructed, this may cause damage to the control power supply circuit of the PWM converter or inverter.
When using such non-grounding system power supply, use an insulation transformer for the input to the auxiliary control power input terminal of the PWM converter or inverter as illustrated in Figure 6.3.15-10 to insulate the power receiving voltage.
When insulating with the insulation transformer, it is not necessary to insert the "b"-contact of the MC.
Additionally, if the power supply system is not clear, it is also recommended to install the transformer in the same manner.


Figure 6.3.15-10: Example of connections with insulation transformer installed
Note When connecting an earth leakage circuit breaker (ELCB), connect the terminals R0 and T0 to the primary side (power supply side) of the earth leakage circuit breaker.
If connected to the secondary side of the earth leakage circuit breaker, the earth leakage circuit breaker may malfunction since the terminals R0 and T0 of the main power supply inputs of the PWM converter (L1/R to $L 3 / T$ ) are single phase in response to three-phase inputs. When connecting terminals R0 and T0 to the primary side of the earth leakage circuit breaker, be sure to connect the transformer for insulation or the auxiliary "b" contact of the electromagnetic contactor (MC) to the position illustrated in the figure below.

* The following figure describes the PWM converter as an example. For a diode rectifier, perform also the connections in the same manner.


Figure 6.3.15-11: Connection of earth leakage circuit breaker (ELCB)

## (6) Other cautions

Be sure to connect to a power supply with required power supply capacity or more stated in "6.3.2 Standard specifications".
If the power supply capacity is smaller than required, the initial charging cannot be performed correctly (power supply is failed) or the protective function of the PWM converter or inverter may operate (alarm trip) due to waveform distortion on the power supply side.
Additionally, if a small capacity transformer is used for the sequence check inside the cabinet, the similar problem may occur. In such case, open (turn OFF) the portion between the "RUN and CM" of the PWM converter, and perform the sequence check of other parts.

### 6.3.15.2 Wire size

The wire size of the main circuit can be calculated based on the equations shown below.
$I_{A C}=\frac{k V A}{\sqrt{3} \times \operatorname{Vin} \times \cos \theta} \quad[A] \cdots \quad$ Equation 6.3.15-1
$I_{\text {filt }}=$ Total r.m.s. value of filter capacitor
$I_{D C}=\frac{P_{C N V}}{V d c}[A] \cdots \cdots \quad$ Equation 6.3.15-2
$I_{C H G}=\frac{\operatorname{Vin}}{\sqrt{3} \times R 0}\left[A_{p-p}\right] \cdots . \quad$ Equation 6.3.15-3

Note Design a structure where the portion from the output of the PWM converter to the DC bus bar is connected with the Cu bar as much as possible.
Additionally, when using a wire, the wiring length must be $\underline{\mathbf{2}}$ mor less.

```
- IAC : PWM converter input current [A]
- Ifilt : Filter circuit current [A]
-IDC : PWM converter output current [A]
- ICHG : Charging circuit current [Ap-p]
```

The reactance components for the capacitor inside the PWM converter or inverter are not taken into consideration. Additionally, as the charging completion time is 1 sec . or less, select an wire with a short-time capacity (12t). (Charging time: 0.5 sec .)

- kVA : Required power capacity of PWM converter [kVA]
- Vin : Input voltage of PWM converter [V]
- $\cos \theta$ : Input power factor of PWM converter
- Pcnv : Rated capacity of PWM converter [kW]
- Vdc : Output voltage of PWM converter [V]
-R0 : Charging resistance [ $\Omega$ ]
<Precautions for selecting wire (for all types)>
Note (1) An "IV wire," a "600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.
(2) Wire size is selected at supply voltage of 400 VAC.
(3) The wire size of the charging circuit is calculated based on the short-time allowable current.
(4) The grounding wire is cited from the permissible short circuit current defined in internal wire regulations.
(5) RHC630B to 800B-4D $\square$ is phase-by-phase stack type (single-phase composition per stack). Therefore, wire connected per stack is given here.


## （1）3－phase 400 V series（MD spec）

## 1）Ambient temperature： $40^{\circ} \mathrm{C}$

| RHC $\square$－4D $\square$ | Main input（including peripheral equipment） |  |  |  |  | Resistance circuit for filter |  |  |  | Charging circuit |  |  | Output：P（＋），N（－） |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature （Note 1） |  |  | Bus bar size ［ $\mathrm{mm}^{2}$ ］ | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{D}} \\ & \stackrel{0}{0} \\ & \vdots \end{aligned}$ | Permissible temperature （Note 1） |  |  |  | Permissible temperature （Note 1） |  |  | Permissible temperature （Note 1） |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |
|  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132 S | 100 | 60 | 60 |  | 233 | 5.5 | 3.5 | 2 | 33 | 2 | 2 | 133 | 100 | 100 | 60 |  | 235 | 22 | 1.25 |
| 160S | 150 | 100 | 100 | $t 5 \times 30$ | 282 |  |  |  |  |  |  |  | 150 |  | 100 | $\mathrm{t} 4 \times 40$ | 285 | 38 |  |
| 2005 | 200 | 150 |  |  | 353 | 8 | 5.5 | 3.5 | 44 |  |  | 266 | 200 | 150 |  |  | 355 | 60 |  |
| 220 S | 200 |  |  |  | 384 |  |  |  |  |  |  |  | 250 |  | 150 |  | 386 |  |  |
| 280S | 325 | 200 | 150 | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 489 | 14 | 8 | 5.5 | 58 | 3.5 | 3.5 | 532 | 325 | 250 | 200 | $\begin{gathered} \mathrm{t} 8 \times 50 \\ (400) \end{gathered}$ | 491 |  |  |
| 315S | 2×200 | 250 | 200 |  | 550 |  |  | 8 | 64 |  |  |  | 2×200 |  |  |  | 552 |  |  |
| 630B | $4 \times 325$ | $2 \times 325$ | $2 \times 250$ |  | 1099 | 100 | 60 | 38 | 183 | 3.5 | 3.5 | 532 | － | － | － |  | 1102 | 150 |  |
| 710B | － | $3 \times 325$ | $2 \times 325$ | 125 | 1239 |  |  |  | 207 |  |  |  | － | － | － | $\begin{aligned} & \mathrm{t} \times 50 \\ & (400) \end{aligned}$ | 1243 |  |  |
| 800B | － | $4 \times 325$ |  |  | 1396 |  |  | 60 | 233 |  |  |  | － | － | － |  | 1400 |  |  |

＊For the RHC630 to 800B－4Dロ，the wire or bus bar size is one phase（unit）worth．

## 2）Ambient temperature： $50^{\circ} \mathrm{C}$

| RHC $\square$－4D $\square$ | Main input（including peripheral equipment） |  |  |  |  | Resistance circuit for filter |  |  |  | Charging circuit |  |  | Output：P（＋），N（－） |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature （Note 1） |  |  | Bus bar size ［ $\mathrm{mm}^{2}$ ］ | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{\omega}} \\ & \stackrel{U}{0} \mathbb{U} \\ & \hline \end{aligned}$ | Permissible temperature （Note 1） |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{0}} \\ & \stackrel{0}{2} \\ & \frac{0}{3} \\ & 0 \end{aligned}$ | Permissible temperature （Note 1） |  |  | Permissible temperature （Note 1） |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\omega} \\ & \frac{0}{3} \\ & \underset{3}{0} \end{aligned}$ |  |  |
|  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132S | 200 | 100 | 60 | $\begin{aligned} & t 5 \times 30 \\ & (150) \end{aligned}$ | 233 | 8 | 3.5 | 3.5 | 33 | 2 | 2 | 133 | 200 | 100 | 60 | $\begin{gathered} t 4 \times 40 \\ (160) \end{gathered}$ | 235 | 22 | 1.25 |
| 160S | 250 | 150 | 100 |  | 282 |  |  |  |  |  |  |  | 250 | 150 | 100 |  | 285 | 38 |  |
| 2005 | 325 |  | 150 |  | 353 | 14 | 5.5 | 5.5 | 44 |  |  | 266 | 325 | 200 | 150 |  | 355 | 60 |  |
| 220 S | $2 \times 200$ | 200 |  | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 384 |  |  |  |  |  |  |  | $2 \times 200$ |  |  | $\begin{aligned} & t 8 \times 50 \\ & (400) \end{aligned}$ | 386 |  |  |
| 280 S | $2 \times 250$ | 250 | 200 |  | 489 | 22 | 14 | 8 | 58 | 3.5 | 3.5 | 532 | 2x250 | $\begin{gathered} 325 \\ 2 \times 325 \end{gathered}$ | 200 |  | 491 |  |  |
| 315S | $2 \times 325$ | 325 | 250 |  | 550 |  |  |  | 64 |  |  |  | $2 \times 325$ |  | 250 |  | 552 |  |  |
| 630B | － | $3 \times 325$ | $2 \times 325$ | $\begin{gathered} \mathrm{t} 10 \\ \times 125 \\ (1250) \end{gathered}$ | 1099 | 150 | 60 | 38 | 183 | 3.5 | 3.5 | 532 | － | － | － | $\begin{aligned} & \mathrm{t} 8 \times 50 \\ & (400) \end{aligned}$ | 1102 | 150 |  |
| 710B | － | $4 \times 325$ | $3 \times 250$ |  | 1239 |  | 100 | 60 | 207 |  |  |  | － | － | － |  | 1243 |  |  |
| 800B | － | － | $3 \times 325$ |  | 1396 | 200 |  |  | 233 |  |  |  | － | － | － |  | 1400 |  |  |

＊For the RHC630 to 800B－4D $\square$ ，the wire or bus bar size is one phase（unit）worth．
（2）3－phase 400 V series（LD spec）
1）Ambient temperature： $40^{\circ} \mathrm{C}$

| RHC $\square$－4D $\square$ | Main input（including peripheral equipment） |  |  |  |  | Resistance circuit for filter |  |  |  | Charging circuit |  |  | Output： $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature （Note 1） |  |  | $\left.\begin{gathered} \text { Bus bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered} \right\rvert\,$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\bar{D}} \\ & \vdots ゙ 心 \\ & 0 \\ & \mathbb{O} \end{aligned}$ | Permissible temperature （Note 1） |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \text { Ď } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | Permissible temperature （Note 1） |  |  | Permissible temperature （Note 1） |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{2} \\ & \stackrel{0}{0} \mathbf{0} \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  |  |
|  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132S | 150 | 100 | 100 |  | 282 | 5.5 | 3.5 | 2 | 33 | 2 | 2 | 133 | 150 | 100 | 100 |  | 285 | 38 | 1.25 |
| 160 S | 200 | 150 |  | $\begin{aligned} & t 5 \times 30 \\ & (150) \end{aligned}$ | 353 | 8 | 5.5 | 3.5 | 44 |  |  |  | 200 | 150 |  | $\begin{aligned} & 44 \times 40 \\ & (160) \end{aligned}$ | 355 | 60 |  |
| 200S |  |  |  |  | 384 |  |  |  |  |  |  | 266 | 250 |  | 150 |  | 386 |  |  |
| 280S | $2 \times 200$ | 250 | 200 | $\times 30$ | 550 | 14 | 8 | 8 | 64 | 3.5 | 3.5 | 532 | 2×200 | 250 | 200 | t8×50 | 552 |  |  |
| 315S |  | 325 | 250 | （300） | 619 |  | 14 |  | 72 |  |  |  | $2 \times 250$ | 325 | 250 | （400） | 625 | 100 |  |
| 630B | $5 \times 325$ | $3 \times 325$ | $2 \times 325$ |  | 1239 | 100 | 60 | 38 | 207 | 3.5 | 3.5 | 532 | － | － | － |  | 1243 | 150 |  |
| 710B | － | $4 \times 325$ |  | $125$ | 1396 |  |  | 60 | 233 |  |  |  | － | － | － | $\begin{gathered} \mathrm{t} \times 50 \\ (400) \end{gathered}$ | 1400 |  |  |
| 800B | － | $5 \times 325$ | $4 \times 325$ |  | 1777 | 150 | 100 | 100 | 300 |  |  |  | － | － | － |  | 1750 | 200 |  |

＊For the RHC630 to 800B－4D $\square$ ，the wire or bus bar size is one phase（unit）worth．

## 2) Ambient temperature: $50^{\circ} \mathrm{C}$

| RHC $\square$-4D $\square$ | Main input (including peripheral equipment) |  |  |  |  | Resistance circuit for filter |  |  |  | Charging circuit |  |  | Output: $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | $\begin{aligned} & \stackrel{\rightharpoonup}{\omega} \\ & \frac{1}{3} \\ & 0 \end{aligned}$ | Permissible temperature (Note 1) |  |  |  | Permissible temperature (Note 1) |  |  | Permissible temperature (Note 1) |  |  | $\begin{gathered} \text { Bus } \\ \text { bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ |  |  |  |
|  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132S | 250 | 150 | 100 |  | 282 | 8 | 3.5 | 3.5 | 33 | 2 | 2 | 133 | 250 | 150 | 100 |  | 285 | 38 | 1.25 |
| 160S | 325 |  | 150 | $\begin{aligned} & t 5 \times 30 \\ & (150) \end{aligned}$ | 353 | 14 | 5.5 | 5.5 | 44 |  |  |  | 325 | 200 | 150 | $\begin{gathered} t 4 \times 40 \\ (160) \end{gathered}$ | 355 | 60 |  |
| 200S | 2×200 | 200 |  |  | 384 |  |  |  |  |  |  | 266 | $2 \times 200$ |  |  |  | 386 |  |  |
| 280S | $2 \times 325$ | 325 | 250 | t10×30 | 550 | 22 | 14 | 8 | 64 | 3.5 | 3.5 | 532 | $2 \times 325$ | 325 | 250 | t8×5 | 552 |  |  |
| 315S |  | $2 \times 200$ |  | (300) | 619 | 38 |  | 14 | 72 |  |  |  | $3 \times 325$ | $2 \times 200$ | 325 | (400) | 625 | 100 |  |
| 630B | - | $4 \times 325$ | $2 \times 325$ |  | 1239 | 150 | 100 | 60 | 207 | 3.5 | 3.5 | 532 | - | - | - |  | 1243 | 150 |  |
| 710B | - | $5 \times 325$ | $3 \times 325$ | $\times 125$ | 1396 | 200 |  |  | 233 |  |  |  | - | - | - | t8×50 (400) | 1400 |  |  |
| 800B | - | - | $5 \times 325$ |  | 1777 | 250 | 150 | 100 | 300 |  |  |  | - | - | - |  | 1750 | 200 |  |

* For the RHC630 to 800B-4D $\square$, the wire or bus bar size is one phase (unit) worth.
(3) Three-phase 690 V series, IEC standard (MD spec.)

1) Ambient temperature: $40^{\circ} \mathrm{C}$

| RHC $\square$-69D $\square$ | Main input (including peripheral equipment) |  |  |  | Output: $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature ${ }^{(\text {Note 1) }}$ |  | Bus bar size $\left[\mathrm{mm}^{2}\right]$ | Current [A] | Permissible temperature ${ }^{\text {(Note 1) }}$ |  | Bus bar size $\left[\mathrm{mm}^{2}\right]$ | Current [Adc] |  |  |
|  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132 S | 38 | 22 | t5 $\times 30$ | 135 | 38 | 22 | t4×40 | 140 | 22 | 1.25 |
| 160S |  | 38 | (150) | 163 |  | 38 | (160) | 170 |  |  |
| 200S | 95 |  |  | 205 | 60 | 60 |  | 212 |  |  |
| 250S | 100 | 60 | t10×30 | 253 | 100 |  | t8×50 | 261 | 38 |  |
| 280S |  | 100 | (300) | 283 |  | 100 | (400) | 293 |  |  |
| 315S |  |  |  | 319 | 150 |  |  | 329 |  |  |
| 355S | 150 |  |  | 359 |  |  |  | 373 |  |  |
| 400S |  | 150 |  | 405 |  | 150 |  | 418 | 60 |  |
| 450S | 200 |  |  | 455 | 200 |  |  | 470 |  |  |

Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.
(4) Three-phase 690 V series, IEC standard (LD spec.)

1) Ambient temperature: $40^{\circ} \mathrm{C}$

| RHC $\square$-69D $\square$ | Main input (including peripheral equipment) |  |  |  | Output: $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature (Note 1) |  | Bus bar size $\left[\mathrm{mm}^{2}\right]$ | Current <br> [A] | Permissible temperature ${ }^{\text {(Note 1) }}$ |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current [Adc] |  |  |
|  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132 S | 38 | 38 | t5×30 | 163 | 38 | 38 | t4×40 | 170 | 22 | 1.25 |
| 160S | 60 |  | (150) | 205 | 60 | 60 | (160) | 212 |  |  |
| 200S |  | 60 |  | 253 |  |  |  | 231 |  |  |
| 250 S | 100 | 100 | t10×30 | 283 | 100 | 100 | t8×50 | 293 | 38 |  |
| 280S |  |  | (300) | 319 | 150 |  | (400) | 329 |  |  |
| 315S | 150 |  |  | 359 |  |  |  | 373 |  |  |
| 355S |  | 150 |  | 405 |  | 150 |  | 418 | 60 |  |
| 400S | 200 |  |  | 455 | 200 |  |  | 470 |  |  |

Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.
(5) Three-phase 690V series, domestic selection (MD spec.)

1) Ambient temperature: $40^{\circ} \mathrm{C}$

| RHC $\square$-69D $\square$ | Main input (including peripheral equipment) |  |  |  | Output: $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current [A] | Permissible temperature ${ }^{\text {(Note 1) }}$ |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current [A] |  |  |
|  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132S | 38 | 22 | t5×30 | 135 | 38 | 22 | t4×40 | 140 | 22 | 1.25 |
| 160 S |  | 38 | (150) | 163 |  | 38 | (160) | 170 |  |  |
| 200S | 60 |  |  | 205 | 60 | 60 |  | 212 |  |  |
| 250S | 100 | 60 | t10×30 | 253 | 100 |  | t8×50 | 261 | 38 |  |
| 280S |  | 100 | (300) | 283 |  | 100 | (400) | 293 |  |  |
| 315S |  |  |  | 319 | 150 |  |  | 329 |  |  |
| 355S | 150 |  |  | 359 |  |  |  | 373 |  |  |
| 400 S |  | 150 |  | 405 |  | 150 |  | 418 | 60 |  |
| 450S | 200 |  |  | 455 | 200 |  |  | 470 |  |  |

Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$. Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.
(6) Three-phase 690 V series, domestic selection (LD spec.)

1) Ambient temperature: $40^{\circ} \mathrm{C}$

| RHCD-69D $\square$ | Main input (including peripheral equipment) |  |  |  | Output: $\mathrm{P}(+), \mathrm{N}(-)$ |  |  |  |  | 은 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Permissible temperature ${ }^{\text {(Note 1) }}$ |  | Bus bar size $\left[\mathrm{mm}^{2}\right]$ | Current [A] | Permissible temperature ${ }^{\text {(Note 1) }}$ |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current [A] |  |  |
|  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |
| 132 S | 38 | 38 | t5×30 | 163 | 38 | 38 | t4×40 | 170 | 22 | 1.25 |
| 160S | 60 |  | (150) | 205 | 60 | 60 | (160) | 212 |  |  |
| 2005 |  | 60 |  | 253 |  |  |  | 231 |  |  |
| 250S | 100 | 100 | t10×30 | 283 | 100 | 100 | t8×50 | 293 | 38 |  |
| 280S |  |  | (300) | 319 | 150 |  | (400) | 329 |  |  |
| 315S | 150 |  |  | 359 |  |  |  | 373 |  |  |
| 355S |  | 150 |  | 405 |  | 150 |  | 418 | 60 |  |
| 400S | 200 |  |  | 455 | 200 |  |  | 470 |  |  |

Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

### 6.3.16 External dimensions

### 6.3.16.1 List of external dimensions - RHC-D series (stack type)

| Power supply voltage | Model | 㲴 | W | H | D | Approx. mass [kg] | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 400 \mathrm{~V} \\ & \text { series } \end{aligned}$ | RHC132S-4D $\square$ | A | 226.2 | 1100 | 565 | 95 |  |
|  | RHC160S-4D $\square$ |  |  |  |  |  |  |
|  | RHC200S-4D $\square$ |  |  |  |  |  |  |
|  | RHC220S-4D $\square$ | B | 226.2 | 1400 | 565 | 125 |  |
|  | RHC280S-4D $\square$ |  |  |  |  | 135 |  |
|  | RHC315S-4D $\square$ |  |  |  |  |  |  |
|  | RHC630B-4D $\square$ | C | 226.2 | 1400 | 565 | $135 \times 3$ | A set of three stacks constitutes a single inverter unit. |
|  | RHC710B-4D $\square$ |  |  |  |  |  |  |
|  | RHC800B-4D $\square$ |  |  |  |  |  |  |
| 690 V series | RHC132S-69D $\square$ | A | 226.2 | 1100 | 565 | 105 |  |
|  | RHC160S-69D $\square$ |  |  |  |  |  |  |
|  | RHC200S-69D $\square$ |  |  |  |  |  |  |
|  | RHC250S-69D $\square$ | B | 226.2 | 1400 | 565 | 140 |  |
|  | RHC280S-69D $\square$ |  |  |  |  |  |  |
|  | RHC315S-69D $\square$ |  |  |  |  |  |  |
|  | RHC355S-69D $\square$ |  |  |  |  |  |  |
|  | RHC400S-69D $\square$ |  |  |  |  |  |  |
|  | RHC450S-69D $\square$ |  |  |  |  |  |  |

### 6.3.16.2 External dimensions

(1) Figure A (Frame 3 size: RHC132S-4D $\square$ to RHC200S-4D $\square$, RHC132S-69D $\square$ to RHC200S-69D $\square$ )

[Unit: mm]
(2) Figure B (Frame 4 size: RHC220S-4D $\square$ to RHC315S-4D $\square$, RHC250S-69D $\square$ to RHC450S-69D $\square$ )

(3) Figure C (Frame 4 size: RHC630B-4D $\square$ to RHC800B-4D $\square$ )



### 6.3.17 Terminal positions

(1) Main circuit terminals


> Select terminal screws that allow for a distance of 10 mm or greater to the chassis．


## View from bottom

底面から見る

Figure 6．3．17－2：Frame 4 size（RHC220S to 315S－4D $\square$ ）

> Select terminal screws that allow for a distance of 10 mm or greater to the chassis.


Figure 6.3.17-3: Frame 4 size (RHC630B to 800B-4D $\square$, S-phase)

Select terminal screws that allow for a
Unit: [mm]


Figure 6.3.17-4: Frame 4 size (RHC630B to 800B-4D $\square$, R-phase, T-phase)


Figure 6．3．17－5：Frame 3 size（RHC132S to 200S－69D $\square$ ）

Select terminal screws that allow for a distance of 10 mm or greater to the chassis.

Unit: [mm]


Figure 6.3.17-6: Frame 4 size (RHC250S to 450S-69D $\square$ )
(2) Control Circuit terminals

■ 400V series


Screw size: M3


Screw size: M4


Figure 6.3.17-7: Control terminal layout (400V series)


Screw size: M3


Screw size: M4


Screw size: M4


Figure 6.3.17-8 Control terminal layout ( 690 V series)

### 6.3.18 Peripheral equipment external dimensions

(1) Pressurizing reactor (LR4- $\square \square \square C$ )

Figure A


Figure C



Details of terminals

Details of terminals


LR4-710C: CuP.t8×100 LR4-800C: CuP.t10×100 LR4-1000C: CuP.t12×100

| Voltage | Model | Rated current [A] | Dimensions [mm] |  |  |  |  |  |  |  | Mass [kg] | Figure | Heat resistant class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | W | WP | D | DP | DT | H | K | M $\phi$ |  |  |  |
| $\begin{aligned} & > \\ & \text { 악 } \end{aligned}$ | LR4-160C | 304 | 380 | 125 | 300 | 260 | 185 | 550 | 15 | M12 | 140 | A | H |
|  | LR4-220C | 418 | 450 | 150 | 330 | 290 | 230 | 620 | 15 | M12 | 200 |  |  |
|  | LR4-280C | 532 | 480 | 160 | 330 | 290 | 240 | 740 | 15 | M16 | 250 |  |  |
|  | LR4-315C | 599 | 480 | 160 | 340 | 300 | 250 | 760 | 15 | M16 | 270 |  |  |
|  | LR4-355C | 674 | 480 | 160 | 355 | 315 | 255 | 830 | 15 | M16 | 310 |  |  |
|  | LR4-400C | 760 | 480 | 160 | 380 | 330 | 260 | 890 | 19 | M16 | 340 |  |  |
|  | LR4-500C | 950 | 525 | 175 | 410 | 360 | 290 | 960 | 19 | M16 | 420 |  |  |
|  | LR4-630C | 1200 | 600 | 200 | 440 | 390 | 285 | 640 | 19 | - | 450 | B |  |
|  | LR4-710C | 1350 | 645 | 215 | 440 | 390 | 295 | 730 | 19 | - | 510 | C |  |
|  | LR4-800C | 1520 | 690 | 230 | 450 | 400 | 290 | 850 | 19 | - | 600 |  |  |
|  | LR4-1000C | 1750 | 770 | 255 | 550 | 480 | 340 | 940 | 23 | - | 950 |  |  |

(2) Filter reactor (LFC4- $\square \square \square C$ )

Figure A


Figure B



| Voltage | Model | Rated current [A] | Dimensions [mm] |  |  |  |  |  |  |  |  |  | Mass [kg] | Figure | Heat resistant class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | W | WP | D | DP | DT | H | K | M | CW | CH |  |  |  |
| ৪ | LFC4-160C | 304 | 255 | 85 | 137 | 110 | 150 | 245 | 10 | M12 | - | - | 22 | A | H |
|  | LFC4-220C | 418 | 300 | 100 | 210 | 180 | 170 | 320 | 10 | M12 | - | - | 35 | B |  |
|  | LFC4-280C | 532 | 330 | 110 | 230 | 195 | 195 | 330 | 12 | M16 | - | - | 43 |  |  |
|  | LFC4-315C | 599 | 315 | 105 | 230 | 195 | 200 | 365 | 12 | M16 | - | - | 48 |  |  |
|  | LFC4-355C | 674 | 315 | 105 | 235 | 200 | 210 | 395 | 12 | M16 | - | - | 53 |  |  |
|  | LFC4-400C | 760 | 345 | 115 | 235 | 200 | 235 | 420 | 12 | M16 | - | - | 60 |  |  |
|  | LFC4-500C | 950 | 345 | 115 | 240 | 205 | 240 | 480 | 12 | M16 | - | - | 72 |  |  |
|  | LFC4-630C | 1200 | 435 | 145 | 295 | 255 | 200 | 550 | 15 | - | 75 | 17.5 | 175 | c |  |
|  | LFC4-710C | 1350 | 480 | 160 | 295 | 255 | 215 | 570 | 15 | - | 100 | 30 | 190 |  |  |
|  | LFC4-800C | 1520 | 480 | 160 | 320 | 270 | 220 | 600 | 15 | - | 100 | 30 | 220 |  |  |
|  | LFC4-1000C | 1750 | 480 | 160 | 320 | 270 | 240 | 700 | 15 | - | 100 | 30 | 240 |  |  |

(3) Filter capacitor (CF4- $\square \square \square$ C)

Figure A


Figure B


Note

- Install vertically. Do not install horizontally.
- Be sure to fasten all the mounting legs to the panel, etc. Figure A: Two (2) mounting legs, Figure B: Four (4) mounting legs

Vibration or impact may cause breakage.

| Voltage | Model | Dimensions [mm] |  |  |  |  |  |  |  |  | Mass [kg] | Figure | Quantity used |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | W | W1 | D | D1 | E | F | H | H1 | J |  |  |  |
| $\begin{aligned} & > \\ & \text { ৪ } \end{aligned}$ | CF4-160C | 280 | 265 | 90 | 55 | 80 | 7 | 260 | - | M6 | 6.0 | A | 1 |
|  | CF4-220C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 310 | 125 | M12 | 13.0 | B |  |
|  | CF4-280C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 350 | 165 | M12 | 15.0 | B |  |
|  | CF4-315C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 460 | 275 | M12 | 20.0 | B |  |
|  | CF4-355C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 520 | 335 | M12 | 23.0 | B |  |
|  | CF4-400C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 610 | 425 | M12 | 27.0 | B |  |
|  | CF4-500C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 310 | 125 | M12 | 13.0 | B | 2 |
|  | CF4-630C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 460 | 275 | M12 | 20.0 | B |  |
|  | CF4-710C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 520 | 335 | M12 | 23.0 | B |  |
|  | CF4-800C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 610 | 425 | M12 | 27.0 | B |  |
|  | CF4-1000C | 435 | 400 | 100 | - | 80 | $15 \times 20$ <br> slotted hole | 610 | 425 | M12 | 27.0 | B | 3 |

Note 1) The models CF4-500C to CF4-800C use two capacitors while the CF4-1000C use three capacitors. (Parallel connection)
If ordered with quantity $=$ " 1 ", two capacitors will be delivered for the CF4-500C to CF4-800C or three capacitors for the CF4-1000C.

## (4) Filter resistor

Figure A


| Model | Dimensions [mm] |  |  |  |  |  |  |  |  |  | Mass [kg] | Figure | Quantity used |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | M | L | $l$ | D | G | H | K | A | J | $\varphi \mathrm{C}$ |  |  |  |
| GRZG400 $0.38 \Omega$ | 411 | 385 | 330 | 47 | 40 | 40 | 46 | 16 | 9.5 | 8.2 | 0.85 | A | 3 |
| GRZG400 $0.26 \Omega$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| GRZG400 $0.53 \Omega$ |  |  |  |  |  |  |  |  |  |  |  |  |  |

(Filter resistor - continued)


Figure C


| Voltage | Model | Dimensions [mm] |  |  |  |  |  |  | $\begin{gathered} \text { Mass } \\ {[\mathrm{kg}]} \end{gathered}$ | $\begin{aligned} & 00 \\ & \text { 은 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | W | W1 | D | D1 | D2 | H | H1 |  |  |  |
| $\begin{aligned} & > \\ & 8 \\ & \hline \end{aligned}$ | RF4-160C | 400 | 370 | 470 | 460 | 320 | 240 | 55 | 22 | B | 1 |
|  | RF4-220C |  |  |  |  |  |  |  | 25 |  |  |
|  | RF4-280C | 655 | 625 | 470 | 460 | 320 | 240 | 55 | 31 | C |  |
|  | RF4-315C |  |  |  |  |  |  |  | 35 |  |  |
|  | RF4-355C |  |  |  |  |  |  |  | 36 |  |  |
|  | RF4-400C |  |  |  |  |  |  |  | 38 |  |  |
|  | RF4-500C |  |  |  |  |  |  |  | 41 |  |  |
|  | RF4-630C | 655 | 625 | 530 | 520 | 320 | 440 | 55 | 70 |  |  |
|  | RF4-710C |  |  |  |  |  |  |  |  |  |  |
|  | RF4-800C |  |  |  |  |  |  |  | 80 |  |  |
|  | RF4-1000C | 755 | 725 | 530 | 520 | 320 | 440 | 55 | - |  |  |

## (5) Charging resistor

Figure A


Figure B


Figure C


| Model | Dimensions [mm] |  |  |  |  |  |  |  |  |  | Mass [kg] |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | M | L | $l$ | D | G | H | K | A | $J$ | $\varphi \mathrm{C}$ |  |  |  |
| GRZG120 $2 \Omega$ | 217 | 198 | 165 | 33 | 22 | 22 | 32 | - | 6 | 5.5 | 0.25 | A | 3 |
| GRZG400 $1 \Omega$ | 411 | 385 | 330 | 47 | 40 | 40 | 46 | - | 9.5 | 5.5 | 0.85 |  |  |
| TK50B $30 \Omega \square$ (HF5B0416) | See Figure B |  |  |  |  |  |  |  |  |  | 0.15 | B |  |
| $80 W 7.5 \Omega$ (HF5C5504) | See Figure C |  |  |  |  |  |  |  |  |  | 0.19 | C |  |

(6) AC fuse

Figure A



Figure B

*Side view of A70P1600-4TA

*Side view of A70P2000-4




### 6.3.19 Generated loss

### 6.3.19.1 Generated loss in MD mode

| 400V |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Converter |  | Pressurizing reactor |  | Filter reactor |  | Filter resistor |  |  |
| Model |  | Model | $\begin{aligned} & \text { 에N } \\ & \vdots \\ & \frac{\pi}{0} \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | Model | $\begin{aligned} & \text { 에N } \\ & \stackrel{N}{0} \\ & \frac{\pi}{0} \\ & \stackrel{N}{0} \\ & 0 \end{aligned}$ | Model |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \frac{0}{0} \\ & \frac{0}{0} \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ |
| RHC132S-4D $\square$ | 2450 | LR4-160C | 1000 | LFC4-160C | 160 | RF4-160C | 1 | 568 |
| RHC160S-4D $\square$ | 2850 |  |  |  |  |  |  |  |
| RHC200S-4D $\square$ | 3500 | LR4-220C | 1240 | LFC4-220C | 200 | RF4-220C | 1 | 751 |
| RHC220S-4D $\square$ | 4000 |  |  |  |  |  |  |  |
| RHC280S-4D $\square$ | 4900 | LR4-280C | 1430 | LFC4-280C | 220 | RF4-280C | 1 | 1027 |
| RHC315S-4D $\square$ | 5500 | LR4-315C | 1660 | LFC4-315C | 260 | RF4-315C | 1 | 1154 |
| RHC630B-4D $\square$ | 10550 | LR4-630C | 2300 | LFC4-630C | 510 | RF4-630C | 1 | 4722 |
| RHC710B-4D $\square$ | 11500 | LR4-710C | 2600 | LFC4-710C | 630 | RF4-710C | 1 | 5361 |
| RHC800B-4D $\square$ | 13100 | LR4-800C | 2900 | LFC4-800C | 620 | RF4-800C | 1 | 6024 |


| 690 V |  |
| :---: | :---: |
| Converter stack |  |
| Model |  |
| RHC132S-69D $\square$ | 2650 |
| RHC160S-69D $\square$ | 3050 |
| RHC200S-69D $\square$ | 3900 |
| RHC250S-69D $\square$ | 5000 |
| RHC280S-69D $\square$ | 5450 |
| RHC315S-69D $\square$ | 6000 |
| RHC355S-69D $\square$ | 4150 |
| RHC400S-69D $\square$ | 4700 |
| RHC450S-69D $\square$ | 5300 |

* The generated loss of the filters shown above is the value for all quantities.


### 6.3.19.2 Generated loss in LD mode

| 400V |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Converter |  | Pressurizing reactor |  | Filter reactor |  | Filter resistor |  |  |
| Model | $\begin{aligned} & \text { D} \\ & \stackrel{N}{0} \sum_{0} \\ & \frac{0}{0} \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ | Model | $\begin{aligned} & \overline{0} \\ & \stackrel{\otimes}{0} \sum \\ & \frac{0}{0} \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ | Model | $\begin{aligned} & \overline{0} \\ & \stackrel{ \pm}{0} \\ & \stackrel{y}{0} \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | Model |  | $\begin{aligned} & \overline{0} \\ & \stackrel{\otimes}{0} \sum \\ & \frac{0}{0} \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ |
| RHC132-4D $\square$ | 2950 | LR4-160C | 1000 | LFC4-160C | 160 | RF4-160C | 1 | 568 |
| RHC160-4D $\square$ | 3450 | LR4 220 C | 1240 | LFC4 220 C | 200 | RF4 220 C | 1 |  |
| RHC200-4D $\square$ | 3800 | LR |  | LFC4-2 |  | RF4-220 | 1 |  |
| RHC280-4D $\square$ | 5450 | LR4-315C | 1660 | LFC4-315C | 260 | RF4-315C | 1 | 1154 |
| RHC315-4D $\square$ | 6100 | LR4-355C | 1910 | LFC4-355C | 300 | RF4-355C | 1 | 1286 |
| RHC630B-4D $\square$ | 11850 | LR4-710C | 2600 | LFC4-710C | 630 | RF4-710C | 1 | 5361 |
| RHC710B-4D $\square$ | 12900 | LR4-800C | 2900 | LFC4-800C | 620 | RF4-800C | 1 | 6024 |
| RHC800B-4D $\square$ | 16200 | LR4-1000C | 4500 | LFC4-1000C | 1080 | RF4-1000C | 1 | 7728 |


| 690 V |  |
| :---: | :---: |
| Converter stack |  |
| Model |  |
| RHC132S-69D $\square$ | 3150 |
| RHC160S-69D $\square$ | 3750 |
| RHC200S-69D $\square$ | 4250 |
| RHC250S-69D $\square$ | 5550 |
| RHC280S-69D $\square$ | 6100 |
| RHC315S-69D $\square$ | 6700 |
| RHC355S-69D $\square$ | 4600 |
| RHC400S-69D $\square$ | 5200 |

[^10]
### 6.4 Filter stack (RHF-D series)

### 6.4.1 Features

- This filter stack is dedicated to use with the RHC-D series high-efficiency power regeneration PWM converters .
<Lineup>
Applicable to the 400 V series PWM converters for 132 kW to 315 kW
Applicable to the 690V series PWM converters for 132 kW to 450 kW
* Cannot be used with unit type PWM converters (RHC-C).
- All peripherals (filter circuit, pressurizing reactor, charging circuits, etc.) required to run a PWM converter are packaged in a single unit.
This eliminates the need to separately procure peripherals (such as a pressurizing reactor, filter reactor, filter capacitor, charging box, charging resistor).
- It is possible to save wiring work and installation space for peripherals.
- Built on the same stack design and shape as inverters and PWM converters. These products effectively help reduce the panel size.


Note The filter stacks (RHF-D) are dedicated to the use with stack type PWM converters (RHC-D series) indicated below. It is not applicable to any other PWM converters.
-400V series: RHC132S-4D $\square$ to RHC315S-4D $\square$
-690V series: RHC132S-69D $\square$ to RHC450S-69D $\square$
(1) For information on the peripheral equipment for the PWM converters (RHC-D), refer to "6.3.12 Configuration of peripherals".

### 6.4.2 Standard specifications

### 6.4.2.1 3-phase 400V series

| Filter model |  |  | RHF160S-4D $\square$ | RHF220S-4D $\square$ | RHF280S-4D $\square$ | RHF355S-4D $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Applicable converter model RHC $\square \square \square S$-4D |  | MD mode | 132 | 200 | 280 | 315 |
|  |  | 160 | 220 | - | - |
|  |  | LD mode | 132 | 160 | - | 315 |
|  |  | - | 200 | - | - |
| Rated current (A) |  |  | 282 | 384 | 489 | 619 |
| 헤20를를 | Main power supply <br> Number of phases, voltage, and frequency |  | 3-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $460 \mathrm{~V} / 60 \mathrm{~Hz}$ |  |  |  |
|  | Fan power supply Number of phases, voltage, and frequency |  | 400 V input | Single-phase, 380 to $440 \mathrm{~V} / 50 \mathrm{~Hz}, 380$ to $460 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{* 1}$ |  |  |  |
|  |  | 200 V input | Single-phase, 200 to $220 \mathrm{~V} / 50 \mathrm{~Hz}, 200$ to $230 \mathrm{~V} / 60 \mathrm{~Hz}{ }^{*}$ |  |  |  |
|  | Allowable fluctuation |  | Voltage: $-15 \%$ to $+10 \%$, Frequency: $-5 \%$ to $+5 \%$, Voltage unbalance ratio: $2 \%$ or less *3 |  |  |  |
| Permissible carrier frequency |  |  | $2.5 \mathrm{kHz}, 5 \mathrm{kHz}$ |  |  |  |
| Approx.mass [kg] |  |  | 155 | 195 | 230 | 250 |
| Enclosure |  |  | IP00 open type |  |  |  |
| Noise level |  |  | 75dB (condition: A-range, distance: 1 m ) ${ }^{*} 4$ |  |  |  |

*1 For 380 to $398 \mathrm{~V} / 50 \mathrm{~Hz}$ or 380 to $430 \mathrm{~V} / 60 \mathrm{~Hz}$ power supply, switching of the filter stack internal terminals (U1, U2) is required.
*2 200 V power supply can also be used. For details, refer to "6.2.4 Terminal functions".
*3 Interphaseunbalance rate $(\%)=\frac{\text { Max. voltage[V] }- \text { Min. voltage[V] }}{3 \text {-phase average voltage }} \times 67$
*4 This is the noise level measured when the filter stack is connected with a PWM converter and inverter of the same capacity and runs at its ratings.

### 6.4.2.2 3-phase 690V series

| Filter model |  |  | RHF160S-69D | RHF220S-69D $\square$ | RHF280S-69D■ | RHF355S-69D | RHF450S-69D $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Applicable converter model RHCDS-69Dロ |  | MD mode | 132 | 200 | 250 | 315 | 400 |
|  |  | 160 | - | 280 | 355 | 450 |
|  |  | LD mode | 132 | 160 | - | 280 | 355 |
|  |  | - | 200 | 250 | 315 | 400 |
| Rated current (A) |  |  | 163 | 223 | 283 | 359 | 455 |
|  | Main power supply Number of phases, voltage, and frequency |  | 3-phase, 3-wire type, 660 to $690 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ <br> 3-phase, 3-wire type, 575 to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ Voltage: $-15 \%$ to $+10 \%$, Frequency: $-5 \%$ to $+5 \%$ |  |  |  |  |
|  | Fan power supply Number of phases, voltage, and frequency |  | 690 V input | Single-phase, 660 to 690 V, $50 / 60 \mathrm{~Hz}$ Single-phase, 575 to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}{ }^{* 1}$ Voltage: $-15 \%$ to $+10 \%$, Frequency: $-5 \%$ to $+5 \%$ |  |  |  |  |
|  |  | 200 V input | Single-phase, 200 to $220 \mathrm{~V} / 50 \mathrm{~Hz}, 200$ to $230 \mathrm{~V} / 60 \mathrm{~Hz}$ Voltage: $-15 \%$ to $+10 \%$, Frequency: $-5 \%$ to $+5 \%$ |  |  |  |  |
|  | Allowable fluctuation |  | Voltage: -15\% to +10\%, Frequency: $-5 \%$ to $+5 \%$, Voltage unbalance ratio: 2\% or less |  |  |  |  |
| Permissible carrier frequency |  |  | $2.5 \mathrm{kHz}, 5 \mathrm{kHz}$ |  |  |  |  |
| Approx.mass [kg] |  |  | 180 | 205 | 230 | 255 | 280 |
| Enclosure |  |  | IP00 open type |  |  |  |  |
| Noise level ${ }^{* 2}$ |  |  | 75dB (condition: A-range, distance: 1 m ) |  |  |  |  |

*1 For 575 to $600 \mathrm{~V}, 50 / 60 \mathrm{~Hz}$ power supply, switching of the filter stack internal terminals (U1, U2) is required.
*2 This is the noise level measured when the filter stack is connected with a PWM converter and inverter of the same capacity and runs at its ratings.

### 6.4.3 Basic connection diagrams



Figure 6.4.3-1: Basic connection diagram
(Note 1) Connect a step-down transformer to ensure that the sequence circuit voltages are exactly the same as shown in the Figure 6.4.3-1.
(Note 2) Be sure to connect the PWM converter and inverter auxiliary power input terminals (R0, T0) to the main power via contact $b$ of the power supply electromagnetic contactor (52). When using the product with a non-grounded power supply, it is necessary to add an insulated transformer. For more information, refer to "6.3.15-(5)" in Chapter 6.
(Note 3) Be sure to connect the power supply for the inverter's AC fan to the main power directly (not via contact b of \#52) so that the power can be fed through terminals R1 and T1.
(Note 4) Create a sequence in which the PWM converter gets ready for operation before the run signal is input to the inverter.
(Note 5) Set the timer for 52 T to 1 second.
(Note 6) Be sure to assign the PWM converter digital input terminal (X1) to the external alarm (THR), and to connect the filter stack overheat signal outputs (1, 2). Set contact b input with function code E14 to input with contact b. Furthermore, connect the microswitch for AC fuse blow detection to the digital input terminal (X1) in series with all microswitches and the overheat signal outputs (1, 2).
(Note 7) Ensure correct phase sequence when connecting wires to terminals L1/R, L2/S, L3/T, R2, T2, R1, S1, and T1.
(Note 8) When inputting 200 VAC as the fan power supply, remove jumper wires from between terminals R11 and R12 and from between terminals T11 and T12, and then connect the input to terminals R12 and T12. Note that these terminals are dedicated to the internal fan power supply. Do not use them for any other purposes.
(Note 9) Be sure to set the timer for 73 T to 5 seconds.
(Note 10) For the 400 V series, connect "Fdc (fuse)" to the $\mathrm{P}(+)$ side. No "Fdc (fuse)" is required at the $\mathrm{N}(-)$ side. For the 690 V series, connect "Fdc (fuse)" to the $\mathrm{P}(+)$ side and $\mathrm{N}(-)$ side.
Furthermore, use two microswitches and connect them in series.
(Note 11) With the 690V series, there are no R3 or T3 short-circuit wires.

## $\triangle$ WARNING

- Be sure to assign the PWM converter digital input terminal (X1) to the external alarm (THR), and to connect the filter stack overheat signal outputs (1, 2).
- Be sure to stop the PWM converter and inverter when the overheat signal is output. Furthermore, shut off electromagnetic contactors 52 and 73.
Risk of fire, accident


### 6.4.4 Terminal functions

| Terminal symbol |  | Name | Specifications |
| :---: | :---: | :---: | :---: |
|  | L1, L2, L3 | Main power input | Connect to a 3-phase power supply. |
|  | U0, V0, W0 | Filter output | Connect to the PWM converter's power input terminals L1/R, L2/S, and L3/T. |
|  | L4, L5, L6 | Charging circuit input | Connect to a 3-phase power supply. |
|  | E(G) | For filter grounding | Grounding terminal for the chassis (case) of the filter stack. |
|  | R3, T3 | Fan power input | Connection terminals for the AC cooling fan power supply inside the stack. If the fan uses the same voltage as the main power supply, connect this terminal to the power supply. |
|  | R11, R12 <br> T11, T12*1 | Fan power input (for 200 V input) | Use this terminal when inputting 200 VAC as the power to the AC cooling fan inside the stack. <br> When using a 200 V power supply, remove the jumper wires connected when shipped from the factory and connect terminals R12 and T12 to the power supply. <br> When using the same voltage as the main power supply, ensure that jumper wires are connected between R11 and R12 and between T11 and T12 (factory default). |
|  | U1, U2 *2 | Supply voltage switching terminal | Change the terminal connection depending on the power supply connected to the fan power input terminals. <br> (Refer to Figure 6.4.4-1.) |
|  | $\begin{aligned} & 73-1 \\ & 73-2 \end{aligned}$ | Charging circuit contactor Control input | These are control signal input terminals for the charging circuit contactor. <br> <Coil rated capacity> <br> - 400V series <br> When turned ON ... $200 \mathrm{~V} / 50 \mathrm{~Hz}: 120 \mathrm{VA}, 220 \mathrm{~V} / 60 \mathrm{~Hz}$ : 135 VA <br> When retained ... $200 \mathrm{~V} / 50 \mathrm{~Hz}: 12.7 \mathrm{VA}, 220 \mathrm{~V} / 60 \mathrm{~Hz}: 12.4 \mathrm{VA}$ |
|  | ONA ONB ONC | Charging circuit operation signal | These are auxiliary contact output terminals for the charging circuit contactor. <br> To be used as signal for operational check of charging circuit. <br> - Contact rating: 24 VDC 3 A <br> * Min. working voltage/current: 5 VDC 3 mA |
|  | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | Overheat signal output | Signal is output when internal parts of filter stack are overheated. <br> - Contact rating: 24 VDC (max. 27 V ), max. 0.3A/max. 6 W <br> * Min. usage voltage, current: $1 \mathrm{VDC}, 0.1 \mathrm{~mA}$ |

*1 Terminals R11, R12, T11, and T12 are 200 V power terminals and their withstand voltage is 2000 VAC for 1 minute.
*2 Terminals U1 and U2 can be switched as shown in Figure 6.4.4-1.


Figure 6.4.4-1: Supply voltage switching terminal

## 4 WARNING

- Be sure to assign the PWM converter digital input terminal (X1) to the external alarm (THR), and to connect the filter stack overheat signal outputs $(1,2)$.
- Be sure to stop the PWM converter and inverter when the overheat signal is output. Furthermore, shut off electromagnetic contactors 52 and 73.

Risk of fire, accident

### 6.4.5 Check before use

Unpack the package and check the following:
Check that you have properly received the product main unit and the following accessories.

## Accessories Instruction manual

The inverter has not been damaged during transportation-there should be no dents or parts missing. The main nameplates are attached to the main unit. The main nameplate is located on the front face of the main unit (as shown in Figure 6.4.6-2 and Figure 6.4.6-3). Check these main nameplates to see that the inverter is exactly the type you ordered.

(a) Main Nameplate

## TYPE RHF160S-4DJ SER.No. 28A456A0003BA

(b) Sub Nameplate

Figure 6.4.5-1: Main nameplate

TYPE: Filter stack (RHF-D)


Specifications in each mode are printed on the main nameplate.


If you suspect the product is not working properly or if you have any questions about your product, contact your Fuji Electric representative.
[10] Refer to Chapter 3 "Transportation and Storage" for information on transportation and long-term storage of filter stacks.
[1] Refer to Chapter 4 "Installation and Wiring" for information on installation of filter stacks. For information on the main circuit wire sizes, refer to "6.4.11 Wire size".

### 6.4.6 External views

### 6.4.6.1 Warning label and falling warning label




Figure 6.4.6-1: Warning label and falling warning label

### 6.4.6.2 Appearance



Figure 6.4.6-2: Frame 3 size
(RHF160S to RHF220S-4D $\square$,RHF160S-69D $\square$ )


Figure 6.4.6-3: Frame 4 size
(RHF280S to RHF355S-4D $\square$,RHF220S to RHF355S-69D $\square$ )


Figure 6.4.6-4: Frame 5 size (RHF450S-69D $\square$ )

### 6.4.7 External dimensions

### 6.4.7.1 List of external dimensions - RHF-D series (stack type)

Unit: [mm]

| Power supply voltage | Model | Figure | W | H | D | Approx. mass [kg] | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 400 \mathrm{~V} \\ & \text { series } \end{aligned}$ | RHF160S-4D $\square$ | A | 226.2 | 1166 | 565 | 155 |  |
|  | RHF220S-4D $\square$ |  |  |  |  | 195 |  |
|  | RHF280S-4D $\square$ | B | 226.2 | 1400 | 565 | 230 |  |
|  | RHF355S-4D $\square$ |  |  |  |  | 250 |  |
| $\begin{aligned} & 690 \mathrm{~V} \\ & \text { series } \end{aligned}$ | RHF160S-69D $\square$ | A | 226.2 | 1166 | 565 | 180 |  |
|  | RHF220S-69D $\square$ | C | 226.2 | 1400 | 565 | 215 |  |
|  | RHF280S-69D $\square$ |  |  |  |  | 230 |  |
|  | RHF355S-69D $\square$ |  |  |  |  | 255 |  |
|  | RHF450S-69D $\square$ | D | 336.2 | 1400 | 565 | 280 |  |

### 6.4.7.2 External dimensions

(1) Figure A (Frame 3 size: RHF160S-4D $\square$, RHF220S-4D $\square$, RHF160S-6D $\square$ )

(2) Figure B (Frame 4 size: RHF280S-4D $\square$, RHF355S-4D $\square$ )

(3) Figure C (Frame 4 size: RHF220S to 355S-69D $\square$ )

(4) Figure D (Frame 5 size: RHF450S-69D $\square$ )


## 6．4．8 Terminal positions

## 6．4．8．1 Main circuit terminals

## Note

Install relay bar terminals at the cabinet side for the main power supply output terminals．
Furthermore，secure firmly with an insulator to prevent terminal shorting．

| Terminal <br> name | Terminal <br> symbol | Bolt size |
| :---: | :---: | :---: |
| Main power <br> supply input | $\mathrm{L} 1, \mathrm{~L} 2, \mathrm{~L} 3$ |  |
| Main power <br> supply output | U0，V0，W0 | M12 |
| Grounding <br> terminal | G |  |
|  |  |  |

Select terminal screws that allow for a distance of 10 mm or greater to the chassis．


View from bottom
底百から見る

Figure 6．4．8－1：Frame 3 size（RHF160S－4D $\square$ ，RHF220S－4D $\square$ ，RHF160S－69D $\square$ ）

Select terminal screws that allow for a distance of 10 mm or greater to the chassis．


Install relay bar terminals at the cabinet side for the main power supply output terminals．

Furthermore，secure firmly with an insulator to prevent terminal shorting．

| Terminal <br> name | Terminal <br> symbol | Bolt size |
| :---: | :---: | :---: |
| Main power <br> supply input | $\mathrm{L} 1, \mathrm{~L} 2, \mathrm{~L} 3$ |  |
| Main power <br> supply output | $\mathrm{U} 0, \mathrm{~V} 0, \mathrm{~W} 0$ | M 12 |
| Grounding <br> terminal | G |  |

## View from bottom

奃面から見る

Figure 6．4．8－2：Frame 4 size（RHF280S－4D $\square, R H F 355 S-4 D \square$ ）

Select terminal screws that allow for a distance of 10 mm or greater to the chassis．

Unit：［mm］

## Note

Install relay bar terminals at the cabinet side for the main power supply output terminals．
Furthermore，secure firmly with an insulator to prevent terminal shorting．

| Terminal <br> name | Terminal <br> symbol | Bolt size |
| :---: | :---: | :---: |
| Main power <br> supply input | $\mathrm{L} 1, \mathrm{~L} 2, \mathrm{~L} 3$ |  |
| Main power <br> supply output | $\mathrm{U} 0, \mathrm{~V} 0, \mathrm{~W} 0$ | M12 |
| Grounding <br> terminal | G |  |



View from bottom
底面から見る

Figure 6．4．8－3：Frame 4 size（RHF220S to 355S－69D $\square$ ）

Select terminal screws that allow for a distance of 10 mm or greater to the chassis.


## Note

Install relay bar terminals at the cabinet side for the main power supply output terminals.
Furthermore, secure firmly with an insulator to prevent terminal shorting.

| Terminal <br> name | Terminal <br> symbol | Bolt size |
| :---: | :---: | :---: |
| Main power <br> supply input | $\mathrm{L} 1, \mathrm{~L} 2, \mathrm{~L} 3$ |  |
| Main power <br> supply output | $\mathrm{U} 0, \mathrm{~V} 0, \mathrm{WO}$ | M 12 |
| Grounding <br> terminal | G |  |

Figure 6.4.8-4: Frame 5 size (RHF450S-69D $\square$ )

### 6.4.8.2 Control circuit terminal



Figure 6.4.8-5: Control terminal layout

### 6.4.9 Configuration of peripherals

(1) In the case of MD

|  | PWM converter model | Filter stack |  | MCCB/ELCB rated current <br> [A] | Electromagnetic contactor |  | AC Fuse |  | Microswitch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model | $\begin{aligned} & 10 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \hline 0 \\ & \hline \end{aligned}$ |  | Model | 年 | Model | ( | Model |  |
|  | RHC132S-4D $\square$ | RHF160S-4D $\square$ | 1 | 300 | SC-N8 | 1 | 170M5446 | 3 | 170H3027 | 3 |
|  | RHC160S-4D $\square$ | RHF160S-4D $\square$ | 1 | 350 | SC-N11 | 1 | 170M6546 | 3 |  |  |
|  | RHC200S-4D $\square$ | RHF220S-4D $\square$ | 1 | 500 | SC-N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC220S-4D $\square$ | RHF220S-4D $\square$ | 1 | 500 | SC-N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC280S-4D $\square$ | RHF280S-4D $\square$ | 1 | 600 | SC-N14 | 1 | 170M6499 | 3 |  |  |
|  | RHC315S-4D $\square$ | RHF355S-4D $\square$ | 1 | 700 | SC-N14 | 1 | 170M6500 | 3 |  |  |
|  | RHC132S-69D $\square$ | RHF160S-69D $\square$ | 1 | 175 | SC-N6 | 1 | 70M5447 | 3 |  |  |
|  | RHC160S-69D $\square$ | RHF160S-69D $\square$ | 1 | 200 | SC-N7 | 1 | 俍5447 | 3 |  |  |
|  | RHC200S-69D $\square$ | RHF220S-69D $\square$ | 1 | 250 | SC-N8 | 1 | 170M5448 | 3 |  |  |
|  | RHC250S-69D $\square$ | RHF280S-69D $\square$ | 1 | 300 | SC-N8 | 1 | 170M6548 | 3 |  |  |
|  | RHC280S-69D $\square$ | RHF280S-69D $\square$ | 1 | 350 | SC-N11 | 1 |  |  |  |  |
|  | RHC315S-69D $\square$ | RHF355S-69D $\square$ | 1 | 400 | SC-N11 | 1 |  |  |  |  |
|  | RHC355S-69D $\square$ | RHF355S-69D $\square$ | 1 | 500 | SC-N12 | 1 | 170M6500 | 3 |  |  |
|  | RHC400S-69D $\square$ | RHF450S-69D $\square$ | 1 | 500 | SC-N12 | 1 |  |  |  |  |
|  | RHC450S-69D $\square$ | RHF450S-69D $\square$ | 1 | 600 | SC-N14 | 1 |  |  |  |  |

(2) In the case of LD

|  | PWM converter model | Filter stack |  | MCCB/ELCB rated current <br> [A] | Electromagnetic contactor |  | AC Fuse |  | Microswitch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model |  |  | Model | ? | Model | (1) | Model | 2 |
|  | RHC132S-4D $\square$ | RHF160S-4D $\square$ | 1 | 350 | SC-N11 | 1 | 170M5446 | 3 | 170H3027 | 3 |
|  | RHC160S-4D $\square$ | RHF220S-4D | 1 | 500 | SC-N12 | 1 | 170M6546 | 3 |  |  |
|  | RHC200S-4D $\square$ | RHF220S-4D $\square$ | 1 | 500 | SC-N12 | 1 | 170M6547 | 3 |  |  |
|  | RHC280S-4D $\square$ | RHF355S-4D | 1 | 700 | SC-N14 | 1 | 170M6499 | 3 |  |  |
|  | RHC315S-4D $\square$ | RHF355S-4D $\square$ | 1 | 800 | SC-N14 | 1 | 170M6500 | 3 |  |  |
|  | RHC132S-69D $\square$ | RHF160S-69D $\square$ | 1 | 200 | SC-N7 | 1 | 70M5447 | 3 |  |  |
|  | RHC160S-69D $\square$ | RHF220S-69D $\square$ | 1 | 250 | SC-N8 | 1 | 70M5447 |  |  |  |
|  | RHC200S-69D $\square$ | RHF220S-69D $\square$ | 1 | 300 | SC-N8 | 1 | 170M5448 | 3 |  |  |
|  | RHC250S-69D $\square$ | RHF280S-69D $\square$ | 1 | 350 | SC-N11 | 1 | 170M6548 | 3 |  |  |
|  | RHC280S-69D $\square$ | RHF355S-69D $\square$ | 1 | 400 | SC-N11 | 1 |  |  |  |  |
|  | RHC315S-69D $\square$ | RHF355S-69D $\square$ | 1 | 500 | SC-N12 | 1 |  |  |  |  |
|  | RHC355S-69D $\square$ | RHF450S-69D $\square$ | 1 | 500 | SC-N12 | 1 | 170M6500 | 3 |  |  |
|  | RHC400S-69D $\square$ | RHF450S-69D $\square$ | 1 | 600 | SC-N14 | 1 |  |  |  |  |

Note The "MCCB/ELCB rated current" column shows the recommended rated current values at panel temperatures $50^{\circ} \mathrm{C}$ or lower.

* Since the ambient temperature is $40^{\circ} \mathrm{C}$, the installation environment standards for MCCBs or ELCBs have been selected taking into account the correction coefficient depending on the temperature conditions ( 0.90 for 800 AF or lower; 0.85 for 1000AF or higher). To select a specific model, consider the short-circuit breaking capacity of the equipment.
[1] Refer to "6.2.12.3 Use of molded case circuit breakers (MCCBs)" and "6.2.12.4 Use of earth leakage circuit breakers (ELCBs)".


### 6.4.10 AC fuse external view

Table 6.4.10-1: AC fuse external dimensions table

| Drawing No. | Dimensions [mm] |  |  |  |  |  |  | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | D | E | F | G | H |  |
| 170M5446 | 80 | 81 | 77 | 61 | M10 | 10 | ø24 | 0.9 |
| 170M5447 |  |  |  |  |  |  |  |  |
| 170M5448 |  |  |  |  |  |  |  |  |
| 170M6546 | 81 | 83 | 92 | 76 | M12 | 10 | $ø 30$ | 1.25 |
| 170M6547 |  |  |  |  |  |  |  |  |
| 170M6548 |  |  |  |  |  |  |  |  |
| 170M6499 | 81 | 91 | 92 | 76 | M12 | 10 | $\varnothing 30$ | 1.25 |
| 170M6500 |  |  |  |  |  |  |  |  |

Note) Column H shows the fuse main circuit terminals.



Figure 6.4.10-2: Microswitch external shape


Figure 6.4.10-1: Microswitch contact structure

Note Attach the microswitch to the fuse so that its tabterminals face down.
Press in the microswitch so that attachment claws hook firmly onto the fuse body.

This red block protrudes if the fuse is blown.


Figure 6.4.10-3: Microswitch attachment method

### 6.4.11 Wire size

### 6.4.11.1 3-phase 400V series

(1) Ambient temperature: $40^{\circ} \mathrm{C}$

| Applicable <br> PWM <br> converters capacity [kW] | RHF $\square$-4D $\square$ | Main input (L1, L2, L3) Output (U0, V0, W0) |  |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Charging circuit (L4) <br> (L5) (L6) [ $\mathrm{mm}^{2}$ ] | $\begin{gathered} \text { Other } \\ (\mathrm{R} 3, \mathrm{~T} 3) \\ (73-1, \quad 73-2) \\ (\mathrm{R} 11, \mathrm{R} 12) \\ (\mathrm{T} 11, \mathrm{~T} 12) \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | Control terminal $(1,2)$ (ONA) (ONB) (ONC) [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wire size $\left[\mathrm{mm}^{2}\right]$ (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current <br> [A] |  |  |  |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| 132 | 160 S | 100 | 100 | 60 | $\begin{gathered} \mathrm{t} 5 \times 30 \\ (150) \end{gathered}$ | 235 | 22 | 2 | 2 | 1.25 |
| 160 |  | 150 |  | 100 |  | 282 | 38 |  |  |  |
| 200 | 220 S | 200 | 150 |  |  | 355 |  |  |  |  |
| 220 |  |  |  |  |  | 384 | 60 |  |  |  |
| 280 | 280S | $2 \times 200$ | $2 \times 150$ | $2 \times 100$ | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 489 |  | 3.5 |  |  |
| 315 | 355S |  |  |  |  | 560 |  |  |  |  |
| 355 |  |  |  |  |  | 619 | 100 |  |  |  |

(2) Ambient temperature: $50^{\circ} \mathrm{C}$

| Applicable PWM converters capacity [kW] | RHF $\square$-4D $\square$ | Main input (L1, L2, L3) Output (U0, V0, W0) |  |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Charging circuit (L4) (L5) (L6) [ $\mathrm{mm}^{2}$ ] | Other (R3, T3) (73-1, 73-2) (R11, R12) (T11, T12) [ $\mathrm{mm}^{2}$ ] | Control terminal $(1,2)$ (ONA) (ONB) (ONC) [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wire size $\left[\mathrm{mm}^{2}\right]$ (Permissible temperature) (Note 1) |  |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current <br> [A] |  |  |  |  |
|  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| 132 | $160 S$ | 200 | 100 | 60 | $\begin{gathered} \mathrm{t} 5 \times 30 \\ (150) \end{gathered}$ | 235 | 22 | 2 | 2 | 1.25 |
| 160 |  | 250 | 150 | 100 |  | 282 | 38 |  |  |  |
| 200 | 220 S | $2 \times 150$ |  | 150 |  | 355 |  |  |  |  |
| 220 |  | $2 \times 200$ | 200 |  |  | 384 | 60 |  |  |  |
| 280 | 280S | 2×325 | $2 \times 200$ | $2 \times 150$ | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 489 |  | 3.5 |  |  |
| 315 | 355S |  |  |  |  | 560 |  |  |  |  |
| 355 |  |  |  |  |  | 619 | 100 |  |  |  |

The power supply voltage is 400 VAC.
(Note 1) An "IV wire," a "600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.
(Note 2) The grounding wire is cited from the permissible short circuit current defined in internal wire regulations

### 6.4.11.2 3-phase 690V series

(1) IEC standard, ambient temperature $40^{\circ} \mathrm{C}$

| Applicable PWM converters capacity [kW] | RHF $\square$-69D $\square$ | Main input (L1, L2, L3) Output (U0, V0, W0) |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Charging circuit (L4) (L5) (L6) [ $\mathrm{mm}^{2}$ ] | Other <br> (R3, T3) <br> (73-1, 73-2) <br> (R11, R12) <br> (T11, T12) <br> [ $\mathrm{mm}^{2}$ ] | Control terminal $(1,2)$ (ONA) (ONB) (ONC) [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wire size [ $\mathrm{mm}^{2}$ ] (Permissible temperature) (Note 1) |  | $\begin{gathered} \text { Bus bar } \\ \text { size } \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | Current <br> [A] |  |  |  |  |
|  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| 132 | 160 S | 70 | 35 | $\begin{gathered} t 5 \times 30 \\ (150) \end{gathered}$ | 135 | 35 | 2.5 | 2.5 | 0.75 |
| 160 |  |  | 50 |  | 163 |  |  |  |  |
| 200 | 220S | 95 | 70 |  | 205 | 50 |  |  |  |
| 250 | 280S | 150 | 95 | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 253 | 95 | 4 |  |  |
| 280 |  | 185 | 120 |  | 283 |  |  |  |  |
| 315 | 355S | 240 | 150 |  | 319 | 120 |  |  |  |
| 355 |  |  |  |  | 359 |  |  |  |  |
| 400 | 450S | 300 | 185 |  | 405 | 150 |  |  |  |
| 450 |  | 2x150 | 2x95 |  | 455 |  |  |  |  |

(Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$, and the wire sizes were selected based on the permissible current under the following conditions. If usage conditions differ, select wire sizes based on usage conditions that comply with IEC 60364-5-52:2001 (JIS C 60364-5-52:2006)
Ambient temperature: $40^{\circ} \mathrm{C}$, Multicore cable: 3 cores (conductor: copper), Single cable: aerial wiring, Two or more cables: electric duct wiring
(Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

## (2) Domestic selection, ambient temperature $40^{\circ} \mathrm{C}$

| Applicable PWM converters capacity [kW] | RHF $\square$-69D $\square$ | Main input (L1, L2, L3) Output (U0, V0, W0) |  |  |  | Grounding wire [ $\mathrm{mm}^{2}$ ] <br> (Note 2) | Charging circuit (L4) <br> (L5) <br> (L6) [ $\mathrm{mm}^{2}$ ] | $\begin{gathered} \text { Other } \\ \text { (R3, T3) } \\ (73-1,73-2) \\ \text { (R11, R12) } \\ (\mathrm{T} 11, \mathrm{~T} 12) \\ {\left[\mathrm{mm}^{2}\right]} \end{gathered}$ | Control terminal $(1,2)$ (ONA) (ONB) (ONC) [ $\mathrm{mm}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\qquad$ <br> Wire size [ $\mathrm{mm}^{2}$ ] (Permissible temperature) (Note 1) |  | Bus bar size [ $\mathrm{mm}^{2}$ ] | Current <br> [A] |  |  |  |  |
|  |  | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| 132 | 160 S | 38 | 22 | $\begin{gathered} \text { t5 } \times 30 \\ (150) \end{gathered}$ | 135 | 22 | 2 | 2 | 1.25 |
| 160 |  |  | 38 |  | 163 |  |  |  |  |
| 200 | 220S | 60 | 60 |  | 205 |  |  |  |  |
| 250 | 280S | 100 |  | $\begin{gathered} \mathrm{t} 10 \times 30 \\ (300) \end{gathered}$ | 253 | 38 | 3.5 |  |  |
| 280 |  |  | 100 |  | 283 |  |  |  |  |
| 315 | 355S | 150 |  |  | 319 |  |  |  |  |
| 355 |  |  |  |  | 359 |  |  |  |  |
| 400 | 450 S |  | 150 |  | 405 | 60 |  |  |  |
| 450 |  | 200 |  |  | 455 |  |  |  |  |

(Note 1) PVC was used for permissible temperature of $70^{\circ} \mathrm{C}$, and XLPE for permissible temperature of $90^{\circ} \mathrm{C}$.
(Note 2) Refer to Appendix 9 for information on wire permissible current based on ambient temperature.

### 6.4.12 Generated loss

Table 6.4.12-1 shows filter stack generated losses.
Table 6.4.12-1: Filter stack generated losses

| Power-based series | Model | Generated loss [W] |
| :---: | :--- | :---: |
| 3 3-phase 400V | RHF160S-4D $\square$ | 2850 |
|  | RHF220S-4D $\square$ | 3700 |
|  | RHF280S-4D $\square$ | 4600 |
|  | RHF355S-4D $\square$ | 5250 |
|  | RHF160S-69D $\square$ | 2550 |
|  | RHF220S-69D $\square$ | 3350 |
|  | RHF280S-69D $\square$ | 4150 |
|  | RHF355S-69D $\square$ | 5050 |
|  | RHF450S-69D $\square$ | 6550 |

### 6.5 Braking system (braking unit, braking resistor)

The braking system (braking unit and braking resistor) provides a braking system that consumes regenerative energy from a motor as thermal energy by use of the resistor.
It can be used when using the RHD-D series diode rectifiers to construct a system where regenerative energy is generated.

### 6.5.1 Overview of braking resistor (DBR)

The FRENIC-VG provides two kinds of braking resistors (DBR):10\%ED and 20\%ED.
[1] For information on how to select a braking resistor, refer to "9.1.3.3 Selecting the braking resistor with the correct rating" in Chapter 9 of the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019).


A braking resistor overheat error function that detects the overheat error of the braking resistor is available.
The overheat error signal should be taken into the FRENIC-VG to prevent burning of the braking resistor.
$\mathbb{\square}]$ For information on the specifications, external dimensions, and connection method, refer to "8.5.1.1 overview of braking resistor (DBR)" in Chapter 8 of the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019).

### 6.5.2 Overview of braking unit

This braking unit for braking control is intended to consume the regenerative energy from the motor as thermal energy.
It is used in conjunction with the braking resistor.
The standard duty cycle of the braking unit is the $10 \%$ ED rating. When the fan unit (option:
BU-F) is installed, however, the braking capacity is increased to the $30 \%$ ED.
Additionally, up to 15 braking units can be connected in parallel.
In addition to the standard series, BUC560-4C with a continuous regenerative capacity of 560 kW is also available.


This section describes the braking unit on the assumption of using the standard series braking unit.
[0] For details, refer to the instruction manuals listed below.
Instruction manual for braking unit: INR-HF51196*
Supplemental description of instruction manual for braking unit: INR-HF51614*
Table 6.5.2-1: Standard braking unit specifications


### 6.5.3 Standard combination

(1) $10 \% \mathrm{ED}$ spec

Table 6.5.3-1: List of regenerative performance (10\%ED spec)

| $\begin{aligned} & \mathbb{\otimes} \\ & \stackrel{0}{0} \end{aligned}$ |  |  | $\begin{aligned} & \text { E } \\ & \stackrel{\mathbb{N}}{0} \end{aligned}$ |  | Stand | dard combinatio |  |  |  | braking [\%] | orque | Continuou (150\% | braking torque | Repetiti (Cycle | braking 100 sec . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 8 \\ & \geq \end{aligned}$ |  | 举 | 粫 | Braking |  | Braking | resistor |  |  |  |  | convers | n value) |  | ess) |
| $\overline{0}$ | spec | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{0} \\ & \hline 0 \\ & \hline 0 \end{aligned}$ | $\stackrel{.0}{\bar{O}}$ |  |  |  |  | $\stackrel{\otimes}{\subset}$ |  | rque | ] |  |  |  | Average |
| $\begin{aligned} & \text { No } \\ & \sum_{0}^{2} \\ & \hline \end{aligned}$ |  | $\underset{\sim}{\square}$ | $\begin{aligned} & 0 \\ & \hline 0 \\ & \hline 0 \end{aligned}$ | Model |  | Model |  |  |  | $\begin{aligned} & 50 \\ & \mathrm{~Hz} \end{aligned}$ | $\begin{aligned} & 60 \\ & \mathrm{~Hz} \end{aligned}$ | time [s] | capability <br> [kWs] | cycle <br> [\%ED] | loss <br> [kW] |
|  |  | 3.7 |  |  |  | DB3.7V-41B | 1 | 96 | 150 | 35.3 | 29.4 | 10 | 27.8 | 10 | 0.278 |
|  |  | 5.5 |  |  |  | DB5.5V-41B | 1 | 64 |  | 52.5 | 43.8 |  | 41.3 |  | 0.413 |
|  |  | 7.5 |  |  |  | DB7.5V-41B | 1 | 48 |  | 71.6 | 59.7 |  | 56.3 |  | 0.563 |
|  |  | 11 |  | BU37-4C | 1 | DB11V-41B | 1 | 32 |  | 105 | 87.5 |  | 82.5 |  | 0.825 |
|  |  | 15 |  |  |  | DB15V-41B | 1 | 24 |  | 143 | 119 |  | 113 |  | 1.13 |
|  |  | 18.5 |  |  |  | DB18.5V-41B | 1 | 18 |  | 177 | 147 |  | 139 |  | 1.39 |
|  |  | 22 |  |  |  | DB22V-41B | 1 | 16 |  | 210 | 175 |  | 165 |  | 1.65 |
|  |  | 30 | A | B455-4C |  | DB30V-41B | 1 | 10 |  | 286 | 239 |  | 225 |  | 2.25 |
|  |  | 37 |  |  |  | DB37V-41B | 1 | 9.0 |  | 353 | 294 |  | 278 |  | 2.78 |
|  |  | 45 |  | BU90-4C | 1 | DB45V-41B | 1 | 8.0 |  | 430 | 358 |  | 338 |  | 3.38 |
|  |  | 55 |  | BU0-4C |  | DB55V-41C | 1 | 6.5 |  | 525 | 438 |  | 413 |  | 4.13 |
|  | MD | 75 |  | BU132-4C | 1 | DB75V-41C | 1 | 4.7 |  | 716 | 597 |  | 563 |  | 5.63 |
|  | spec | 90 |  | BU132-4C |  | DB90V-41C | 1 | 3.9 |  | 859 | 716 |  | 675 |  | 6.75 |
|  |  | 110 |  |  |  | DB110V-41C | 1 | 3.2 |  | 1050 | 875 |  | 825 |  | 8.25 |
|  |  | 132 |  | BU220-4C | 1 | DB132V-41C | 1 | 2.6 |  | 1261 | 1050 |  | 990 |  | 9.90 |
|  |  | 160 | C |  |  | DB160V-41C | 1 | 2.2 |  | 1528 | 1273 |  | 1200 |  | 12.0 |
|  |  | 200 |  |  |  | DB200V-41C | 1 | 3.5/2 |  | 1910 | 1592 |  | 1500 |  | 15.0 |
|  |  | 220 |  | BU220-4C | 2 | DB220V-41C | 1 | 3.2/2 |  | 2101 | 1751 |  | 1650 |  | 16.5 |
|  |  | 280 |  |  | 2 | DB160V-41C | 2 | 2.2/2 |  | 2674 | 2228 |  | 2100 |  | 21.0 |
|  |  | 315 |  |  |  | DB160V-41C | 2 | 2.2/2 |  | 3008 | 2507 |  | 2363 |  | 23.6 |
|  |  | 355 |  |  |  | DB132V-41C | 3 | 2.6/3 |  | 3390 | 2825 |  | 2663 |  | 26.6 |
|  |  | 400 |  | BU220-4C |  | DB132V-41C | 3 | 2.6/3 |  | 3820 | 3183 |  | 3000 |  | 30.0 |
|  |  | 500 | G | - 220 - |  | DB132V-41C | 4 | 2.6/4 |  | 4775 | 3979 |  | 3750 |  | 37.5 |
|  |  | 630 | H |  |  | DB160V-41C | 4 | 2.2/4 |  | 6016 | 5013 |  | 4725 |  | 47.3 |
|  | $\begin{gathered} \text { LD } \\ \text { spec } \end{gathered}$ | 37 | A | BU55-4C | 1 | DB30V-41B | 1 | 10 | 110 | 259 | 216 | 10 | 204 | 10 | 2.25 |
|  |  | 45 |  |  |  | DB37V-41B | 1 | 9.0 |  | 315 | 263 |  | 248 |  | 2.78 |
|  |  | 55 |  | BU90-4C | 1 | DB45V-41B | 1 | 8.0 |  | 385 | 321 |  | 303 |  | 3.38 |
|  |  | 75 |  | BU90-4C | 1 | DB55V-41C | 1 | 6.5 |  | 525 | 438 |  | 413 |  | 4.13 |
|  |  | 90 |  | BU132-4C |  | DB75V-41C | 1 | 4.7 |  | 630 | 525 |  | 495 |  | 5.63 |
|  |  | 110 |  | BU132-4C |  | DB90V-41C | 1 | 3.9 |  | 770 | 642 |  | 605 |  | 6.75 |
|  |  | 132 |  |  |  | DB110V-41C | 1 | 3.2 |  | 924 | 770 |  | 726 |  | 8.25 |
|  |  | 160 |  | BU220-4C | 1 | DB132V-41C | 1 | 2.6 |  | 1120 | 934 |  | 880 |  | 9.9 |
|  |  | 200 | C |  |  | DB160V-41C | 1 | 2.2 |  | 1401 | 1167 |  | 1100 |  | 12.0 |
|  |  | 220 |  |  |  | DB200V-41C | 1 | 3.5/2 |  | 1541 | 1284 |  | 1210 |  | 15.0 |
|  |  | 280 | D | BU220-40 |  | DB220V-41C | 1 | 3.2/2 |  | 1961 | 1634 |  | 1540 |  | 16.5 |
|  |  | 355 |  | BU220-4C |  | DB160V-41C | 2 | 2.2/2 |  | 2486 | 2072 |  | 1953 |  | 21.0 |
|  |  | 400 | E |  |  | DB160V-41C | 2 | 2.2/2 |  | 2801 | 2334 |  | 2200 |  | 23.6 |
|  |  | 450 |  |  |  | DB132V-41C | 3 | 2.6/3 |  | 3151 | 2626 |  | 2475 |  | 26.6 |
|  |  | 500 | F | BU220-4C | 3 | DB132V-41C | 3 | 2.6/3 |  | 3501 | 2918 |  | 2750 |  | 30.0 |
|  |  | 630 | G | BU220-4C | 4 | DB132V-41C | 4 | 2.6/4 |  | 4412 | 3677 |  | 3465 |  | 37.5 |
|  |  | 710 | H |  |  | DB160V-41C | 4 | 2.2/4 |  | 4972 | 4143 |  | 3905 |  | 47.3 |

The models DB160V-41C to DB220V-41C use two braking resistors per unit.
Example) Four braking resistors are used for two units of the model DB160V-41C.
(2) $20 \%$ ED spec

Table 6.5.3-2: List of regenerative performance (20\%ED spec)

|  | MD/LD spec |  |  | Standard combination |  |  |  |  | Max. braking torque $\qquad$ <br> [\%] <br> Torque $[\mathrm{N} \cdot \mathrm{m}]$ |  |  | $\begin{array}{\|c\|} \hline \text { Continuous braking } \\ \text { (150\%-torque } \\ \text { conversion value) } \\ \hline \end{array}$ |  | Repetition braking (Cycle is 100 sec . or less) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Braking unit |  | Braking resistor |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | $\underset{\sim}{\otimes}$ |  |  |  |  | Dis- |  |  |
|  |  |  |  | Model | $\begin{array}{ll} 1 \\ 0 \\ 0 \\ 0 & 0 \\ 0 & 0 \\ 5 \end{array}$ | Model |  | $\begin{aligned} & \stackrel{\pi}{0} \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \stackrel{y}{0} \end{aligned}$ |  | 50 Hz | $\begin{aligned} & 60 \\ & \mathrm{~Hz} \end{aligned}$ | time [s] | charging capability [kWs] | cycle <br> [\%ED] | loss <br> [kW] |
|  |  | 3.7 |  |  |  | DB3.7V-42B | 1 | 96 | 150 | 35.3 | 29.4 | 20 | 55.5 | 20 | 0.555 |
|  |  | 5.5 |  |  |  | DB5.5V-42B | 1 | 64 |  | 52.5 | 43.8 |  | 82.5 |  | 0.825 |
|  |  | 7.5 |  |  |  | DB7.5V-42B | 1 | 48 |  | 71.6 | 59.7 |  | 113 |  | 1.13 |
|  |  | 11 |  |  | 1 | DB11V-42B | 1 | 32 |  | 105 | 87.5 |  | 165 |  | 1.65 |
|  |  | 15 |  |  |  | DB15V-42B | 1 | 24 |  | 143 | 119 |  | 225 |  | 2.25 |
|  |  | 18.5 |  |  |  | DB18.5V-42B | 1 | 18 |  | 177 | 147 |  | 278 |  | 2.78 |
|  |  | 22 |  |  |  | DB22V-42B | 1 | 16 |  | 210 | 175 |  | 330 |  | 3.30 |
|  |  | 30 | A | BU55-4C |  | DB30V-42C | 1 | 12 |  | 286 | 239 |  | 450 |  | 4.50 |
|  |  | 37 |  | +BU-F |  | DB37V-42C | 1 | 9.0 |  | 353 | 294 |  | 555 |  | 5.55 |
|  |  | 45 |  | BU90-4C |  | DB45V-42C | 1 | 8.0 |  | 430 | 358 |  | 675 |  | 6.75 |
|  |  | 55 |  | +BU-F |  | DB55V-42C | 1 | 6.5 |  | 525 | 438 |  | 825 |  | 8.25 |
|  | MD | 75 |  | BU132-4C |  | DB75V-42C | 1 | 4.7 |  | 716 | 597 |  | 1125 |  | 11.3 |
|  | spec | 90 |  | +BU-F |  | DB90V-42C | 1 | 3.9 |  | 859 | 716 |  | 1350 |  | 13.5 |
|  |  | 110 |  |  |  | DB110V-42C | 1 | 3.2 |  | 1050 | 875 |  | 1650 |  | 16.5 |
|  |  | 132 |  |  | 1 | DB132V-42C | 1 | 2.6 |  | 1261 | 1050 |  | 1980 |  | 19.8 |
|  |  | 160 | C |  |  | DB160V-42C | 1 | 2.2 |  | 1528 | 1273 |  | 2400 |  | 24.0 |
|  |  | 200 | D |  |  | DB200V-42C | 1 | 3.5/2 |  | 1910 | 1592 |  | 3000 |  | 30.0 |
|  |  | 220 |  | BU220-4C |  | DB220V-42C | 1 | 3.2/2 |  | 2101 | 1751 |  | 3300 |  | 33.0 |
|  |  | 280 | E | +BU-F |  | DB160V-42C | 2 | 2.2/2 |  | 2674 | 2228 |  | 4200 |  | 42.0 |
|  |  | 315 | E |  |  | DB160V-42C | 2 | 2.2/2 |  | 3008 | 2507 |  | 4725 |  | 47.3 |
|  |  | 355 | F | BU220-4C | 3 | DB132V-42C | 3 | 2.6/3 |  | 3390 | 2825 |  | 5325 |  | 53.3 |
|  |  | 400 |  | +BU-F |  | DB132V-42C | 3 | 2.6/3 |  | 3820 | 3183 |  | 6000 |  | 60.0 |
|  |  | 500 | G | BU220-4C | 4 | DB132V-42C | 4 | 2.6/4 |  | 4775 | 3979 |  | 7500 |  | 75.0 |
|  |  | 630 | H | +BU-F |  | DB160V-42C | 4 | 2.2/4 |  | 6016 | 5013 |  | 9450 |  | 94.6 |
|  | $\begin{gathered} \text { LD } \\ \text { spec } \end{gathered}$ | 37 | A | BU55-4C | 1 | DB30V-42C | 1 | 12 | 110 | 259 | 216 | 20 | 407 | 20 | 4.50 |
|  |  | 45 |  | +BU-F | 1 | DB37V-42C | 1 | 9.0 |  | 315 | 263 |  | 495 |  | 5.55 |
|  |  | 55 |  | BU90-4C |  | DB45V-42C | 1 | 8.0 |  | 385 | 321 |  | 605 |  | 6.75 |
|  |  | 75 |  | +BU-F | 1 | DB55V-42C | 1 | 6.5 |  | 525 | 438 |  | 825 |  | 8.25 |
|  |  | 90 |  | BU132-4C |  | DB75V-42C | 1 | 4.7 |  | 630 | 525 |  | 990 |  | 11.3 |
|  |  | 110 |  | \|+BU-F |  | DB90V-42C | 1 | 3.9 |  | 770 | 642 |  | 1210 |  | 13.5 |
|  |  | 132 |  |  |  | DB110V-42C | 1 | 3.2 |  | 924 | 770 |  | 1452 |  | 16.5 |
|  |  | 160 |  |  | 1 | DB132V-42C | 1 | 2.6 |  | 1120 | 934 |  | 1760 |  | 19.8 |
|  |  | 200 | C |  |  | DB160V-42C | 1 | 2.2 |  | 1401 | 1167 |  | 2200 |  | 24.0 |
|  |  | 220 |  | $\begin{aligned} & \text { BU220-4C } \\ & + \text { BU-F } \end{aligned}$ | 2 | DB200V-42C | 1 | 3.5/2 |  | 1541 | 1284 |  | 2420 |  | 30.0 |
|  |  | 280 |  |  |  | DB220V-42C | 1 | 3.2/2 |  | 1961 | 1634 |  | 3080 |  | 33.0 |
|  |  | 355 |  |  |  | DB160V-42C | 2 | 2.2/2 |  | 2486 | 2072 |  | 3905 |  | 47.3 |
|  |  | 400 |  |  |  | DB132V-42C | 3 | 2.6/3 |  | 2801 | 2334 |  | 4400 |  | 53.3 |
|  |  | 450 | F | BU220-4C | 3 | DB132V-42C | 3 | 2.6/3 |  | 3151 | 2626 |  | 4950 |  | 53.3 |
|  |  | 500 |  | +BU-F |  | DB132V-42C | 3 | 2.6/3 |  | 3501 | 2918 |  | 5500 |  | 60.0 |
|  |  | 630 | G | $\begin{aligned} & \text { BU220-4C } \\ & \text { +BU-F } \end{aligned}$ | 4 | DB132V-42C | 4 | 2.6/4 |  | 4412 | 3677 |  | 6930 |  | 75.0 |
|  |  | 710 | H |  |  | DB160V-42C | 4 | 2.2/4 |  | 4972 | 4143 |  | 7810 |  | 94.6 |

Note (1) This option is a custom order production product.
(2) The fan unit (BU-F) is needed for the braking unit.

The models DB200V-42C and DB220V-42C use two braking resistors per unit.
Example) Two braking resistors are used for one unit of the model DB200V-42C.

### 6.5.4 Installation

## Braking resistor (DBR)

(1) In the case of continuous regeneration, the braking resistor heats the average loss of the repetition braking (cycle: 100 sec .) stated in the List of regenerative performance values in Section 6.5.3.
Additionally, when the braking resistor uses metallic grid resistance elements, its surface temperature may reach $100^{\circ} \mathrm{C}$ or more.
Therefore, it is recommended to install the braking resistor on the top of the cabinet. ( $\mathbb{R}$ Refer to "12.5.2 Principles in designing layout in cabinets" in Chapter 12.)
(2) When storing the braking resistor into the cabinet, heat radiation measures must be investigated sufficiently. (Investigate a structure where the heat of the DBR does not adversely affect units stored inside the cabinet.)

## Braking unit

(1) Install vertically. Do not install upside down or horizontally.
(2) Keep a space as illustrated in Figure 6.5.4-1. Additionally, since the heat radiates toward the upper portion, do not install units vulnerable to the heat at the upper portion of the braking unit.
(3) Cooling fins are installed on the rear of the braking unit. When the braking unit operates continuously, the fin temperature may increase to approx. $90^{\circ} \mathrm{C}$. So, appropriate materials that can endure the temperature increase should be used for the rear.
(4) When using multiple braking units, arrange them horizontally to minimize the mutual heat interference. However, when installing the braking units vertically due to restrictions on space inside the cabinet, partition plates or the like should be mounted to prevent the effects of the heat at the lower portion on the upper portion. ( $\mathbb{C l}$ Refer to "12.5.2 Principles in designing layout in cabinets" in Chapter 12.)


Figure 6.5.4-1: Restrictions on braking unit installation

### 6.5.5 Protective operation

If an error stated in Table 6.5.5-1 occurs, the braking unit stops the DB drive and outputs the alarm signal (for any alarm) from terminals 1 and 2. (The alarm signal (for any alarm) has no error content classifications.) It is necessary to use this alarm signal so as to put the inverter in the coast-to-a-stop status (i.e., [OH2: external alarm] or [BX: coast-to-a-stop command] is input to the $X$ terminal).

Table 6.5.5-1: Contents of protective operation

| Item | Contents (Structure) |
| :--- | :--- |
| Fuse blown | Operates if the fuse in the braking unit main circuit is blown by short-circuit or breakage of <br> the circuit. |
| Cooling unit overheat | Operates if the temperature of the unit cooling fins increases due to frequent braking <br> operation exceeding the specifications, high ambient temperature, or clogging of cooling <br> fins. |
| IGBT (switching element) <br> conduction error | Operates if the IGBT (switching element) detects the conduction even when the DB drive <br> signal shows the stop status. |
| Braking resistor overheat | Operates if the operation frequency of the braking resistor becomes high and the <br> temperature of the braking resistor increases. |

### 6.5.6 Cautions on use of terminal functions

### 6.5.6.1 Braking resistor (DBR)

Table 6.5.6-1: List of braking resistor (DBR) terminals

| Terminal <br> symbol | Terminal name | Description |
| :--- | :--- | :--- |
| P, DB | DB unit connection terminal | Connect the P(+)R and DB terminals of the braking unit to these <br> terminals. |
| 1,2 | Braking resistor overheat error | Braking resistor overheat error detection terminal |
| $\boldsymbol{\Theta}$ G | For braking resistor grounding | Grounding terminal |

### 6.5.6.2 Braking unit

(1) Main circuit and grounding terminal connections

Table 6.5.6-2: Functions of main circuit and grounding terminals

| Terminal <br> symbol | Terminal name | Description |
| :--- | :--- | :--- |
| $\mathrm{P}(+), \mathrm{DB}(-)$ | Braking resistor <br> connection terminal | Connect to the $\mathrm{P}(+) \mathrm{R}$ and DB terminals of the braking resistor. |
| $\mathrm{P}(+) \mathrm{R}, \mathrm{DB}$ | Braking resistor <br> connection terminals | Connect to the braking resistor. |
| $\boldsymbol{\Theta} \mathrm{G}$ | For braking unit <br> grounding | Grounding terminal |

(1) $D C$ interconnecting terminals $[(P(+), N(-)]$

1) Connect the $D C$ intermediate circuit terminals $P(+)$ and $N(-)$ of the inverter to the terminals $P(+)$ and $N(-)$ of the braking unit.
2) Lay out the units so that the wiring length is 5 m or less. Additionally, perform the twist wiring or close-contact (parallel) wiring for two wires.
(2) Braking resistor connection terminals [ $(P(+) R$ and $D B)]$
3) Connect the terminals $P$ and $D B$ of the braking resistor to the terminals $P(+) R$ and $D B$ of the braking unit.
4) Lay out the units so that the wiring length is 10 m or less. Additionally, perform the twist wiring or close-contact (parallel) wiring for two wires.
(3) Unit grounding terminal [G]

To ensure the safety and take noise prevention measures, be sure to ground the unit grounding terminal $\boldsymbol{\oplus} \boldsymbol{G}$. In the Electrical Equipment Technical Standards, it is instructed to perform the grounding to the metallic frame of the electrical equipment so as to prevent accidents, such as electric shock or fire.
When making connections, observe the following:

1) According to the Electrical Equipment Technical Standards, connect the grounding terminal to the grounding pole where the class C grounding work has been made.
2) Connect a thick wire to the grounding terminal with a short distance and connect the grounding terminal to the grounding pole dedicated to the inverter system.
For more details, refer to Section 6.5.8.1.
(2) Control terminal connections

Table 6.5.6-3: Functions of control terminals

| Terminal <br> symbol | Terminal name | Description |
| :--- | :--- | :--- |
| 1,2 | Braking unit alarm output <br> (for any alarm) | Outputs a failure signal, such as IGBT overheat or fuse blown <br> inside the braking unit <br> Additionally, this terminal also detects an alarm to stop the DB <br> operation when an error signal is input from the braking unit or <br> braking resistor. <br> Rating: 24 VDC, 3 to 30 mA (max) |
| $\mathrm{i1}, \mathrm{i2}$ | DB drive slave input terminal | Use this terminal when connecting braking units in parallel. <br> Remaining slave units are controlled at the DB operation <br> detection level of the master unit. <br> (Cal For details, refer to "6.5.6.2 (3) Examples of connection <br> diagrams". |
| o1, o2, | DB drive master output terminal |  |
| CN5, CN6 | Option fan power supply connection <br> connector | Connect the fan power wires when an optional fan is installed. |

## 2-1) Braking unit alarm output (for any alarm) [1, 2]

Connect the braking unit and braking resistor terminals to the contact inputs assigned to the external alarm input in series like $1 \Rightarrow 2 \Rightarrow 1 \Rightarrow 2$. A photo-coupler is used inside the braking unit to detect an error signal from other braking unit or braking resistor as illustrated in Figure 6.5.6-1. This photo-coupler has a voltage drop of approx. 1 V . When multiple braking units are connected as a loop, the alarm does not operate by the voltage drop of the photo-coupler.

Therefore, the DB error detection loop connection is restricted as follows.

- Direct input to INV: Up to 3 units
- Detection by relay: Up to 4 units


Figure 6.5.6-1: Braking unit and DBR alarm detection circuit (example)
[a] For details on relay connections, refer to Figure 6.5.6-6 "Circuit diagram when detecting DB error by relay".
2-2) DB drive master-slave terminals [input: i1, i2, output: o1, o2]
(1) These terminals are used when two or more braking units are connected in parallel.
(Master-slave wiring.)
For details about how to connect the terminals, refer to Figure 6.5.6-5.
(2) When using a single braking unit, set SW1 as illustrated in Figure 6.5.6-2-a. (Factory default)
(3) When using braking units in the parallel connection, the SW1 is as follows:


Figure 6.5.6-2: Switching braking unit's SW1

- Master: Short-circuit 2-3 of a). (Factory default)
- Slave: Short-circuit 1-2 of b).
(4) To prevent malfunction by noise, use a twisted wiring for the "master-slave wiring" and make the connection with a wiring length of 1.5 m or less (as a rough guideline).


## 2-3) Option fan power supply connection connectors (CN5 and CN6)

(1) Connect the DC power supply of the BU-F fan unit (option).
(2) The connectors CN5 and CN6 have the same function.
(3) Do not short-circuit the connectors when they are not used.

Note (1) Separate the control wiring from the main circuit wiring.
(Preventive measures against malfunction by noise.)
(2) Secure the control wiring inside the braking unit so that it is not directly in contact with the electrically live part of the main circuit (terminal block of main circuit).
[a] For details, refer to the braking unit instruction manual (INR-HF51196*).


Figure 6.5.6-3: Braking unit control PCB

## (3) Examples of connection diagrams



Figure 6.5.6-4: Basic connection diagram


Figure 6.5.6-5: Connection diagram with braking units used in parallel

## (4) DB circuit error is detected by relay

When detecting the error signal of the braking unit or braking resistor by the relay or when stopping multiple inverters, use the configuration illustrated in Figure 6.5.6-6.


Figure 6.5.6-6: Circuit diagram when detecting DB error by relay
Note (1) Use a relay that excites the coil using a minute current for the relay, to which the error signal of the braking unit is input. (Recommended: RS4N-DE 24VDC)
(2) In this circuit example, "DB error" to be input to the inverter is normally ON (ON during normal operation). Therefore, the DB error $(\mathrm{OH} 2)$ is given if the inverter control power starts up earlier than the external 24 V power supply.
(3) When using the DBR for the equipment that restarts after momentary stop, back up the 24 V power supply. If measures for momentary stop are not taken, the DB error $(\mathrm{OH} 2)$ is given.

### 6.5.7 Peripheral equipment

The peripherals used in the braking system as shown in Figure 6.5.7-1 have the following circuits.

| NSW: | A circuit breaker used to separate the braking unit from the DC bus bar (PN). <br> Since this circuit breaker is used in the common bus bar (DC) shared with the inverter, do not use <br> a molded case circuit breaker (MCCB) with braking characteristics. Be sure to use a non-auto <br> switch. |
| :--- | :--- |
| Charging circuit: | This circuit is intended for initial charging of the braking unit. The circuit is composed of an initial <br> charging resistor, a magnetic contactor, and an option box "MCA-VG7-VSU". |

It is not particularly necessary to install the peripheral equipment for normal operation applications.


Figure 6.5.7-1: Peripheral equipment configuration for braking system

|  | Quantity used | Circuit breaker (NSW) | Charging circuit |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Magnetic contactor (73) | Charging resistor | Voltage detector |
| BU37-4C | 1 | BW400RAS-4P | SC-N1+SZ-SP3 | GZG100W 20』J (JRM) | MCA-VG7-VSU |
| BU55-4C | 1 |  |  |  |  |
| BU90-4C | 1 |  |  |  |  |
| BU132-4C | 1 |  |  |  |  |
| BU220-4C | 1 |  |  |  |  |
|  | 2 |  | SC-N3+SZ-SP4 | 80W7.5 <br> (HF5C5504) |  |
|  | 3 | BW630RAS-4P | SC-N6+SZ-SP6 |  |  |
|  | 4 |  | SC-N7+SZ-SP7 |  |  |

*1. SZ-SP $\square$ : 3-phase parallel terminal plate (for short-circuiting of main contact of magnetic contactor)
Note (1) Open or close the circuit breaker while the DC bus bar is not turned ON. When operating the circuit breaker while the DC bus bar is turned ON, the external handle that can be operated when the cabinet door is closed should be combined with a non-auto switch.
(2) The circuit breaker should be used in the common DC bus bar shared with the inverter. Therefore, a molded case circuit breaker (MCCB) or an earth leakage circuit breaker (ELCB) with braking characteristics cannot be used.
(3) A 4-pole non-auto switch for DC that can keep the withstand voltage should be used for the circuit breaker.
(4) When using multiple braking units, perform the branch wiring from the secondary side of the unit (73), etc.

### 6.5.8 Wire size selection

The wire size of the main circuit is calculated from the current value shown below.

$$
\begin{aligned}
& I_{D B(A V G)}=\sqrt{\frac{P_{A V G}}{\mathrm{R}_{\mathrm{DB}}}}[A] \quad \cdots \quad \text { Equation 6.5.8-1 •IDB(AVG): } \quad \mathrm{DB} \text { average current }[\mathrm{A}] \text { when converting it into the } \\
& \text { average loss } \\
& \text { - IDB (PEAK): DB peak current [A] in max. braking-regenerative } \\
& \text { time period }
\end{aligned}
$$

Normally, the wire size is calculated from the average loss of the braking resistor. If the maximum electric power is large with low frequency, the wire size should be also calculated from the short-time allowable current in the peak current-regenerative time period.

### 6.5.8.1 Wire size (obtained from braking unit specifications)

The wire size of a braking unit is selected so that it meets the braking resistor specifications. This section describes applicable wire sizes from the braking unit specifications. For information on how to select the wire size based on the braking resistor specifications, see Section 6.5.8.2.
The DB average current is calculated from "Table 6.5.2-1 Standard braking unit specifications" in "6.5.2 Overview of braking unit" to select appropriate wire sizes, using Equation 6.5.8-1.

Table 6.5.8-1: Recommended wire size based on the braking unit specifications

|  | Terminal size Main circuit grounding wire | Main circuit: $\mathrm{P}(+), \mathrm{N}(-), \mathrm{P}(+) \mathrm{R}, \mathrm{DB}$ |  |  |  |  |  |  |  | Grounding wire G | Control wire |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 10\%ED (Standard) |  |  |  | 30\%ED (BU-F installed) |  |  |  |  |  |
|  |  | $\mathrm{I}_{\mathrm{DB}(\mathrm{AVG})}$ [A] | Temperature inside cabinet is $40^{\circ} \mathrm{C}$ or less. |  |  | $I_{\mathrm{DB}(\mathrm{AVG})}$ <br> [A] | Temperature inside cabinet is $50^{\circ} \mathrm{C}$ or less. |  |  |  |  |
|  |  |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $90^{\circ} \mathrm{C}$ |  |  |
| BU37-4C | M4 | 12.0 | 2 | 2 | 2 | 21.6 | 5.5 | 2 | 2 | 2 | 1.25 |
| BU55-4C | M5 | 19.4 |  |  |  | 33.6 | 8 | 5.5 | 3.5 |  |  |
| BU90-4C | M6 | 31.0 | 5.5 | 3.5 |  | 53.6 | 22 | 8 | 5.5 | 3.5 |  |
| BU132-4C | M8 | 47.5 | 8 | 5.5 | 5.5 | 82.2 | 38 | 22 | 14 | 5.5 |  |
| BU220-4C | M10 | 79.5 | 22 | 14 | 14 | 137.7 | 100 | 38 | 38 | 14 |  |

Note An "IV wire," a "600 V HIV insulated wire," and a " 600 V cross-linked polyethylene insulated wire" were used at permissible temperatures of $60^{\circ} \mathrm{C}, 75^{\circ} \mathrm{C}$, and $90^{\circ} \mathrm{C}$, respectively, and the values represent aerial wiring.

### 6.5.8.2 Wire size (obtained from braking resistor specifications)

Table 6.5.8-2: Applicable wire size in various combinations of standard baking resistors


### 6.5.9 External dimensions

### 6.5.9.1 Braking resistor (DBR)

Figure A




For items marked as $\square$ in the table above, two resistors of the same shape are used as one set. Carefully check this point when investigating the installation space.
When ordering one unit of this model, one set (two resistors) will be delivered.

### 6.5.9.2 Braking unit (10\%ED)



### 6.5.9.3 Braking unit (Applicable to 30\%ED)

As the fan unit is installed, the braking unit capability is increased.

- Fan unit



| Model | Dimensions (mm) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | W4 | H5 | D2 | L (Fan power <br> supply wire) |  |
|  | 149 | 44 | 76 | 320 |  |

Braking unit and fan unit


| $\begin{aligned} & \underset{\sim}{0} \\ & \frac{\pi}{0} \end{aligned}$ | Model | Dimensions [mm] |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | W | W5 | W6 | H | H6 | H7 | D | D1 | D3 |
| $\begin{aligned} & > \\ & \text { 名 } \end{aligned}$ | $\begin{aligned} & \hline \text { BU37-4C } \\ & +B U-F \end{aligned}$ | 150 | 135 | 7.5 | 280 | 30 | 310 | 160 | 1.2 | 64 |
|  | BU55-4C +BU-F | 230 |  | 47.5 |  |  |  |  |  |  |
|  | $\begin{gathered} \hline \text { BU90-4C } \\ + \text { BU-F } \end{gathered}$ |  |  |  |  |  |  |  |  |  |
|  | $\begin{array}{r} \text { BU132-4C } \\ \text { +BU-F } \end{array}$ | 250 |  | 57.5 | 370 |  | 400 |  |  |  |
|  | $\begin{aligned} & \text { BU220-4C } \\ & +B U-F \end{aligned}$ |  |  |  | 450 |  | 480 |  |  |  |

## FRENIC-VG

## Chapter 7 EMC Compatible <br> Peripherals

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### 7.1 Configuring the FRENIC-VG

The following figure shows a typical installation of the PWM converter.


### 7.2 Anti-noise devices

### 7.2.1 Output circuit filter (OFL filter)

(1) The OFL filter is an LC filter used at the output side of the inverter for the following purposes:

- Protects the motor from insulation damage caused by micro surge voltage from the inverters.
- Suppresses leakage current (in-line leakage current) in long-distance wiring.
- Suppresses induction noise from the inverter output side wiring. Effective for suppression of surge/in-line leakage current in long wiring length such as in-plant facilities.
(2) Use output circuit filters in your desired combination, since they are available for each of the reactor and the capacitor unit.
(3) Use of output circuit filters is recommended for wiring length in excess of 50 m .
[4] For more information, refer to the Output Circuit Filter (OFL-A) Instruction Manual (INR-HF52131*).


### 7.2.1.1 Specifications

| Powerbased series | Applied motor capacity [kW] | Filter model (Procurement type) |  | Individual type |  |  | Rated value specifications |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Reactor | Capacitor unit |  | Rated current [A] | $\text { t } \begin{gathered} \text { Overload } \\ \text { capacity [\%] } \end{gathered}$ | Max. output frequency [Hz] | Rated voltage [V] |
| 400V | 30 |  | OFL-30-4A | OFL-30-4A-L | OFL-30-4A-R |  | 60 | $150 \% / 1 \mathrm{~min}$ 180\%/0.5 s | 120 Hz | 380 to 480 V |
|  | 37 |  | OFL-37-4A | OFL-37-4A-L | OFL-37-4A-R |  | 75 |  |  |  |
|  | 45 |  | OFL-45-4A | OFL-45-4A-L | OFL-45-4A-R |  | 91 |  |  |  |
|  | 55 |  | OFL-55-4A | OFL-55-4A-L | OFL-55-4A-R |  | 112 |  |  |  |
|  | 75 |  | OFL-75-4A | OFL-75-4A-L | OFL-75-4A-R |  | 150 |  |  |  |
|  | 90 |  | OFL-90-4A | OFL-90-4A-L | OFL-90-4A-R |  | 176 |  |  |  |
|  | 110 |  | OFL-110-4A | OFL-110-4A-L | OFL-110-4A-R |  | 210 |  |  |  |
|  | 132 |  | OFL-132-4A | OFL-132-4A-L | OFL-132-4A-R |  | 253 |  |  |  |
|  | 160 |  | OFL-160-4A | OFL-160-4A-L | OFL-160-4A-R |  | 304 |  |  |  |
|  | 200 |  | OFL-200-4A | OFL-200-4A-L | OFL-200-4A-R |  | 377 |  |  |  |
|  | 220 |  | OFL-220-4A | OFL-220-4A-L | OFL-220-4A-R |  | 415 |  |  |  |
|  | 280 |  | OFL-280-4A | OFL-280-4A-L | OFL-280-4A-R |  | 520 |  |  |  |
|  | 315 |  | OFL-315-4A | OFL-315-4A-L | OFL-400-4A-R |  | 585 |  |  |  |
|  | 355 |  | OFL-355-4A | OFL-355-4A-L |  |  | 650 |  |  |  |
|  | 630 | OFL-630-4A |  | OFL-630-4A-L | OFL-500-4A-R |  | 1170 |  |  |  |
|  | 710 |  |  | Contact your Fuji Electric representative for details. |  |  |  |  |  |  |
|  | 800 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 1000 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Location of use | - Shall be installed indoor (free from corrosive gases, flammable gases, dusts, oil mist). Pollution degree 2: IEC60664-1 <br> - Shall not be exposed to direct sunlight. |  |  |  |  |  |  |  |  |
|  | Temperature | $-10 \text { to } 50^{\circ} \mathrm{C}$ |  |  |  | Storage temperature |  | -25 to $+65^{\circ} \mathrm{C}$ (max. $+30^{\circ} \mathrm{C}$ for long-term storage) |  |  |
|  | Ambient humidity | 5 to $95 \% \mathrm{RH}$ (without condensation) |  |  |  | Storage humidity |  | 5 to 95\% RH (without condensation) |  |  |
|  | Altitude | 1000 m or lower |  |  |  |  |  |  |  |  |
| Max. output wiring length |  |  | 400 m or lower |  |  |  |  |  |  |  |
| Withstand voltage/insulation resistance |  |  | $2500 \mathrm{VAC/min}, 1 \mathrm{M} \Omega$ or higher (500 VDC megger) |  |  |  |  |  |  |  |

Note (1) The following range of inverter carrier frequencies can be used:

- OFL-30-4A to OFL-55-4A: 2 to 15 kHz
- OFL-75-4A to OFL-355-4A: 2 to 10 kHz
(2) Reactor and capacitor unit are delivered as a set if ordered in form as specified according to the "Filter model (Procurement type)" in this table. As for device nameplate on reactor and capacitor unit, the above individual type numbers are indicated.
(3) Resistance of capacitor unit will discharge heat when inverter is in operation. Hence, it is recommended to install it on top of the cabinet.
(4) In vector control where output circuit filter is used and wiring length is long, current vibration or torque shortage may occur due to lack of normal motor control, being affected by the inductance of output circuit filter or wiring.
Be sure to select a location for installing inverter and motor by taking into account the wiring length between inverter and motor of 100 m or less, even in the case of using output circuit filter.


### 7.2.1.2 External dimensions and applicable wire sizes



Figure C


Figure D


Figure E


■ Capacitor unit
Figure F


The reactor, capacitor and resistor for
filter OFL-30-4A or larger have to be
installed separately.
Those items are not included in the mass indicated in the table
below. They are shipped as a set by ordering the filter.)

Figure G


| Filter model | Figure | Dimensions (mm) |  |  |  |  |  |  |  |  |  | Approx. mass (kg) |  | Generated loss [W] |  | $\begin{gathered} \text { Wire size }\left[\mathrm{mm}^{2}\right] \\ { }^{2} 1 \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | A | B | C | D | E | F | G |  | $J$ | K | Reactor | Capacitor | Reactor | Capacitor | Reactor | Capacitor |
| OFL-30-4A | C/F | 210 | 175 | 210 | 70 | 140 | 90 | 160 | - | M5 | M6 | 12 | 3 | 100 | 470 |  | $\begin{gathered} 2 \\ (\mathrm{M} 4) \end{gathered}$ |
| OFL-37-4A |  | 220 | 190 | 220 | 75 | 150 | 95 | 160 | - | M5 | M6 | 15 | 5.5 | 110 | 500 |  |  |
| OFL-45-4A | D/F | 220 | 195 | 265 | 70 | 155 | 140 | 160 | - | M6 | M8 | 17 | 5.5 | 150 | 660 |  |  |
| OFL-55-4A |  | 260 | 200 | 275 | 85 | 160 | 150 | 160 | - | M6 | M8 | 22 | 5.5 | 170 | 740 |  |  |
| OFL-75-4A |  | 260 | 210 | 290 | 85 | 170 | 150 | 233 | - | M8 | M10 | 25 | 10 | 180 | 1020 |  |  |
| OFL-90-4A |  | 260 | 210 | 290 | 85 | 170 | 155 | 233 | - | M8 | M10 | 28 | 10 | 190 | 1170 |  |  |
| OFL-110-4A |  | 300 | 230 | 330 | 100 | 190 | 170 | 233 | - | M8 | M10 | 38 | 10 | 240 | 1170 |  |  |
| OFL-132-4A |  | 300 | 240 | 340 | 100 | 200 | 170 | 233 | - | M10 | M10 | 42 | 10 | 260 | 1540 |  |  |
| OFL-160-4A |  | 300 | 240 | 340 | 100 | 200 | 180 | 233 | - | M10 | M10 | 48 | 13 | 300 | 1910 |  |  |
| OFL-200-4A |  | 320 | 270 | 350 | 105 | 220 | 190 | 333 | - | M10 | M12 | 60 | 16 | 330 | 2190 |  |  |
| OFL-220-4A |  | 340 | 300 | 390 | 115 | 250 | 190 | 333 | - | M10 | M12 | 70 | 16 | 400 | 2190 |  |  |
| OFL-280-4A |  | 350 | 300 | 430 | 115 | 250 | 200 | 333 | - | M10 | M12 | 78 | 19 | 450 | 3120 |  |  |
| OFL-315-4A | E/G | 440 | 275 | 450 | 150 | 230 | 170 | - | - | M12 | M12 | 90 | 36 | 650 | 2640 |  |  |
| OFL-355-4A |  | 440 | 290 | 480 | 150 | 245 | 175 | - | - | M12 | M12 | 100 | 36 | 680 | 2640 |  |  |
| OFL-630-4A |  | 480 | 335 | 560 | 160 | 280 | 240 | - | - | M12 | M12 | 170 | 36 | 1300 | 3400 |  |  |

*1 Regarding the wires to be connected to the output circuit filter, use those with an appropriate size as explained below:

- For I/O wiring of the filter reactor, use the wires with the same size as those for the inverter to be used.
- For wiring of the filter capacitor, use the $" 75^{\circ} \mathrm{C} 600 \mathrm{~V}$ HIV insulated wires" or " $90^{\circ} \mathrm{C} 600 \mathrm{~V}$ cross-linked polyethylene-insulated wires". The maximum applicable wire is $5.5 \mathrm{~mm}^{2}$ (M4 size).


## (1) The wiring length for the filter capacitor must be within 3 m as shown in Figure 7.2.1-1, and the wiring

 must be separated from the control circuit.(2) The wire to be connected to the filter capacitor must not touch (closely contact) the resistance elements. If there is a possibility that the wire might contact the resistance elements, be sure to take a measure to protect the wires (for instance, cover the wires with a glass tube).
(3) Install the output circuit filter on the inverter side. Wiring length between inverter and OFL filter should be within 5 m as a rough guideline. However, wiring length longer than this will not pose any particular problem.

### 7.2.2 Radio noise reducing zero-phase reactor (ACL)

A radio noise reducing zero-phase reactor (ACL) reduces the radio noise generated from the inverter output wiring by leading the inverter output wiring through it 4 times. Three inverter output wires and one grounding wire ( 4 wires in all) should be led through the reactor 4 times in the same direction. If a shielded wire is used, it should also be led through 4 times. Be sure to use wires rated at $75^{\circ} \mathrm{C}$ or higher temperatures.
The ACL may generate a large amount of heat because it absorbs high frequency noise components and radiates into the air as heat. If this is the case, take appropriate measures such as lowering the carrier frequency, using wires with higher heat resistance, increasing the number of ACLs to reduce the number of lead-throughs (turns) per ACL, and/or using a larger sized ACL.
The wire sizes that can be used are determined by the dimension (inside diameter) and installation conditions of the radio noise reducing zero-phase reactor (ACL).
Refer to Table 7.2-1: Applicable wire sizes.

### 7.2.2.1 Specifications



Figure 7.2.2-1: External dimensions of ACL
Table 7.2-1: Applicable wire sizes

| Model | Operating conditions |  | Wire size $\left[\mathrm{mm}^{2}\right]$ |
| :---: | :---: | :---: | :--- |
|  | Quantity | No. of lead-throughs (turns) |  |
| ACL-40B | 1 | 4 | $2.0,3.5,5.5$ |
|  | 2 | 2 |  |
|  | 4 | 1 | $22,38,5.5 \times 2,8 \times 2,14 \times 2,22 \times 2$ |
| ACL-74B | 1 | 4 | 8,14 |
|  | 2 | 2 | $22,38,60,5.5 \times 2,8 \times 2,14 \times 2,22 \times 2$ |
|  | 4 | 1 | $100,150,200,250,325,38 \times 2,60 \times 2,100 \times 2$ |
| F200160 | 4 | 1 | $150 \times 2,200 \times 2,250 \times 2,325 \times 2$, <br> F200160PB |

[^11]
## Operating environment



Figure 7.2.2-2: Leading the grounding wire through the ACL

### 7.2.3 Power filter (power filter for input by Fuji Electric Technica)

Noise current generated from inverter (converter) is suppressed by installing this filter on the input supply side of converter.

## Note

(1) Do not use a ground capacitor in combination with the power filter.
(2) Since leakage current as given in the specification below will flow constantly, care should be taken for sensitivity current settings of any earth leakage circuit breaker (ELCB) or leakage detector that is used.
(There will be an electrostatic capacity between the power filter and the ground since a ground capacitor is installed in the power filter.)


### 7.2.3.1 Specifications

| Model | Rated current <br> [A] | Leakage current [mA] | Rated voltage [V] | Voltage drop [V] | Withstand voltage [V] | Wire size [ $\mathrm{mm}^{2}$ ] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Main circuit | Grounding |
| RNFMCH1-40 | 150 | - 2.1 mA or lower (neutral point grounding) <br> - 19.0 mA or lower (S-phase grounding) | 480 | $\begin{gathered} 1.0 \mathrm{~V} \\ \text { or lower } \end{gathered}$ | 2500 VAC/minute (between wires and ground) | Same as applicable converters | IV $2 \mathrm{~mm}^{2}$ or higher |
| RNFMC2H-40 | 200 |  |  |  |  |  |  |
| RNFMC3H-40 | 300 |  |  |  |  |  |  |
| RNFMC4H-40 | 400 |  |  |  |  |  |  |
| RNFMC5H-40 | 500 | 9.9 mA or lower (neutral point grounding) |  |  |  |  |  |
| RNFMC6H-40 | 600 |  |  |  |  |  |  |
| RNFMC9H-40 | 900 |  |  |  |  |  |  |
| RNFMC12H-40 | 1260 |  |  |  |  |  |  |


|  | Location of use | - Indoor (There must be no corrosive gas, flammable gas, dust, or oil mist.) <br> - Must not be exposed to direct sunlight. |
| :---: | :---: | :---: |
|  | Temperature | -10 to $50^{\circ} \mathrm{C}$ (Storage temperature: -10 to $+60^{\circ} \mathrm{C}$ ) |
|  | Humidity | 5 to $95 \% \mathrm{Rh}$ (There must be no dew condensation.) |
|  | Altitude | 1000 m or lower |

### 7.2.3.2 Precautions on use



Figure 7.2.3-1: Example configuration where a power filter is used

Note (1) Connect wires in accordance with the product nameplate.
(2) Be sure to ground power filter. To reduce the ground wire resistance, select the same wire size as the converter and lay the wiring at a minimum distance.
(3) Do not use devices other than those are recommended by Fuji Electric. It may cause risk of burning.
(4) Shorten the wiring length between the power filter and the converter/inverter (wiring c) as much as possible.
(5) Separate the input line (wiring a) of the power filter from the input/output lines (wiring b) of the converter/inverter as much as possible.

### 7.2.3.3 External dimensions



### 7.2.4 Filter capacitor (ground capacitor) for radio noise reduction

A filter capacitor is effective to reduce AM radio frequency band ( 1 MHz or lower) noises. Using this filter together with a zero-phase reactor (ACL) enhances the effectiveness.
If you use this ground capacitor, be sure to use one for each input power supply line regardless of the capacity of the converter (inverter).
Model: NFM60M315KPD


* The letter in ( ) of the ground capacitors shows the wire sheath color: (B) for blue or (BK) for black.

Figure 7.2.4-1: Example of circuit


Figure 7.2.4-2: External dimensions

Note (1) Take care when selecting an earth leakage circuit breaker (ELCB) or leakage detector, because the leakage current is increased when a ground capacitor is installed.
(2) Do not use a ground capacitor together with an EMC filter. (It does not conform to EMC directive.)
(3) Do not use an RNFMC type power filter in conjunction with a ground capacitor.
(4) Do not apply a ground capacitor to the DC bus bar or the output side of the inverter. (Doing so might break the ground capacitor.)
(5) Do not apply a ground capacitor to a PWM converter system. (Doing so might break the ground capacitor.)
(6) About wiring:

- Ground it together with the target device. Make wiring of the ground capacitor as short as possible.
- Do not store this capacitor in the wiring duct for other control wires. (Separate the wiring from other wires.)
(7) When you conduct a pressure test or insulation resistance test, disconnect the ground capacitor so that test voltage will not apply to it. If you conduct a pressure test or the like in the normal state, the ground capacitor will be broken.
(8) Cannot be used for 690 V series.


### 7.2.5 Spark killer

A spark killer is a CR filter that absorbs surge and noise generated from an electromagnetic contactor or a solenoid valve and prevents malfunctions and breakage of the devices.


Internal configuration


Specifications

| Model | Rated voltage | Capacitance $\mu \mathrm{F} \pm 20 \%$ | $\begin{aligned} & \text { Resistance } \\ & \Omega \pm 30 \% \end{aligned}$ | Outside dimensions (mm) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | W | H | T | A |
| S1-B-0 | AC250 V | 0.1 | 200 (1/2 W) | 17.5 | 40 | 7.1 | 20 |
| S2-A-0 |  | 0.2 | 500 (1/2 W) | 27.5 |  | 10.4 | 30 |

Temperature: -40 to $85^{\circ} \mathrm{C}$
Humidity: 5 to $95 \%$ Rh
Note The notes 6) and 7) in 7.2.4 also apply.

Figure 7.2.5-1: External dimensions

### 7.2.6 Noise cut transformer (TRAFY)

In a general insulation transformer, the primary coil and secondary coil electrically insulate the commercial power supply with a commercial frequency, and the voltage of the secondary coil based on the turns ratio is generated. While common mode noise at low frequencies that is close to the commercial frequency can be prevented, if normal mode noise at high frequencies enters, it is transmitted from the primary coil to the secondary coil by electromagnetic induction and static electricity induction.
As a measure for this problem, a shielded transformer, in which a shield (screen) is inserted between the primary coil and secondary coil, is available.
TRAFY is an insulation transformer designed for noise prevention that shields the primary coil, secondary coil, and the whole device (in a three-tier shielding structure) and has a noise attenuation feature across broad frequency bands.
In the case that noise enters from a power supply system, and it causes malfunction of an electronic device, etc., you can prevent the malfunction by connecting TRAFY to the power supply system of that electronic device.

1 Ill For more information, refer to the catalog "Fuji Noise/Surge Prevention Device TRAFY (HS152)".

Table 7.2-2: Comparison of features of transformers

| Type of transformer | Insulation transformer | Shielded transformer | TRAFY <br> Sold by Fuji Electric Technica |
| :---: | :---: | :---: | :---: |
| Common mode noise | $\triangle$ (Low frequencies only) | (Frequency bands around low frequency and high frequency) | $\square$ |
| Normal mode noise | $\times$ | $\times$ | $\square$ |
| Structure | Insulates between the primary and secondary coils to prevent transmission of noise from the primary coil to the secondary coil. | In addition to the structure of an insulation transformer, a shield to block electrostatic is installed between the primary and secondary coils to prevent transmission of high frequency noise from the primary coil to the secondary coil. | 1) 3-tier shielding structure. Shielding of the primary coil, secondary coil, and between primary and secondary coils. <br> 2) Alternate arrangement of coils. Leakage reactance between the primary and secondary coils is increased. |
| Effect of noise prevention | Prevents common mode noise at low frequencies. | Prevents common mode noise at low frequency and high frequency. (Common mode noise at the primary coil is transmitted to the ground through the distribution capacitance between the primary coil and shield.) | Prevents both normal mode noise and common mode noise. <br> - Normal mode noise Prevented mainly by the alternate coil arrangement structure. <br> - Common mode noise Prevented mainly by the 3-tier shielding structure. |
| Problems | 1) High frequency noise becomes low impedance due to small floating capacitance between the primary and secondary coils and the noise is transmitted to the secondary coil. <br> 2) Normal mode noise is transmitted to the secondary coil almost as it is. | 1) Since the induction coefficient seen from the primary coil, distribution capacitance against the shield and iron core are imbalance, imbalanced common mode noise turns into normal mode noise at the secondary coil. <br> 2) Normal mode noise is transmitted to the secondary coil almost as it is. |  |

### 7.2.6.1 Specifications

| Series | SA (Standard) | HA (High performance) | DA (with power cord) | CA (with outlet) |
| :---: | :---: | :---: | :---: | :---: |
| Model | FFT-SA | FFT-HA | FFT-DA | FFT-CA |
| Rated capacity [VA] | 50,100, 200, 300, 500, 750, 1 K , 1.5 K, 2 K, 3 K, 5 K, 7.5 K, 10 K | $\begin{aligned} & 100,200,300,500,750,1 \mathrm{~K}, 1.5 \mathrm{~K}, \\ & 2 \mathrm{~K}, 3 \mathrm{~K}, 5 \mathrm{~K}, 7.5 \mathrm{~K}, 10 \mathrm{~K} \end{aligned}$ | 500, 750, 1 K |  |
| No. of phase (Note 1) | Single phase (3 phases) |  | Single phase |  |
| Rated voltage [V] (Note 1) | 100/100, 200/100, (200/200), (400/200) |  | 100/100 |  |
| Rated current | 0.5 to 100 A at $100 \mathrm{~V}, 0.25$ to 50 A at 200 V |  | 5, 7.5, 10 A at 100 V |  |
| Rated frequency [Hz] | 50/60 |  |  |  |
| Leakage current [ $\mu \mathrm{A}$ ] | 100 or less |  |  |  |
| Insulation type | Type B |  |  |  |
| Voltage fluctuation range (Note 2) | $\pm 4 \%$ ( $\pm 10 \%$ for 50 VA ) |  |  |  |
| Efficiency [\%] | 50 VA: 85 or more, 100 to 750 VA: 90 or more, 1 to $10 \mathrm{kVA}: 95$ or more |  |  |  |
| Withstand voltage | 2000 VAC - 1 min |  | 1500 VAC - 1 min |  |
| Base standard | JEC-2200 (1995) |  |  |  |

[^12](Note 2) Voltage fluctuating range is the value of power factor 0.9.
(Note 3) Please contact us other than the above.

### 7.2.7 Arrester (arrester for power supply)

An arrester absorbs lightning surge that enters from a power supply system and prevents breakage of electronic devices.


### 7.2.7.1 Specifications (an excerpt)

|  |  | Without an alarm contact |  |  | With an alarm contact |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | CN5112 | CN5132 | CN5134 | CN5212 | CN5232 | CN5234 |
| Applicable circuit/rated voltage$(50 / 60 \mathrm{~Hz})$ |  | $1 \varphi 2 \mathrm{~W}, 120 \mathrm{~V}$ $1 \varphi 2 \mathrm{~W}, 240 \mathrm{~V}$ 110 VDC | $1 \varphi 3 \mathrm{~W}, 100 / 200 \mathrm{~V}$ $3 \varphi 3 \mathrm{~W}, 240 \mathrm{~V}$ | $3 \varphi 3 \mathrm{~W}, 440 \mathrm{~V}$ $3 \varphi 4 \mathrm{~W}, 440 \mathrm{~V}$ | $1 \varphi 2 \mathrm{~W}, 120 \mathrm{~V}$ 192W, 240 V 110 VDC | 1ب3W,100/200 V 3ب3W,240 V | $3 \varphi 3 \mathrm{~W}, 440 \mathrm{~V}$ <br> $3 \varphi 4 \mathrm{~W}, 440 \mathrm{~V}$ |
| Max. continuous voltage Uc ( $50 / 60 \mathrm{~Hz}$ ) |  | 280 VAC/140 VDC | 280 VAC | 490 VAC | 280 VAC/140 VDC | 280 VAC | 490 VAC |
| Test class |  | JIS C 5381-1 Class IIIIEC61643-1 class II |  |  |  |  |  |
| Nominal discharge current In ( $8 / 20 \mu \mathrm{~s}$ ) | To ground | 5 kA |  |  | 10 kA |  |  |
|  | Between lines | 3 kA |  | 2.5 kA | 3 kA |  | 2.5 kA |
| Max. discharge current $\operatorname{Imax}(8 / 20 \mu \mathrm{~s})$ | To ground | 10 kA |  |  | 20 kA |  |  |
|  | Between lines | 6 kA |  | 5 kA | 6 kA |  | 5 kA |
| Total discharge current I total ( $8 / 20 \mu \mathrm{~s}$ ) |  | 20 kA | 30 kA |  | 40 kA | 60 kA |  |
| $350 \mu$ s current Impulse*1 | To ground | 1 kA |  |  | 2 kA |  | 1.5 kA |
| Voltage protection level up | To ground | 1500 V or lower |  | 2500 V or lower | 1500 V or lower |  | 2500 V or lower |
|  | Between lines | 1500 V or lower |  | 2500 V or lower | 1500 V or lower |  | 2500 V or lower |
|  | N - to ground | - |  | 1500 V or lower | - |  | 1500 V or lower |
| Operating conditions |  | Temperature: -40 to $70^{\circ} \mathrm{C}$, relative humidity $95 \% \mathrm{RH}$ or less; There must be no dew condensation or freezing. |  |  |  |  |  |
| Connection terminal/wire |  | Screw terminal connection method: M5 (with protection cover of the charging unit) |  |  |  |  |  |
|  |  | Connectable wire: 3.5 to $14 \mathrm{~mm}^{2}$ |  |  |  |  |  |

*1 Shows the performance that electricity can pass through the positive electrode and negative electrode one time each.

### 7.2.7.2 Precautions on use

In JIS C5381-12: 2004 "Surge protective devices connected to low-voltage power distribution systems -- Selection and application principles", it is recommended to install a backup breaker (separator) in series with an arrester (SPD). In this connection, we have conducted tests of separators in combination with SPD.

As a result of these tests, it is recommended to use a plug-type fuse as an SPD separator.
In addition, a molded case circuit breaker (MCCB) is also applicable. However, if you use an MCCB as an SPD separator, protective coordination with upper stream must be considered. At least, you need to select the breaking capacity equivalent to that of the breaker for the wiring in the upper stream.

Table 7.2-3: Combination of CN51 (Max. discharge current: 10 kA ) series and backup breakers

| Breaking capacity | 600 VAC 100 KA | 230 VAC 25 KA 440 VAC 10 KA | 230 VAC 10 KA 440 VAC 7.5 KA | 230 VAC 5 KA 440 VAC 2.5 KA | 230 VAC 2.5 KA 440 VAC 1.5 KA |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Separator type | AFaC-30X (3 units) | BW50RAG-3P 30 | BW50SAG-3P 30 | BW32SAG-3P 30 | BW32AAG-3P 30 |
| Name | Plug-type fuse | Molded case circuit breaker for wiring (MCCB) |  |  |  |

$\mathbb{I}$ I For information about the CN52 Series, refer to Fuji Surge Prevention Device Catalog (HS118 $\square$ ).

Note When you conduct a pressure test and/or an insulation resistance test of devices and/or wirings, be sure to remove the fuse or turn OFF the auto breaker. If you conduct a pressure test or the like in the normal state, it causes breakage of the arrester and/or incorrect measurement.

### 7.2.7.3 Examples of circuits

Single phase (120/240 VAC)


3-phase (240/440 VAC)


Figure 7.2.7-1: Example of circuit
Note (1) Induction lightning surge enters via wires connected to buildings, facilities, or devices. To prevent induction lightning surge from entering inside, install an arrester near the port.
For facilities far from the port, you need to install another arrester.
(2) About wiring of an arrester:

- Be sure to ground the arrester together with the devices to be protected. The grounding wire between the arrester and the cabinet must be wired as short as possible. (The devices in the cabinet must be connected to the common grounding wire of the cabinet.)
If they are grounded separately, the devices in the cabinet cannot be protected.
- The grounding wire of the arrester plays a role to immediately discharge the lightning surge entering from devices and facilities to the ground. Be sure to connect the grounding wire to the grounding terminal with a relatively thick $\left(5.5 \mathrm{~mm}^{2}\right)$ wire in the shortest distance.
The IEC standard stipulates that an arrester for power must be connected to the grounding terminal of a cabinet or equipment with a $3 \mathrm{~mm}^{2}$ wire or a larger wire in the shortest distance ( 0.5 m or less is recommended).
Similarly, make the wiring of the power supply side using the same size wire in the shortest distance. (The surge amount that the arrester can protect varies according to the wiring impedance connected to the arrester. If wiring is too long, sufficient performance cannot be expected.)
- Perform grounding work in reference to "Restrictions on sharing grounding wires and grounding poles (1350-13)" of Internal Wiring Regulations.
- Do not store the grounding wire in the wiring duct for other control wires.
(Separate the wiring from other wires.)
- If wiring via the arrester is available at the power supply side, connect wires in V-shape.


Figure 7.2.7-2: Example of V-shape wire connection

### 7.2.7.4 External dimensions

| CN5112/CN5132/CN5134, CN5212/CN5232 | CN5234 |
| :---: | :---: |
| * The 2-pole products are equipped with the operation lamp on the left only. |  |

### 7.3 Noise prevention

The noise prevention devices and wiring methods explained in "7.2 Anti-noise devices" are classified by purpose as shown in Table 7.3-1 and Table 7.3-2. While malfunctions attributable to noise can be alleviated by anti-noise devices, most malfunctions attributable to noise can be also prevented by grounding and wiring.

- Grounding: Noise can be reduced by taking a measure to prevent leakage current that contains a high frequency component of the inverter (converter), which is the source of noise, from entering other grounding path.
- Wiring: Noise can be reduced by wiring that is not affected by conduction noise and radiation noise of wiring.

In addition to the information about the noise prevention explained in this section, refer to the following section as well.
(1) Appendix 5 "Proficient way to use inverters (on preventing electric noise)"

Table 7.3-1: Noise prevention at input circuit side

| (®) Quite effective, $\bigcirc$ : Effective, $\triangle$ : Slightly effective) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Means | $\qquad$ | Direct current reactor (DCL) | EMC filter Power filter | Zero-phase reactor (ACL) | Ground capacitor | Wiring construction |  | Remarks |
|  |  |  |  |  |  | Wiring*1 means | Shield wiring Metal pipe wiring |  |
| Reduction of noise terminal voltage (Leakage noise current on input side) | - | - | ( | $\triangle^{*}{ }^{2}$ | $\bigcirc{ }^{*}$ | - | - |  |
| Reduction of radiation noise from input wiring | - | - | $\bigcirc$ | $\triangle^{*}{ }^{2}$ | - | - | ( ${ }^{*} 4$ |  |
| Prevention of induction failure from input wiring | - | - | $\bigcirc$ | $\triangle^{*}{ }^{2}$ | $\triangle$ | ( | (0) ${ }^{4}$ |  |
| Reduction of input higher harmonic current <br> (Improvement of input power factor) | $\bigcirc$ | ( | - | - | - | - | - |  |
| Prevention of ELCB trip | - | - | - | - | - | - | - | Use of ELCB by Fuji Electric Co., Ltd. (anti-high frequency products and inverter reinforced products should be used) |

Table 7.3-2: Noise prevention at output circuit side
(@: Quite effective, $O$ : Effective, $\triangle$ : Slightly effective)

|  | OFL filter (OFL-***-4A) | Zero-phase reactor <br> (ACL) | Wiring construction |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Wiring*1 means | Shield wiring Metal pipe wiring |  |
| Suppression of micro surge voltage | ( | - | - | - |  |
| Reduction of radiation noise from output wiring | - | $\bigcirc$ | - | ( ${ }^{*} 4$ |  |
| Prevention of induction failure from output wiring | $\bigcirc$ | ○* | ( | ( ${ }^{*} 4$ |  |
| Reduction of leakage noise current (Leakage noise current at output side) | - | (0) ${ }^{2}$ | - | (0) ${ }^{4}$ | Use of OFL filter against in-line leakage current is effective "○". |
| Prevention of ELCB trip |  |  |  |  | If you use ELCB by Fuji Electric, trip can be prevented. (Use countermeasure products for high frequency or products with enhanced inverters.) |

Note *1 Wiring means refer to wiring between the main input and main output, separate wiring between the main circuit and control circuit, and bundled wiring of inverter output ( $\mathrm{U}, \mathrm{V}$, and W ).
*2 If the turn number of wires connected to the zero-phase reactor (ACL) is increased, noise resistance is enhanced.
*3 Effect of noise prevention is attained by using both ground capacitor and zero phase reactor (ACL).
*4 Poor grounding, even with the use of shielded wire and metal wiring, may reduce noise reduction effect. (Failure or malfunction of other devices may be caused.)

### 7.3.1 Grounding

Be sure to ground the inverter, anti-noise devices, devices with a grounding terminal, frame and board of the transformer, etc. The purposes of grounding are explained below.
(1) Grounding for safety purpose to prevent disasters such as electric shock caused by electric leakage.
(2) Grounding for noise prevention purpose to prevent transmission of noise generated in the inverter and prevent entry of noise from outside.

According to "Appendix 6 Grounding as noise countermeasure and ground noise", the following 3 points are important for grounding for noise prevention. Be sure to comply with them when connecting wires and perform wiring.

- Reduce the impedance of the circuit as much as possible.

Table 7.3-3: Grounding of low voltage devices

| stipulated by "National Electrical Code" |  |  |  |
| :---: | :---: | :---: | :---: |
| Rated <br> voltage | Type of <br> grounding <br> work | Grounding <br> resistance | Thickness of <br> grounding wire |
| 300 V or <br> lower | Type D | $100 \Omega$ or <br> less | Diameter 1.6 mm <br> or more |
| More <br> than <br> 300 V | Type C | $10 \Omega$ or <br> less |  |

- Do not share impedance.
- Separate the wires from noise sources so that induction voltage will not be induced.


## (1) Wire size

## Safety

It is stipulated to ground an external package (metal cabinet) of a low voltage device as shown in Table 7.3.1-1 of "Technical Standards Concerning Electrical Equipment".
In addition, the grounding wire sizes for Class D (Class 3) or Special Class C (Class 3) grounding work are stipulated in "Indoor wiring regulations JEAC8001". (Table 7.3.1-2)
With these sizes, wires can be protected until the MCCB blocks the ground current when a wiring route contacts the external metal cover connecting to the ground.

## Noise prevention

Use electric wires with small impedance, in other words, large size (thick) wires. Even if large size wires cannot be used because of the connecting terminal size, it is desirable to use at least $5.5 \mathrm{~mm}^{2}$ wires from the aspect of noise prevention.

Table 7.3-4: Thickness of grounding wire for Class C (Class 3) grounding work in inner wiring regulations table 1-16

| Rated capacity (current) of breaker installed in grounding protection circuit [A] | Min. thickness of grounding wire (thickness of copper wire) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | General wire |  | Core or valve of movable wire for multiple cores |  |
|  | Single wire [ $\mathrm{mm}^{2}$ ] | Twisted wire [ $\mathrm{mm}^{2}$ ] | When single-wire is used [ $\mathrm{mm}^{2}$ ] | Single core using a valve for 2 cores [ $\mathrm{mm}^{2}$ ] |
| 20 | 1.6 | 2.0 | 1.25 | 0.75 |
| 30 |  |  | 2 | 1.25 |
| 50 | 2.0 | 3.5 | 3.5 | 2 |
| 100 | 2.6 | 5.5 | 5.5 | 3.5 |
| 200 | - | 14 | 14 | 5.5 |
| 400 |  | 22 | 22 | 14 |
| 600 |  | 38 | 38 | 22 |
| 800 |  | 60 | 50 | 30 |
| 1000 |  |  | 60 |  |
| 1200 |  | 100 | 80 | 38 |

## (2) Wiring

## 1) Grounding of motor

Use four wires on the motor (at the output side of the inverter) and connect one of the four wires as a grounding wire to the grounding bus of the cabinet.
If you use shield pipes, metal pipes, or four-core shielded cabtire cables, etc., connect the shield to the grounding bus of the cabinet.


In the case that the wires are grounded near the motor, if leakage current from the inverter flows, the grounding potential becomes different between the grounding section of the cabinet and that of the motor.
In this case, not only induction noise from motor wiring but also from motor grounding will be increased. This, in turn, will affect the control wire laid in the vicinity of the motor.
(1) Refer to "Appendix 6".

## Cabinet



Figure 7.3.1-1: Grounding of inverter and peripherals

## 2) Grounding in cabinet

General grounding in the cabinet is explained below:

- Install a grounding bus in the cabinet and connect the grounding terminals of the devices in the cabinet to the grounding bus using wires as thick as possible in the shortest distance.
- Use a thick wire as a grounding wire from the cabinet to the ground and connect them in the shortest distance.

With the grounding explained above, both the circuit impedance and common impedance will be lowered.
If you use a board which does not use a grounding bus, install a terminal with which electric wires from the grounding pole can be connected to the board close to the grounding point.
3) Connect the grounding terminals of the inverter and devices and the grounding bus separately (individually).

In the case of serial connection as shown in Figure 7.3.1-2, common impedance exists, and Device A is affected by noise of Device B and Device $C$, and a failure might occur. Viewing from the ground, the impedance of Device $C$ is increased by the amount equivalent to the impedance of Device A and Device B.
Be sure to connect the grounding wire of each device separately as shown in Figure 7.3.1-3.


Figure 7.3.1-2: Serial connection of grounding wires


Figure 7.3.1-3: Example of connection of grounding wires

### 7.3.2 Wiring of main circuit of inverter (PWM converter)

In the wires of the main circuit system of the inverter (PWM converter), large current containing a high frequency component flows. In addition, there is induction noise of leakage current from the inverter (converter). For these reasons, it is essential to take noise prevention measures on the wiring of the main circuit.

## Effective measures

(1) Install the zero-phase reactor (ACL) and filters near the main circuit terminal of the inverter (converter) in the shortest distance so that the wiring will not be a noise source.
(2) Connect the wires of the main circuit separately from the control wires without installing them side by side as shown in Figure 7.3.3-9: Space and crossing of wires (page 7-22).
(3) Do not attempt to lay the main input section and inverter output wirings side by side because doing so would cause noise to be conducted between lines, impairing the noise prevention effect. (Refer to Figure 7.3.2-1 and Figure 7.3.2-2.)
(If you lay them side by side, be sure to block them from each other using shield pipes, etc.)


Figure 7.3.2-1: Example of inverter unit wiring

(b) Good example

Figure 7.3.2-2: Example of wiring of EMC filter/power filter
(4) Closely connect the main circuit wires in a same route (such as the main input section and inverter output section). If you use twistable thin wires, twist them.
(5) Avoid a loop-shaped wiring pattern as shown in Figure 7.3.2-4(a). If current flows through such wiring, magnetic flux occurs, becoming a noise source.

If only one phase is connected in a different route, induction noise becomes larger.


Figure 7.3.2-3: Wiring route

(a) Wo

(c) Good wiring with cables twisted

Figure 7.3.2-4: Installation of cables (Reference: Earth and Noise by Kenichi Ito, Nikkan Kogyo Shimbun, Ltd.)
(1) Precautions on in-line high frequency leakage current

When the wiring length from the inverter to motor is long, overheat and over-current trip of the inverter occur due to the effect of leakage current containing a higher frequency component that passes through the floating capacitance between wires of each phase. Moreover, leakage current might increase, and accuracy of current indication might not be secured. Excessive leakage current might flows depending on the condition, resulting in breakage of the inverter.
Therefore, the wiring length between inverter and motor must be 100 m or less.
( 50 m or less is a rough guideline for 30 kW or less, taking voltage drop caused by wiring impedance into consideration.)

In-line leakage current can be suppressed by using an output circuit filter (OFL filter) for length exceeding 100 m .

- Up to 400 m is acceptable if an OFL filter is used in the case of a V/f control system (single drive system).
- In vector control where output circuit filter is used and wiring length is long, current vibration or torque shortage may occur due to lack of normal motor control, being affected by the inductance of output circuit filter or wiring
Be sure to select a location for installing inverter and motor by taking into account the wiring length between inverter and motor of 100 m or less, even in the case of using output circuit filter.
This naturally increases the length of PG signal line, which may also create a distortion in waveform in PG detected waveform, causing malfunction. It is recommended that you consider using pulse amplifier to amplify PG waveform.
(2) Points to note when multiple-core cable is used

When there are multiple sets of inverters and motors, do not use a multiple-core cable to house the wires of the multiple sets.

400 m or less


Figure 7.3.2-5: Wiring length when an output circuit filter is used


Figure 7.3.2-6: Do not use multiple-core cable
(3) Surge voltage during inverter driving

When a motor is driven by a PWM system inverter, the surge voltage generated by the switching action of the inverter element will be increased by the output voltage and applied to the motor terminal. (Refer to Appendix 8.)
One of the following measures should be taken especially in long motor wiring.

- Use a motor with reinforced insulation. (Our standard motors feature reinforced insulation.)
- Connect an output circuit filter (OFL$\square$ A) to the output side (secondary side) of the inverter.
- Keep the wiring length from the inverter to the motor as short as possible. (at maximum, 10 to 20 m ).


### 7.3.3 Wiring of control terminals of inverter (PWM converter)

The control terminals (for general contact input and analog I/O signals) of the main unit and option card of the inverter (PWM converter) can operated with small current. Therefore, they are easily affected by noise, and it is essential to take measures for noise prevention.
Noise can be divided into the 4 types as shown in Figure 7.3.3-1. Most of them can be prevented by using an appropriate wiring route (separate wiring, etc.), a twisted cable, and a shielded cable. It is also effective to use a zero phase reactor (wind 5 to 10 times around the zero phase reactor).
As for conduction noise, it is effective to isolate signals from the control terminal side using a control relay or insulation converter (isolator).

Fil For information on noise and how to take measures, refer to Appendix 5 as well.


Figure 7.3.3-1: Noise types

## (1) How to install twisted cables and shielded cables

## 1-1) Twisted cables

Regarding the wiring of signal cables, it is recommended to twist and wire the cables as shown in Figure 7.3.3-2.
In addition, it is recommended to use a 0.5 to $1.25 \mathrm{~mm}^{2}$ KIV wire (JIS C 3316 ), which is a flexible and easy-to-use $60^{\circ} \mathrm{C}$ and 600 V rated insulated wire.

## 1-2) Shielded cables

There are two types of the shielded wire: One is a shielded wire in which a bundle of wires are shielded, and the other is a twisted-pair shielded wire in which a wire is twisted and shielded.
(As shielded twisted pair cables, a 1-pair cable, 2-pair cable, and 3 -pair cable, etc. are available.)
In addition, there are two types of the shielded twisted pair cable: One has a knitted wire mesh shielding cover, and the other has a shield winding around inner cables. Although the knitted wire mesh shield is more effective in shielding, the working efficiency is lowered (refer to Figure 7.3.3-3).

10 For information on PROFIBUS-DP and DeviceNet and other open buses, and for the serial PG interface for motors (OPC-VG1-SPGT), refer to the installation manual of each bus and the instruction manual of the option card.


Figure 7.3.3-2: Twisting of vinyl insulated wires

(a) Knitted wire mesh shield

(b) Winding shield

Figure 7.3.3-3: Shielded twisted pair cable

Shield processing of a shielded cable should basically be done by shield clamp connection.
See shield processing below for cases where this is not feasible due to connected equipment.

## Shield clamp method

A termination method in which the shielded part of a shielded cable is exposed by removing its outer layer, and held firmly together with the grounding bus of the cabinet by conductive clamp material (shield clamp).
<Treatment of the edge of the shielding cover>
(1) Edge to which the shielding cover is not connected
As shown in Figure 7.3.3-5, treat the edge in a way that the shielding cover does not come close to the core cable.


Figure 7.3.3-4: Clamping of shielded wire (example)


Figure 7.3.3-5: Treatment of the edge to which shielding cover is not connected
(2) Edge to which the shielding cover is connected

Treat the edge as shown in Figure 7.3.3-6 for a shielded wire wound around the wire cover or as shown in Figure 7.3.3-7 for a knitted shielded wire, and then install the insulation tube and crimp terminal as shown in Figure 7.3.3-8.


Figure 7.3.3-6: Treatment of winding shield

(a) Pulling out of shielding cover to the front side


Figure 7.3.3-7: Treatment of knitted shield

(b) Pulling out of shielding cover to the rear side

Figure 7.3.3-8: Treatment of the edge to which shielding cover is connected

## (2) How to install wires

If the wires to the control terminals of the inverter or converter are installed closely to the wires of the main circuit or any other possible noise sources and the wiring length is long, or they are installed side by side, noise has a large impact. For this reason, when you wire the cables to the control terminals of the devices, ensure the shortest possible wiring length while keeping them away from the cables of the main circuit, relay sequence circuit, and transformer circuit for measuring instruments, etc.

## 1) Main circuit and inverter control circuit

Leave the wire of the control terminal away from that of the main circuit by at least 100 mm . (See Figure 7.3.3-9.) If it is installed near the main circuit out of necessity, put either of the wires into a wire bundling tube with shield, or block the wire with a shielding plate (steel plate), etc., and connect the shielded section to the grounding bus of the cabinet.

If the wire crosses the main circuit, install it at the right angle so that induction of induction noise will be reduced.

Hr must be 100 mm or more.


Figure 7.3.3-9: Space and crossing of wires
2) Relay sequence circuit/transformer circuit for measuring instrument and inverter control circuit

Install the wires as keeping them away from the cables of the electromagnetic contactor and other excitation coil circuits because the wires are affected by surge voltage generated when such circuits are opened and closed and by noise entering from outside.
To be more specific, separate the wires of the relay sequence circuit and ${ }^{\top}$ those of the transformer circuit for measuring instrument in order not to store the cables of the control terminals into one wiring duct.
(If they are separated even if the distance is small, it has a substantial effect.)
If two wiring routes cannot be separated, bundle either of the wires and install them outside the wiring duct. (Refer to Figure 7.3.3-10.)

## (3) Contact input

Connect the wires of the contact input terminals of the inverter (converter) as short as possible to reduce the effect of noise. If the wiring length exceeds 20 m , insulate the signals using a control relay. Even when you connect the contacts of the control relay to the contact inputs of the inverter (converter), be sure to twist the wires. When you use a shielded wire, connect the shield to the common terminal.
When you connect the contacts to more than one inverter, connect a different contact to each inverter. Do not share the contact as shown in Figure 7.3.3-13 (a).


Figure 7.3.3-11: Shield processing

(a) Bad example

(b) Good example

Figure 7.3.3-13: Separation of contacts
(1) Analog input/output (11, M) and digital input (CM), and transistor output (CMY) are separated (electrically insulated) on a circuit by circuit basis so as to prevent mutual interference between the circuits. The common terminals of them are separated from the grounding terminal of the inverter or converter. Be sure to follow the instructions given below, otherwise it will lower the noise resistance.

- Especially in the analog circuit and contact input transistor output, do not connect the common terminals to each other. Refrain from connecting the common terminal or the shield of a shielded wire to the ground.
- The shield of a signal line should be connected to the ground when corresponding to the EMC command (CE marking compatible).
However, malfunction caused by noise may be induced by connecting this shield to the ground.
(2) Do not connect the common terminals (CM) of multiple inverters to each other. If the common terminals of multiple inverters are connected to each other, the noise resistance will be lowered


## Prevention of recovery failure due to floating capacitance of AC operation relay

In an AC operation relay, if the wiring of the control circuit is long (e.g., the location of the relay is far from the location of the switch to operate the relay), the floating capacitance between the wires prevents the relay from recovering even if the switch is turned OFF. The allowable wiring length not affected by the floating capacitance of our control relay is shown below.
[al For precautions such as those to take when the wiring exceeds the allowable wiring length, refer to the catalog of the relay or other relevant documentation.

Table 7.3-5: Long wiring model


Table 7.3-6: Allowable wiring length not affected by floating capacitance

|  |  | 100 V |  |  | 200 V |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Allowable capacitance ( $\mu \mathrm{F}$ ) | Allowable cable length (m) |  | Allowable capacitance ( $\mu \mathrm{F}$ ) | Allowable cable length (m) |  |
|  |  | Operation method <br> (1) | Operation method <br> (2) | Operation method <br> (1) |  | Operation method <br> (2) |
| HH5 $\square$ | 50 Hz |  | 0.051 | 170 | 85 | 0.013 | 43 | 21 |
| HH62 | 60 Hz | 0.038 | 120 | 60 | 0.0097 | 32 | 16 |
| HH63 | 50 Hz | 0.078 | 260 | 130 | 0.018 | 60 | 30 |
| H\%63 | 60 Hz | 0.063 | 210 | 100 | 0.015 | 50 | 25 |
|  | 50 Hz | 0.096 | 320 | 160 | 0.024 | 80 | 40 |
|  | 60 Hz | 0.078 | 260 | 130 | 0.018 | 60 | 30 |
|  | 50 Hz | 0.170 | 570 | 280 | 0.042 | 140 | 70 |
|  | 60 Hz | 0.150 | 500 | 250 | 0.036 | 120 | 60 |

(Note) The allowable cable length is calculated on the condition that the floating capacitance between cables is 0.3 ( $\mu \mathrm{F} / \mathrm{km}$ ) (measurement example of CVV $2 \mathrm{~mm}^{2}$ ).

If a malfunction occurs although you took into consideration the relationship between the floating capacitance and wiring length, perform the following procedures:
(1) Connect a resistor in parallel with the excitation coil of the relay.
(2) Lower the coil power and change the operation from AC to DC.

If the current flowing (running) through the relay circuit is increased or changed to DC power, the effect of the floating capacitance can be reduced or eliminated. Note that change of the operation power is a large-scale modification, therefore it must be used as an emergency measure.

Table 7.3-7: Example of recommended parallel resistance

(Note) Taking into consideration temperature rise, application is partially limited.

## (4) Analog input and output

Since the analog signals are weak ( 0 to 10 VDC, 4 to 20 mADC ), they are easily affected by noise. Use a twisted wire or a shielded wire to prevent noise.
If the wiring distance exceeds 20 m , install an insulation converter, etc. For the signals that require response as in the case of torque control, check the response speed of the insulation converter. The analog input has the primary delay soft filter setting as one of the function settings. If you set the filtering time suitable for the system, you can reduce the impact by noise. A zero-phase reactor and LC filter for signals are also effective means.
Note (1) Keep the wiring distance between insulation converter and inverter as short as possible.
(2) Response speed may decline as an effect of filter when using an LC filter.

## Wiring method (1)

Use a twisted pair shielded wire up to the input of the converter. (Connect the shield to the common terminal of the converter.)


Figure 7.3.3-14: Shield processing (1)
If you ground the shield, process the ends at the insulation converter side and connect it to the grounding terminal.


Figure 7.3.3-15: Shield processing (2)

## Wiring method (2)

If you connect the analog input and output terminals of multiple inverters, insulate them from analog signals entering from outside.
If not, the analog common terminals are connected between the inverters, and the noise resistance is lowered.
*1 Twist wiring or twisted pair shielded wires (Connect the shield to the common side of the converter.)


Figure 7.3.3-16: Twist processing

When you relay shielded wires via the terminal block, do not connect them to the relay terminal of the common terminal circuit. Install a dedicated terminal for shielded wires.

a) Good example


Do not connect shielded cables to the common terminal of the signal line at the relay unit.
b) Bad example

Figure 7.3.3-17: Example of use of a relay terminal block

## (5) Common terminal circuit

The common terminal (11) of the analog I/O, common terminal (CM) of the contact input, and common terminal (CMY) of the transistor output separate (electrically insulate) their own signals.
Be sure not to connect the common terminal of the analog I/O to that of other circuits to share the common terminal. If it is connected to other common terminals, a malfunction might occur due to mutual interference between the circuits.
In addition, do not ground the common terminals.
If the common terminals are not sufficient, install a relay terminal block near the inverter control terminal. If you connect the relay terminal block and inverter control terminal with a thick cable, you can reduce the impact of noise.


## (6) Speed detection unit (PG detection)

1) It is recommended to use a $2 \mathrm{~mm}^{2}$ shielded wire for the pulse generator for motor speed detection. Anti-noise measures such as creating signals by using pulse amplifier (insulated type) are effective when wiring length is considerably long.
2) Winding this PG wire on a zero phase reactor (ACL) 5 to 10 turns is an effective anti-noise measure.

Note - Shield is connected to motor side.
However, if inverter should malfunction by the effect of noise, noise may be reduced by connecting the shield to the PGM of the inverter instead of connecting it to the motor side.

- Use of a serial PG and a PG card to drive the synchronous motor, etc. requires a dedicated PG interface option card.


Figure 7.3.3-19: Example of PG wiring

Ea Refer to the instruction manual of the dedicated PG interface option card.

## (7) Temperature sensor (NTC thermistor)

It is recommended to use a $2 \mathrm{~mm}^{2}$ shielded wire for the NTC detection thermistor used for motor temperature correction control and overheat protection function. If the wiring length is considerably long, the overheat protection function of the motor may not operate normally due to malfunction of the detection circuit in the NTC thermistor. Using temperature detection signal of the motor as overheat detection/protection by using PTC thermistor or clixon is also an effective anti-noise measure. (Motor temperature correction calculation in this case, however, will not be performed.)

[^13]

Figure 7.3.3-20: Example of NTC thermistor wiring

## (8) Control power circuit

When control power is supplied from the main circuit power system for the converter (inverter), there might be impact of noise from the converter (inverter). However, most of the impact can be reduced by wiring of the main circuit and arrangement of devices.
The main circuit power system is a 400 V system, therefore a general control power prepares power using a step-down transformer with small capacity.
Use an insulation transformer as a step-down transformer. (It is recommended to use a noise-cut transformer or TRAFY.)


Use an insulation transformer as a step-down transformer. (It is recommended to use a noise-cut transformer or TRAFY.)


A noise filter with high attenuation is recommended.

Figure 7.3.3-22: Example of circuit configuration (when a noise filter is used)

## FRENIC-

## Chapter 8 Operation

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### 8.1 Function codes

This section lists the function codes.
For more information on the control block diagrams and the function codes, refer to the separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019).
[D] For more details of the control block diagrams (Section 8.1.2), refer to "4.1 Control block diagrams" in Chapter 4 of the separate volume.
For more details of the function codes (Section 8.1.3), refer to "4.3 Function code details" in Chapter 4 of the separate volume.

### 8.1.1 Function code table

### 8.1.1.1 Function code groups and identification codes

## F***



Table 8.1-1: Function code classification

| Function codes |  | Function | Remarks |
| :---: | :---: | :---: | :---: |
| Fundamental function | F00 to F85 | Fundamental functions |  |
| $\underline{\text { Extensional terminal function }}$ | E01 to E118 | Terminal functions |  |
|  |  | E51, E52 | For the option OPC-VG1-AIO |
|  |  | E55, E56 |  |
|  |  | E59, E60 |  |
|  |  | E63, E64 |  |
|  |  | E67, E68 |  |
|  |  | E72, E73 |  |
|  |  | E77, E78 |  |
|  |  | E82, E83 |  |
|  |  | E103, E104 |  |
|  |  | E107, E108 |  |
| Control function | C01 to C73 | Control function |  |
| Motor Parameter function | P01 to P51 | Motor parameter function M1 |  |
| $\underline{\text { High performance function }}$ | H01 to H228 | High performance functions |  |
| $\underline{\text { Alternative motor parameters }}$ | A01 to A171 | Motor parameter functions M2 and M3 |  |
| option function | o05 to o197 | Option function |  |
|  |  | 001 to 004 | For the options OPC-VG1-DIA and -DIB |
|  |  | -05 | For the option OPC-VG1-PG (PD) |
|  |  | 006 to o08 | For the option OPC-VG1-PG (LD) |
|  |  | o09 to o11 | For the option OPC-VG1-PMPG |
|  |  | o12 to o19 | For the option OPC-VG1-PG (PR) |
|  |  | o30 to o32 | For communications options (such as OPC-VG1-TL and OPC-VG1-CCL) |
|  |  | o33, o34, o50 | For the terminal block dedicated to the OPC-VG1-TBSI high-speed serial communications |
|  |  | o38 to 040 | For the option OPC-VG1-UPAC |
|  |  | o101 to o197 | For communications options (such as OPC-VG1-TL and OPC-VG1-CCL) |
| Lift function | L01 to L15 | Lift functions |  |
| User function | U01 to U64 | User functions (UPAC) | Intended for use with the UPAC option |
|  | $\begin{aligned} & \text { U101 to } \\ & \text { U150 } \end{aligned}$ | User functions | Reserved for manufacturer use |


| SaFety function | SF00 to <br> SF31 | Safety function | Intended for use when functional safety is implemented <br> For more details, refer to the Functional Safety Option <br> Instruction Manual. |
| :--- | :--- | :--- | :--- |
| Serial communication function | S01 to S17 | Command functions | Operable from the LOC (Keypad), COM (Link: T link, <br> RS-485, SIU, SX, field bus) and UPAC |
| $\underline{\text { Monitoring function }}$ | M01 to M222 | Data monitor functions |  |

### 8.1.1.2 Function code table headers

The function code table uses the headers listed below (8.1.1.3).
Table 8.1-2: Function code table header list

| Item |  | Description |
| :---: | :---: | :---: |
| Function code |  | Identification code of function code <br> * The function code of $\square$ is a parameter varying between unit type and stack type. <br> Although it may be displayed or set for stack type, it will be an invalid function code. |
| Communications address | 485 No. | Address to be used to refer to or change function code data using a communications option. <br> Available for all communications options except OPC-VG1-TL. |
|  | Link No. | Address to be used to refer to or change function code data using a communications option (OPC-VG1-TL, OPC-VG1-SX, etc.). Blank link number fields mean that the corresponding function codes cannot be accessed. |
| Name |  | Name assigned to a function code. |
| Dir |  | Number of second layer codes in the keypad function code data directory structure. <br> 0 : First layer code (no second layer), 1: Second layer code, <br> 2 or more: First layer code (Value will show the number of second layer codes) |
| Data setting range |  | Allowable data setting range and definition of each data. |
| Change when running |  | Indicates whether or not the function code data can be changed when the inverter is running. <br> O: Change while running allowed, $X$ : Change while running not allowed |
| Factory default value |  | Data preset by factory default. When data is changed, * (asterisks) appears on the keypad screen. Initial factory default value can be restored by using the initialization function code. |
| Data copying |  | Identifies the function code used when you copy all the data stored in the keypad memory of a source inverter to other destination inverters. |
| Initialization |  | Identifies the function code used to perform initialization (revert to the factory default values) by H03 "Data initialization". Most of the function codes will be initialized. <br> O: Data initialized, X: Data not initialized |
| Format type *1 |  | Indicates the format type used to refer to or change data via the communications link. |
| Control method: Enable/Disable |  | Indicates whether or not the function code is available according to the individual control method. <br> Control method <br> PG : Vector control (Induction motor) <br> LES : Sensor-less vector control (Induction motor) <br> VF : V/f control (Induction motor) <br> SM : Vector control (PMSM) |

*1 For more information on function code classifications, refer to "4.2.4 Data format list" in Chapter 4 of the separate volume "Unit Type Function Code Edition" (24A7-J-0019).

## 8．1．1．3 Function code table

## －Fundamental functions（F：Fundamental Functions）

| $\begin{aligned} & \text { 毋 } \\ & \stackrel{8}{8} \end{aligned}$ | $C o m m u n i c a t i o n s$address |  | Name | Dir | Data setting range |  |  |  |  | $\begin{aligned} & \hline \text { Control } \\ & \text { method: } \\ & \text { Enable/ } \\ & \text { Disable } \\ & \hline \end{aligned}$ |  |  |  | $\stackrel{\text { ® }}{\stackrel{\text { ® }}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No． | Link No． |  |  |  |  |  |  |  |  | （ $\begin{aligned} & \text { L } \\ & \text { E } \\ & \text { S }\end{aligned}$ | V | S |  |
| F00 | Oh | 50h | Data protection | 0 | 0 to 1 <br> 0 ：Data change allowed <br> 1：Data protection <br> Write－protects data from the keypad． <br> H29＂Link write protect＂defines the write－protect from links <br> （T－link，485，etc．）． | $\times$ | 0 |  | 40 |  | 0 | 0 | － |  |
| F01 | 1h | h | Speed setting N1 | 0 | 0 to 9 <br> 0：Keypad（ $⿴ 囗 ⿰ 丿 ㇄$ <br> 1：Analog 12 input（ 0 to $\pm 10 \mathrm{~V}$ ） <br> 2：Analog 12 input（ 0 to +10 V ） <br> 3：UP／DOWN（initial value 0 ） <br> 4：UP／DOWN（initial value：previous value） <br> 5：UP／DOWN（initial value：creep speed 1，2） <br> 6：DIA card input <br> 7：DIB card input <br> 8：Ai（N－REFV）input <br> 9：Ai2（N－REFC）input <br> Defines how to set a speed command． | $\times$ | 0 |  | 41 |  | 0 | 0 | 0 |  |
| F02 | 2 h | h | Operation method | 0 | ```0 to } 0: Key operation ( (%) , (RE) and *oom keys) (LOCAL mode) 1: External signal (FWD and REV terminals) (REMOTE mode) Defines how to input the operation method.``` | $\times$ | 0 | $\bigcirc$ | 42 |  | 0 | 0 | O |  |
| F03 | 3h | 51h | M1 Maximum speed | 3 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | $0 \times$ | 0 |  | 0 | $\bigcirc$ | 0 |  |
| F04 | 4h | 52h | M1 Rated speed | 1 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | Depends on capacity | $\bigcirc \times$ | 0 |  | $\bigcirc$ | 0 | － |  |
| F05 | 5 h | 53h | M1 Rated voltage | 1 | 80 to 999 V | $\times$ | Depends on capacity | $\bigcirc \times$ | 0 |  | $\bigcirc$ | 0 | O |  |
| F07 | 7h | 54h | Acceleration time 1 | 0 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 1000 \text { to } 3600 \mathrm{~s} \end{aligned}$ | $\bigcirc$ | 5.00 | $\bigcirc$ | 13 | － | 0 | O | 0 |  |
| F08 | 8h | 55h | Deceleration time 1 | 0 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 1000 \text { to } 3600 \mathrm{~s} \end{aligned}$ | 0 | 5.00 | 0 | 13 | － | 0 | － | 0 |  |
| F10 | Ah | 56h | M1 Electronic thermal （Operation selection） | 3 | 0 to 2 <br> 0 ：No operation（when using exclusive motor for VG） <br> 1：Operation（for general purpose motors：use in the case of self－cooling fan） <br> 2：Operation（for inverter motors：use in the case of externally powered fan） | 0 | 0 | $0 \times$ | 85 |  | 0 | 0 | 0 |  |
| F11 | Bh | 57h | M1 Electronic thermal （Detection level） | 1 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~A} \\ & 100.0 \text { to } 999.9 \mathrm{~A} \\ & 1000 \text { to } 2000 \mathrm{~A} \\ & \hline \end{aligned}$ | 0 | $\begin{array}{\|c\|} \hline \text { Depends } \\ \text { on capacity } \end{array}$ | $\bigcirc \times$ | 13 |  | 0 | 0 | O |  |
| F12 | Ch | 58h | $\begin{aligned} & \hline \text { M1 Electronic thermal } \\ & \text { (Thermal time constant) } \end{aligned}$ | 1 | 0.5 to 75.0 min | 0 | Depends on capacity | $0 \times$ | 2 |  | 0 | 0 | 0 |  |
| F14 | Eh | h | Restart after momentary power failure（Operation selection） | 0 | 0 to 5 <br> 0：No operation（No restart，immediate alarm i（i） <br> 1：No operation（No restart，alarm on power return $2 \mathrm{~L}, \mathrm{i})$ <br> 2：No operation（No restart，alarm after slow down and stop $i(i)$ <br> 3：Operation（Restart，continue operation） <br> 4：Operation（Restart，operate at speed when power was cut off） <br> 5：Operation（Restart，operate at starting speed） | 0 | 0 | $\bigcirc$ | 0 |  | 0 | 0 | 0 |  |
| F17 | 11h | h | Gain（for speed setting on terminal ［12］） | 0 | 0.0 to 200．0\％ <br> Ratio to analog speed setting value on control terminal［12］． Limited at $\pm 110 \%$ of maximum speed． | 0 | 100.0 |  | 2 |  | 0 | － | － |  |
| F18 | 12h | h | Bias（for speed setting on terminal ［12］） | 0 | -30000 to $30000 \mathrm{r} / \mathrm{min}$ <br> Bias to analog speed setting value on control terminal［12］． Limited at $\pm$ maximum speed． | 0 | 0 |  | 5 |  | 0 | 0 | 0 |  |
| F20 | 14h | 59h | DC Braking（Braking starting speed） | 3 | 0 to $3600 \mathrm{r} / \mathrm{min}$ | 0 | 0 | $\bigcirc$ | 0 |  | 0 | 0 | $\times$ |  |
| F21 | 15h | 5Ah | DC Braking（Braking level） | 1 | 0 to 100\％ | 0 | 0 | 0 | 16 | $\bigcirc$ | 0 | 0 | $\times$ |  |
| F22 | 16h | 5Bh | DC Braking（Braking time） | 1 | $\begin{aligned} & 0.0 \text { to } 30.0 \mathrm{~s} \\ & 0.0: \text { No operation } \\ & 0.1 \text { to } 30.0 \mathrm{~s} \text { : Operation } \end{aligned}$ | 0 | 0.0 |  | 2 |  | 0 | 0 | $\times$ |  |
| F23 | 17h | 5Ch | Starting speed | 0 | 0.0 to $150.0 \mathrm{r} / \mathrm{min}$ <br> Restrict to over 0.1 Hz （for sensor－less，VF control） <br> Starting speed can be set to secure the torque for starting． | $\times$ | 0.0 |  | 2 |  | 0 | 0 | － |  |
| F24 | 18h | 5Dh | Starting speed（Holding time） | 0 | 0.00 to 10.00 s | $\times$ | 0.00 | 0 | 3 | $\bigcirc$ | 0 | O | 0 |  |
| F26 | 1Ah | 5Eh | Motor sound（Carrier frequency） <br> ＊Function code invalid for setting change | － |  | $\times$ | 2 | $100$ | 10 |  | 0 | 0 | － |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  |  |  | Control method: Enable/ Disable |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | V | S |  |
| F36 | 24h | h | 30RY Drive mode | 0 | 0 to 1 <br> 0: Excitation operation on alarm <br> 1: Normal excitation operation | $\times$ | 0 | 0 O | 43 | $\bigcirc 0$ | - | $\bigcirc$ |  |
| F37 | 25h | 60h | Stop speed | 3 | 0.0 to $150.0 \mathrm{r} / \mathrm{min}$ <br> Restrict to over 0.1 Hz (for sensor-less, VF control) | $\times$ | 10.0 | 0 O | 2 | 0 | $\bigcirc$ | $\bigcirc$ |  |
| F38 | 26h | 61h | Stop speed (Detection mode) | 1 | 0 to 1 <br> 0: Detected speed value <br> 1: Speed command value <br> Only speed command value is valid, regardless of the setting value, under sensor-less vector control or V/F control. | $\times$ | 0 | 0 O | 90 | 0 | $\times$ | $\bigcirc$ |  |
| F39 | 27h | 62h | Stop speed (Zero speed control holding time) | 1 | 0.00 to 10.00 s Applies to when timing the application of the mechanical brake. | $\times$ | 0.50 | 0 O | 3 | 0 | $\times$ | $\bigcirc$ |  |
| F40 | 28h | 63h | Torque limiter mode 1 | 12 | 0 to 3 <br> 0 : Limit disable <br> 1: Torque limit <br> 2: Power limit <br> 3: Torque current limit | ${ }^{\times}$ | 0 | $0$ | 44 | $\bigcirc 0$ | $\bigcirc$ | $\bigcirc$ |  |
| F41 | 29h | 64h | Torque limiter mode 2 | 1 | 0 to 3 <br> 0: Same for 4 quadrants at level 1 <br> 1: Drive (Level 1) and brake (Level 2) <br> 2: Upper limit (Level 1), lower limit (Level 2) <br> 3: Switch between levels 1 and 2 for all the 4 quadrants Levels 1 and 2 are specified by the sources defined by F42 and F43, respectively. | $\times$ | 0 |  | 45 | 0 | 0 | 0 |  |
| F42 | 2Ah | 65h | Torque limiter value (Level 1) selection | 1 | 0 to 5 0: Function code (F44) 1: Ai [TL-REF1] 2: DIA card 3: DIB card 4: Link enable 5: PID output | $\times$ | 0 |  | 46 | $\bigcirc 0$ | O | $\bigcirc$ |  |
| F43 | 2Bh | 66h | Torque limiter value (Level 2) selection | 1 |  | $\times$ | 0 | $010$ | 47 | $\bigcirc$ | 0 | 0 |  |
| F44 | 2Ch | 67h | Torque limiter value (Level 1) | 1 | -300 to 300\% | $\bigcirc$ | 150 | 0 O | 5 | 0 | $\bigcirc$ | $\bigcirc$ |  |
| F45 | 2Dh | 68h | Torque limiter value (Level 2 ) | 1 | -300 to 300\% | $\bigcirc$ | 10 | 0 O | 5 | $\bigcirc \bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| F46 | 2Eh | 69h | Mechanical loss compensation value | 1 | -300.00 to 300.00\% | $\bigcirc$ | 0.00 | O- | 7 | - 0 | $\times$ | $\bigcirc$ |  |
| F47 | 2Fh | 6Ah | Torque bias T1 | 1 | $\begin{array}{\|l} \hline-300.00 \text { to } 300.00 \% \\ \text { Torque biases T1 to T3 are switchable with DI. } \\ \hline \end{array}$ | $\bigcirc$ | 0.00 | O 0 | 7 | 0 | $\times$ | $\bigcirc$ |  |
| F48 | 30h | h | Torque bias T2 | 1 | -300.00 to 300.00\% | $\bigcirc$ | 0.00 | O 0 | 7 | $\bigcirc 0$ | $\times$ | 0 |  |
| F49 | 31h | h | Torque bias T3 | 1 | -300.00 to 300.00\% | $\bigcirc$ | 0.00 | OO | 7 | $\bigcirc \bigcirc$ | $\times$ | $\bigcirc$ |  |
| F50 | 32h | h | Torque bias startup timer | 1 | 0.00 to 1.00 s <br> Specifies the time required for generating $300 \%$ torque. | $\bigcirc$ | 0.00 |  | 3 | $\bigcirc$ | $\times$ | $\bigcirc$ |  |
| F51 | 33h | FBh | Torque command monitor (Polarity selection) | 1 | 0 to 1 <br> 0 : Torque polarity <br> 1: + on drive, - on brake <br> Specifies the polarity of torque related data output (e.g., AO <br> monitor, keypad LED monitor, and keypad LCD monitor). | $\bigcirc$ | 0 |  | 48 | 0 O | 0 | $\bigcirc$ |  |
| F52 | 34h | h | LED Monitor (Display coefficient A) | 8 | -999.00 to 999.00 <br> Specifies the conversion coefficient for displaying the load shaft speed and line speed on the keypad LED monitor. <br> Display value $=$ Motor speed $\times(0.01$ to 200.00) <br> Data is valid only between 0.01 and 200.00, out of range data will be restricted. | $\bigcirc$ | 1.00 |  | 12 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| F53 | 35h | h | LED Monitor (Display coefficient B) | 1 | -999.00 to 999.00 <br> Display coefficient A: Maximum value <br> Display coefficient B : Minimum value <br> Display coefficients $A$ and $B$ are used to set the conversion coefficients for determining the display values for the PID command value, PID feedback amount, and PID output (Process amount). <br> Display value $=($ Command or feedback value) $\times$ (Display coefficient A - B) + B | $\bigcirc$ | 1.00 |  | 12 | 0 | 0 | $\bigcirc$ |  |
| F54 | 36h | h | LED Monitor (Display filter) | 1 | 0.0 to 5.0 s | $\bigcirc$ | 0.2 | $\bigcirc \mathrm{O}$ | 2 | 0 | $\bigcirc$ | $\bigcirc$ |  |
| F55 | 37h | H | LED Monitor (Display selection) | 1 | 00 to 32 <br> 00: <br> Speed detection 1/Speed command (r/min) (F56 switches <br> the display while motor is stopped) <br> 01: Speed setup 4 (ASR input) (r/min) <br> 02: Output frequency command value (slide in) (Hz) <br> 03: Torque current command value (\%) <br> 04: Torque command value (\%) <br> 05: Torque calculated value (\%) <br> 06: <br> Power consumption (Motor output) <br> (switched by F60) (kW, HP) <br> 07: Output current detected value (A) <br> 08: Output voltage detected value (V) <br> 09: DC link bus voltage detected value (V) <br> 10: Magnetic flux command value (\%) <br> 11: Magnetic flux calculated value (\%) <br> 12: Motor temperature ( ${ }^{\circ} \mathrm{C}$ ) (when NTC thermistor is not used, <br> "----" is displayed) | $\bigcirc$ | 0 |  |  | 0 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> O 0 <br> 0 0 <br> O 0 <br> O 0 | 0 <br>  <br> $\times$ <br> $\times$ <br> $\times$ <br> $\times$ <br>  <br> $\times$ <br> $\times$ | 0 0 0 0 0 0 0 0 0 0 0 0 $\times$ $\times$ 0 0 0 |  |


| $\begin{aligned} & \text { s } \\ & \text { D } \\ & 0 \\ & 0 \\ & \text { 음 } \\ & \text { ᄃ } \\ & \hline \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  |  |  | Control method: Enable/ Disable |  |  |  | $\xrightarrow[\text { ® }]{\stackrel{\text { ® }}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | $\begin{array}{l\|l} \mathrm{L} & \mathrm{~F} \\ \mathrm{E} & \mathrm{~F} \\ \mathrm{~S} \end{array}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}$ | S |  |
| F55 | 37h | H | LED Monitor (Display selection) | 1 | 16: Ai adjusted value (Ai1) (\%) <br> 17: Ai adjusted value (Ai2) (\%) <br> 18: Ai adjusted value (Ai3) (\%) <br> 19: Ai adjusted value (Ai4) (\%) <br> The following data will be hidden depending upon the mode or <br> options. <br> 20: PID command value (\%) <br> 21: PID feedback value (\%) <br> 22: PID output value (\%) <br> 23: Option monitor 1 (HEX) <br> 24: Option monitor 2 (HEX) <br> 25: Option monitor 3 (DEC) <br> 26: Option monitor 4 (DEC) <br> 27: Option monitor 5 (DEC) <br> 28: Option monitor 6 (DEC) <br> 29: - <br> 30: Load factor (\%) <br> 31: Input power (F60 switches units.) (kW/HP) <br> 32: Input watt-hour (x 100 kWh) | 0 | 0 | $\bigcirc$ | 49 | 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> 0 0 <br> -  <br> 0 0 <br> 0 0 <br> 0 0 | 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> - <br> 0 <br> 0 <br> 0 <br> 0 |  | 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br>  <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> - <br> 0 <br> 0 <br> 0 |  |
| F56 | 38h | H | LED Monitor (Display when stopped) | 1 | 0 to 1 <br> 0 : Display command value <br> 1: Display actual value <br> The display with the motor stopped is switchable with F55. Relevant data are speed (0), load axis rotational speed (13), and line speed (14). | 0 | 0 |  | 50 | - | O | 0 | O |  |
| F57 | 39h | h | LCD Monitor (Display selection) | 1 | 0 to 1 <br> 0: Display operation guidance screen (Operating condition, Rotation direction) <br> Display bar graph of operation data (Speed detect 1, Current, Torque command value) <br> Switches the running mode screen on the keypad. | 0 | 0 | 0 | 51 | 0 | 0 | 0 | 0 |  |
| F58 | 3Ah | h | LCD Monitor (Language selection) | 1 | 0 to 7 0: Japanese 1: English 2-5: - 6: Chinese 7: Korean | 0 | 0 |  | 52 | 0 | 0 | 0 | O |  |
| F59 | 3Bh |  | LCD Monitor (Contrast adjustment) | 1 | 0 (Low) to 10 (High) | 0 | 5 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 |  |
| F60 | 3Ch |  | Output unit (HP/kW) setting | 0 | 0 to 1 <br> 0: kW <br> 1: HP <br> Switches the display unit for the inverter output (power consumption) of the keypad LED and LCD monitors and the selection list (kW-HP) for P02 "Motor selection (M1)". | 0 | 0 | $\bigcirc$ | 53 | 0 | 0 | 0 | O |  |
| F61 | 3Dh | 6Bh | ASR1-P (Gain) | 10 | 0.1 to 500.0 times | 0 | 10.0 | 0 | 2 |  | 0 | $\times$ | O |  |
| F62 | 3Eh | 6Ch | ASR1-I (Integral constant) | 1 | 0.000 to 10.000 s P control when set to 0.000 | 0 | 0.200 | 0 | 4 | 0 | 0 | $\times$ | 0 |  |
| F63 | 3Fh | 6Dh | ASR1-FF (Gain) | 1 | 0.000 to 9.999 s | 0 | 0.000 | $\bigcirc$ | 4 | $\bigcirc$ | 0 | $\times$ | 0 |  |
| F64 | 40h | 6Eh | ASR1 Input filter | 1 | 0.000 to 5.000 s | 0 | 0.040 | $\bigcirc$ | 4 | 0 | $\bigcirc$ | O | O |  |
| F65 | 41h | 6Fh | ASR1 Detection filter | 1 | $0.000 \text { to } 0.100 \mathrm{~s}$ <br> Specifies the first order delay filter time constant for the detected speed value. | 0 | 0.005 | 0 | 4 | 0 | 0 | $\times$ | 0 |  |
| F66 | 42h | 70h | ASR1 Output filter | 1 | 0.000 to 0.100 s <br> Specifies the first order delay filter time constant for the torque command. | ${ }^{\times}$ | 0.002 | 00 | 4 | 0 | 0 | $\times$ | 0 |  |
| F67 | 43h | 71h | S-curve acceleration 1 (Start) | 1 | 0 to 50\% | 0 | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | - | 0 |  |
| F68 | 44h | 72h | S-curve acceleration 1 (End) | 1 | 0 to 50\% | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | $\bigcirc$ | 0 |  |
| F69 | 45h | 73h | S-curve deceleration 1 (Start) | 1 | 0 to 50\% | 0 | 0 | 0 | 0 | $\bigcirc$ | O | O | 0 |  |
| F70 | 46h | 74h | S-curve deceleration 1 (End) | 1 | 0 to 50\% | $\bigcirc$ | 0 | OO | 0 | 0 | 0 | $\bigcirc$ | 0 |  |
| F72 | 48h | h | Pre-excitation operation selection | 4 | 0 to 1 <br> 0 : Operates when starting operation. <br> Pre-excitation continues for the duration specified by F74. <br> 1: Operates when starting and stopping operation. <br> Pre-excitation continues for the duration specified by F74 or until the magnetic flux command reaches the level specified by E48, whichever is earlier. | ${ }^{\times}$ | 0 |  | 230 | 0 | 0 | $\times$ | $\times$ |  |
| F73 | 49h | h | Magnetic flux level at light load | 1 | 10 to 100\% | $\bigcirc$ | 100 | 0 | 16 | $\bigcirc$ | $\times \times$ | $\times$ | $\times$ |  |
| F74 | 4Ah | 75h | Pre-excitation (Duration) | 1 | 0.0 to 10.0 s When the operation command is turned ON (FWD, REV), the unit automatically enters the pre-excitation state for the time specified in this function code. | $\times$ | 0.0 | $\bigcirc$ | , |  | 0 | $\times$ | $\times$ |  |
| F75 | 4Bh | 76h | Pre-excitation (Initial level) | 1 | 100 to 400\% | $\times$ | 100 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | $\times$ | O |  |
| F76 | 4Ch | h | Speed limiter (Mode selection) | 3 | ```0 to 3 0: Limits to Normal: Level 1, Reverse: level 2. 1: Limits to Normal: Level 1, Reverse: level 1. 2: Limits to upper limit at level 1, lower limit at level 2. 3: Limits to Normal: Level 1, Reverse: level 2. Terminal [12] input added as a bias``` | ${ }^{\times}$ | 0 | 0 | 91 | 0 | O | $\bigcirc$ | 0 |  |
| F77 | 4Dh | 4Fh | Speed limiter (Level 1) | 1 | -110.0 to 110.0\% | 0 | 100.0 | 0 | 6 | $\bigcirc$ | O |  | 0 |  |
| F78 | 4Eh | FEh | Speed limiter (Level 2) | 1 | -110.0 to 110.0\% | 0 | 100.0 | $\bigcirc$ | 6 | O | O | O | 0 |  |
| F79 | 4Fh | 77h | Motor selection (M1, M2, M3) | 0 | 0 to 2 <br> 0: M1 selected <br> Note that switching of contacts by X functions has priority over this function code setting. <br> 1: $\quad \mathrm{M} 2$ selected ( X function disable) <br> 2: M3 selected ( $X$ function disable) <br> Select a motor to be used from M1, M2 and M3. | $\times$ | 0 |  | 54 | O | O | $\bigcirc$ | O |  |


| Function codes | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | 苟 | $\begin{aligned} & \text { 耏 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\left\lvert\, \begin{aligned} & \mathrm{L} \\ & \mathrm{E} \\ & \mathrm{~S} \end{aligned}\right.$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}$ | S |  |
| F80 | 50h | h | Current rating switching | 0 | 0 to 3 <br> Stack type <br> $0,2,3$ : MD (high duty overload current $150 \%-1 \mathrm{~min}$ ) <br> 1 : LD (low duty overload current 110\%-1min) <br> It switches the dual ratings (MD, LD) of inverter. As for <br> keypad display, HD display is operated in accordance with MD spec. <br> Unit type <br> 0,2 : HD (high duty overload current $150 \%-1 \mathrm{~min} / 200 \%-3 \mathrm{sec}$ ) <br> 1 : LD (low duty overload current $120 \%-1 \mathrm{~min}$ ) <br> : MD (medium duty overload current 150\%-1min) <br> It switches the triple ratings (HD, LD, MD) of inverter. | $\times$ | 0 | 0 | $\times$ | 56 | O | $\bigcirc$ | $\bigcirc$ | 0 |  |
| F81 | 51h | h | Offset for speed setting on terminal [12] | 3 | -30000 to $30000 \mathrm{r} / \mathrm{min}$ <br> Specifies the offset for analog speed setting value on control terminal [12]. | 0 | 0 | O | O | 5 | 0 | 0 | 0 | 0 |  |
| $\begin{aligned} & \text { F82 } \\ & (* 1) \end{aligned}$ | 52h | h | Dead zone for speed setting on terminal [12] | 1 | 0.0 to $150.0 \mathrm{r} / \mathrm{min}$ <br> Limits the speed command value below specified value $\pm$ to 0 <br> $\mathrm{r} / \mathrm{min}$ for analog speed setting value on control terminal [12]. | 0 | 0.0 | 0 | O | 2 | 0 | $\bigcirc$ | 0 | 0 |  |
| F83 | 53h | h | Filter for speed setting on terminal [12] | 1 | 0.000 to 5.000 s | $\bigcirc$ | 0.005 | 0 | O | 4 | O | $\bigcirc$ | 0 | 0 |  |
| F84 | 54h | h | Display coefficient for input watt-hour data <br> * Invalid for use in stack type | 0 | 0.000 to 9999 <br> Specifies a display coefficient for displaying the input watt-hour data (M116). <br> M116 = F84 x M115 "Input watt-hour" (kWh) <br> Specification of 0.000 clears the input watt-hour data. | 0 | 0.010 | 0 | O | 101 | O | 0 | 0 | 0 |  |
| F85 | 55h | h | Display filter for calculated torque | 0 | 0.000 to 1.000 s <br> Specifies a display filter for calculated torque output for monitoring (keypad LED monitor and keypad LCD monitor). | 0 | 0.100 | 0 | O | 4 | O | 0 | 0 | 0 |  |

(*1) Supported by ROM version H1/2 0019 or later.

## Terminal functions (E: Extensional terminal Functions)




*1 Availble in the ROM version H1/2 02ara, which supports PROFINET-IRT.
*2 Available when the ROM version is $\mathrm{H} 1 / 20020$ or later.



## - Control functions (C: Control Functions)

| $\begin{aligned} & \stackrel{y}{8} \\ & \stackrel{8}{8} \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  |  | ( |  | Control method: Enable/ Disable |  |  |  | $\underset{\sim}{\stackrel{\sim}{\square}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \stackrel{\rightharpoonup}{5} \\ & \stackrel{\rightharpoonup}{4} \end{aligned}$ | 485 No. | Link No. |  |  |  |  |  |  |  |  |  | L | V | S |  |
| C01 | 201h | h | Jump speed 1 | 4 | 0 to $30000 \mathrm{r} / \mathrm{min}$ <br> Enables the inverter to jump over a point on the reference speed in order to skip a resonance point of the driven machinery (load) and the motor speed. Up to three different jump points can be specified. | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | O | O | $\bigcirc$ |  |
| C02 | 202h | h | Jump speed 2 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min}$ | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | O | O | O |  |
| C03 | 203h | h | Jump speed 3 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min}$ | 0 | 0 | $\bigcirc$ | - | 0 | O | O | - | O |  |
| C04 | 204h | h | Jump width | 1 | 0 to $1000 \mathrm{r} / \mathrm{min}$ | 0 | 0 | $\bigcirc$ | - | 0 | - | 0 | - | O |  |
| C05 | 205h | 9Eh | Multistep speed 1 | 17 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \% /$ 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) Multistep speeds 1 to 15 can be switched by turning terminal commands SS1, SS2, SS4 and SS8 ON/OFF. | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.00 / \\ 0.0 \end{array}$ | $\bigcirc$ | - | 0 | $\bigcirc$ | - | - | - |  |
| C06 | 206h | 9 Fh | Multistep speed 2 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.00 \mathrm{f} \\ 0.0 \\ \hline \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | 0 | O | $\bigcirc$ |  |
| C07 | 207h | AOh | Multistep speed 3 | 1 | $\begin{aligned} & 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% \text { / } \\ & 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with C21) } \end{aligned}$ | 0 | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | O | 0 | 0 | O | O | O | - |  |
| C08 | 208h | A1h | Multistep speed 4 | 1 | $\begin{array}{\|l\|} \hline 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% / \\ 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with C21) } \\ \hline \end{array}$ | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | - | O | $\bigcirc$ |  |
| C09 | 209h | A2h | Multistep speed 5 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{c\|} \hline 0 / 0.000 \\ 0.0 \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | - | O | $\bigcirc$ |  |
| C10 | 20Ah | A3h | Multistep speed 6 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | $\bigcirc$ | 0 | 0 | $\bigcirc$ | O | O | - |  |
| C11 | 20Bh | A4h | Multistep speed 7 | 1 | $\begin{aligned} & 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% \text { / } \\ & 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with C21) } \end{aligned}$ | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | O | O | 0 | O | $\bigcirc$ | - | O |  |
| C12 | 20Ch | h | Multistep speed 8 | 1 | $\begin{array}{\|l\|} \hline 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% / \\ 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with } \mathrm{C} 21 \text { ) } \\ \hline \end{array}$ | 0 | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | O | 0 | 0 | $\bigcirc$ | O | O | 0 |  |
| C13 | 20Dh | h | Multistep speed 9 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | - | O | $\bigcirc$ |  |
| C14 | 20Eh | h | Multistep speed 10 | 1 | $\begin{array}{\|l\|} \hline 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% / \\ 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with } \mathrm{C} 21 \text { ) } \\ \hline \end{array}$ | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | O | 0 | 0 | $\bigcirc$ | O | - | - |  |
| C15 | 20Fh | h | Multistep speed 11 | 1 | $\begin{aligned} & 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% \text { / } \\ & 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with } 21 \text { ) } \end{aligned}$ | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | O | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | O | $\bigcirc$ |  |
| C16 | 210h | h | Multistep speed 12 | 1 | $\begin{array}{\|l\|} \hline 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% / \\ 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with } \mathrm{C} 21 \text { ) } \\ \hline \end{array}$ | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.001 \\ 0.0 \\ \hline \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | O | - | $\bigcirc$ |  |
| C17 | 211h | h | Multistep speed 13 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.00 / \\ 0.0 \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | O | $\bigcirc$ |  |
| C18 | 212h | h | Multistep speed 14/Creeping speed 1 | 1 | $\begin{aligned} & 0 \text { to } 30000 \mathrm{r} / \mathrm{min} / 0.00 \text { to } 100.00 \% / \\ & 0.0 \text { to } 999.9 \mathrm{~m} / \mathrm{min} \text { (switch with } \mathrm{C} 21 \text { ) } \\ & \mathrm{C} 18 \text { and } \mathrm{C} 19 \text { apply also to the creep speed under } \\ & \text { UP/DOWN control. } \end{aligned}$ | $\bigcirc$ | $\begin{array}{c\|} \hline 0 / 0.000 \\ 0.0 \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | - | - | O | $\bigcirc$ |  |
| C19 | 213h | h | Multistep speed 15/Creeping speed 2 | 1 | 0 to $30000 \mathrm{r} / \mathrm{min} / 0.00$ to $100.00 \%$ / 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ (switch with C21) | $\bigcirc$ | $\begin{array}{\|c\|} \hline 0 / 0.000 \\ 0.0 \end{array}$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ |  |
| C20 | 214h | h | Multistep speed agreement timer | 1 | 0.000 to 0.100 s <br> When SS1, SS2, SS4 and SS8 are kept at the same status for the duration specified by this function code, the inverter switches the speed setting value. | 0 | 0.000 | $\bigcirc$ | $\bigcirc$ | 4 | $\bigcirc$ | - | O | $\bigcirc$ |  |
| C21 | 215h | h | Multistep speed setting definition | 1 | 0 to 2 <br> 0: 0 to $30000 \mathrm{r} / \mathrm{min}$ <br> 1: 0.00 to $100.00 \%$ <br> 2: 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ <br> Defines the unit of multistep speed specified by C05 to C19. <br> When $\mathrm{C} 21=1$, the percentage of the maximum speed <br> (F03/A06/A106) of the selected motor applies. | $\times$ | 0 | $\bigcirc$ | 0 | 93 | $\bigcirc$ | O | $\bigcirc$ | - |  |
| C25 | 219h | h | Speed setting N2 | 0 | 0 to 9 <br> 0: Keypad $(\otimes / \otimes$ keys $)$ <br> 1: Analog 12 input ( 0 to $\pm 10 \mathrm{~V}$ ) <br> 2: Analog 12 input ( 0 to +10 V ) <br> 3: UP/DOWN (initial value 0 ) <br> 4: UP/DOWN (initial value: previous value) <br> 5: UP/DOWN (initial value: creep velocity 1,2 ) <br> 6: DIA card input <br> 7: DIB card input <br> 8: Ai (N-REFV) input <br> 9: Ai2 (N-REFC) input <br> The speed command specified by this function code takes effect when X terminal function $\mathrm{N} 2 / \mathrm{N} 1$ is turned ON. | $\times$ | 0 | O | - | 41 | $\bigcirc$ |  | O | 0 |  |
| C29 | 21Dh | h | Jogging speed | 0 | 0 to $30000 \mathrm{r} / \mathrm{min}$ <br> Specifies the speed to be applied when the motor jogs. | $\bigcirc$ | 50 | $\bigcirc$ | O | 0 | $\bigcirc$ | 0 | O | O |  |
| C30 | 21Eh | h | ASR-P (Gain) JOG | 9 | 0.1 to 500.0 times | 0 | 10.0 | 0 | 0 | 2 | $\bigcirc$ | 0 | $\times$ | $\bigcirc$ |  |
| C31 | 21Fh | h | ASR-I (Integral constant) JOG | 1 | 0.000 to 10.000 s <br> P control when set to 0.000 | $\bigcirc$ | 0.200 | $\bigcirc$ | O | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ | $\bigcirc$ |  |
| C32 | 220h | h | ASR-JOG (Input filter) | 1 | 0.000 to 5.000 s | 0 | 0.040 | $\bigcirc$ | O | 4 | $\bigcirc$ | O | $\bigcirc$ | $\bigcirc$ |  |
| C33 | 221h | h | ASR-JOG (Detection filter) | 1 | 0.000 to 0.100 s | $\bigcirc$ | 0.005 | $\bigcirc$ | 0 | 4 | 0 | 0 | $\times$ | 0 |  |
| C34 | 222h | h | ASR-JOG (Output filter) | 1 | 0.000 to 0.100 s | $\times$ | 0.002 | $\bigcirc$ | - | 4 | 0 | $\bigcirc$ | $\times$ | $\bigcirc$ |  |
| C35 | 223h | h | Acceleration time JOG | 1 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 100 \text { to } 3600 \mathrm{~s} \end{aligned}$ | $\bigcirc$ | 5.00 | $\bigcirc$ | O | 13 | 0 | 0 | $\bigcirc$ | - |  |
| C36 | 224h | h | Deceleration time JOG | 1 |  | 0 | 5.00 | $\bigcirc$ | - | 13 | $\bigcirc$ | $\bigcirc$ | - | O |  |
| C37 | 225h | h | S-curve JOG (Start side) | 1 | 0 to 50\% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 |  |
| C38 | 226h | h | S-curve JOG (End side) | 1 | 0 to 50\% | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | O | $\bigcirc$ | 0 |  |
| C40 | 228h | h | ASR2-P (Gain) | 10 | 0.1 to 500.0 times | 0 | 10.0 | $\bigcirc$ | 0 | 2 | 0 | $\bigcirc$ | $\times$ | $\bigcirc$ |  |

## Motor parameter functions M1 (P: Motor Parameter Functions)

| Function codes | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  | $\stackrel{\text { ¢ }}{\stackrel{\infty}{\square}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  | $\left\lvert\, \begin{gathered} \frac{\pi}{0} \\ \stackrel{0}{0} \\ \hline \end{gathered}\right.$ | 号 | \% | P | $\begin{array}{l\|l} L & V \\ E & V \\ S & F \end{array}$ | V $\begin{gathered}\text { s } \\ M\end{gathered}$ |  |
| P01 | 301h | h | M1 Drive control | 0 | ```0 to } 0: Vector control (Induction motor) 1: Sensor-less vector control (Induction motor) 2: Simulated operation mode 3: Vector control (PMSM) 4: - 5: V/f control (Induction motor)``` | $\times$ | 0 | $\bigcirc$ | $\times$ | 55 | $\bigcirc$ | 0 | 0 |  |
| P02 | 302h | h | M1 Motor selection | 26 | 0 to 50 <br> Display (kW, HP) changes by setting $\mathrm{F} 60=0,1$. <br> 00 to 35: FRENIC-VG dedicated motor setup <br> Data at F04, F05, and P03 to P27 are automatically set. <br> Data at F04, F05, and P03 to P27 are automatically set and write-protected. <br> P-OTHER (keypad display is P-OTR) <br> Data at F04, F05, and P03 to P27 are write-protected and cannot be overwritten. <br> Data at F04, F05, and P03 to P27 are automatically set and write-protected. <br> 37: OTHER <br> Data at F04, F05, and P03 to P27 are write-protected and cannot be overwritten. <br> Write protection of F04, F05, and P03 to P27 is not performed. <br> 38 to 50: FRENIC-VG dedicated setup (type 8) <br> Data at F04, F05, and P03 to P27 are automatically set. <br> Data at F04, F05, and P03 to P27 are automatically set and write-protected. <br> For the relationship between the setting data and the motor type, refer to "List of applicable motors" in Section 4.3.3.2, [82] codes. | ${ }^{\times}$ | Depends on capacity | 0 | $\times$ | 82 | O | 0 O | 0 |  |
| P03 | 303h | A7h | M1 Rated capacity | 1 | For inverters of 400 kW or less <br> 0.00 to 500.00 kW when $\mathrm{F} 60=0$ <br> 0.00 to 600.00 HP when $\mathrm{F} 60=1$ <br> For inverters of 500 kW or more <br> 0.00 to 1200 kW when $\mathrm{F} 60=0$ <br> 0.00 to 1600 HP when $\mathrm{F} 60=1$ <br> For multiwinding motors, set the motor capacity per wiring. | $\times$ | Depends on capacity | 0 | $\times$ | $\begin{gathered} 3 \\ 13 \end{gathered}$ | $\bigcirc$ | 0 O | - |  |
| P04 | 304h | A8h | M1 Rated current | 1 | 0.01 to 99.99A 100.0 to 999.9A 1000 to 2000A | $\times$ | Depends on capacity | 0 | $\times$ | 13 | $\bigcirc$ | 0 | - |  |
| P05 | 305h | A9h | M1 Number of poles | 1 | 2 to 100 poles | $\times$ | 4 | $\bigcirc$ | $\times$ | 1 | $\bigcirc$ | $\bigcirc$ | O |  |
| P06 | 306h | AAh | M1 \%R1 | 1 | 0.00 to 30.00\% | 0 | Depends on capacity | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | 0 O | - |  |
| P07 | 307h | ABh | M1 \%X | 1 | 0.00 to 200.00\% | $\bigcirc$ | Depends on capacity | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | 0 O | - |  |
| P08 | 308h | ACh | M1 Exciting current/Magnetic flux weakening current (-ld) | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 13 | $\bigcirc$ | 0 | - |  |
| P09 | 309h | ADh | M1 Torque current | 1 | 0.01 to 99.99 A 100.0 to 999.9A 1000 to 2000A | 0 | Depends on capacity | 0 | $\times$ | 13 | $\bigcirc$ | 0 | - |  |
| P10 | 30Ah | AEh | M1 Slip frequency (For driving) | 1 | 0.001 to 10.000 Hz | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| P11 | 30Bh | AFh | M1 Slip frequency (For braking) | 1 | 0.001 to 10.000 Hz | 0 | Depends on capacity | 0 | $\times$ | 4 | $\bigcirc$ | 0 | $\times$ |  |
| P12 | 30 Ch | B0h | M1 Iron loss factor 1 | 1 | 0.00 to 10.00\% | $\bigcirc$ | Depends on capacity | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| P13 | 30Dh | B1h | M1 Iron loss factor 2 | 1 | 0.00 to 10.00\% | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 3 | O | 0 | $\bigcirc$ |  |
| P14 | 30Eh | B2h | M1 Iron loss factor 3 | 1 | 0.00 to 10.00\% | 0 | Depends on capacity | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| P15 | 30Fh | B3h | M1 Magnetic saturation factor 1 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $93.75 \%$. | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 2 | 0 | 0 | $\times$ |  |
| P16 | 310h | B4h | M1 Magnetic saturation factor 2 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $87.5 \%$. | 0 | Depends on capacity | 0 | $\times$ | 2 | $\bigcirc$ | 0 | ${ }^{x}$ |  |
| P17 | 311h | B5h | M1 Magnetic saturation factor 3 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $75 \%$. | 0 | Depends on capacity | 0 | $\times$ | 2 | $\bigcirc$ | 0 | $\times$ |  |
| P18 | 312h | B6h | M1 Magnetic saturation factor 4 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $62.5 \%$. | 0 | Depends on capacity | 0 | $\times$ | 2 | $\bigcirc$ | 0 | ${ }^{x}$ |  |
| P19 | 313h | B7h | M1 Magnetic saturation factor 5 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $50 \%$. | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 2 | $\bigcirc$ | 0 | ${ }^{x}$ |  |
| P20 | 314h | B8h | M1 Secondary time constant | 1 | 0.001 to 9.999 s | 0 | Depends on capacity | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | 0 | ${ }^{\times}$ |  |
| P21 | 315h | B9h | M1 Induced voltage factor | 1 | 0 to 999 V | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| P22 | 316h | BAh | M1 R2 Correction factor 1 | 1 | 0.500 to 5.000 | 0 | Depends on capacity | 0 | $\times$ | 4 | O | 0 | $\bigcirc$ |  |
| P23 | 317h | BBh | M1 R2 Correction factor 2 | 1 | 0.500 to 5.000 | $\bigcirc$ | Depends on capacity | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| P24 | 318h | BCh | M1 R2 Correction factor 3 | 1 | 0.010 to 5.000 | 0 | Depends on capacity | 0 | $\times$ | 4 | $\bigcirc$ | $0 \times$ | $\times$ |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  |  | . |  | Control method: Enable/ Disable |  |  |  | $\stackrel{\text { n }}{\substack{\text { n }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | 完 | $\stackrel{\substack{0}}{0}$ | P | L | V | $\begin{aligned} & \mathrm{S} \\ & \mathrm{M} \end{aligned}$ |  |
| P25 | 319h | BDh | M1 Exciting current correction factor | 1 | 0.000 to 5.000 | 0 | Depends on capacity | 0 | $\times$ | 4 | 0 | 0 | $\times$ | $\times$ |  |
| P26 | 31Ah | BEh | M1 ACR-P (Gain) | 1 | 0.1 to 20.0 | $\bigcirc$ | 1.0 | 0 | $\times$ | 2 | 0 | 0 | $\times$ | 0 |  |
| P27 | 31Bh | BFh | M1 ACR-I (I-time) | 1 | 0.1 to 100.0 ms | $\bigcirc$ | 1.0 | 0 | $\times$ | 2 | $\bigcirc$ | 0 | $\times$ | O |  |
| P28 | 31Ch | COh | M1 PG Pulse resolution | 0 | $\begin{aligned} & 100 \text { to } 60000 \\ & { }_{*}^{*} \quad \text { Set P28 to } 32768 \text { when using the option card } \\ & \text { OPC-VG1-SPGT. } \end{aligned}$ | $\times$ | 1024 | 0 | $\times$ | 0 | 0 | $\times$ | $\times$ | 0 |  |
| P29 | 31Dh | D6h | M1 External PG correction factor | 0 | 0000 to 4FFF | $\times$ | 4000 | 0 | $\times$ | 9 | 0 | $\times$ | $\times$ | O |  |
| P30 | 31Eh | C1h | M1 Thermistor selection | 0 | 0 to 3 <br> 0 : No thermistor <br> 1: NTC thermistor selected <br> 2: PTC thermistor selected <br> 3: Ai [M-TMP] <br> The protection level of the motor protective functions should be specified by E30 to E32. | $\times$ | 1 | 0 | $\times$ | 84 | 0 | 0 | 0 | 0 |  |
| P32 | 320h | h | M1 Online Auto tuning | 0 | 0 to 1 <br> 0 : Disable <br> 1: Enable <br> Selects the compensation function for the resistance change caused by the temperature rise of the motor running. | 0 | 0 | 0 | $\times$ | 0 | 0 | 0 | $\times$ | $\times$ |  |
| P33 | 321h | h | M1 Maximum output voltage/Maximum voltage limit value | 0 | 80 to 999 V | $\times$ | $\begin{gathered} 220 / \\ 440 \end{gathered}$ | 0 | $\times$ | 0 | $\times$ | $\times$ | 0 | 0 |  |
| P34 | 322h | h | M1 Slip compensation | 3 | -20.000 to 5.000 Hz | 0 | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times$ | 0 | $\times$ |  |
| P35 | 323h | h | M1 Torque boost | 1 | 0.0 to 20.0  <br> Function specific to V/f control. The following selections are  <br> $0.0:$ possible. <br> Automatic torque boost (for fixed torque <br> characteristic load)  <br> 0.1 to $0.9:$ For squared torque characteristic load <br> 1.0 to 1.9: For proportional torque characteristic load <br> 2.0 to $20.0:$ For fixed torque characteristic load | 0 | 0.0 | 0 | $\times$ | 2 | $\times$ | $\times$ | 0 | $\times$ |  |
| P36 | 324h | h | M1 Current fluctuation damping gain | 1 | 0.00 to 1.00 | 0 | 0.20 | 0 | $\times$ | 3 | $\times$ | $\times$ | 0 | $\times$ |  |
| P42 | 32Ah | h | M1 q axis inductance magnetic saturation coefficient | 10 | 0.0 to 100.0\% | 0 | 100.0 | 0 | $\times$ | 2 | $\times$ | $\times$ | $\times$ | 0 |  |
| P43 | 32Bh | h | M1 Magnetic flux limiting value | 1 | 50.0 to 150.0\% | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 2 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| P44 | 32Ch | h | M1 Overcurrent protection level | 1 | $\begin{aligned} & \text { 0.00: No operation } \\ & 0.01 \text { to } 99.99 \mathrm{~A} \\ & 100.0 \text { to } 999.9 \mathrm{~A} \\ & 1000 \text { to } 2000 \mathrm{~A} \end{aligned}$ <br> Specifies the allowable current value to prevent the permanent magnet of a PMSM from getting demagnetized. If the current exceeding this setting value flows, an overcurrent alarm (OC) occurs. | $\times$ | 0.00 | 0 | $\times$ | 13 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| P45 | 32Dh | h | M1 Torque correction gain 1 | 1 | 0.00 to 10.00 | 0 | $\begin{array}{\|c\|} \hline \text { Depends } \\ \text { on capacity } \\ \hline \end{array}$ | 0 | $\times$ | 3 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| P46 | 32Eh | h | M1 Torque correction gain 2 | 1 | 0.00 to 10.00 | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 3 | $\times$ | $\times$ | $\times$ | O |  |
| P47 | 32Fh | h | M1 Torque correction gain 3 | 1 | -1.000 to 1.000 | $\bigcirc$ | Depends on capacity | 0 | $\times$ | 8 | $\times$ | $\times$ | $\times$ | O |  |
| P48 | 330h | h | M1 Torque correction gain 4 | 1 | -1.000 to 1.000 | 0 | Depends on capacity | 0 | $\times$ | 8 | $\times$ | $\times$ | $\times$ | 0 |  |
| P49 | 331h | h | M1 Torque correction gain 5 | 1 | -50.00 to 50.00 | O | Depends on capacity | 0 | $\times$ | 7 | $\times$ | $\times$ | $\times$ | O |  |
| P50 | 332h | h | M1 Torque correction gain 6 | 1 | -50.00 to 50.00 | O | Depends on capacity | 0 | $\times$ | 7 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| P51 | 333h | h | M1 Torque correction gain 7 | 1 | -1.000 to 1.000 | O | Depends on capacity | 0 | $\times$ | 8 | $\times$ | $\times$ | $\times$ | O |  |

High performance functions (H: High Performance Functions)

| $\begin{aligned} & \text { e } \\ & 0 \\ & 0 \\ & 0 \\ & \text { ob } \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\left\|\begin{array}{l} 0 \\ .0 \\ 0 . \\ 0 \\ 0 \\ 0 \\ \frac{0}{0} \\ 0 \end{array}\right\|$ |  |  | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \overline{\mathrm{O}} \\ & \stackrel{1}{5} \end{aligned}$ | 485 No. | Link No. |  |  |  |  |  |  | 号 |  | P | L | V | S |  |
| H01 | 401h | h | Tuning operation selection | 0 | 0 to 4 <br> 0 : No operation | $\times$ | 0 | $\times$ | $\times$ | 61 | $\bigcirc$ | - | $\bigcirc$ | O |  |
|  |  |  |  |  | 1: ASR auto tuning (To be supported soon) |  |  |  |  |  | 0 | 0 | $\times$ | $\bigcirc$ |  |
|  |  |  |  |  | 2: Motor constant auto tuning: R1, L $\sigma$ |  |  |  |  |  | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ |  |
|  |  |  |  |  | 3: Motor stop auto tuning |  |  |  |  |  | $\bigcirc$ | O | 0 | $\times$ |  |
|  |  |  |  |  | 4: Motor rotation auto tuning After writing the data, this function's data code automatically returns to 0 . To save the tuned data, perform the Full save function (H02). |  |  |  |  |  | $\bigcirc$ | $\bigcirc$ | O | $\times$ |  |
| H02 | 402h | Eh | Full save function | 0 | 0 to 1 <br> When auto tuning is executed at H 01 , or when the data is written by way of the link system (T-Link, field bus, and RS-485, etc.), the data goes out when the power supply of the inverter is turned off. <br> This function must operate when preservation is necessary. After writing the data, this function's data code automatically returns to 0 . | 0 | 0 | $\times$ | $\times$ | 11 | - | O | - | O |  |
| H03 | 403h | h | Data initialization | 0 | 0 to 1 <br> Setting H03 to "1" reverts the function code data modified by the customer to the factory defaults. <br> Initialization targets include all fields of F, E, C, H, o, L and U codes except motor parameter fields (P, A) and F04, F05, F10 to F12, and F58. <br> Upon completion of the initialization, the H 03 data automatically reverts to " 0 ." | $\times$ | 0 | $\times$ | $\times$ | 11 | O | $\bigcirc$ | O | 0 |  |
| H04 | 404h | h | Auto-reset (Times) | 0 | ```0 to 10 0 : No operation 1 to 10 times The auto-resetting signal can be output to the output terminal.``` | * | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | - | 0 |  |
| H05 | 405h | h | Auto-reset (Reset interval) | 0 | 0.01 to 20.00 s | $\times$ | 5.00 | $\bigcirc$ | 0 | 3 | O | 0 | 0 | 0 |  |
| H06 | 406h | h | Cooling fan ON/OFF control | 0 | 0 to 1 <br> 0 : No operation <br> 1: Operation It is possible to output the FAN (cooling fan in operation) signal in conjunction with this function. <br> This control detects the temperature of the heat sink in the inverter unit and turns the cooling fan ON/OFF automatically. | $\times$ | 0 | O | 0 | 68 | 0 | O | O | O |  |
| H08 | 408h | h | Rev. phase sequence lock | 0 | $\begin{aligned} & \hline 0 \text { to } 1 \\ & \text { 0: Disable } \\ & \text { 1: Enable } \end{aligned}$ | O | 0 | 0 | 0 | 68 | 0 | 0 | $\times$ | O |  |
| H09 | 409h | C2h | Starting mode (Auto search) | 0 | 0 to 2 <br> 0: No operation <br> 1: Operation (only when restarting from momentary power failure) <br> 2: Operation <br> Auto search detects the idling motor speed at starting and drives the motor at the same speed. | 0 | 2 | 0 | 0 | 0 | $\times$ | O | 0 | $\times$ |  |
| H10 | 40Ah | C3h | Energy-saving operation | 0 | $\begin{aligned} & \hline 0 \text { to } 1 \\ & \text { 0: Disable } \\ & \text { 1: Enable } \end{aligned}$ | $\times$ | 0 | 0 | 0 | 68 | 0 | $\times$ | $\times$ | $\times$ |  |
| H11 | 40Bh | h | Automatic operation OFF function | 0 | 0 to 4 <br> 0: Decelerate to stop when OFF between FWD-CM and REV-CM <br> 1: Operation OFF when below stop speed in F37 even if ON between FWD-CM and REV-CM <br> 2: Coast to a stop when OFF between FWD-CM and REV-CM <br> 3: ASR deceleration to stop when OFF between FWD-CM and REV-CM (under torque control) <br> 4: Coast to a stop when OFF between FWD-CM and REV-CM (under torque control) | O | 0 | 0 | 0 | 0 | 0 | O | O | O |  |
| H13 | 40Dh | C4h | Restart mode after momentary power failure setting (Wait time) | 5 | 0.1 to 5.0 s | ${ }^{\times}$ | 0.5 | $\bigcirc$ | 0 | 2 | 0 | O | O | 0 |  |
| H14 | 40Eh | h | ```Momentary power failure restart settingNone``` | 1 | 1 to $3600 \mathrm{r} / \mathrm{min} / \mathrm{s}$ | O | 500 | 0 | 0 | 0 | $\times$ | $\times$ | 0 | $\times$ |  |
| H15 | 40Fh | h | Momentary power failure restart setting (Operation continuation level) | 1 | 3-phase 200 V : 200 to 300 V <br> 3-phase $400 \mathrm{~V}: 400$ to 600 V <br> This setting applies when F14 (Operation selection) $=2$ <br> (Trip after recovery from power failure) or F14 = 3 (Continue to run). | 0 | $\begin{gathered} \hline 235 / \\ 470 \end{gathered}$ | 0 | 0 | 0 | 0 | O | O | O |  |
| H16 | 410h | h | Momentary power failure restart setting (Self-holding specification of operation command) | 1 | 0 to 1 <br> 0: Specified in H 17 <br> 1: Max. time (operating commands are retained by the inverter while the control power supply is established inside the inverter, or while the DC intermediate circuit voltage is approximately zero) | $\times$ | 1 | 0 | 0 | 94 | 0 | O | O | 0 |  |
| H17 | 411h | h | Momentary power failure restart <br> setting <br> (Self-holding time in operation <br> command) | 1 | 0.0 to 30.0 s | $\times$ | 30.0 | $\bigcirc$ | 0 | 2 | 0 | 0 | - | 0 |  |
| H19 | 413h | C5h | Active drive | 0 | ```0 to 1 0: Disable 1: Enable Under vector control, this function automatically limits the output torque to avoid an overload trip, etc.``` | $\times$ | 0 | 0 | 0 | 68 | 0 | O | O | 0 |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  | $\stackrel{\text { ¢ }}{\stackrel{\text { ® }}{\text { ¢ }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | $\left\lvert\, \begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}\right.$ | $\begin{array}{\|l\|l\|} \hline \mathrm{L} & \mathrm{~V} \\ \mathrm{E} & \mathrm{~F} \\ \mathrm{~S} & \\ \hline \end{array}$ | \% s |  |
| H20 | 414h | C6h | PID Control (Operation selection) | 8 | 0 to 3 <br> 0 : No operation <br> 1: Operation <br> 2: Reverse operation 1 <br> 3: Reverse operation 2 | $\times$ | 0 | 0 | $\bigcirc$ | 69 | 0 | 0 | $\bigcirc$ |  |
| H21 | 415h | C7h | PID Control (Command selection) | 1 | $\begin{aligned} & 0 \text { to } 1 \\ & \text { 0: Keypad or } 12 \text { input } \\ & \text { 1: Analog input [PID-REF] } \end{aligned}$ | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 70 | 0 | 0 | $\bigcirc$ |  |
| H22 | 416h | C9h | PID Control (P-action) | 1 | 0.000 to 10.000 times | 0 | 1.000 | 0 | 0 | 4 | 0 | 00 | $\bigcirc$ |  |
| H23 | 417h | CAh | PID Control (l-action) | 1 | 0.00 to 100.00 s | $\bigcirc$ | 1.00 | O | $\bigcirc$ | 3 | 0 | 0 O | O |  |
| H24 | 418h | CBh | PID Control (D-action) | 1 | 0.000 to 10.000 s | $\bigcirc$ | 0.000 | O | $\bigcirc$ | 4 | 0 | 0 O | O |  |
| H25 | 419h | C8h | PID Control (Upper limit value) | 1 | -300 to 300\% | $\times$ | 100 | 0 | $\bigcirc$ | 5 | 0 | 00 | 0 |  |
| H26 | 41Ah | CCh | PID Control (Lower limit value) | 1 | -300 to 300\% | $\times$ | -100 | O | $\bigcirc$ | 5 | 0 | 00 | O |  |
| H27 | 41Bh | CEh | PID Control (Speed command selection) | 1 | 0 to 2 0: Disable 1: PID selection 2: Speed adjustment selection | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 95 | 0 | 0 | O |  |
| H28 | 41Ch | CFh | Droop control | 0 | 0.0 to 25.0\% | 0 | 0.0 | O | $\bigcirc$ | 2 | 0 | 0 | 0 |  |
| H29 | 41Dh | h | Link function (Code protection) | 2 | 0 to 1 <br> 0 : Writing code from link allowed <br> 1: Write-protects code from link <br> Setting H29 to "1" protects function code data from getting changed mistakenly via the link (T-Link, RS-485, etc.). Via the link, data can be written to the "normal code fields" (given above) or "command data fields" (S fields). The S fields are defined by H30. | $\bigcirc$ | 0 | - | - | 40 | $\bigcirc$ | 0 O | 0 |  |
| H30 | 41Eh | DOh | Link function (Linked operation) | 1 | 0 to 3    <br>  Monitor Command <br> data Operation (FWD, REV) <br> $0:$ 0 $\times$ $\times$ <br> $1:$ 0 0 $\times$ <br> $2:$ 0 $\times$ 0 <br> $3:$ 0 0 0 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | 72 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| H31 | 41Fh | h | RS-485 Setup <br> (Station address) | 10 | 0 to 255 Broadcast: 0: RTU), (99: Fuji) address: 1 to 255 Specifies the station address of RS-485. | $\times$ | 1 | $\bigcirc$ | $\times$ | 0 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| H32 | 420h | h | RS-485 Setup (Selection of operation when error occurs) | 1 | 0 to 3 <br> Forced stop (E, (-S) <br> Stop after continuing operation for timer operating time <br>  <br> 2: Stop if transmission failure continues longer than timer operating time $(\mathrm{H} 33)($ E,- <br> 3: Continue operation | 0 | 3 | 0 | $\bigcirc$ | 73 | 0 | 00 | 0 |  |
| H33 | 421h | h | RS-485 Setup (Timer operating time) | 1 | 0.01 to 20.00 s | 0 | 2.00 | 0 | $\bigcirc$ | 3 | 0 | 0 O | $\bigcirc$ |  |
| H34 | 422h | h | RS-485 Setup <br> (Transmission speed) | 1 | 0 to 4 0: 38400 bps 1: 19200 bps 2: 9600 bps 3: 4800bps 4: 2400bps | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ | 74 | 0 | 0 | $\bigcirc$ |  |
| H35 | 423h | h | RS-485 Setup (Data length) | 1 | $\begin{aligned} & 0 \text { to } 1 \\ & 0: 8 \mathrm{bit} \\ & 1: 7 \mathrm{bit} \end{aligned}$ | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ | 75 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| H36 | 424h | h | RS-485 Setup (Selection of parity bit) | 1 | 0 to 2 o: None 1: Even parity 2: Odd parity | 0 | 1 | $\bigcirc$ | $\times$ | 76 | 0 | 00 | $\bigcirc$ |  |
| H37 | 425h | h | RS-485 Setup (Selection of stop bit) | 1 | $\begin{aligned} & 0 \text { to } 1 \\ & \text { 0: 2bit } \\ & \text { 1: 1bit } \end{aligned}$ | 0 | 1 | $\bigcirc$ | $\times$ | 77 | 0 | 00 | $\bigcirc$ |  |
| H38 | 426h | h | RS-485 Setup <br> (Communication interrupt time) | 1 | $\begin{array}{\|l\|} \hline 0.0 \text { to } 60.0 \mathrm{~s} \\ 0.0: \text { Interrupt detection disable } \\ 0.1 \text { to } 60.0: \text { Interrupt detection enable } \\ \hline \end{array}$ | $\bigcirc$ | 60.0 | $\bigcirc$ | $\bigcirc$ | 2 | 0 | 00 | $\bigcirc$ |  |
| H39 | 427h | h | RS-485 Setup (Response interval time) | 1 | 0.00 to 1.00 s | $\bigcirc$ | 0.01 | $\bigcirc$ | $\bigcirc$ | 3 | 0 | 00 | $\bigcirc$ |  |
| H40 | 428h | h | RS-485 Setup (Protocol selection) | 1 | 0 to 2 <br> 0 : Fuji general purpose inverter protocol <br> 1: SX protocol (Loader protocol) <br> 2: Modbus RTU protocol <br> When using FRENIC-VG loader, specify "1: SX protocol". | $\times$ | 1 | $\bigcirc$ | $\times$ | 78 | 0 | 0 | $\bigcirc$ |  |
| H41 | 429h | D1h | Torque command selection | 4 | 0 to 5 0: Internal ASR enable 1: Ai (T-REF) enable 2: DIA card enable 3: DIB card enable 4: Link enable 5: PID enable | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 64 | 0 | $0 \times$ | $\bigcirc$ |  |
| H42 | 42Ah | D2h | Torque current command selection | 1 | 0 to 4 <br> 0: Internal ASR enable <br> 1: Ai (IT-REF) enable <br> 2: DIA card enable <br> 3: DIB card enable <br> 4: Link enable | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 65 | 0 | $0 \times$ | $\bigcirc$ |  |
| H43 | 42Bh | D3h | Magnetic flux command selection | 1 | 0 to 3 <br> 0: Internal calculation enable <br> 1: Ai (MF-REF) enable <br> 2: Function code H 44 enable <br> 3: Link enable | $\times$ | 0 | $\bigcirc$ | 0 | 66 | 0 | $\times \times$ | $\times$ |  |
| H44 | 42Ch | D4h | Magnetic-flux command value | 1 | 10 to 100\% | $\times$ | 100 | 0 | $\bigcirc$ | 16 | 0 | $\times \times$ | $\times$ |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  | 0 <br>  <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 |  |  | Control method: Enable/ Disable |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | = |  | $\stackrel{\text { P }}{ }$ | L | S |  |
| H46 | 42Eh | D7h | Observer (Mode selection) | 7 | 0 to 2 0: Observer not operational 1: Load disturbance observer 2: Oscillation suppression observer | $\times$ | 0 | 0 | 0 | 79 | 0 | - $\times$ | 0 |  |
| H47 | 42Fh | D8h | Observer (M1 Compensation gain) | 1 | 0.00 to 1.00 times | 0 | 0.00 | 0 | 0 | 3 | $\bigcirc$ | $0 \times$ | 0 |  |
| H48 | 430h | h | Observer (M2 Compensation gain) | 1 | 0.00 to 1.00 times | $\bigcirc$ | 0.00 | O | O | 3 | $\bigcirc$ | 0 | 0 |  |
| H49 | 431h | D9h | Observer (M1 I-time) | 1 | 0.005 to 1.000 s | $\bigcirc$ | 0.100 | O | $\bigcirc$ | 4 | $\bigcirc$ | 0 | O |  |
| H50 | 432h | h | Observer (M2 I-time) | 1 | 0.005 to 1.000 s | $\bigcirc$ | 0.100 | 0 | $\bigcirc$ | 4 | $\bigcirc$ | 0 | 0 |  |
| H51 | 433h | DAh | Observer (M1 load inertia) | 1 | $0.001 \text { to } 50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> The magnification is switchable by H 228 . | $\bigcirc$ | Depe nds on capaci ty | 0 | $\times$ | 4 | O | 0 | 0 |  |
| H52 | 434h | h | Observer (M2 load inertia) | 1 | 0.001 to $50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ The magnification is switchable by H 228 . | $\bigcirc$ | 0.001 | 0 | $\times$ | 4 | 0 | - $\times$ | 0 |  |
| H53 | 435h | D5h | Line speed feedback selection | 0 | 0 to 3 <br> 0: Line speed disable (internal PG enable) <br> However, higher value is selected between Ai input and PG (LD) on UPAC. <br> 1: Analog line speed detect (AI-LINE) <br> 2: Digital line speed detect (PG (LD)) <br> 3: High selector (selects the higher level between motor speed and line speed) | $\bigcirc$ | 0 | 0 | O | 67 | 0 | 0 | 0 |  |
| H55 | 437h | h | Zero speed control (Gain) | 2 | 0 to 100 times <br> For details, refer to terminal X function LOCK assigned by any of E01 to E13. | 0 | 5 | 0 | 0 | 0 | 0 | $\times \times$ | 0 |  |
| H56 | 438h | h | Zero speed control (Completion range) | 1 | 0 to 100 pulses | 0 | 100 | 0 | 0 | 0 | $\bigcirc$ | $\times \times$ | 0 |  |
| H57 | 439h | h | Overvoltage suppression | 2 | $\begin{array}{\|l\|} \hline 0 \text { to } 1 \\ \text { 0: No operation } \\ \text { 1: Operation } \\ \hline \end{array}$ | $\times$ | 0 | 0 | 0 | 68 | $\bigcirc$ | 0 | 0 |  |
| H58 | 43Ah | h | Overcurrent suppression | 1 | $\begin{aligned} & 0 \text { to } 1 \\ & \text { 0: No operation } \\ & \text { 1: Operation } \end{aligned}$ | $\times$ | 0 | 0 | 0 | 68 | 0 | 0 | 0 |  |
| H60 | 43Ch | h | Load weighting control (Definition 1 of load weighting control function) | 7 | 0 to 3 <br> 0: Disable <br> 1: Method 1 <br> 2: Method 2 <br> 3: Method 3 | $\times$ | 0 | 0 | 0 | 80 | 0 | $\times \times$ | 0 |  |
| H61 | 43Dh | h | Load weighting control (Definition 2 of load weighting control function) | 1 | 0 to 1 <br> 0: Hoisting with motor rotating normally <br> 1: Lowering with motor rotating normally | $\times$ | 0 | 0 | 0 | 81 | 0 | $\times \times$ | 0 |  |
| H62 | 43Eh | h | Load weighting control (Hoisting speed) | 1 | 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ | $\times$ | 0.0 | 0 | 0 | 2 | 0 | $\times \times$ | 0 |  |
| H63 | 43Fh | h | Load weighting control (Counter weight mass) | 1 | 0.00 to 600.00 t | $\times$ | 0.00 | 0 | 0 | 3 | 0 | $\times \times$ | 0 |  |
| H64 | 440h | h | Load weighting control (Safety factor) | 1 | 0.50 to 1.20 | $\times$ | 1.00 | 0 | 0 | 3 | 0 | $\times$ | 0 |  |
| H65 | 441h | h | Load weighting control (Machine efficiency) | 1 | 0.500 to 1.000 | $\times$ | 0.500 | O | 0 | 4 | $0 \times$ | $\times \times$ | 0 |  |
| H66 | 442h | h | Load weighting control (Rated load) | 1 | 0.00 to 600.00 t | $\times$ | 0.00 | 0 | 0 | 3 | 0 | $\times \times$ | 0 |  |
| H68 | 444h | h | Alarm data deletion | 0 | 0 to 1 <br> After writing the data, this function's data code automatically returns to 0 . <br> Setting H 68 to " 1 " deletes all of the alarm history, alarm causes and alarm information held in the inverter memory. | $\bigcirc$ | 0 | ${ }^{\times}$ | $\times$ | 11 | $\bigcirc$ | 0 | 0 |  |
| H70 | 446h | h | For manufacturer 1 | 2 | 0 to 9999 Reserved. (Do not access this function code.) | $\times$ | 0 | 0 | $\times$ | 0 | 0 | - $\times$ | 0 |  |
| H71 | 447h | h | For manufacturer 2 | 1 | 0 to 10 Reserved. (Do not access this function code.) | $\times$ | 0 | $\times$ | $\times$ | 62 | 0 | 0 | 0 |  |
| H74 | 44Ah | h | PG detection circuit self-diagnosis selection | 0 | 0 to 1 <br> 0: Disable <br> 1: Enable <br> This function activates the inverter's function for self-diagnosis of the speed detection circuit by PG (Pulse generator) signal input (PA, PB). | $\times$ | 0 | 0 | - | 225 | $\bigcirc$ | $\times \times$ | $\times$ |  |
| H75 | 44Bh | h | Phase sequence configuration of main circuit output wires | 0 | 0 to 1 <br> 0: Normal phase U-V-W <br> 1: Reverse phase U-W-V <br> Switches the phase sequence of the inverter main circuit. | $\times$ | 0 | 0 | 0 | 197 | 0 | 0 | $\times$ |  |
| H76 | 44Ch | h | Main power down detection <br> * Invalid for use in stack type | 0 | 0 to 1 <br> 0: No operation <br> 1: Operation <br> Set this function to "Operation" to enable the AC power monitoring function. <br> Set this function to "No operation" when DC power is supplied, e.g., connecting with a power regenerative converter but the inverter AC input power is not supplied. | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| H77 | 44Dh | h | Cooling fan ON-OFF control continuation timer | 0 | 0 to 600 s <br> Specifies the condition of the cooling fan ON/OFF control by H06. | 0 | 600 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| H78 | 44Eh | h | Initialization of startup counter/total run time | 6 | 0 to 6 <br> 0 : No operation <br> 1: M1 Number of startups <br> 2: M2 Number of startups <br> 3: M3 Number of startups <br> 4: M1 Cumulative run time <br> 5: M2 Cumulative run time <br> 6: M3 Cumulative run time <br> Initializes the number of startups and cumulative run time for each of M1 to M3. | $\times$ | 0 | $\times$ | $\times$ | 0 | 0 | 0 | 0 |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | P\| | L | V $\begin{aligned} & \text { S } \\ & M\end{aligned}$ |  |
| H79 | 44Fh | h | Cooling fan operation cumulative time initialization setting | 1 | 0 to 65535 (in units of 10 hours) <br> Initializes the cumulative run time when the cooling fan is replaced. <br> Usually, write "0" after replacement. | $\times$ | 0 | $\times$ | $\times$ | 0 | O | 0 O | O |  |
| H80 | 450h | h | Capacity of main circuit capacitor initial value measurement <br> * Invalid for use in stack type | 1 | 0 to 32767 <br> When the capacitance measurement is user mode (H104), setting this function code to " 0 " and shutting down the inverter power starts measuring the initial value of the capacitance and writes the measurement result to this function code. | $\times$ | 0 | $\times$ | 0 | 0 | 0 | 0 | 0 |  |
| H81 | 451h | h | Initialization of cumulative life of main circuit capacitor | 1 | 0 to 65535 (in units of 10 hours) Initializes the elapsed time of the main circuit capacitor. | $\times$ | 0 | $\times$ | O | 0 | $\bigcirc$ | 0 | 0 |  |
| H82 | 452h | h | Number of startups for maintenance | 1 | 0 to 65535 <br> Specifies the number of startups for performing maintenance of the machinery. | $\bigcirc$ | 0 | $\times$ | O | 0 | $\bigcirc$ | 0 | O |  |
| H83 | 453h | h | Maintenance Interval | 1 | 0 to 65535 (in units of 10 hours) Specifies the maintenance interval for performing maintenance of the machinery. | 0 | 8760 | $\times$ | 0 | 0 | 0 | 0 | - |  |
| $\begin{gathered} \mathrm{H} 84 \\ { }^{2} 1 \end{gathered}$ | 454h | h | Speed calculation period when extremely low speed (for maker) | 0 | $0.0 \text { to } 200.0 \mathrm{~ms}$ <br> The sampling period setting of the encoder pulse in extremely low speed region. <br> This is a function code for maker. Do not access this function code. | N | 0.0 | Y | Y | 2 | Y | N N | Y |  |
| H85 | 455h | h | Calendar clock (Year/month) | 4 | 0000 to FFFF <br> Upper 2 digits: Year, Lower 2 digits: Month | 0 | 0001 | $\times$ | 0 | 143 | O | 00 | 0 |  |
| H86 | 456h | h | Calendar clock (Day/hour) | 1 | 0000 to FFFF <br> Upper 2 digits: Day, Lower 2 digits: Hour | 0 | 0100 | $\times$ | O | 144 | 0 | 0 | 0 |  |
| H87 | 457h | h | Calendar clock (Minute/second) | 1 | 0000 to FFFF Upper 2 digits: Minute, Lower 2 digits: Second | $\bigcirc$ | 0000 | $\times$ | O | 145 | $\bigcirc$ | 0 | 0 |  |
| H88 | 458h | h | Calendar clock (Setting up clock) | 1 | 0 to 1 <br> 0: No operation <br> 1: Setting up clock <br> Setting H88 to "1" sets up the calendar clock in accordance with the settings of H 85 to H 87 . <br> After that, the H 88 data automatically reverts to " $0 . "$ | $\bigcirc$ | 0 | $\times$ | $\times$ | 11 | O | 0 | - |  |
| H90 | 45Ah | h | Overspeed alarm detection level | 0 | 100 to $160 \%$ | $\bigcirc$ | 120 | - | $\bigcirc$ | 0 | O | O | O |  |
| $\underset{*_{1}}{\mathrm{H} 96}$ | 460h | h | ASR operation selecting | 0 | ```o to 3 0: P priority (VG1) 1: I priority (compatible with VM5 ) 2: P priority (compatible with VM5 ) 3: For maker (Do not select this)``` | N | 0 | Y | Y | 201 | Y | N | , Y |  |
| H101 | 1F01h | h | PID command filter time constant | 0 | 0 to 5000 ms <br> Specifies the time constant of the PID command filter (after switched by H21). | 0 | 0 | O | O | 0 | 0 | 00 | O |  |
| H103 | 1F03h | h | Protective/Maintenance function selection 1 <br> * Invalid for use in stack ty | 9 | 0000 to 1111 <br> Selects the protective functions individually. <br> [0: Disable, 1: Enable] <br>  <br> Hundreds digit: Ground fault alarm (I, <br> Tenths digit: Output phase loss alarm ( <br>  | 0 | 0101 | $\bigcirc$ | 0 | 9 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| H104 | 1F04h | h | Protective/Maintenance function selection 2 <br> * Invalid for use in stack ty |  | 0000 to 1111 <br> Selects the protective/other functions individually. <br> [0: Disable, 1: Enable] <br> Thousands digit: PG wire break alarm ( <br> Hundreds digit: Lower the carrier frequency <br> Tenths digit: Judge the life of main circuit capacitor <br> Units digit: Select capacitance measurement of main circuit <br> ( 0 : Referenced on factory default value, 1 : <br> Referenced on user measurement) | 0 | 1110 | - | 0 | 9 | 0 | 00 | $\bigcirc$ |  |
| H105 | 1F05h |  | Protective/Maintenance Function Selection 3 | 1 | 0000 to 1111 <br> Selects the protective/maintenance functions individually. <br> (0: Disable, 1: Enable) <br> Thousands digit: -- <br> Hundreds digit: Speed disaccord alarm <br> Tenths digit: Speed disaccord alarm E-Goperation 2 <br> Units digit: Save the integrated value of motor electronic thermal | $\begin{aligned} & \circ \\ & { }^{* 1} \\ & { }^{*} 1 \end{aligned}$ | 0000 | $\bigcirc$ | - | 9 | O | 0 | $\bigcirc$ |  |
| H106 | 1F06h | h | Light alarm object definition 1 | 1 | ```0000 to 1111 [0: Heavy alarm ( Digit of 1000: OH4 "motor overheat" Digit of 100: OL1-OL3 "motor overload" (common for M1-M3) Digit of 10: nrb "NTC thermistor disconnected" Digit of 1: OH2 "external failure"``` | $\bigcirc$ | 0000 | $\bigcirc$ | - | 9 | $\bigcirc$ | 0 O | $\bigcirc$ |  |
| H107 | 1F07h | h | Light alarm object definition 2 | 1 | 0000 to 1111  <br> [0: Heavy alarm (I,-,-), 1: Light alarm ( $\left.\left.L^{2}-R_{1}^{\prime \prime}\right)\right]$  <br> Digit of 1000: Er5 "RS-485 failure" <br> Digit of 100: Er4 "network failure" <br> Digit of 10: Reserved <br> Digit of 1: ArF "toggle failure error" | 0 | 0000 | O | O | 9 | O | 00 | $\bigcirc$ |  |
| H108 | 1F08h | h | Light alarm object definition 3 | 1 | ```0000 to 1111```  ```Digit of 1000: Err "mock alarm" Digit of 100: dFA "DC fan lock" Digit of 10: Er9 "speed disagreement" LOC "Start delay" Digit of 1: ArE "E-SX bus tact synchronization error"``` | $\bigcirc$ | 0000 | - | - | 9 | - |  | $\bigcirc$ |  |

[^14]| $\begin{aligned} & \text { ๗ } \\ & \text { D } \\ & 0 \\ & 0 \\ & \text { 을 } \\ & \text { C } \\ & \text { L } \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\left\lvert\, \begin{aligned} & 0 \\ & .0 \\ & \vdots \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \tilde{0} \\ & 0 \\ & 0 \end{aligned}\right.$ |  | Control method: Enablel Disable |  |  | $\xrightarrow[\text { ¢ }]{\substack{\text { ¢ } \\ \text { ¢ } \\ \text { ¢ }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  | $\stackrel{P}{P}$ | V | S |  |
| H109 | 1F09h | h | Light alarm object definition 4 | 1 |  | $\bigcirc$ | 0000 | 0 | 9 | 0 | O | 0 |  |
| H110 | 1F0Ah | h | Light alarm object definition 5 | 1 |  | $\bigcirc$ | 0000 | 0 | 9 | 0 | - | O |  |
| H111 | 1FOBh | h | Light alarm object definition 6 | 1 | 0 to 1 <br> 0: Disable ( $L-F_{1}^{\prime \prime}$ no indication) <br> 1: Enable ( $L-i_{L}^{\prime \prime}$ indicated) <br> Specifies whether or not to display $i$ - 侯 monitor when a light alarm occurs. | $\bigcirc$ | 1 | $\bigcirc$ | 68 | - | - | 0 |  |
| H112 | 1F0Ch | h | M1 Magnetic saturation extension coefficient 6 | 7 | 0.0 to $100.0 \%$ Compensation factor for exciting current when the magnetic flux command is $43.75 \%$. | 0 | 43.8 | $\bigcirc$ | 2 | 0 | $\times$ | $\times$ |  |
| H113 | 1FODh | h | M1 Magnetic saturation extension coefficient 7 | 1 | 0.0 to $100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $37.5 \%$. | 0 | 37.5 | $\bigcirc$ | 2 | 0 | $\times$ | $\times$ |  |
| H114 | 1F0Eh | h | M1 Magnetic saturation extension coefficient 8 | 1 | 0.0 to $100.0 \%$ Compensation factor for exciting current when the magnetic flux command is $31.25 \%$. | 0 | 31.3 | $\bigcirc$ | 2 | 0 | $\times$ | $\times$ |  |
| H115 | 1F0Fh | h | M1 Magnetic saturation extension coefficient 9 | 1 | 0.0 to $100.0 \%$ Compensation factor for exciting current when the magnetic flux command is $25 \%$. | 0 | 25.0 | $\bigcirc$ | 2 | 0 | $\times$ | $\times$ |  |
| H116 | 1F10h | h | M1 Magnetic saturation extension coefficient 10 | 1 | 0.0 to $100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $18.75 \%$. | 0 | 18.8 | $\bigcirc$ | 2 | $0 \times$ | $\times$ | $\times$ |  |
| H117 | 1F11h | h | M1 Magnetic saturation extension coefficient 11 | 1 | 0.0 to $100.0 \%$ Compensation factor for exciting current when the magnetic flux command is $12.5 \%$. | 0 | 12.5 | $\bigcirc$ | 2 | $0 \times$ | $\times$ | $\times$ |  |
| H118 | 1F12h | h | M1 Magnetic saturation extension coefficient 12 | 1 | $0.0 \text { to } 100.0 \%$ <br> Compensation factor for exciting current when the magnetic flux command is $6.25 \%$. | 0 | 6.3 | $\bigcirc$ | 2 | $\bigcirc$ | $\times$ | $\times$ |  |
| H125 | 1F19h | h | Observer (M3 compensation gain) | 3 | 0.00 to 1.00 times | $\bigcirc$ | 0.00 | O | 3 | 0 | $\times$ | O |  |
| H126 | 1F1Ah | h | Observer (M3 1-time) | 1 | 0.005 to 1.000 s | $\bigcirc$ | 0.100 | - | 4 | 0 | $\times$ | $\bigcirc$ |  |
| H127 | 1F1Bh | h | Observer (M3 load inertia) | 1 | $0.001 \text { to } 50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> The magnification is switchable by H 228 . | $\bigcirc$ | 0.001 | $\bigcirc$ | 4 | - | $\times$ | $\bigcirc$ |  |
| H134 | 1F22h | h | Speed drop detection delay timer | 5 | $\begin{aligned} & \text { 0.000: No operation } \\ & 0.001 \text { to } 10.000 \mathrm{~s} \end{aligned}$ | $\times$ | 0.000 | $\bigcirc$ | 4 | O | $\times$ | O |  |
| H135 | 1F23h | h | Speed command detection level (FWD) | 1 | 0.0: No operation 0.1 to $150.0 \mathrm{r} / \mathrm{min}$ | $\times$ | 0.0 | $\bigcirc$ | 2 | O | $\times$ | $\bigcirc$ |  |
| H136 | 1F24h | h | Speed command detection level (REV) | 1 | 0.0: No operation 0.1 to $150.0 \mathrm{r} / \mathrm{min}$ | $\times$ | 0.0 | $\bigcirc$ | 2 | O | $\times$ | $\bigcirc$ |  |
| H137 | 1F25h | h | Speed drop detection level | 1 | 0.0: No operation 0.1 to $150.0 \mathrm{r} / \mathrm{min}$ | $\times$ | 0.0 | $\bigcirc$ | 2 | O | $\times$ | $\bigcirc$ |  |
| H138 | 1F26h | h | Speed drop detection delay timer | 1 | 0.000 to 10.000 s | $\times$ | 0.000 | $\bigcirc$ | 4 | 0 | $\times$ | 0 |  |
| H140 | 1F28h | h | Start delay detection (Detection level) | 2 | 0.0 to 300.0 \% | $\bigcirc$ | 150.0 | $\bigcirc$ | 2 | 0 | $\times$ | O |  |
| H141 | 1F29h | h | Start delay detection (Detection timer) | 1 | 0.000 to 10.000 s | 0 | 1.000 | $\bigcirc$ | 4 | 0 | $\times$ | 0 |  |
| H142 | 1F2Ah | h | Mock alarm | 0 | 0 to 1 <br> 0: No operation <br> 1. A mock alarm occurs <br> When H 108 does not define a mock alarm as a light alarm, a heavy alarm ( $\left(\Sigma_{1},--\right)$ occurs; when it defines a mock alarm as a light alarm, a light alarm ( $\left.\mathcal{L}^{\prime}-h_{L}^{\prime \prime}\right)$ occurs. <br> Depressing the $\square$ ( 500 ) + (20II) keys on the keypad for 3 seconds will also cause the alarm. | $\bigcirc$ | 0 | $\times$ | 11 | 0 | - | O |  |
| H144 | 1F2Ch | h | Toggle data error timer | 0 | $\begin{aligned} & 0.01 \text { to } 20.00 \mathrm{~s} \\ & \text { Specifies the toggle signal error detection time. } \end{aligned}$ | $\bigcirc$ | 0.10 | 0 | 3 | 0 | O | 0 |  |
| H145 | 1F2Dh | h | Reverse rotation prevention for sensor-less control (Selection of lower limit frequency operation) | 3 | ```0 to 3 Disable Enable for FWD polarity operation Enable for REV polarity operation Enable for both FWD/REV polarities``` | $\times$ | 0 | - | 202 | O | $\times$ | $\times$ |  |
| H146 | 1F2Eh | h | Reverse rotation prevention for sensor-less control (Lower limit frequency (FWD)) | 1 | 0.000 to 10.000 Hz | $\times$ | 0.000 | $\bigcirc$ | 4 | $\times$ | ${ }^{x}$ | $\times$ |  |
| H147 | 1F2Fh | h | Reverse rotation prevention for sensor-less control (Lower limit frequency (REV)) | 1 | 0.000 to 10.000 Hz | $\times$ | 0.000 | $\bigcirc$ | 4 | $\times$ | ${ }^{x}$ | $\times$ |  |
| H148 | 1F30h | h | First order frequency filter | 0 | 0 to 100 ms Increase this setting if the speed fluctuation is large under sensor-less vector control. | $\times$ | 0 | $\bigcirc$ | 0 | $\times$ | $\times$ | $\times$ |  |
| H149 | 1F31h | h | Machine runaway detection speed setting | 0 | 0.0 to $20.0 \%$ 0.0 : Disable 0.1 to $20.0 \%$ Assuming the maximum speed as $100 \%$. | $\times$ | 0.0 | $\bigcirc$ | 2 | 0 | $\times$ | 0 |  |
| H160 | 1F3Ch | h | M1 Initial magnetic polarity position detection method | 3 | 0 to 3 <br> 0: Pull-in by current for IPMSM (Interior Permanent Magnet Synchronous Motor) 1-3: - | $\times$ | 0 | $\bigcirc$ | 0 | $\times$ | $\times$ | $\bigcirc$ |  |
| H161 | 1F3Dh | h | M1 Draw current command | 1 | 10 to $200 \%$ $100 \% /$ Motor rated current | $\times$ | 80 | 0 | 0 | $\times$ | $\times$ | 0 |  |
| H162 | 1F3Eh | h | M1 Pull-in frequency | 1 | 0.1 to 10.0 Hz | $\times$ | 1.0 | $0 \times$ | 2 | $\times$ |  | $\bigcirc$ |  |


| $\begin{aligned} & \text { ๗ } \\ & \text { D } \\ & 0 \\ & 0 \\ & \text { 을 } \\ & \text { ᄃ } \\ & \hline \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\left\|\begin{array}{l} 0 \\ .0 \\ \vdots \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array}\right\|$ |  | 등.0$0 . \overline{0}$4000 | Control method: Enable/ Disable |  |  | $\xrightarrow[\text { ® }]{\stackrel{\text { ¢ }}{0}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | P  <br> P L <br> E  <br> E  <br> S  | L | S |  |
| H170 | 1F46h | h | M2 Initial magnetic polarity position detection method | 3 | 0 to 3 <br> 0: Pull-in by current for IPMSM (Interior Permanent Magnet Synchronous Motor) <br> 1-3: - | $\times$ | 0 | $\bigcirc$ | $\times$ | 0 | $\times \times$ | $\times$ | $\bigcirc$ |  |
| H171 | 1F47h | h | M2 Draw current command | 1 | $\begin{array}{\|l\|} \hline 10 \text { to } 200 \text { \% } \\ 100 \% / \text { Motor rated current } \\ \hline \end{array}$ | $\times$ | 80 | $\bigcirc$ | $\times$ | 0 | $\times \times$ | $\times$ | $\bigcirc$ |  |
| H172 | 1F48h | h | M2 Pull-in frequency | 1 | 0.1 to 10.0 Hz | $\times$ | 1.0 | $\bigcirc$ | $\times$ | 2 | $\times$ | $\times$ | $\bigcirc$ |  |
| H180 | 1F50h | h | M3 Initial magnetic polarity position detection method | 3 | 0 to 3 <br> 0: Pull-in by current for IPMSM (Interior Permanent Magnet Synchronous Motor) <br> 1-3: - | $\times$ | 0 | $\bigcirc$ | $\times$ | 0 | $\times \times$ | $\times \times$ | $\bigcirc$ |  |
| H181 | 1F51h | h | M3 Draw current command | 1 | $\begin{array}{\|l\|} \hline 10 \text { to } 200 \% \\ 100 \% / \text { Motor rated current } \\ \hline \end{array}$ | $\times$ | 80 | $\bigcirc$ | $\times$ | 0 | $\times \times$ | $\times \times$ | $\bigcirc$ |  |
| H182 | 1F52h | h | M3 Pull-in frequency | 1 | 0.1 to 10.0 Hz | $\times$ | 1.0 | $\bigcirc$ | $\times$ | 2 | $\times$ | $\times \times$ | $\bigcirc$ |  |
| H201 | 2001h | h | Load weighting control <br> (Switching of load weighting control <br> parameters) <br> (To be supported soon) | 13 | $\begin{aligned} & 0 \text { to } 1 \\ & \text { 0: H51, H64, H65 enable, H202-H213 disable } \\ & \text { 1: H51, H64, H65 disable, H202-H213 enable } \end{aligned}$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\times{ }^{\times}$ | 0 |  |
| H202 | 2002h | h | Load weighting control <br> (Load inertia (hoisting 1)) <br> (To be supported soon) | 1 | 0.001 to $50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> Applies to winding-up operation when AN-P2/1 is OFF. <br> The magnification is switchable by H 228 . | $\times$ | 0.001 | O | $\bigcirc$ | 4 | $\bigcirc$ | $\times{ }^{\times}$ | 0 |  |
| H203 | 2003h | h | Load weighting control <br> (Safety factor (hoisting 1)) <br> (To be supported soon) | 1 | $\begin{aligned} & 0.50 \text { to } 1.20 \\ & \text { Applies to winding-up operation when AN-P2/1 is OFF. } \end{aligned}$ | $\times$ | 1.00 | O | $\bigcirc$ | 3 | $0 \times$ | $\times \times$ | 0 |  |
| H204 | 2004h | h | Load weighting control (Mechanical efficiency (hoisting 1)) (To be supported soon) | 1 | $\begin{aligned} & 0.500 \text { to } 1.000 \\ & \text { Applies to winding-up operation when AN-P2/1 is OFF. } \end{aligned}$ | $\times$ | 0.500 | O | O | 4 | $\bigcirc$ | $\times \times$ | 0 |  |
| H205 | 2005h | h | Load weighting control (Load inertia (hoisting 2)) (To be supported soon) | 1 | $0.001 \text { to } 50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> Applies to winding-up operation when AN-P2/1 is ON. <br> The magnification is switchable by H 228 . | $\times$ | 0.001 | O | 0 | 4 | $\bigcirc$ | $\times \times$ | 0 |  |
| H206 | 2006h | h | Load weighting control (Safety factor (hoisting 2)) (To be supported soon) | 1 | $\begin{aligned} & 0.50 \text { to } 1.20 \\ & \text { Applies to winding-up operation when AN-P2/1 is ON. } \end{aligned}$ | $\times$ | 1.00 | $\bigcirc$ | O | 3 | 0 | $\times \times$ | 0 |  |
| H207 | 2007h | h | Load weighting control <br> (Mechanical efficiency (hoisting 2)) <br> (To be supported soon) | 1 | $\begin{aligned} & 0.500 \text { to } 1.000 \\ & \text { Applies to winding-up operation when AN-P2/1 is ON. } \end{aligned}$ | $\times$ | 0.500 | $\bigcirc$ | $\bigcirc$ | 4 | 0 | ${ }^{\times} \times$ | 0 |  |
| H208 | 2008h | h | Load weighting control (Load inertia (lowering 1)) (To be supported soon) | 1 | $0.001 \text { to } 50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> Applies to winding-down operation when AN-P2/1 is OFF. <br> The magnification is switchable by H 228 . | $\times$ | 0.001 | $\bigcirc$ | $\bigcirc$ | 4 | 0 | $\times{ }^{\times}$ | 0 |  |
| H209 | 2009h | h | Load weighting control (Safety factor (lowering 1)) <br> (To be supported soon) | 1 | 0.50 to 1.20 Applies to winding-down operation when AN-P2/1 is OFF. | $\times$ | 1.00 | $\bigcirc$ | $\bigcirc$ | 3 | 0 | $\times \times$ | 0 |  |
| H210 | 200Ah | h | Load weighting control (Mechanical efficiency (lowering 1)) (To be supported soon) | 1 | $\begin{aligned} & 0.500 \text { to } 1.000 \\ & \text { Applies to winding-down operation when AN-P2/1 is OFF. } \end{aligned}$ | $\times$ | 0.500 | O | $\bigcirc$ | 4 | $\bigcirc$ | $\times \times$ | 0 |  |
| H211 | 200Bh | h | Load weighting control (Load inertia (lowering 2)) (To be supported soon) | 1 | 0.001 to $50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ <br> Applies to winding-down operation when AN-P2/1 is ON. <br> The magnification is switchable by H 228 . | $\times$ | 0.001 | O | O | 4 | $\bigcirc$ | $\times \times$ | O |  |
| H212 | 200Ch | h | Load weighting control (Safety factor (lowering 2)) (To be supported soon) | 1 | $\begin{aligned} & 0.50 \text { to } 1.20 \\ & \text { Applies to winding-down operation when AN-P2/1 is ON. } \end{aligned}$ | $\times$ | 1.00 | $\bigcirc$ | O | 3 | $\bigcirc$ | $\times \times$ | 0 |  |
| H213 | 200Dh | h | Load weighting control (Mechanical efficiency (lowering 2)) (To be supported soon) | 1 | $\begin{aligned} & 0.500 \text { to } 1.000 \\ & \text { Applies to winding-down operation when AN-P2/1 is ON. } \end{aligned}$ | $\times$ | 0.500 | $\bigcirc$ | 0 | 4 | 0 | $\times \times$ | 0 |  |
| H214 | 200Eh | h | Load weighting control <br> (Multi limit speed pattern function <br> selection) <br> (To be supported soon) | 14 | $\begin{aligned} & \text { 0 to } 1 \\ & \text { 0: H60 definition enable, } \mathrm{H} 215-\mathrm{H} 224 \text { disable } \\ & \text { 1: } \mathrm{H} 60 \text { definition disable, } \mathrm{H} 215-\mathrm{H} 224 \text { enable } \end{aligned}$ | $\times$ | 0 | 0 | O | 0 | $\bigcirc$ | $\times \times$ | 0 |  |
| H215 | 200Fh | h | Load weighting control (Multi limit speed pattern (maximum speed)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the maximum speed. } \end{aligned}$ | $\times$ | 50.0 | $\bigcirc$ | 0 | 2 | 0 | $\times \times$ | 0 |  |
| H216 | 2010h | h | Load weighting control (Multi limit speed pattern (rated speed)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed. } \end{aligned}$ | $\times$ | 100.0 | O | O | 2 | $\bigcirc$ |  | 0 |  |
| H217 | 2011h | h | Load weighting control (Multi limit speed pattern (rated speed $x$ 1.1)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*1.1. } \end{aligned}$ | $\times$ | 90.9 | 0 | 0 | 2 | 0 | $\times \times$ | 0 |  |
| H218 | 2012h | h | Load weighting control (Multi limit speed pattern (rated speed x 1.2)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*1.2. } \end{aligned}$ | $\times$ | 83.3 | - | 0 | 2 | 0 | $\times{ }^{\times}$ | 0 |  |
| H219 | 2013h | h | Load weighting control <br> (Multi limit speed pattern <br> (rated speed x 1.4)) <br> (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*1.4. } \end{aligned}$ | $\times$ | 71.4 | $\bigcirc$ | 0 | 2 | $\bigcirc$ | $\times \times$ | 0 |  |
| H220 | 2014h | h | Load weighting control <br> (Multi limit speed pattern <br> (rated speed x 1.6)) <br> (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*1.6. } \end{aligned}$ | $\times$ | 62.5 | $\bigcirc$ | 0 | 2 | $\bigcirc$ | $\times \times$ | 0 |  |
| H221 | 2015h | h | Load weighting control (Multi limit speed pattern (rated speed $x$ 1.8)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*1.8. } \end{aligned}$ | $\times$ | 55.5 | $\bigcirc$ | 0 | 2 | $\bigcirc$ | ${ }^{\times} \times$ | 0 |  |
| H222 | 2016h | h | Load weighting control <br> (Multi limit speed pattern <br> (rated speed $\times 2.0$ )) <br> (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*2.0. } \end{aligned}$ | $\times$ | 50.0 | $\bigcirc$ | 0 | 2 | $\bigcirc$ |  | 0 |  |


| 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}$ | S |  |
| H223 | 2017h | h | Load weighting control (Multi limit speed pattern (rated speed x 2.5)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*2.5. } \end{aligned}$ | $\times$ | 40.0 | 0 | 0 | 2 | 0 | $\times$ | $\times$ | O |  |
| H224 | 2018h | h | Load weighting control (Multi limit speed pattern (rated speed x 3.0)) (To be supported soon) | 1 | $\begin{aligned} & 0.1 \text { to } 100.0 \% \\ & \text { Specifies the torque level at the rated speed*3.0. } \end{aligned}$ | $\times$ | 33.3 | 0 | 0 | 2 | 0 | $\times$ | $\times$ | 0 |  |
| H225 | 2019h | h | Load weighting control <br> (Speed limit determination section <br> (start speed)) <br> (To be supported soon) | 1 | 0.1 to $100.0 \%$ <br> Specifies the starting speed of the determination section. <br> The rated speed is assumed as $100 \%$. | $\times$ | 75.0 | 0 | 0 | 2 | 0 | $\times$ | $\times$ | 0 |  |
| H226 | 201Ah | h | Load weighting control <br> (Speed limit determination section <br> (ending speed)) <br> (To be supported soon) | 1 | 0.1 to $100.0 \%$ <br> Specifies the end speed of the determination section. The rated speed is assumed as $100 \%$. | $\times$ | 93.7 | 0 | 0 | 2 | 0 | $\times$ | $\times$ | 0 |  |
| H227 | 201Bh | h | Load weighting control (Functional definition 3) (To be supported soon) | 1 | 0 to 2 <br> 0 : Calculation of hoisting and lowering speed limit individually <br> 1: Drive lowering using speed limit of previous hoisting Enable the winding-down speed limit calculation under specific conditions <br> 2: Drive lowering using speed limit of previous hoisting Limit the winding-down speed with the rated speed under specific conditions | $\times$ | 0 | 0 | 0 | 0 | 0 | $\times$ | $\times$ | 0 |  |
| H228 | 201Ch | h | Load inertia magnification setting | 0 | 0 to 2 <br> 0: Multiplied by 1 ( 0.001 to $50.000 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ ) <br> 1: Multiplied by $10\left(0.01\right.$ to $\left.500.00 \mathrm{~kg} \cdot \mathrm{~m}^{2}\right)$ <br> 2: Multiplied by 100 ( 0.1 to $5000.0 \mathrm{~kg} \cdot \mathrm{~m}^{2}$ ) <br> H51, H52, H202, H205, H208, H211 <br> Switch the specified scaling factor for the "load inertia". | $\times$ | 630 kW or less 0 710 kW, 800 kW 1 1000 kW 2 | 0 | 0 | 193 | 0 | $\times$ | $\times$ | 0 |  |
| H322 | 2116h | h | Notch filter 1 (Resonance frequency) | 6 | 10 to 2000 Hz | $\bigcirc$ | 1000 | 0 | 0 | 0 | 0 | 0 | $\times$ | 0 |  |
| H323 | 2117h | h | Notch filter 1 (Attenuation level) | 1 | 0 to 40 dB | $\bigcirc$ | 0 | 0 | O | 0 | 0 | 0 | $\times$ | O |  |
| H324 | 2118h | h | Notch filter 1 (Frequency range) | 1 | 0 to 3 | $\bigcirc$ | 2 | 0 | 0 | 0 | 0 | 0 | $\times$ | O |  |
| H325 | 2119h | h | Notch filter 2 (Resonance frequency) | 1 | 10 to 2000 Hz | $\bigcirc$ | 1000 | 0 | O | 0 | 0 | 0 | $\times$ | 0 |  |
| H326 | 211Ah | h | Notch filter 2 (Attenuation level) | 1 | 0 to 40 dB | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | $\times$ | O |  |
| H327 | 211Bh | h | Notch filter 2 (Frequency range) | 1 | 0 to 3 | $\bigcirc$ | 2 | 0 | 0 | 0 | 0 | 0 | $\times$ | O |  |

## - Motor parameter functions M2, M3 (A: Alternative Functions)

| $\begin{aligned} & \text { ๗ } \\ & \frac{0}{0} \\ & \hline 0 \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\left\|\begin{array}{l} \text { O} \\ \stackrel{\rightharpoonup}{\lambda} \end{array}\right\|$ |  |  | Control method: Enable/ Disable |  |  | $\stackrel{\sim}{\stackrel{\sim}{0}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $$ | 485 No. | Link No. |  |  |  |  |  | $\left\|\begin{array}{l} \stackrel{\pi}{\pi} \\ \stackrel{\rightharpoonup}{0} \end{array}\right\|$ | E | $\bigcirc$ | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\begin{array}{l\|l} \mathrm{L} & \mathrm{~V} \\ \mathrm{E} & \mathrm{~F} \\ \mathrm{~S} \end{array}$ | S |  |
| A01 | 501h | h | M2 Drive control | 29 | ```0 to 5 Vector control (Induction motor) Sensor-less vector control (Induction motor) Vector control (PMSM) - V/f control (Induction motor)``` | $\times$ | 0 | $\bigcirc$ | $\times$ | 228 | 0 | 00 | - |  |
| A02 | 502h | h | M2 Rated capacity | 1 | ```For inverters of 400 kW or less 0.00 to 500.00 kW when \(\mathrm{F} 60=0\) 0.00 to 600.00 HP when \(\mathrm{F} 60=1\) For inverters of 500 kW or more 0.00 to 1200 kW when \(\mathrm{F} 60=0\) 0.00 to 1600 HP when \(\mathrm{F} 60=1\) For multiwinding motors, set the motor capacity per wiring.``` | $\times$ | 0.00 | $\bigcirc$ | $\times$ | $3$ $13$ | 0 | 00 | O |  |
| A03 | 503h | h | M2 Rated current | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | $\times$ | 0.01 | $\bigcirc$ | $\times$ | 13 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| A04 | 504h | h | M2 Rated voltage | 1 | 80 to 999 V | $\times$ | 80 | $\bigcirc$ | $\times$ | 0 | 0 | 0 O | $\bigcirc$ |  |
| A05 | 505h | h | M2 Rated speed | 1 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | $\bigcirc$ | $\times$ | 0 | 0 | 0 | $\bigcirc$ |  |
| A06 | 506h | h | M2 Max. speed | 1 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | $\bigcirc$ | $\times$ | 0 | $\bigcirc$ | 0 | O |  |
| A07 | 507h | h | M2 Number of poles | 1 | 2 to 100 poles | $\times$ | 4 | $\bigcirc$ | $\times$ | 1 | 0 | 00 | $\bigcirc$ |  |
| A08 | 508h | h | M2 \%R1 | 1 | 0.00 to 30.00\% | $\bigcirc$ | 0.00 | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | $\bigcirc 0$ | O |  |
| A09 | 509h | h | M2 \%X | 1 | 0.00 to 200.00\% | 0 | 0.00 | $\bigcirc$ | $\times$ | 3 | 0 | 0 O | O |  |
| A10 | 50Ah | h | M2 Exciting current/Magnetic flux weakening current (-Id) | 1 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~A} \\ & 100.0 \text { to } 999.9 \mathrm{~A} \\ & 1000 \text { to } 2000 \mathrm{~A} \end{aligned}$ | $\bigcirc$ | 0.01 | $\bigcirc$ | $\times$ | 13 | $\bigcirc$ | 00 | - |  |
| A11 | 50Bh | h | M2 Torque current | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | 0 | 0.01 | $\bigcirc$ | $\times$ | 13 | 0 | 0 | - |  |
| A12 | 50Ch | h | M2 Slip frequency (For driving) | 1 | 0.001 to 10.000 Hz | $\bigcirc$ | 0.001 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | 0 | $\times$ |  |
| A13 | 50Dh | h | M2 Slip frequency (For braking) | 1 | 0.001 to 10.000 Hz | $\bigcirc$ | 0.001 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A14 | 50Eh | h | M2 Iron loss factor 1 | 1 | 0.00 to 10.00\% | $\bigcirc$ | 0.00 | $\bigcirc$ | $\times$ | 3 | $\bigcirc$ | 0 | O |  |
| A15 | 50Fh | h | M2 Iron loss factor 2 | 1 | 0.00 to 10.00\% | 0 | 0.00 | $\bigcirc$ | $\times$ | 3 | 0 | 0 | $\bigcirc$ |  |
| A16 | 510h | h | M2 Iron loss factor 3 | 1 | 0.00 to 10.00\% | $\bigcirc$ | 0.00 | $\bigcirc$ | $\times$ | 3 | 0 | $\bigcirc$ | O |  |
| A17 | 511h | h | M2 Magnetic saturation factor 1 | 1 | 0.0 to 100.0\% | $\bigcirc$ | 93.8 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | 0 | $\times$ |  |
| A18 | 512h | h | M2 Magnetic saturation factor 2 | 1 | 0.0 to 100.0\% | 0 | 87.5 | $\bigcirc$ | $\times$ | 2 | 0 | 0 | $\times$ |  |
| A19 | 513h | h | M2 Magnetic saturation factor 3 | 1 | 0.0 to 100.0\% | 0 | 75.0 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A20 | 514h | h | M2 Magnetic saturation factor 4 | 1 | 0.0 to 100.0\% | 0 | 62.5 | $\bigcirc$ | $\times$ | 2 | 0 | $\bigcirc \times$ | $\times$ |  |
| A21 | 515h | h | M2 Magnetic saturation factor 5 | 1 | 0.0 to 100.0\% | $\bigcirc$ | 50.0 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | ${ }^{-1} \times$ | $\times$ |  |
| A22 | 516h | h | M2 Secondary time constant | 1 | 0.001 to 9.999 s | $\bigcirc$ | 0.001 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A23 | 517h | h | M2 Induced voltage factor | 1 | 0 to 999 V | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ | 0 | - | 0 | 0 |  |
| A24 | 518h | h | M2 R2 Correction factor 1 | 1 | 0.000 to 5.000 | 0 | 1.000 | $\bigcirc$ | $\times$ | 4 | 0 | $0 \times$ | $\bigcirc$ |  |
| A25 | 519h | h | M2 R2 Correction factor 2 | 1 | 0.000 to 5.000 | 0 | 1.000 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | ${ }^{0} \times$ | $\times$ |  |
| A26 | 51Ah | h | M2 R2 Correction factor 3 | 1 | 0.010 to 5.000 | $\bigcirc$ | 1.000 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | 0 | $\times$ |  |
| A27 | 51Bh | h | M2 Exciting current correction factor | 1 | 0.000 to 5.000 | 0 | 0.000 | $\bigcirc$ | $\times$ | 4 | 0 | $0 \times$ | $\times$ |  |
| A28 | 51Ch | h | M2 ACR-P (Gain) | 1 | 0.1 to 20.0 | 0 | 1.0 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| A29 | 51Dh | h | M2 ACR-I (l-time) | 1 | 0.1 to 100.0 ms | $\bigcirc$ | 1.0 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | $\bigcirc \times$ | 0 |  |
| A30 | 51Eh | h | M2 PG Pulse resolution | 0 | 100 to 60000 | $\times$ | 1024 | $\bigcirc$ | $\times$ | 0 | 0 | $\times \times$ | $\bigcirc$ |  |
| A31 | 51Fh | h | M2 Thermistor selection | 0 | ```0 to 3 No thermistor NTC thermistor selected PTC thermistor selected Ai [M-TMP] The protection level of the motor protective functions should be specified by E30 to E32.``` | ${ }^{\times}$ | 1 | $\bigcirc$ | $\times$ | 84 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| A32 | 520h | h | M2 Electronic thermal (Operation selection) | 3 | 0 to 2  <br> $0:$ No operation (when using exclusive motor for VG) <br> 1: Operation (for general purpose motors: use in the case <br> of self-cooling fan)  <br> 2: Operation (for inverter motors: use in the case of <br>  <br> externally powered fan) | 0 | 0 | $\bigcirc$ | $\times$ | 85 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| A33 | 521h | h | M2 Electronic thermal (Detection level) | 1 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~A} \\ & 100.0 \text { to } 999.9 \mathrm{~A} \\ & 1000 \text { to } 2000 \mathrm{~A} \\ & \hline \end{aligned}$ | 0 | 0.01 | $\bigcirc$ | $\times$ | 13 | 0 | 0 | $\bigcirc$ |  |
| A34 | 522h | h | M2 Electronic thermal (Thermal time constant) | 1 | 0.5 to 75.0 min | 0 | 0.5 | $\bigcirc$ | $\times$ | 2 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| A51 | 533h | h | M2 External PG correction factor | 0 | 0000 to 4FFF | $\times$ | 4000 | $\bigcirc$ | $\times$ | 9 | 0 | $\times \times$ | $\bigcirc$ |  |
| A52 | 534h | h | M2 Online auto tuning | 0 | $\begin{array}{\|l\|} \hline 0 \text { to } 1 \\ \text { 0: Disable } \\ \text { 1: Enable } \\ \hline \end{array}$ | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ | 0 | 0 | $\bigcirc \times$ | $\times$ |  |
| A53 | 535h | h | M2 Maximum output voltage/Maximum voltage limit value | 0 | 80 to 999 V | $\times$ | 80 | $\bigcirc$ | $\times$ | 0 | $\times \times$ | O | $\bigcirc$ |  |
| A54 | 536h | h | M2 Slip compensation | 3 | -20.000 to 5.000 Hz | $\bigcirc$ | 0.000 | $\bigcirc$ | $\times$ | 8 | $\times{ }^{\times}$ | 0 | $\times$ |  |
| A55 | 537h | h | M2 Torque boost | 1 | 0.0 <br> Fo 20.0 <br> Function specific to V/f control. The following selections are <br> possible.  <br> $0.0:$ Automatic torque boost (for fixed torque <br> 0.1 to $0.9:$ characteristic load) <br> 1.0 to $1.9:$ For squared torque characteristic load <br> 2.0 to $20.0:$ For fixed torque characteristic load | 0 | 0.0 | $\bigcirc$ | $\times$ | 2 | $\times \times$ | $\bigcirc$ | $\times$ |  |
| A56 | 538h | h | M2 Current fluctuation damping gain | 1 | 0.00 to 1.00 | 0 | 0.20 | 0 |  | 3 | $\times$ |  | $\times$ |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  | $\left\|\begin{array}{c} 0 \\ .0 \\ \vdots 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array}\right\|$ |  |  | Control method: Enable/ Disable |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | 든 |  |  | $\begin{array}{\|l\|l} \mathrm{L} & \mathrm{~V} \\ \mathrm{E} & \mathrm{~F} \\ \mathrm{~S} \end{array}$ | $V$ $S$ <br> $F$ M |  |
| A59 | 53Bh | h | M2 ABS signal input definition | 13 | 0 to 16 <br> Specifies according to the encoder specifications. <br> Defines the interface to detect magnetic polarity position. <br> 0 : 1 bit (Terminal; F0) $Z$ phase interface <br> 1: 3bit (Terminal; F0, F1, F2) U, V, W phase interface <br> 2: 4bit (Terminal; F0, F1, F2, F3) grey code interface <br> 3 to 5: Reserved <br> 6: SPGT 17 bit serial interface <br> 7 to 16: Reserved | $\times$ | 0 | 0 | $\times$ | 0 | $\times$ | $\times \times$ | O |  |
| A60 | 53Ch | h | M2 Magnetic pole position offset | 1 | 0.0 to 359.9 ( $0^{\circ}$ to $359.9^{\circ}$ CCW direction) Specifies the offset value for the encoder reference position and the actual motor magnetic pole position. | 0 | 0.0 | 0 | $\times$ | 2 | $\times$ | $\times \times$ | O |  |
| A61 | 53Dh | h | M2 Salient pole ratio (\%Xq/\%Xd) | 1 | $\begin{aligned} & 1.000 \text { to } 5.000 \\ & \text { Specifies the saliency ratio of PMSM. } \\ & \text { Setting value }=\text { Lq/Ld } \\ & \text { To drive a SPM motor, set } 1.000 \text {. } \\ & \hline \end{aligned}$ | $\times$ | 1.000 | 0 | $\times$ | 4 | $\times$ | $\times \times$ | O |  |
| A62 | 53Eh | h | M2 q axis inductance magnetic saturation coefficient | 1 | 0.0 to 100.0\% | 0 | 100.0 | $\bigcirc$ | $\times$ | 2 | $\times$ | $\times \times$ | O |  |
| A63 | 53Fh | h | M2 Magnetic flux limiting value | 1 | 50.0 to 150.0\% | 0 | 100.0 | 0 | $\times$ | 2 | $\times$ | $\times \times$ | O |  |
| A64 | 540h | h | M2 Overcurrent protection levels | 1 | ```0.00: No operation 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 5000 A Specifies the allowable current value to prevent the permanent magnet of a PMSM from getting demagnetized. If the current exceeding this setting flows, an overcurrent alarm (OC) occurs.``` | $\times$ | 0.00 | $\bigcirc$ | $\times$ | 13 | $\times$ | $\times$ | O |  |
| A65 | 541h | h | M2 Torque correction gain 1 | 1 | 0.00 to 10.00 | 0 | 1.00 | 0 | $\times$ | 3 | $\times$ | $\times \times$ | 0 |  |
| A66 | 542h | h | M2 Torque correction gain 2 | 1 | 0.00 to 10.00 | 0 | 1.00 | 0 | $\times$ | 3 | $\times$ | $\times \times$ | O |  |
| A67 | 543h | h | M2 Torque correction gain 3 | 1 | -1.000 to 1.000 | $\bigcirc$ | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times \times$ | O |  |
| A68 | 544h | h | M2 Torque correction gain 4 | 1 | -1.000 to 1.000 | $\bigcirc$ | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times \times$ | O |  |
| A69 | 545h | h | M2 Torque correction gain 5 | 1 | -50.00 to 50.00 | $\bigcirc$ | 0.00 | 0 | $\times$ | 7 | $\times$ | $\times \times$ | O |  |
| A70 | 546h | h | M2 Torque correction gain 6 | 1 | -50.00 to 50.00 | 0 | 0.00 | 0 | $\times$ | 7 | $\times$ | $\times \times$ | O |  |
| A71 | 547h | h | M2 Torque correction gain 7 | 1 | -1.000 to 1.000 | $\bigcirc$ | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times \times$ | O |  |
| A101 | 2401h | h | M3 Drive control | 29 | ```0 to } Vector control (Induction motor) Sensor-less vector control (Induction motor) Vector control (PMSM) - V/f control (Induction motor)``` | $\times$ | 5 | 0 | $\times$ | 228 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| A102 | 2402h | E5h | M3 Rated capacity | 1 | For inverters of 400 kW or less <br> 0.00 to 500.00 kW when $\mathrm{F} 60=0$ <br> 0.00 to 600.00 HP when $\mathrm{F} 60=1$ <br> For inverters of 500 kW or more <br> 0.00 to 1200 kW when $\mathrm{F} 60=0$ <br> 0.00 to 1600 HP when $\mathrm{F} 60=1$ <br> For multiwinding motors, set the motor capacity per wiring. | $\times$ | 0.00 | 0 | $\times$ | $3$ $13$ | $\bigcirc$ | 0 | 0 |  |
| A103 | 2403h | E6h | M3 Rated current | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | $\times$ | 0.01 | 0 | $\times$ | 13 | $\bigcirc$ | 0 | 0 O |  |
| A104 | 2404h | E7h | M3 Rated voltage | 1 | 80 to 999 V | $\times$ | 80 | 0 | $\times$ | 0 | $\bigcirc$ | 0 | $\bigcirc 0$ |  |
| A105 | 2405h | E9h | M3 Rated speed | 1 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | 0 | $\times$ | 0 | $\bigcirc$ | 0 | 0 O |  |
| A106 | 2406h | EAh | M3 Max. Speed | 1 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | 0 | $\times$ | 0 | 0 | 0 | $\bigcirc 0$ |  |
| A107 | 2407h | EBh | M3 Number of poles | 1 | 2 to 100 poles | $\times$ | 4 | 0 | $\times$ | , | $\bigcirc$ | 0 | $\bigcirc$ |  |
| A108 | 2408h | ECh | M3 \%R1 | 1 | 0.00 to 30.00\% | 0 | 0.00 | 0 | $\times$ | 3 | $\bigcirc$ | 0 | $\bigcirc 0$ |  |
| A109 | 2409h | EDh | M3 \%X | 1 | 0.00 to 200.00\% | $\bigcirc$ | 0.00 | 0 | $\times$ | 3 | $\bigcirc$ | 0 | 0 O |  |
| A110 | 240Ah | EEh | M3 Exciting current/Magnetic flux weakening current (-Id) | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | $\bigcirc$ | 0.01 | $\bigcirc$ | $\times$ | 13 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| A111 | 240Bh | h | M3 Torque current | 1 | 0.01 to 99.99 A 100.0 to 999.9 A 1000 to 2000 A | 0 | 0.01 | 0 | $\times$ | 13 | $\bigcirc$ | $0 \times$ | O |  |
| A112 | 240Ch | h | M3 Slip frequency (For driving) | 1 | 0.001 to 10.000 Hz | 0 | 0.001 | 0 | $\times$ | 4 | $\bigcirc$ | 0 | $\times \times$ |  |
| A113 | 240Dh | h | M3 Slip frequency (For braking) | 1 | 0.001 to 10.000 Hz | $\bigcirc$ | 0.001 | 0 | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A114 | 240Eh | h | M3 Iron loss factor 1 | 1 | 0.00 to 10.00\% | 0 | 0.00 | 0 | $\times$ | 3 | $\bigcirc$ | $\bigcirc$ | O |  |
| A115 | 240Fh | h | M3 Iron loss factor 2 | 1 | 0.00 to 10.00\% | 0 | 0.00 | 0 | $\times$ | 3 | $\bigcirc$ | $\bigcirc$ | O |  |
| A116 | 2410h | h | M3 Iron loss factor 3 | 1 | 0.00 to 10.00\% | 0 | 0.00 | 0 | $\times$ | 3 | $\bigcirc$ | 0 | 0 |  |
| A117 | 2411 h | h | M3 Magnetic saturation factor 1 | 1 | 0.0 to 100.0\% | 0 | 93.8 | 0 | $\times$ | 2 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A118 | 2412h | h | M3 Magnetic saturation factor 2 | 1 | 0.0 to 100.0\% | 0 | 87.5 | 0 | $\times$ | 2 | 0 | 0 | $\times \times$ |  |
| A119 | 2413h | h | M3 Magnetic saturation factor 3 | 1 | 0.0 to 100.0\% | 0 | 75.0 | 0 | $\times$ | 2 | 0 | $\bigcirc$ | $\times \times$ |  |
| A120 | 2414h | h | M3 Magnetic saturation factor 4 | 1 | 0.0 to 100.0\% | 0 | 62.5 | 0 | $\times$ | 2 | 0 | O | $\times \times$ |  |
| A121 | 2415h | h | M3 Magnetic saturation factor 5 | 1 | 0.0 to 100.0\% | $\bigcirc$ | 50.0 | 0 | $\times$ | 2 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A122 | 2416h | h | M3 Secondary time constant | 1 | 0.001 to 9.999 s | 0 | 0.001 | 0 | $\times$ | 4 | 0 | $\bigcirc$ | $\times$ |  |
| A123 | 2417h | h | M3 Induced voltage factor | 1 | 0 to 999 V | 0 | 0 | 0 | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| A124 | 2418h | h | M3 R2 Correction factor 1 | 1 | 0.500 to 5.000 | 0 | 1.000 | 0 | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | O |  |
| A125 | 2419h | h | M3 R2 Correction factor 2 | 1 | 0.500 to 5.000 | 0 | 1.000 | 0 | $\times$ | 4 | 0 | $\bigcirc$ | $\times \times$ |  |
| A126 | 241Ah | h | M3 R2 Correction factor 3 | 1 | 0.010 to 5.000 | $\bigcirc$ | 1.000 | $\bigcirc$ | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times \times$ |  |
| A127 | 241Bh |  | M3 Exciting current correction factor | 1 | 0.000 to 5.000 | 0 | 0.000 | 0 | $\times$ | 4 | $\bigcirc$ | $\bigcirc$ | $\times$ |  |
| A128 | 241Ch | h | M3 ACR-P (Gain) | 1 | 0.1 to 20.0 | 0 | 1.0 | 0 | $\times$ | 2 | O | O | O |  |
| A129 | 241Dh | , | M3 ACR-I time | 1 | 0.1 to 100.0 ms | $\bigcirc$ | 1.0 | $\bigcirc$ | $\times$ | 2 | 0 | $\bigcirc$ | O |  |
| A130 | 241Eh | h | M3 PG pulse resolution | 0 | 100 to 60000 | $\times$ | 1024 | 0 | $\times$ | 0 | $\bigcirc$ | $\times \times$ | O |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  | $\left\lvert\, \begin{aligned} & 0 \\ & \stackrel{\rightharpoonup}{\lambda} \\ & \text { ㅇ } \end{aligned}\right.$ |  |  | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  | $\left\|\begin{array}{c} \frac{\pi}{\widetilde{0}} \\ \stackrel{\rightharpoonup}{0} \end{array}\right\|$ | 星 | $\begin{aligned} & \frac{0}{0} \\ & \frac{0}{0} \end{aligned}$ | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\left\|\begin{array}{l} \mathrm{L} \\ \mathrm{E} \\ \mathrm{~S} \end{array}\right\|$ | V | S |  |
| A131 | 241Fh | F1h | M3 Thermistor selection | 0 | 0 to 3 <br> No thermistor <br> NTC thermistor selected <br> PTC thermistor selected <br> Ai [M-TMP] <br> The protection level of the motor protective functions should be specified by E30 to E32. | $\times$ | 1 | 0 | $\times$ | 84 | 0 | 0 | O | $\bigcirc$ |  |
| A132 | 2420h | F2h | M3 Electronic thermal (Operation selection) | 3 | 0 to 2 <br> 0: No operation (when using exclusive motor for VG) <br> 1: Operation (for general purpose motors: use in case of self-cooling fan) <br> 2: Operation (for inverter motors: use in case of externally powered fans) <br> Using an NTC thermistor of a FRENIC-VG-dedicated motor activates the motor overheat protection. If it happens, disable the electronic thermal overload protection. | 0 | 0 | 0 | $\times$ | 85 | 0 | 0 | O | O |  |
| A133 | 2421h | F3h | M3 Electronic thermal (Detection level) | 1 | $\begin{aligned} & 0.01 \text { to } 99.99 \mathrm{~A} \\ & 100.0 \text { to } 999.9 \mathrm{~A} \\ & 1000 \text { to } 2000 \mathrm{~A} \end{aligned}$ | 0 | 0.01 | 0 | $\times$ | 13 | 0 | 0 | O | 0 |  |
| A134 | 2422h | F4h | M3 Electronic thermal (Thermal time constant) | 1 | 0.5 to 75.0 min | O | 0.5 | 0 | $\times$ | 2 | 0 | 0 | O | 0 |  |
| A151 | 2433h | h | M3 External PG correction factor | 0 | 0000 to 4FFF | $\times$ | 4000 | 0 | $\times$ | 9 | 0 | $\times$ | $\times$ | 0 |  |
| A152 | 2434h | h | M3 Online Auto tuning | 0 | 0 to 1 0: Disable 1: Enable | $\bigcirc$ | 0 | $\bigcirc$ | $\times$ | 0 | 0 | $\bigcirc$ | $\times$ | $\times$ |  |
| A153 | 2435h | E8h | M3 Maximum output voltage/Maximum voltage limit value | 0 | 80 to 999 V | $\times$ | 80 | 0 | $\times$ | 0 | $\times$ | $\times$ | 0 | 0 |  |
| A154 | 2436h | EFh | M3 Slip compensation | 3 | -20.000 to 5.000 Hz | O | 0.000 | O | $\times$ | 8 | $\times$ | $\times$ | O | $\times$ |  |
| A155 | 2437h | FOh | M3 Torque boost | 1 |  | $\bigcirc$ | 0.0 | $\bigcirc$ | $\times$ | 2 | $\times$ | $\times$ | 0 | $\times$ |  |
| A156 | 2438h | h | M3 Current fluctuation damping gain | 1 | 0.00 to 1.00 | $\bigcirc$ | 0.20 | $\bigcirc$ | $\times$ | 3 | $\times$ | $\times$ | 0 | $\times$ |  |
| A159 | 243Bh | h | M3 ABS signal input definition | 13 | 0 to 16 <br> Specifies according to the encoder specifications. <br> Defines the interface to detect magnetic polarity position. <br> 0: 1 bit (Terminal; F0) $Z$ phase interface <br> 1: $\quad 3$ bit (Terminal; F0, F1, F2) U, V, W phase interface <br> 2: 4bit (Terminal; F0, F1, F2, F3) grey code interface <br> 3 to 5: Reserved <br> 6: SPGT 17 bit serial interface <br> 7 to 16: Reserved | $\times$ | 0 | $\bigcirc$ | $\times$ | 0 | $\times$ | $\times$ | $\times$ | 0 |  |
| A160 | 243Ch | h | M3 Magnetic pole position offset | 1 | 0.0 to 359.9 ( $0^{\circ}$ to $359.9^{\circ}$ CCW direction) Specifies the offset value for the encoder reference position and the actual motor magnetic pole position. | 0 | 0.0 | 0 | $\times$ | 2 | $\times$ | $\times$ | $\times$ | O |  |
| A161 | 243Dh | h | M3 Salient pole ratio (\%Xq/\%Xd) | 1 | $\begin{aligned} & 1.000 \text { to } 5.000 \\ & \text { Specifies the saliency ratio of PMSM. } \\ & \text { Setting value }=\mathrm{Lq} / \mathrm{Ld} \\ & \text { To drive a SPM motor, set } 1.000 \text {. } \end{aligned}$ | $\times$ | 1.000 | 0 | $\times$ | 4 | $\times$ | $\times$ | $\times$ | 0 |  |
| A162 | 243Eh | h | M3 q axis inductance magnetic saturation coefficient | 1 | 0.0 to 100.0 \% | 0 | 100.0 | 0 | $\times$ | 2 | $\times$ | $\times$ | $\times$ | 0 |  |
| A163 | 243Fh | h | M3 Magnetic flux limiting value | 1 | 50.0 to 150.0 \% | 0 | 100.0 | 0 | $\times$ | 2 | $\times$ | $\times$ | $\times$ | 0 |  |
| A164 | 2440h | h | M3 Overcurrent protection level | 1 | 0.00: No operation <br> 0.01 to 99.99 A <br> 100.0 to 999.9 A <br> 1000 to 5000A <br> Specifies the allowable current value to prevent the permanent magnet of a PMSM from getting demagnetized. If the current exceeding this setting flows, an overcurrent alarm (OC) occurs. | $\times$ | 0.00 | $\bigcirc$ | $\times$ | 13 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| A165 | 2441h | h | M3 Torque correction gain 1 | 1 | 0.00 to 10.00 | 0 | 1.00 | 0 | $\times$ | 3 | $\times$ | $\times$ | $\times$ | 0 |  |
| A166 | 2442h | h | M3 Torque correction gain 2 | 1 | 0.00 to 10.00 | 0 | 1.00 | 0 | $\times$ | 3 | $\times$ | $\times$ | $\times$ | 0 |  |
| A167 | 2443h | h | M3 Torque correction gain 3 | 1 | -1.000 to 1.000 | 0 | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times$ | $\times$ | 0 |  |
| A168 | 2444h | h | M3 Torque correction gain 4 | 1 | -1.000 to 1.000 | 0 | 0.000 | 0 | $\times$ | 8 | $\times$ | $\times$ | $\times$ | 0 |  |
| A169 | 2445h | h | M3 Torque correction gain 5 | 1 | -50.00 to 50.00 | 0 | 0.00 | 0 | $\times$ | 7 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |
| A170 | 2446h | h | M3 Torque correction gain 6 | 1 | -50.00 to 50.00 | 0 | 0.00 | 0 | $\times$ | 7 | $\times$ | $\times$ | $\times$ | 0 |  |
| A171 | 2447h | h | M3 Torque correction gain 7 | 1 | -1.000 to 1.000 | 0 | 0.000 | $\bigcirc$ | $\times$ | 8 | $\times$ | $\times$ | $\times$ | $\bigcirc$ |  |

## - Option functions (O: Option Functions)

|  | Communications address |  | Name | Dir | Data setting range |  |  |  |  | 은0.040000 | Control method: Enable/ Disable |  |  |  | $\stackrel{\sim}{\stackrel{n}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | P | $\begin{aligned} & \mathrm{L} \\ & \mathrm{E} \\ & \mathrm{~S} \end{aligned}$ | V | S |  |
| 001 | 601h | F5h | DIA function selection | 4 | $\begin{aligned} & \hline 0 \text { to } 1 \\ & \text { 0: Binary } \\ & \text { 1: BCD } \end{aligned}$ | $\times$ | 0 | O | $\bigcirc$ | 86 | $\bigcirc$ | O | O | - |  |
| 002 | 602h | F6h | DIB function selection | 1 | $\begin{aligned} & 0 \text { to } 1 \\ & 0: \text { Binary } \\ & \text { 1: BCD } \end{aligned}$ | $\times$ | 0 | O | $\bigcirc$ | 86 | $\bigcirc$ | O | O | O |  |
| 003 | 603h | h | DIA BCD input setting | 1 | 99 to 7999 | $\times$ | 1000 | $\bigcirc$ | 0 | 0 | 0 | 0 | - | 0 |  |
| 004 | 604h | h | DIB BCD input setting | 1 | 99 to 7999 | $\times$ | 1000 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | O |  |
| 005 | 605h | h | PG (PD) option setting (Return pulse selection) | 0 | 0 to 1 <br> 0: Main unit PG <br> 1: PG (PD) option | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 96 | $\bigcirc$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 006 | 606h | h | $\begin{array}{\|l\|} \hline \text { PG (LD) option setting } \\ \text { (Digital line speed detect definition/ } \\ \text { (Encoder pulse resolution)) } \\ \hline \end{array}$ | 3 | 100 to 60000 P/R | 0 | 1024 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| 007 | 607h | h | $\begin{array}{\|l\|} \hline \text { PG (LD) option setting } \\ \text { (Digital line speed detect definition/ } \\ \text { (Detected pulse correction 1)) } \\ \hline \end{array}$ | 1 | 1 to 9999 | 0 | 1000 | - | $\bigcirc$ | 0 | 0 | O | - | O |  |
| 008 | 608h | h | $\begin{array}{\|l\|} \hline \text { PG (LD) option setting } \\ \text { (Digital line speed detect definition/ } \\ \text { (Detected pulse correction 2)) } \\ \hline \end{array}$ | 1 | 1 to 9999 | 0 | 1000 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| 009 | 609h | h | M1 ABS signal input definition | 3 | 0 to 16 <br> Specifies according to the encoder specifications. <br> Defines the interface to detect magnetic polarity position. <br> 0: 1bit (Terminal; F0) Z phase interface <br> 1: 3bit (Terminal; F0, F1, F2) U, V, W phase interface <br> 2: 4bit (Terminal; F0, F1, F2, F3) grey code interface <br> 3 to 5: Reserved <br> 6: SPGT 17 bit serial interface <br> 7 to 16: Reserved | $\times$ | 0 | $\bigcirc$ | $\times$ | 0 | $\times$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 010 | 60Ah | h | M1 Magnetic pole position offset | 1 | 0.0 to 359.9 ( $0^{\circ}$ to $359.9^{\circ}$ CCW direction) Specifies the offset value for the encoder reference position and the actual motor magnetic pole position. | $\bigcirc$ | 0.0 | 0 | $\times$ | 2 | $\times$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 011 | 60Bh | h | M1 Salient pole rate (\%Xq/\%Xd) | 1 | $\begin{aligned} & 1.000 \text { to } 5.000 \\ & \text { Specifies the saliency ratio of PMSM. } \\ & \text { Setting value }=\mathrm{Lq} / \mathrm{Ld} \\ & \text { To drive a SPM motor, set } 1.000 \text {. } \\ & \hline \end{aligned}$ | $\times$ | 1.000 | 0 | $\times$ | 4 | $\times$ | $\times \times$ | $\times$ | O |  |
| 012 | 60Ch | h | PG (PR) pulse-train option setting (Command pulse selection) | 8 | $\begin{aligned} & \hline 0 \text { to } 1 \\ & \text { 0: PG (PR) option } \\ & \text { 1: Internal speed command } \\ & \hline \end{aligned}$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | 97 | 0 | $\times \times$ | * | $\bigcirc$ |  |
| 013 | 60Dh | h | PG (PR) pulse-train option setting (Pulse-train input style selection) | 1 | 0 to 2 <br> 0 : A, B phase 90 degrees phase difference <br> 1: A phase: command pulse, B phase: command code <br> 2: A phase: normal pulse, B phase: reverse pulse | $\times$ | 0 | - | $\bigcirc$ | 98 | 0 | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 014 | 60Eh | F7h | PG (PR) pulse-train option setting (Command pulse correction 1) | 1 | 1 to 9999 | $\bigcirc$ | 1000 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | $\times{ }^{\times}$ | $\times$ | $\bigcirc$ |  |
| 015 | 60Fh | F8h | PG (PR) pulse-train option setting (Command pulse correction 2) | 1 | 1 to 9999 | $\bigcirc$ | 1000 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 016 | 610h | F9h | PG (PR) pulse-train option setting (APR gain 1) | 1 | 0.1 to 999.9 times | $\bigcirc$ | 1.0 | $\bigcirc$ | $\bigcirc$ | 2 | $\bigcirc$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 017 | 611h | FAh | PG (PR) pulse-train option setting (F/F gain 1) | 1 | 0.0 to 1.5 times | $\bigcirc$ | 0.0 | - | $\bigcirc$ | 2 | $\bigcirc$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 018 | 612h | h | PG (PR) pulse-train option setting (Width exceeding deviation) | 1 | 0 to 65535 pulses | $\bigcirc$ | 65535 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 019 | 613h | h | PG (PR) pulse-train option setting (Zero width deviation) | 1 | 0 to 1000 pulses | $\bigcirc$ | 20 | 0 | $\bigcirc$ | 0 | 0 | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 020 | 614h | h | APR gain 2 (To be supported soon) | 1 | 0.1 to 999.9 times | 0 | 1.0 | $\bigcirc$ | 0 | 2 | $\bigcirc$ | $\times \times$ | $\times$ | 0 |  |
| 021 | 615h | h | F/F gain 2 (To be supported soon) | 1 | 0.0 to 1.5 times | $\bigcirc$ | 0.0 | $\bigcirc$ | 0 | 2 | $\bigcirc$ | $\times$ | $\times$ | 0 |  |
| 022 | 616h | h | Position control gain switching selection <br> (To be supported soon) | 3 | 0 to 3 <br> 0 : No operation <br> 1: Position deviation ( $\times 10$ ) <br> 2: Speed detection (10000/max speed) <br> 3: Speed command ( $10000 /$ max speed) <br> Select a trigger to switch between the 1st and 2nd gains of the position control system. <br> Switching gains can reduce noise or vibration when the inverter is stopped. | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | 229 | $\bigcirc$ | $\times$ | $\times$ | $\bigcirc$ |  |
| 023 | 617h | h | $\begin{array}{\|l\|} \hline \begin{array}{l} \text { Position control switching level } \\ \text { (To be supported soon) } \end{array} \\ \hline \end{array}$ | 1 | 0 to 10000 | 0 | 0 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | $\times{ }^{\times}$ | $\times$ | $\bigcirc$ |  |
| 024 | 618h | h | Position control gain switch timing (To be supported soon) | 1 | 0 to 1000 ms | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | $\times \times$ | $\times$ | $\bigcirc$ |  |
| 030 | 61Eh | h | Link option setting (Activity at transmission failure) |  | 0 to 3 <br>  <br> 1: Trip after continuing operation for time specified as operation continuance $\left(E--\frac{1}{4}\right)$ <br> 2: Trip when transmission failure continues after operation time $\left(E,-\frac{1}{-1}\right)$ <br> 3: Operation continuance <br> Specifies the error processing to be performed if a communications link error occurs. <br> For CC-Link, when $030=0$ to 3 , the inverter produces different operation from above. | $\times$ | 0 | 0 | $\bigcirc$ | 73 | 0 | 0 | - | - |  |
| 031 | 61Fh | h | Link option setting (Operation time at transmission failure) | 1 | $0.01 \text { to } 20.00 \mathrm{~s}$ <br> Specifies the duration from an occurrence of communications problem on the link until the inverter causes a communications error. | $\times$ | 0.10 | 0 | $\bigcirc$ | 3 | 0 | 0 | O | O |  |


|  | $C$ <br> $\begin{array}{c}\text { Communications } \\ \text { address }\end{array}$ |  | Name | Dir | Data setting range |  |  | 㖣 |  |  | Control method： Enable／ Disable |  |  |  | $\xrightarrow{\stackrel{n}{\square}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No． | Link No． |  |  |  |  |  | $\left\|\begin{array}{\|c\|} \frac{\pi}{5} \\ \hline 1 \end{array}\right\|$ | 号 | － | P |  |  | S |  |
| 032 | 620h | h | Link option setting （Transmission format） | 1 | 0 to 4 <br> 0：Transmission format 1 <br> 1：Transmission format 2 <br> 2：Transmission format 3 <br> 3：Transmission format 4 <br> 4：Transmission format 5 | $\times$ | 0 | 0 | $\times$ | 87 | $\bigcirc$ | 00 | O | $\bigcirc$ |  |
| $\begin{aligned} & \hline 033 \\ & (* 1) \end{aligned}$ | 621h | FDh | Multiplex system（Control mode） | 2 | 0 to 5 <br> 0：Disable <br> 1：Multi－winding system <br> 2：Multiplex system 1 （Direct parallel system） <br> 3：Multiplex system 2 <br> 4：Reserved 1 <br> 5：Reserved 2 <br> Selects whether to use terminal block supporting high speed serial communication as a multi－winding system or as a multiplex system．Single operation is possible when disabled． <br> Refer to MT－CCL（Multiplex system cancel）in the description of E01 to E13（Terminal X function）． | $\times$ | 0 | － | O | 232 | 0 | $\times \times$ | $\times$ | $\times$ |  |
| 034 | 622h | h | Multiplex System（No．of slave stations） | 1 | 1 to 5 <br> Specifies the numbers of slave units except a master unit when the multiplex system is enabled． | $\times$ | 1 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | $\times{ }^{\times}$ | $\times$ | $\times$ |  |
| $\begin{aligned} & 038 \\ & (* 1) \end{aligned}$ | 626h | h | UPAC Start／Stop | 3 | ```0 to 2 0: Stop UPAC 1: Start UPAC 2: Start UPAC (Initial startup) Specifies whether to start or stop UPAC option.``` | $\times$ | 0 | － | O | 68 | 0 | 0 O | － | $\bigcirc$ |  |
| $\begin{aligned} & 039 \\ & (* 1) \end{aligned}$ | 627h | h | UPAC memory mode | 1 | 00 to 1F <br> When UPAC is stopped，this function can be used to specify the affected area． <br> Setting 0；hold／1；zero clear <br> 1bit：IQ area <br> 2bit：M area <br> 3bit：RM area <br> 4bit：FM area <br> 5bit：SFM area <br> When UPAC is stopped from running or in the stopped state，this function defines whether to zero－clear or hold the specified memory area． | $\times$ | 00 | － | 0 | 9 | 0 |  | － | $\bigcirc$ |  |
| $\begin{aligned} & \mathrm{O} 40 \\ & (* 1) \end{aligned}$ | 628h | h | UPAC address | 1 | 100 to 255 <br> Sets up the UPAC station number used to access from PC to UPAC via RS－485 communication． | $\times$ | 100 | 0 | $\times$ | 0 | $\bigcirc$ | 0 | O | $\bigcirc$ |  |
| 050 | 632h | h | Multiplex system（Station number assignment） | 0 | 0 to 5 <br> $0:$ Master <br> 1－5：Slave 1 to 5 | $\times$ | 0 | $\times$ | $\bigcirc$ | 0 | $\bigcirc$ | $\times \times$ | $\times$ | $\times$ |  |
| $\begin{aligned} & \hline 0101 \\ & \left({ }^{(* 2)}\right. \end{aligned}$ | 2501h | h | Free assignment reflection | 0 | 0 to 1 <br> Automatically reset to 0 after data writing． | $\times$ | 0 | $\times$ | $\times$ | 11 | $\bigcirc$ | 0 O | O | $\bigcirc$ |  |
| 0122 | 2516h | h | Write function code assignment 1 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | 0 | 00 | － | $\bigcirc$ |  |
| 0123 | 2517h | h | Write function code assignment 2 | 0 | 0000 to FFFF | $\bigcirc$ | 0000 | O | $\bigcirc$ | 9 | $\bigcirc$ | 0 | O | $\bigcirc$ |  |
| 0124 | 2518h | h | Write function code assignment 3 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | $\bigcirc$ | － | $\bigcirc$ |  |
| 0125 | 2519h | h | Write function code assignment 4 | 0 | 0000 to FFFF | $\bigcirc$ | 0000 | － | $\bigcirc$ | 9 | O | 0 | － | $\bigcirc$ |  |
| 0126 | 251Ah | h | Write function code assignment 5 | 0 | 0000 to FFFF | 0 | 0000 | 0 | $\bigcirc$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| 0127 | 251Bh | h | Write function code assignment 6 | 0 | 0000 to FFFF | $\bigcirc$ | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | 00 | － | $\bigcirc$ |  |
| 0128 | 251Ch | h | Write function code assignment 7 | 0 | 0000 to FFFF | 0 | 0000 | 0 | $\bigcirc$ | 9 | $\bigcirc$ | 00 | $\bigcirc$ | 0 |  |
| 0129 | 251Dh | h | Write function code assignment 8 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ |  |
| 0130 | 251Eh | h | Write function code assignment 9 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | 0 | O | $\bigcirc$ |  |
| 0131 | 251Fh | h | Write function code assignment 10 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | 0 | 00 | － | $\bigcirc$ |  |
| 0132 | 2520h | h | Write function code assignment 11 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ |  |
| 0133 | 2521h | h | Write function code assignment 12 | 0 | 0000 to FFFF | 0 | 0000 | O | $\bigcirc$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ |  |
| 0160 | 253Ch | h | Read function code assignment 1 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | $\bigcirc$ | 00 | － | $\bigcirc$ |  |
| 0161 | 253Dh | h | Read function code assignment 2 | 0 | 0000 to FFFF | 0 | 0000 | 0 | $\bigcirc$ | 9 | $\bigcirc$ | 00 | $\bigcirc$ | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0162 \\ & (* 2) \\ & \hline \end{aligned}$ | 253Eh | h | Read function code assignment 3 | 0 | 0000 to FFFF | $\bigcirc$ | 0000 | O | $\bigcirc$ | 9 | $\bigcirc$ | 0 | － | $\bigcirc$ |  |
| $\begin{gathered} \hline \begin{array}{c} \text { o163 } \\ (* 2) \end{array} \\ \hline \end{gathered}$ | 253Fh | h | Read function code assignment 4 | 0 | 0000 to FFFF | $\bigcirc$ | 0000 | 0 | $\bigcirc$ | 9 | O | 0 | $\bigcirc$ | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0164 \\ & (* 2) \\ & \hline \end{aligned}$ | 2540h | h | Read function code assignment 5 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | － | 9 | 0 | 0 |  | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0165 \\ & (* 2) \\ & \hline \end{aligned}$ | 2541H | h | Read function code assignment 6 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0166 \\ & (* 2) \\ & \hline \end{aligned}$ | 2542h | h | Read function code assignment 7 | 0 | 0000 to FFFF | 0 | 0000 | 0 | $\bigcirc$ | 9 | 0 | 0 O | － | $\bigcirc$ |  |
| $\begin{gathered} \hline 0167 \\ (* 2) \\ \hline \end{gathered}$ | 2543h | h | Read function code assignment 8 | 0 | 0000 to FFFF | 0 | 0000 | O | － | 9 | O | 0 O |  | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0168 \\ & (* 2) \\ & \hline \end{aligned}$ | 2544h | h | Read function code assignment 9 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | － | 9 | O | 0 O |  | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0169 \\ & \hline(* 2) \\ & \hline \end{aligned}$ | 2545h | h | Read function code assignment 10 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | 0 | 0 |  | $\bigcirc$ |  |
| $\begin{aligned} & \hline 0170 \\ & (* 2) \\ & \hline \end{aligned}$ | 2546h | h | Read function code assignment 11 | 0 | 0000 to FFFF | 0 | 0000 | O | $\bigcirc$ | 9 | 0 | 0 |  | $\bigcirc$ |  |
| $\begin{aligned} & 0171 \\ & \left({ }^{(* 2)} \mathbf{~}\right. \end{aligned}$ | 2547h | h | Read function code assignment 12 | 0 | 0000 to FFFF | 0 | 0000 | $\bigcirc$ | $\bigcirc$ | 9 | 0 | 0 |  | $\bigcirc$ |  |

（＊1）Available when the ROM version is $\mathrm{H} 1 / 20020$ or later．
（＊2）Availble in the ROM version H1／2 02口D，which supports PROFINET－IRT．

## Lift functions (L: Lift Functions)

| $\begin{aligned} & \text { d } \\ & \stackrel{8}{0} \\ & \hline \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\left\lvert\, \begin{aligned} & \text { O} \\ & \text { 들 } \end{aligned}\right.$ | $\left\|\begin{array}{c} \stackrel{c}{0} \\ \stackrel{0}{0} \end{array}\right\|$ | $\begin{aligned} & \text { 듣 } \\ & \hline \overline{0} \end{aligned}$ | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  | $\left\|\begin{array}{c} \stackrel{9}{0} \\ \underset{0}{0} \end{array}\right\|$ | 号 | $\begin{aligned} & \mathscr{0} \\ & \frac{0}{0} \end{aligned}$ | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\left.\begin{aligned} & \mathrm{L} \\ & \mathrm{E} \\ & \mathrm{~S} \end{aligned} \right\rvert\,$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}$ | $\begin{array}{\|l} \hline \mathrm{S} \\ \mathrm{M} \end{array}$ |  |
| L01 | 901h | h | Password data 1 | 0 | 0 to 9999 <br> A maximum of 8-digit password can be specified with L01 and L02 to restrict access to change or check function code data. Setting either one of L01 and L02 at any numeral except "0" enables password protection. | O | 0 | $\times$ | $\times$ | 0 | 0 | O | $\times$ | O |  |
| L02 | 902h | h | Password data 2 | 0 | 0 to 9999 | 0 | 0 | $\times$ | $\times$ | 0 | 0 | 0 | $\times$ | 0 |  |
| L03 | 903h | h | Lift rated speed | 0 | 0.0 to $999.9 \mathrm{~m} / \mathrm{min}$ | 0 | 100.0 | $\bigcirc$ | O | 2 | $\bigcirc$ | $\bigcirc$ | $\times$ | 0 |  |
| L04 | 904h | h | Preset S-curve pattern | 11 | 0 to 2 <br> 0: Not used <br> Normal accel/decel, S-curve (15 steps, S-curve 5) <br> 1: Method 1 VG3, VG5 method. SS1, SS2, and SS4 are all OFF with 12 input enable. <br> 2: Method 2 <br> VG7, FRENIC-VG method. SS1, SS2, and SS4 are all OFF with zero speed. <br> Select S-curve pattern and application of multistep speed setting. | 0 | 0 | 0 | O | 80 | O | 0 | $\times$ | 0 |  |
| L05 | 905h | h | Select S-curve pattern 1 | 1 | 0 to 50\% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\times$ | 0 |  |
| L06 | 906h | h | Select S-curve pattern 2 | 1 | 0 to 50\% | 0 | 0 | $\bigcirc$ | O | 0 | $\bigcirc$ | $\bigcirc$ | $\times$ | O |  |
| L07 | 907h | h | Select S-curve pattern 3 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | 0 | $\mathrm{O}^{1}$ | $\times$ | 0 |  |
| L08 | 908h | h | Select S-curve pattern 4 | 1 | 0 to 50\% | 0 | 0 | $\bigcirc$ | O | 0 | $\bigcirc$ | $\bigcirc$ | $\times$ | O |  |
| L09 | 909h | h | Select S-curve pattern 5 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | $\bigcirc$ | $\bigcirc$ | $\times$ | O |  |
| L10 | 90Ah | h | Select S-curve pattern 6 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | 0 | 0 | $\times$ | 0 |  |
| L11 | 90Bh | h | Select S-curve pattern 7 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | 0 | 0 | $\times$ | 0 |  |
| L12 | 90Ch | h | Select S-curve pattern 8 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | 0 | 0 | $\times$ | O |  |
| L13 | 90Dh | h | Select S-curve pattern 9 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | $\bigcirc$ | $\bigcirc$ | $\times$ | O |  |
| L14 | 90Eh | h | Select S-curve pattern 10 | 1 | 0 to 50\% | 0 | 0 | 0 | O | 0 | O | $\bigcirc$ | $\times$ | O |  |

## ■ User functions (UPAC) (U: User Functions)

| $\begin{aligned} & \infty \\ & \stackrel{0}{\circ} \end{aligned}$ | Communication s address |  | Name | Di | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  | $\stackrel{\sim}{\sim}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 5 \\ & \hline 5 \\ & \hline 1 \end{aligned}$ | $485$ No. | Link No. |  |  |  |  |  | $\left\|\begin{array}{l} \frac{\pi}{0} \\ \stackrel{0}{0} \end{array}\right\|$ | - | \% | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\begin{array}{\|l\|l} \mathrm{L} & \mathrm{~V} \\ \mathrm{E} & \mathrm{~F} \\ \mathrm{~S} & \end{array}$ | S |  |
| U01 | B01h | DBh | USER P1 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| U02 | B02h | DCh | USER P2 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | - |  |
| U03 | B03h | DDh | USER P3 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U04 | B04h | DEh | USER P4 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | - |  |
| U05 | B05h | DFh | USER P5 | 0 | -32768 to 32767 | 0 | 0 | 0 | $\bigcirc$ | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U06 | B06h | EOh | USER P6 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| U07 | B07h | E1h | USER P7 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U08 | B08h | E2h | USER P8 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | O | 5 | O | 0 | O |  |
| U09 | B09n | E3h | USER P9 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | $\bigcirc$ | 0 | - |  |
| U10 | B0Ah | E4h | USER P10 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ |  |
| U11 | B0Bh | h | USER P11 SX, E-SX bus Communication format selection | 0 | -32768 to 32767 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | 5 | $\bigcirc$ | $\bigcirc$ | - |  |
| U12 | B0Ch | h | USER P12 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | 0 |  |
| U13 | BODh | h | USER P13 SX bus Station number monitor | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 5 | O | 0 O | - |  |
| U14 | B0Eh | h | USER P14 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | $\bigcirc$ | 0 | O |  |
| U15 | B0Fh | h | USER P15 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | O | 5 | O | 0 | O |  |
| U16 | B10h | h | USER P16 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | 0 |  |
| U17 | B11员 | h | USER P17 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | - |  |
| U18 | B12h | h | USER P18 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U19 | B13h | h | USER P19 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| U20 | B14h | h | USER P20 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | O | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U21 | B15h | h | USER P21 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | O | 0 | $\bigcirc$ |  |
| U22 | B16h | h | USER P22 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U23 | B17h | h | USER P23 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U24 | B18h | h | USER P24 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U25 | B19h | h | USER P25 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | O | 0 | $\bigcirc$ |  |
| U26 | B1Ah | h | USER P26 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | O | 5 | O | 0 | O |  |
| U27 | B1Bh | h | USER P27 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U28 | B1Ch | h | USER P28 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U29 | B1Dh | h | USER P29 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | - |  |
| U30 | B1Eh | h | USER P30 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U31 | B1Fh | h | USER P31 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 |  |
| U32 | B20h | h | USER P32 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ |  |
| U33 | B21n | h | USER P33 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | O | 0 | $\bigcirc$ |  |
| U34 | B22h | h | USER P34 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | 0 |  |
| U35 | B23h | h | USER P35 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U36 | B24h | h | USER P36 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | $\bigcirc$ |  |
| U37 | B25h | h | USER P37 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U38 | B26h | h | USER P38 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U39 | B27h | h | USER P39 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | O |  |
| U40 | B28h | h | USER P40 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U41 | B29h | h | USER P41 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U42 | B2Ah | h | USER P42 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U43 | B2Bh | h | USER P43 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U44 | B2Ch | h | USER P44 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U45 | B2Dh | h | USER P45 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | $\bigcirc$ |  |
| U46 | B2Eh | h | USER P46 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U47 | B2Fh | h | USER P47 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U48 | B30h | h | USER P48 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U49 | B31h | h | USER P49 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U50 | B32h | h | USER P50 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U51 | B33h | h | USER P51 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | $\bigcirc$ | 0 O | O |  |
| U52 | B34h | h | USER P52 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | 0 | 0 | 0 |  |
| U53 | B35h | h | USER P53 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U54 | B36h | h | USER P54 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U55 | B37h | h | USER P55 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 00 | 0 |  |
| U56 | B38h | h | USER P56 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | 0 | 0 | O |  |
| U57 | B39h | h | USER P57 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | O |  |
| U58 | B3Ah | h | USER P58 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | 0 |  |
| U59 | B3Bh | h | USER P59 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U60 | B3Ch | h | USER P60 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | 0 |  |
| U61 | B3Dh | 4Bh | USER P61/U-Ai1 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | 0 |  |
| U62 | B3Eh | 4Ch | USER P62/U-Ai2 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U63 | B3Fh | 4Dh | USER P63/U-Ai3 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| U64 | B40h | 4Eh | USER P64/U-Ai4 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | $\bigcirc$ | 0 | 0 |  |
| U101 | 2701h | h | USER P101 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | 0 |  |
| U102 | 2702h | h | USER P102 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U103 | 2703h | h | USER P103 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | $\bigcirc$ |  |
| U104 | 2704h | h | USER P104 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 00 | O |  |
| U105 | 2705h | h | USER P105 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | O | 0 | $\bigcirc$ |  |
| U106 | 2706h | h | USER P106 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | 0 | 5 | $\bigcirc$ | 00 | $\bigcirc$ |  |
| U107 | 2707h | h | USER P107 | 0 | -32768 to 32767 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |


|  | Communication $s$ address |  | Name | Dir | Data setting range |  |  | $\left\|\begin{array}{l} \text { O} \\ \cdot \stackrel{c}{\lambda} \\ 00 \\ 0 \\ 0 \\ \tilde{0} \\ 0 \\ 0 \end{array}\right\|$ |  |  | Control method: Enable/ Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 485 \\ & \text { No. } \end{aligned}$ | Link No. |  |  |  |  |  |  |  |  | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | L | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}$ | S |  |
| U108 | 2708h | h | USER P108 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U109 | 2709h | h | USER P109 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U110 | 270Ah | h | USER P110 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U111 | 270Bh | h | USER P111 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| U112 | 270Ch | h | USER P112 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U113 | 270Dh | h | USER P113 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U114 | 270Eh | h | USER P114 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | 0 | 0 |  |
| U115 | 270Fh | h | USER P115 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U116 | 2710h | h | USER P116 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | 0 | O |  |
| U117 | 2711h | h | USER P117 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U118 | 2712h | h | USER P118 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U119 | 2713h | h | USER P119 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U120 | 2714h | h | USER P120 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U121 | 2715h | h | USER P121 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U122 | 2716h | h | USER P122 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U123 | 2717h | h | USER P123 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U124 | 2718h | h | USER P124 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| U125 | 2719h | h | USER P125 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U126 | 271Ah | h | USER P126 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U127 | 271Bh | h | USER P127 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| U128 | 271Ch | h | USER P128 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U129 | 271Dh | h | USER P129 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U130 | 271Eh | h | USER P130 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | 0 | 0 |  |
| U131 | 271Fh | h | USER P131 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U132 | 2720h | h | USER P132 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U133 | 2721h | h | USER P133 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | O | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U134 | 2722h | h | USER P134 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U135 | 2723h | h | USER P135 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | 0 | 0 |  |
| U136 | 2724h | h | USER P136 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ | 0 |  |
| U137 | 2725h | h | USER P137 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ | O |  |
| U138 | 2726h | h | USER P138 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 |  |
| U139 | 2727h | h | USER P139 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U140 | 2728h | h | USER P140 | 0 | -32768 to 32767 | 0 | 0 | 0 | O | 5 | 0 | 0 | $\bigcirc$ | 0 |  |
| U141 | 2729h | h | USER P141 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 |  |
| U142 | 272Ah | h | USER P142 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 |  |
| U143 | 272Bh | h | USER P143 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 |  |
| U144 | 272Ch | h | USER P144 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ | O |  |
| U145 | 272Dh | h | USER P145 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U146 | 272Eh | h | USER P146 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | 0 | $\bigcirc$ | 0 |  |
| U147 | 272Fh | h | USER P147 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| U148 | 2730h | h | USER P148 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | 0 | 5 | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| U149 | 2731h | h | USER P149 | 0 | -32768 to 32767 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 |  |
| U150 | 2732h | h | USER P150 | 0 | -32768 to 32767 | $\bigcirc$ | 0 | 0 | O | 5 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |

## ■ Safety functions (SF: Safety Functions)

|  | $\underset{\text { address }}{C o m m u n i c a t i o n s ~}$ address |  | Name | Dir | Data setting range |  |  |  | - |  | Control method: Enable/ Disable |  |  |  | $\stackrel{\text { ® }}{\stackrel{\text { ® }}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 485 \\ & \text { No. } \end{aligned}$ | Link No. |  |  |  |  |  |  |  |  | $\left.\begin{array}{\|l\|} \hline \mathrm{P} \\ \mathrm{G} \end{array} \right\rvert\,$ | $\begin{array}{\|l\|l} \mathrm{L} \\ \mathrm{E} \\ \mathrm{~S} \end{array}$ | $\begin{aligned} & V \\ & F \end{aligned}$ | S |  |
| SF00 | 2800h | h | Password state monitor | 0 | 0 or 1 <br> 0: Locked <br> 1: Unlocked | $\times$ | 0 | $\times$ | $\times$ | 0 | $\bigcirc$ | O | - | $\bigcirc$ |  |
| SF01 | 2801h | h | SS1 Level | 0 | 30 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 150 | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| SF02 | 2802h | h | SS1 Timer | 0 | $\begin{array}{\|l\|} \hline 0.01 \text { to } 99.9 \mathrm{~s} \\ 100.0 \text { to } 999.9 \mathrm{~s} \\ 1000 \text { to } 3600 \mathrm{~s} \end{array}$ | $\times$ | 10.00 | $\times$ | $\times$ | 13 | $\bigcirc$ | - | - | $\bigcirc$ |  |
| SF03 | 2803h | h | SS1/SLS Deceleration time | 0 | $\begin{aligned} & 0.01 \text { to } 99.9 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 1000 \text { to } 3600 \mathrm{~s} \end{aligned}$ | $\times$ | 5.00 | $\times$ | $\times$ | 13 | - | O | O | $\bigcirc$ |  |
| SF04 | 2804h | h | SLS Level | 0 | 30 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 300 | $\times$ | $\times$ | 0 | 0 | O | - | O |  |
| SF05 | 2805h | h | SLS Timer | 0 | $\begin{aligned} & 0.01 \text { to } 99.9 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 1000 \text { to } 3600 \mathrm{~s} \end{aligned}$ | $\times$ | 10.00 | $\times$ | $\times$ | 13 | 0 | - | - | $\bigcirc$ |  |
| SF06 | 2806h | h | SS1/SLS Upper limit value | 0 | 0 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 300 | $\times$ | $\times$ | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ |  |
| SF07 | 2807h | h | Motor maximum speed | 0 | 50 to $30000 \mathrm{r} / \mathrm{min}$ | $\times$ | 1500 | $\times$ | $\times$ | 0 | 0 | $\bigcirc$ | - | $\bigcirc$ |  |
| SF08 | 2808h | h | Upper limit monitor wait time | 0 | $\begin{aligned} & 0.01 \text { to } 99.9 \mathrm{~s} \\ & 100.0 \text { to } 999.9 \mathrm{~s} \\ & 1000 \text { to } 3600 \mathrm{~s} \end{aligned}$ | $\times$ | 0.00 | $\times$ | $\times$ | 13 | 0 | - | $\bigcirc$ | $\bigcirc$ |  |
| SF09 | 2809h | h | PG Breakdown detection | 0 | 0 to 1 <br> 0: Disable <br> 1: Enable | $\times$ | 1 | $\times$ | $\times$ | 68 | 0 | O | 0 | O |  |
| SF10 | 280Ah | h | PG Pulse resolution | 0 | 100 to 60000 | $\times$ | 1024 | $\times$ | $\times$ | 0 | O | O | - | O |  |
| SF11 | 280Bh | h | Speed detection filter | 0 | 0.000 to 0.100 s | $\times$ | 0.010 | $\times$ | $\times$ | 4 | 0 | O | $\bigcirc$ | O |  |
| SF12 | 280Ch | h | STO Diagnosis early warning time | 0 | 0.0 to 1.0 s | $\times$ | 0.0 | $\times$ | $\times$ | 2 | 0 | O | $\bigcirc$ | O |  |
| SF20 | 2814h | h | Terminal [SL1]/[SL2] function selection | 0 | 0 to 2  <br> 0:  <br> 1: So function <br> 2:  <br> 2: SLS function | $\times$ | 0 | $\times$ | $\times$ | 219 | 0 | - | $\bigcirc$ | $\bigcirc$ |  |
| SF21 | 2815h | h | SS1 Stop mode | 0 | 0 to 1 <br> 0: Speed monitoring <br> 1: Time monitoring | $\times$ | 1 | $\times$ | $\times$ | 220 | 0 | $\bigcirc$ | O | $\bigcirc$ |  |
| SF22 | 2816h | h | Encoder selection | 0 | 0 to 2 <br> 0: Recommended PG or PG-less <br> 1: Recommended 15 V encoder <br> 2: Non-recommended 12 V encoder | $\times$ | 0 | $\times$ | $\times$ | 221 | 0 | 0 | - | $\bigcirc$ |  |
| SF23 | 2817h | h | Fault reaction selection | 0 | 0 to 1 o: STO (SBC operation when SBC is enabled) 1: SS1 | $\times$ | 0 | $\times$ | $\times$ | 222 | 0 | - | - | $\bigcirc$ |  |
| SF24 | 2818h | h | SBC Function selection | 0 | 0 to 2 <br> 0: Disable <br> 1: Enable - via safety relay <br> 2: Enable - brake direct connection | $\times$ | 0 | $\times$ | $\times$ | 224 | 0 | O | $\bigcirc$ | O |  |
| SF25 | 2819h | h | SS1 Error processing selection | 0 | 0 to 1 <br> 0: Fault reaction selection <br> 1: Light alarm selection | $\times$ | 0 | $\times$ | $\times$ | 227 | 0 | 0 | - | $\bigcirc$ |  |
| SF26 | 281Ah | h | SLS Deceleration error processing selection | 0 | 0 to 1 <br> 0: Fault reaction selection <br> 1: Light alarm selection | $\times$ | 0 | $\times$ | $\times$ | 223 | 0 | O | - | $\bigcirc$ |  |
| SF27 | 281Bh | h | SLS Upper limit error processing selection | 0 | 0 to 1 <br> 0: Fault reaction selection <br> 1: Light alarm selection | $\times$ | 0 | $\times$ | $\times$ | 223 | 0 | - | $\bigcirc$ | $\bigcirc$ |  |
| SF28 | 281Ch | h | Full save of safety parameters | 0 | $\begin{array}{\|l\|} \hline 0 \text { to } 1 \\ \text { 0: Do not save } \\ \text { 1: Save all (auto-reset to 0) } \\ \hline \end{array}$ | $\times$ | 0 | $\times$ | * | 0 | 0 | O | - | O |  |
| SF30 | 281Eh | h | Safety related password authentication 1 | 0 | 0000 to FFFF | $\times$ | 0 | $\times$ | $\times$ | 9 | 0 | O | $\bigcirc$ | $\bigcirc$ |  |
| SF31 | 281Fh | H | Safety related password authentication 2 | 0 | 0000 to FFFF | $\times$ | 0 | $\times$ | $\times$ | 9 | 0 | O | - | $\bigcirc$ |  |

(1*) Functions SF01 to SF31 are available when the ROM version is $\mathrm{H} 1 / 20020$ or later.

## Command functions (S: Serial Communication Functions)

|  | Communications address |  | Name | Dir | Data setting range |  |  | $\begin{aligned} & 0 \\ & . ㄷ ㅡ ㅇ ~ \end{aligned}$ | . | $\begin{aligned} & \text { ㄷㅡㅠ } \\ & \text { Non } \end{aligned}$ | Control method: <br> Enable/ <br> Disable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  | $\left\|\begin{array}{c} \frac{\pi}{0} \\ 0 \\ 0 \end{array}\right\|$ | 雨 | $\begin{aligned} & \text { N } \\ & \frac{\pi}{U} \end{aligned}$ |  | $\begin{aligned} & \mathrm{L} \\ & \mathrm{E} \\ & \mathrm{~S} \end{aligned}$ | $\left\lvert\, \begin{aligned} & \mathrm{V} \\ & \mathrm{~F} \end{aligned}\right.$ | $\begin{aligned} & \mathrm{S} \\ & \mathrm{M} \end{aligned}$ |  |
| S01 | 701h | 1h | Frequency/Speed command (Setting 1) | 7 | -20000 to 20000 : (data)*Nmax/20000 r/min | 0 | - | $\times$ | $\times$ | 5 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| S02 | 702h | 2h | Torque command | 1 | -327.68 to 327.67\% : 0.01\%/1d | 0 | - | $\times$ | $\times$ | 7 | 0 | 0 | $\times$ | 0 |  |
| S03 | 703h | 3h | Torque current command | 1 | -327.68 to 327.67\% : 0.01\%/1d | 0 | - | $\times$ | $\times$ | 7 | 0 | $\bigcirc$ | $\times$ | 0 |  |
| S04 | 704h | 4h | Magnetic-flux command | 1 | -327.68 to 327.67\% : 0.01\%/1d | 0 | - | $\times$ | $\times$ | 7 | 0 | $\times$ | $\times$ | $\times$ |  |
| S05 | 705h | 5h | Orientation position command | 1 | 0000 to FFFF | 0 | - | $\times$ | $\times$ | 9 | 0 | $\times$ | $\times$ | O |  |
| S06 | 706h | 6h | Run command 1 | 1 | 0000 to FFFF | 0 | - | $\times$ | $\times$ | 32 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| S07 | 707h | 7h | Universal Do | 1 | 0000 to FFFF | 0 | - | $\times$ | $\times$ | 33 | 0 | $\bigcirc$ | $\bigcirc$ | O |  |
| S08 | 708h | 8h | Acceleration time | 2 | 0.0 to 3600.0 s | 0 | - | $\times$ | $\times$ | 2 | 0 | $\bigcirc$ | 0 | 0 |  |
| S09 | 709h | 9h | Deceleration time | 1 | 0.0 to 3600.0 s | 0 | - | $\times$ | $\times$ | 2 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| S10 | 70Ah | Ah | Torque limiter level 1 | 2 | -327.68 to 327.67\% : 0.01\%/1d | 0 | - | $\times$ | $\times$ | 7 | 0 | $\bigcirc$ | $\times$ | O |  |
| S11 | 70Bh | Bh | Torque limiter level 2 | 1 | -327.68 to 327.67\% : 0.01\%/1d | $\bigcirc$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $\bigcirc$ | $\times$ | 0 |  |
| S12 | 70Ch | Ch | Run command 2 | 0 | 0000 to FFFF | $\bigcirc$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | O |  |
| S13 | 70Dh | h | Universal Ao | 0 | -16384 to 16384 (-10 V to +10 V) | 0 | - | $\times$ | $\times$ | 5 | 0 | $\bigcirc$ | 0 | 0 |  |
| S16 | 710h | h | General purpose setting 1 (To be supported soon) | 2 | -32768 to 32767 Assign functions using E90. | $\bigcirc$ | - | $\times$ | $\times$ | 5 | 0 | $\bigcirc$ | 0 | O |  |
| S17 | 711h | h | General purpose setting 2 (To be supported soon) | 1 | - 32768 to 32767 Assign functions using E91. | 0 | - | $\times$ | $\times$ | 5 | 0 | 0 | O | 0 |  |

## - Monitor data functions (M: Monitor Functions)

|  | Communications address |  | Name | Dir | Data setting range |  |  | $\left.\begin{array}{\|c} 0 \\ .0 \\ \vdots 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array} \right\rvert\,$ |  | 든0.040000 | Control method: Enable/ Disable |  |  |  | $\xrightarrow{\stackrel{n}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | 豆 |  | $\mathrm{P}$ | L  <br> E V <br> S F |  | S |  |
| M01 | 801h | Fh | Speed setting 4 (ASR input) | 15 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc 0$ |  | 0 |  |
| M02 | 802h | 10h | Torque command value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M03 | 803h | 11h | Torque current command value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 |  | 0 |  |
| M04 | 804h | 12h | Magnetic-flux command value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $\bigcirc$ |  | $\times$ |  |
| M05 | 805h | 13h | Output frequency command value | 1 | 0.1Hz/1d | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | $\bigcirc 0$ |  | 0 |  |
| M06 | 806h | 14h | Detected speed value | 1 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc \times$ |  | - |  |
| M07 | 807h | 15h | Calculated torque value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | O | $\bigcirc$ |  | O |  |
| M08 | 808h | 16h | Calculated torque current value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 |  | 0 |  |
| M09 | 809h | 17h | Output frequency | 1 | $0.1 \mathrm{~Hz} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |  |
| M10 | 80Ah | 18h | Motor output | 1 | 0.1 kW/1d | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M11 | 80Bh | 19h | Effective output current value | 1 | 0.1 A/1d | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | $\bigcirc$ |  | - |  |
| M12 | 80Ch | 1Ah | Effective output voltage value | 1 | $0.1 \mathrm{~V} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | 0 |  | 0 |  |
| M13 | 80Dh | 1Bh | Run command (Final run command) | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 32 | $\bigcirc$ | 0 |  | 0 |  |
| M14 | 80Eh | 1Ch | Running Status | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 21 | $\bigcirc$ | 0 |  | 0 |  |
| M15 | 80Fh | 1Dh | Output terminals Y1 to Y18 | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 33 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M16 | 810h | 1Eh | Latest alarm data (Multiple alarm, trip cause) | 4 | 0000 to 5540 | $\times$ | - | $\times$ | $\times$ | 14 | $\bigcirc$ | 0 O |  | $\bigcirc$ |  |
| M17 | 811h | 1Fh | Latest alarm history | 1 | 0000 to FF40 | $\times$ | - | $\times$ | $\times$ | 15 | $\bigcirc$ | 0 |  | O |  |
| M18 | 812h | 20h | 1st last alarm history | 1 | 0000 to FF40 | $\times$ | - | $\times$ | $\times$ | 15 | $\bigcirc$ | 0 |  | 0 |  |
| M19 | 813h | 21h | 2nd last alarm history | 1 | 0000 to FF40 | $\times$ | - | $\times$ | $\times$ | 15 | O | O 0 |  | O |  |
| M20 | 814h | 22h | Cumulative run time | 7 | 0 to 65535 h | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 |  | 0 |  |
| M21 | 815h | 23h | DC link bus voltage | 1 | $1 \mathrm{~V} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |  |
| M22 | 816h | 24h | Motor temperature | 1 | $1^{\circ} \mathrm{C} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M23 | 817h | 25h | Model code | 1 | 0000 to FFFF 200 V series: 1313 h 400 V series: 1314 h | $\times$ | - | $\times$ | $\times$ | 29 | $\bigcirc$ | $\bigcirc$ |  | 0 |  |
| M24 | 818h | 26h | Capacity code | 1 | 0 to 34 | $\times$ | - | ${ }^{\times}$ | $\times$ | 28 | $\bigcirc$ | 0 |  | 0 |  |
| M25 | 819h | 27h | Inverter ROM <br> (Main control) version | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | 0 | O 0 |  | 0 |  |
| M26 | 81Ah | 28h | Communications error code | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 34 | 0 | 0 |  | 0 |  |
| M27 | 81Bh | 29h | Alarm (Latest) Speed command value | 19 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ |  | 0 |  |
| M28 | 81Ch | 2Ah | Alarm (Latest) Torque command value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | 0 | $0 \times$ |  | 0 |  |
| M29 | 81Dh | 2Bh | $\begin{array}{\|l\|} \hline \text { Alarm (Latest) } \\ \text { Torque current command value } \\ \hline \end{array}$ | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $0 \times$ |  | $\bigcirc$ |  |
| M30 | 81Eh | 2Ch | Alarm (Latest) <br> Magnetic-flux command value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | O | $0 \times$ |  | $\times$ |  |
| M31 | 81Fh | 2Dh | $\begin{aligned} & \text { Alarm (Latest) } \\ & \text { Output frequency command value } \end{aligned}$ | 1 | $0.1 \mathrm{~Hz} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 2 | 0 | 0 O |  | $\bigcirc$ |  |
| M32 | 820h | 2Eh | Alarm (Latest) Detected speed value | 1 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | 0 | $0 \times$ |  | 0 |  |
| M33 | 821h | 2 Fh | Alarm (Latest) Calculated torque value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 O |  | $\bigcirc$ |  |
| M34 | 822h | 30h | Alarm (Latest) Calculated torque current value | 1 | 0.01\%/1d | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 O |  | $\bigcirc$ |  |
| M35 | 823h | 31h | Alarm (Latest) Output frequency | 1 | $0.1 \mathrm{~Hz} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | 0 O |  | $\bigcirc$ |  |
| M36 | 824h | 32h | Alarm (Latest) Motor output | 1 | 0.1 kW/1d | $\times$ | - | $\times$ | $\times$ | 2 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M 37 | 825h | 33h | Alarm (Latest) <br> Effective output current value | 1 | 0.1 A/1d | $\times$ | - | $\times$ | $\times$ | 2 | 0 | 0 O |  | 0 |  |
| M38 | 826h | 34h | Alarm (Latest) <br> Effective output voltage value | 1 | 0.1 V/1d | $\times$ | - | * | $\times$ | 2 | 0 | 0 |  | $\bigcirc$ |  |
| M39 | 827h | 35h | Alarm (Latest) Run command | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 32 | 0 | 0 O |  | 0 |  |
| M40 | 828h | 36h | Alarm (Latest) Running status | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 21 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M41 | 829h | 37h | Alarm (Latest) Output signals | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 33 | 0 | 0 O |  | 0 |  |
| M42 | 82Ah | 38h | Alarm (Latest) Cumulative run time | 1 | 0 to 65535 h | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 |  | 0 |  |
| M43 | 82Bh | 39h | Alarm (Latest) DC link bus voltage | 1 | $1 \mathrm{~V} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 |  | 0 |  |
| M44 | 82Ch | 3Ah | Alarm (Latest) Inverter internal temperature | 1 | $1^{\circ} \mathrm{C} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 |  | $\bigcirc$ |  |
| M45 | 82Dh | 3Bh | Alarm (Latest) Cooling fin temperature | 1 | $1^{\circ} \mathrm{C} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 5 | 0 | $\bigcirc$ |  | $\bigcirc$ |  |
| M46 | 82Eh | 3Ch | Capacity of main circuit capacitor | 3 | 0 to $100 \%$ | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 O |  | 0 |  |
| M47 | 82Fh | 3Dh | Service life of capacitor on PCB | 1 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | O | $\bigcirc$ |  | $\bigcirc$ |  |
| M48 | 830h | 3Eh | Cooling fan service life | 1 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 |  | 0 |  |
| M49 | 831h | 3 Fh | Speed setting 1 (before multistep speed command) | 3 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |  |
| M50 | 832h | 40h | Speed setting 2 (before calculation of acceleration/deceleration) | 1 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | 0 | 0 |  | 0 |  |
| M51 | 833h | 41h | Speed setting 3 (after speed limiting) | 1 | -32000 to 32000 : (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | 0 | 0 |  | 0 |  |
| M52 | 834h | 42h | Control output 1 | 3 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 125 | $\bigcirc$ | $\bigcirc$ |  | 0 |  |
| M53 | 835h | 43h | Control output 2 | 1 | 0000 to FFFF | ${ }^{\times}$ | - | $\times$ | $\times$ | 126 | $\bigcirc$ | $\bigcirc$ |  | 0 |  |
| M54 | 836h | 44h | Control output 3 | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 127 | $\bigcirc$ | $\bigcirc$ |  | 0 |  |


| $\begin{aligned} & \infty \\ & 0 . \\ & 0 . \\ & 0 \\ & .0 \\ & \hline 0 \\ & \vdots \\ & \vdots \end{aligned}$ | Communications address |  | Name | Dir | Data setting range |  |  | $\begin{aligned} & 0 \\ & \hline 0 \\ & 0.0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  | Control method: Enable/ Disable |  |  |  | $\xrightarrow{\stackrel{n}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | $\left\lvert\, \begin{aligned} & \mathrm{L} \\ & \mathrm{E} \\ & \mathrm{~S} \end{aligned}\right.$ | $\begin{gathered} V \\ F \end{gathered}$ | S |  |
| M55 | 837h | 45h | Option monitor 1 | 6 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | 0 | 0 | 0 |  |
| M56 | 838h | 46h | Option monitor 2 | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| M57 | 839h | 47h | Option monitor 3 | 1 | 0 to 65535 | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| M58 | 83Ah | 48h | Option monitor 4 | 1 | 0 to 65535 | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | 0 | 0 |  |
| M59 | 83Bh | 49h | Option monitor 5 | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| M60 | 83Ch | 4Ah | Option monitor 6 | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | O | 0 | O | O |  |
| M61 | 83Dh | h | Current date, Year/Month | 3 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Year, Lower 2 digits: Month | $\times$ | - | $\times$ | $\times$ | 143 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| M62 | 83Eh | h | Current date, Day/Hour | 1 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Day, Lower 2 digits: Hour | $\times$ | - | $\times$ | $\times$ | 144 | $\bigcirc$ | 0 | O | - |  |
| M63 | 83Fh | h | Current date, Minute/Second | 1 | 0000 to FFFF <br> Upper 2 digits: Minute, Lower 2 digits: Second | $\times$ | - | $\times$ | $\times$ | 145 | $\bigcirc$ | 0 | - | - |  |
| M64 | 840h | h | Date of occurrence of (Latest) alarm, Year/Month | 3 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Year, Lower 2 digits: Month | $\times$ | - | $\times$ | $\times$ | 143 | $\bigcirc$ | 0 | - | 0 |  |
| M65 | 841h | h | Date of occurrence of (Latest) alarm, Day/Hour | 1 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Day, Lower 2 digits: Hour | $\times$ | - | $\times$ | $\times$ | 144 | O | 0 | 0 | 0 |  |
| M66 | 842h | h | Date of occurrence of (Latest) alarm, Minute/Second | 1 | 0000 to FFFF <br> Upper 2 digits: Minute, Lower 2 digits: Second | $\times$ | - | $\times$ | $\times$ | 145 | $\bigcirc$ | 0 | - | 0 |  |
| M67 | 843h | h | Date of removal of (Latest) alarm, Year/Month | 3 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Year, Lower 2 digits: Month | $\times$ | - | $\times$ | $\times$ | 143 | O | 0 | O | 0 |  |
| M68 | 844h | h | Date of removal of (Latest) alarm, Day/Hour | 1 | $0000 \text { to FFFF }$ <br> Upper 2 digits: Day, Lower 2 digits: Hour | $\times$ | - | $\times$ | $\times$ | 144 | $\bigcirc$ | 0 | - | 0 |  |
| M69 | 845h | h | Date of removal of (Latest) alarm, Minute/Second | 1 | 0000 to FFFF <br> Upper 2 digits: Minute, Lower 2 digits: Second | $\times$ | - | $\times$ | $\times$ | 145 | $\bigcirc$ | O 0 | - | 0 |  |
| M70 | 846h | h | (Latest) Alarm extension ID | 18 | 0 to 1 <br> 0 Occurred in local unit <br> 1: Occurred in other unit | $\times$ | - | $\times$ | $\times$ | 212 | $\bigcirc$ | 0 | - | 0 |  |
| M71 | 847h | h | (Latest) Multiple alarm, 2nd | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 14 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| M72 | 848h | h | (Latest) Multiple alarm, 3rd | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 14 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| M73 | 849h | h | (Latest) Multiple alarm, 4th | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 14 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | O |  |
| M74 | 84Ah | h | (Latest) Multiple alarm, 5th | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 14 | O | 0 | - | 0 |  |
| M75 | 84Bh | h | (Latest) Alarm, subcode | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | 0 | 0 | 0 |  |
| M76 | 84Ch | h | (Latest) Alarm, maximum speed | 1 | 0 to $65535 \mathrm{r} / \mathrm{min}$ | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| M77 | 84Dh | h | (Latest) Alarm, input power | 1 | 0.0 to 6553.5 kW | $\times$ | - | $\times$ | $\times$ | 2 | O | 0 | 0 | 0 |  |
| M78 | 84Eh | h | (Latest) Alarm, motor temperature | 1 | $1^{\circ} \mathrm{C} / 1 \mathrm{~d}$ | $\times$ | - | $\times$ | $\times$ | 5 | O | 00 | O | 0 |  |
| M79 | 84Fh | h | (Latest) Alarm, running status 2 (a) | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 141 | $\bigcirc$ | 0 | O | 0 |  |
| M80 | 850h | h | (Latest) Alarm, running status 2 (b) | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 142 | $\bigcirc$ | 0 | O | 0 |  |
| M81 | 851h | h | Alarm (Latest) <br> Run command (Communications link) | 1 | 0000 to FFFF | $\times$ | - | ${ }^{\times}$ | $\times$ | 32 | $\bigcirc$ | $\bigcirc 0$ | O | $\bigcirc$ |  |
| M82 | 852h | h | $\begin{array}{\|l\|} \hline \text { Alarm (Latest) } \\ \text { Run command } 2 \\ \text { (Communications link) } \\ \hline \end{array}$ | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | O | 0 | - | 0 |  |
| M83 | 853h | h | Alarm (Latest) For manufacturer | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ | 0 |  |
| M84 | 854h | h | Alarm (Latest) <br> M1 Number of startups | 1 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | O | O |  |
| M85 | 855h | h | Alarm (Latest) M2 Number of startups | 1 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | - | 0 |  |
| M86 | 856h | h | Alarm (Latest) M3 Number of startups | 1 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | O | 0 | O | 0 |  |
| M87 | 857h | h | Alarm (Latest) <br> EN terminal input | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 100 | O | 0 | - | 0 |  |
| M93 | 85Dh | h | Light alarm (Latest) | 4 | 0 to 255 | $\times$ | - | $\times$ | $\times$ | 102 | $\bigcirc$ | 0 | O | O |  |
| M94 | 85Eh | h | Light alarm (1st last) | 1 | 0 to 255 | $\times$ | - | $\times$ | $\times$ | 102 | O | 0 | O | 0 |  |
| M95 | 85Fh | h | Light alarm (2nd last) | 1 | 0 to 255 | $\times$ | - | $\times$ | $\times$ | 102 | $\bigcirc$ | 0 | O | 0 |  |
| M96 | 860h | h | Light alarm (3rd last) | 1 | 0 to 255 | $\times$ | - | $\times$ | $\times$ | 102 | $\bigcirc$ | 00 | $\bigcirc$ | 0 |  |
| M98 | 862h | h | EN terminal input | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 100 | $\bigcirc$ | 0 | $\bigcirc$ | O |  |
| M100 | 2900h | h | Effective parameter set condition | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | O | 0 | O | O |  |
| M101 | 2901h | h | Run command 2 (Communications link) | 0 | 0000 to FFFF <br> Monitors X terminal functions to be used exclusively via the communications link. | $\times$ | - | $\times$ | $\times$ | 32 | O | 0 | - | 0 |  |
| M102 | 2902h | h | Load factor | 0 | $\begin{array}{\|l\|} \hline-327.68 \text { to } 327.67 \% \\ \text { Motor load factor, Motor rated load/100\% } \\ \hline \end{array}$ | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 | O | O |  |
| M103 | 2903h | h | Input power | 0 | $\begin{array}{\|l\|} \hline 0.0 \text { to } 6553.5 \mathrm{~kW} \\ \text { Input power to inverter } \\ \hline \end{array}$ | $\times$ | - | $\times$ | $\times$ | 2 | O | 0 | 0 | 0 |  |
| M104 | 2904h | h | Running status 2(a) | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 141 | $\bigcirc$ | 0 | O | 0 |  |
| M105 | 2905h | h | Running status 2(b) | 0 | 0000 to FFFF | ${ }^{\times}$ | - | $\times$ | $\times$ | 142 | $\bigcirc$ | 00 | - | 0 |  |
| M106 | 2906h | h | Detected load shaft speed value | 0 | -32000 to 32000 : (data)** $\mathrm{Nax} / 20000 \mathrm{r} / \mathrm{min}$ | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | - | 0 |  |
| M107 | 2907h | h | Detected line speed value | 0 | -32000 to 32000 : (data)**max/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | O | 0 |  |
| M108 | 2908h | h | PID command value | 0 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | 0 | - | 0 |  |
| M109 | 2909h | h | PID feedback amount | 0 | -327.68 to 327.67\% | $\times$ | - | $\times{ }^{\times}$ | $\times$ | 7 | $\bigcirc$ | 00 | - | 0 |  |
| M110 | 290Ah | h | PID output value | 0 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | O | 0 | - | 0 |  |
| M112 | 290Ch | h | Remaining allowance for M1 motor overload | 3 | $\begin{array}{\|l} \hline 0 \text { to 65535\% } \\ \text { When M112 = } 0 \text { (\%), the inverter issues OL1 alarm. } \\ \hline \end{array}$ | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | O | O |  |
| M113 | 290Dh | h | Remaining allowance for M2 motor overload | 1 | $\begin{array}{\|l} \hline 0 \text { to } 65535 \% \\ \text { When M113 = } 0 \text { (\%), the inverter issues OL2 alarm. } \\ \hline \end{array}$ | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | 0 | 0 | 0 |  |


|  | Communications address |  | Name | Dir | Data setting range |  |  |  |  |  | Control method: Enable/ Disable |  |  | $\stackrel{\text { ® }}{\stackrel{\text { L }}{\text { ¢ }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  | 号 |  | P | L | S |  |
| M114 | 290Eh | h | Remaining allowance for M3 motor overload | 1 | $\begin{array}{\|l} \hline 0 \text { to 65535\% } \\ \text { When M114 = } 0 \text { (\%), the inverter issues OL3 alarm. } \end{array}$ | $\times$ | - | $\times$ | $\times$ | 0 | O | 0 | $\bigcirc$ |  |
| M115 | 290Fh | h | Input watt-hour <br> * Invalid for use in stack type | 4 | $\begin{aligned} & 0.000 \text { to } 9999 \\ & 100 \mathrm{kWh} / 1.000 \mathrm{~d} \\ & \text { Limited at } 999900 \mathrm{kWh} . \end{aligned}$ | $\times$ | - | $\times$ | $\times$ | 101 | O | 0 | $\bigcirc$ |  |
| M116 | 2910h | h | Input watt-hour data <br> * Invalid for use in stack type | 1 | 0000 to 9999 <br> $100 \mathrm{kWh} / 1.000 \mathrm{~d}$ *Display coefficient <br> M115 "input watt-hour" x F84 "Display coefficient for input watt-hour data" <br> Specifying the electric rate per 100 kWh with F84 shows the input watt-hour data. | ${ }^{\times}$ | - | $\times$ | $\times$ | 101 | O | 0 | $\bigcirc$ |  |
| M117 | 2911h | h | Input watt-hour (Lower 16 bits) *Invalid for use in stack type | 1 | $(81920 \mathrm{~d} /$ unit $100 \%$ rating [ kW$] \times$ Cumulative time $[\mathrm{s}] \times 2^{\wedge}$ $(-16)$ | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| M118 | 2912h | h | Input watt-hour <br> (Upper 16 bits) <br> *Invalid for use in stack type | 1 | (81920d/unit 100\% rating) [kW] x Cumulative time [s] x 2^ (-32) | $\times$ | - | $\times$ | $\times$ | 9 | 0 | 0 | $\bigcirc$ |  |
| M119 | 2913h | h | Inverter internal temperature (Real-time value) | 2 | -32768 to $32767^{\circ} \mathrm{C}$ | $\times$ | - | $\times$ | $\times$ | 5 | O | $\bigcirc$ | $\bigcirc$ |  |
| M120 | 2914h | h | Cooling fin temperature (Real-time value) | 1 | -32768 to $32767^{\circ} \mathrm{C}$ | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| M121 | 2915h | h | Main circuit capacitor life (Elapsed time) | 0 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 | $\bigcirc$ |  |
| M123 | 2917h | h | M1 Number of startups | 3 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M124 | 2918h | h | M2 Number of startups | 1 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M125 | 2919h | h | M3 Number of startups | 1 | 0 to 65535 times | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M126 | 291Ah | h | M1 Cumulative motor run time | 3 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M127 | 291Bh | h | M2 Cumulative motor run time | 1 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M128 | 291Ch | h | M3 Cumulative motor run time | 1 | 0 to 65535 [10h] | $\times$ | - | $\times$ | $\times$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M129 | 291Dh | h | Run command (Communications link) | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 32 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M130 | 291 Eh | h | Torque bias | 0 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $\bigcirc \times$ | $\bigcirc$ |  |
| M131 | 291Fh | h | Magnetic pole position signal | 0 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\times$ | $\times \times$ | $\bigcirc$ |  |
| M132 | 2920h | h | Universal AO1 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| M133 | 2921n | h | Option AO1 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M134 | 2922h | h | Control input 1 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 133 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| M135 | 2923h | h | Control input 2 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 134 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M136 | 2924h | h | Control input 3 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 135 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M137 | 2925h | h | Control input 4 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 136 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M138 | 2926h | h | Control input 5 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 137 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M139 | 2927h | h | Control input 6 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 138 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M140 | 2928 | h | Control input 7 | 0 | 0000 to FFFF | ${ }^{\times}$ | - | $\times$ | $\times$ | 139 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| M141 | 2929h | h | Control input 8 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 140 | $\bigcirc$ | $\bigcirc$ | O |  |
| M142 | 292Ah | h | Control output 4 | 0 | 0000 to FFFF <br> (bit 0: E-SX bus tact synchronizing signal) | $\times$ | - | $\times$ | $\times$ | 128 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M143 | 292Bh | h | Control output 5 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 129 | O | 0 | $\bigcirc$ |  |
| M144 | 292Ch | h | Control output 6 | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 130 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M146 | 292Eh | h | Detected speed value 2 | 0 | -32000 to $32000 \mathrm{r} / \mathrm{min}$ | ${ }^{\times}$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc \times$ | $\bigcirc$ |  |
| M147 | 292Fh | h | Exciting current command | 0 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $\bigcirc \times$ | $\times$ |  |
| M148 | 2930h | h | Detected exciting current | 0 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | $\bigcirc$ | $\bigcirc \times$ | $\times$ |  |
| M149 | 2931h | h | Magnetic-flux calculation | 0 | 0.00 to 655.35\% | $\times$ | - | $\times$ | $\times$ | 3 | $\bigcirc$ | $\bigcirc \times$ | $\times$ |  |
| M161 | 293Dh | h | Ai adjustment value (12) | 5 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M162 | 293Eh | h | Ai adjustment value (Ai1) | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| M163 | 293Fh | h | Ai adjustment value (Ai2) | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M164 | 2940h | h | Ai adjustment value (Ai3) | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| M165 | 2941h | h | Ai adjustment value (Ai4) | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M166 | 2942h | h | Input signal (Terminal) | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 32 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| M167 | 2943h | h | Analog input signal (12) | 3 | -32768 to 32767 (-16384 to 16384: -10 V to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M168 | 2944h | h | Analog input signal (Ai1) | 1 | -32768 to 32767 (-16384 to 16384: -10 V to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | $\bigcirc$ |  |
| M169 | 2945h | h | Analog input signal (Ai2) | 1 | -32768 to $32767(-16384$ to 16384: -10 V to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M170 | 2946h | h | Analog output signal (Ao1) | 3 | -32768 to 32767 (-16384 to $16384:-10 \mathrm{~V}$ to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc \bigcirc$ | $\bigcirc$ |  |
| M171 | 2947h | h | Analog output signal (Ao2) | 1 | -32768 to $32767(-16384$ to 16384: -10 V to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc \bigcirc$ | $\bigcirc$ |  |
| M172 | 2948h | h | Analog output signal (Ao3) | 1 | -32768 to 32767 (-16384 to 16384: -10 V to +10 V ) | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M173 | 2949h | h | AIO Input/Output status 1 (Ai3) | 4 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M174 | 294Ah | h | AIO Input/Output status 1 (Ai4) | 1 | 32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M175 | 294Bh | h | AIO Input/Output status 2 (Ao4) | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M176 | 294Ch | h | AIO Input/Output status 2 (Ao5) | 1 | 32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | O |  |
| M177 | 294Dh | h | PG (SD) input pulse | 4 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M178 | 294Eh | h | PG (LD) input pulse | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M179 | 294Fh | h | PG (PR) input pulse | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M180 | 2950h | h | PG (PD) input pulse | 1 | -32768 to 32767 | $\times$ | - | $\times$ | $\times$ | 5 | 0 | $\bigcirc$ | $\bigcirc$ |  |
| M181 | 2951h | h | DIOA input status (Terminal) | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 146 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M182 | 2952h | h | DIOA input status (Via communications link) | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 146 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| M183 | 2953h | h | DIOB optional input status | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 26 | 0 | 0 | 0 |  |
| M184 | 2954h | h | DIOB optional output status | 0 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 27 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| M193 | 295Dh | h | General-purpose setting 1 monitor (To be supported soon) | 0 | -32768 to 32767 <br> Monitors the S16 setting value. | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | O |  |


|  | Communicationsaddress |  | Name | Dir | Data setting range |  |  | $\begin{aligned} & \text { O} \\ & . \frac{c}{~} \\ & 0 \\ & 0 \\ & 0 \\ & \frac{\pi}{0} \\ & 0 \end{aligned}$ |  |  | Control method: Enable/ Disable |  |  |  | $\stackrel{\text { n }}{\stackrel{\rightharpoonup}{\text { ® }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 485 No. | Link No. |  |  |  |  |  |  |  |  | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | L | V | S |  |
| M194 | 295Eh | h | General-purpose setting 1 monitor (To be supported soon) | 0 | $\text { -32768 to } 32767$ <br> Monitors the S 17 setting value. | $\times$ | - | $\times$ | $\times$ | 5 | $\bigcirc$ | 0 | O | O |  |
| M200 | 2A00h | h | Pulse-train position command monitor | 5 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | 0 | $\times$ | $\times$ | O |  |
| M201 | 2A01h | h | Detected position monitor | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | $\times$ | $\times$ | O |  |
| M202 | 2A02h | h | Detected position (Z-phase input) monitor | 1 | 0000 to FFFF | $\times$ | - | $\times$ | $\times$ | 9 | $\bigcirc$ | $\times$ | $\times$ | $\bigcirc$ |  |
| M220 | 2A14h | h | Load weighting speed limit | 3 | -32000 to 32000: (data)*Nmax/20000 r/min | $\times$ | - | $\times$ | $\times$ | 5 | 0 | 0 | $\times$ | 0 |  |
| M221 | 2A15h | h | Hoisting load calculation result monitor | 1 | 0 to 65535 kg | $\times$ | - | $\times$ | $\times$ | 0 | 0 | 0 | $\times$ | 0 |  |
| M222 | 2A16h | h | Travel torque calculation monitor | 1 | -327.68 to 327.67\% | $\times$ | - | $\times$ | $\times$ | 7 | 0 | 0 | $\times$ | O |  |

### 8.1.2 Control block diagrams

Refer to "4.1 Control block diagrams" in Chapter 4 of the separate volume "Unit Type Function Code Edition" (24A7-■-0019).

### 8.1.3 Function code details

Refer to "4.3 Function code details" in Chapter 4 of separate volume "Unit Type Function Code Edition" (24A7- $\square$-0019).

### 8.2 Keypad and test run

### 8.2.1 Operating from the keypad

Refer to "3.4 Operating from the keypad" in Chapter 3 of separate volume "Unit Type Function Code Edition" (24A7-■-0019).

### 8.2.2 Trial operation procedures

Refer to "3.5 Trial operation procedures" in Chapter 3 separate volume "Unit Type Function Code Edition" (24A7- $\square-0019$ ).

### 8.3 Using standard RS-485

### 8.3.1 Standard RS-485 communication port

Refer to " 5.1 Standard RS-485 communication port" in Chapter 5 of the separate volume "Option Edition" (24A7- $\square$-0045).

### 8.3.2 Fuji general purpose communication

Refer to "5.2 Fuji general purpose communication" in Chapter 5 of the separate volume "Option Edition" (24A7- $\square-0045$ ).

### 8.3.3 Modbus RTU

Refer to "5.3 Modbus RTU" in Chapter 5 of the separate volume "Option Edition" (24A7- $\square$-0045).

### 8.4 FRENIC-VG Loader (Free version)

Refer to the separate volume "FRENIC-VG Loader (Free version) Instruction Manual (INR-SI47-1588*)".

### 8.5 Control options

Refer to Chapter 6 "Control Options" of the separate volume "Option Edition" (24A7- $\square$-0045).

## FRENIC-VG

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### 9.1 Guidance for capacity selection

### 9.1.1 Selection of capacity for motor and inverter

### 9.1.1.1 Output torque characteristics

Figure 9.1-1 shows the output torque characteristics for the motor dedicated to FRENIC-VG. The characteristics are shown in the following quadrants according to speed and torque polarity.
(Speed) (Torque)

- Quadrant 1: + + $\cdot \bullet$ Normal rotation drive
- Quadrant 2: - + •••Reverse braking
- Quadrant 3: - - •••Reverse rotation drive
- Quadrant 4: + - •••Normal rotation braking

Speed: $100 \%$ at motor base speed Torque: $100 \%$ at continuous rated torque


Figure 9.1-1: Output torque characteristics (MD specification)

## (1) Consecutively allowable torque Curve [a] of quadrants 1 and 3

Curve (a) shows the torque which can be consecutively output in drive mode. When the speed is under base speed $(100 \%)$ in the speed control range ( 0 to $200 \%$ ), rated output torque ( $100 \%$ ) can be output. When speed is over base speed $(100 \%)$, the constant output characteristic curve applies and the torque becomes inversely proportional, decreasing in magnitude.
Especially in "very low speed under speed control range," the allowable torque decreases due to restrictions imposed by the temperature rise inside the inverter. The value is $80 \%$ using inverter output frequency conversion at under 0.1 Hz . When operating the induction motor at under 0.1 Hz , consecutive operation is possible at under 0.1 Hz if the slipping is taken into account. When operating the synchronous motor at under 0.1 Hz , the operation must consider the decrease in torque because the speed is synchronized.

## (2) Short duration maximum braking torque Curve [b] of quadrants 1 and 3

Curve (b) shows the allowable output torque for short durations (60s) in drive mode and is generally used in acceleration and deceleration. The magnitude can be $150 \%$ of the consecutive rated torque.
Especially in "very low speed under speed control range," the allowable torque decreases due to the restrictions imposed by the temperature rise inside the inverter. The value is $100 \%$ when using inverter output frequency conversion at under 0.1 Hz .

## (3) Starting torque near zero speed of quadrants 1 and 3

The torque near zero speed in quadrants 1 and 3 is the starting torque. The consecutive output torque is $80 \%$, but the starting activity passes through the very slow speed range in a short duration under 30 s, so the starting torque is $150 \%$.

## (4) Braking torque quadrants 2 and 4

Quadrants 2 and 4 show the range of "braking mode." Curve (c) shows the braking torque which can be output in the consecutive rated current range of the inverter, and curve (d) shows the braking torque which can be output by the 60s rated current. The decrease of the output torque ( $80 \%$ ) in the very slow speed range is the same as in the case of drive mode.
The time rating of the braking torque is determined by the other dominating condition. As the mechanical energy is regenerated in braking mode, the time rating of the "braking resistor" or the "braking resistance unit" becomes critical.
The time rating of the braking resistor is described in this manual or the catalog as allowance (kW) from the perspective of typical electrical discharge loss and the allowance (kWs) from the perspective of discharge withstand current rating.

Red Refer to Chapter 6 " 6.5 Braking system (braking unit, braking resistor)" for braking-related values when the combination of the braking units and braking resistors is standard.

### 9.1.1.2 Procedures for capacity selection

Figure 9.1-2 Procedures for capacity selection (flowchart) shows a typical procedure for selecting capacity. The steps numbered from (1) to (5) in the flowchart are described in detail on the following pages.

Capacity can be selected easily when restrictions to acceleration and deceleration time are not applied in the selection. The procedure becomes slightly complicated when "a constant restriction is applied to acceleration and deceleration time" or when "acceleration and deceleration are performed frequently."


Figure 9.1-2: Procedures for capacity selection

## (1) Load torque calculation for rated operation (Refer to Section 9.1.2.1 for calculation details)

"Load torque for steady operation" is the converted motor axis torque required to rotate the load at a constant rotation speed. This is calculated considering the reduction gear efficiency ( $\eta \mathrm{G})$.
"Load torque at constant speed operation" in drive mode $=\frac{\text { Actual load torque } \tau_{\mathrm{L}}}{\text { Reduction gear efficiency } \eta_{\mathrm{G}}}$
"Load torque at constant speed operation" in braking mode $=$ Actual load torque $\tau_{L} \times$ Reduction gear efficiency $\eta_{G}$
This calculation must be performed when selecting the capacity for any load.
The load torque at constant speed operation is calculated, and the capacity is temporarily selected such that the motor's consecutive rated torque exceeds this value. Capacity without excess can be selected when the motor's rated rotation speed (especially the base speed) is matched to the load's rated rotation speed (base speed). To match this rated rotation speed, appropriate "transmission gear ratio" and "number of motor poles" must be selected.

When restrictions are not applied to acceleration and deceleration times and the load is not for elevators, the previously mentioned temporary capacity should be used.

## (2) Calculation of the acceleration time (Refer to Section 9.1.2.2 for calculation details)

When a constant requirement is imposed on acceleration time, this calculation is performed. The calculation is performed according to the following procedure.

1) Calculate the load and the motor "Moment of inertia."

If the moment of inertia is large, acceleration becomes difficult, requiring longer acceleration time. Calculate the "load moment of Inertia" referring to "9.1.2.2 Calculation of acceleration and deceleration time." Refer to the motor catalog for the "motor moment of inertia."
2) Calculate the "Minimum acceleration torque." (See Figure 9.1-3)

The difference between the one minute rated value for "9.1.1.1 (2) Short Duration Maximum Drive Torque" and the "Load torque for constant speed operation" calculated above in (1) is the "acceleration torque." Seek the value which minimizes this "acceleration torque" throughout the entire operation pattern with varying speed.
Exercise caution as the torque decreases inversely proportional to speed at speed exceeding the motor rated rotation speed.


Figure 9.1-3: Example of minimizing acceleration torque
3) Calculate the "Acceleration time."

Substitute the above value into equation (9.1.2-15) in "9.1.2.2
Calculation of acceleration and deceleration time" to compute the acceleration time.
When the acceleration time does not satisfy the requirement, increase the capacity of the inverter and the motor by one rank and perform the calculation again.

## (3) Calculation of the deceleration time (Refer to Section 9.1.2.2 for calculation details)

Calculate the deceleration time as in the case of acceleration time by researching the deceleration torque characteristics of the motor throughout the entire range of varying speed.

1) Calculate the "Moment of inertia" of the load and the motor.

This is the same as in the case of acceleration time. When the moment of inertia is large, the deceleration time increases.
2) Calculate the "Minimum deceleration torque." (Refer to Figure 9.1-4 and Figure 9.1-5)

When the load torque is positive, see Figure 9.1-4.
When the load torque is negative in cases such as the braking load in elevators, see Figure 9.1-5. Exercise caution in this case as the minimum deceleration torque is decreased due to the regeneration activity.


Figure 9.1-4: Example of minimizing deceleration torque (1)


Figure 9.1-5: Example of minimizing deceleration torque (2)

## 3) Calculate the "Deceleration time."

As in the case of acceleration time, substitute the above value into equation (9.1.2-16) to calculate the deceleration time. When the deceleration time does not satisfy the requirement, increase the capacity of the inverter and motor by one rank and perform the calculation again.

## (4) Review of the braking resistor rating (Refer to Section 9.3.3.1 for calculation details)

Review of the braking resistor rating can be divided into two types depending on the repeat period of the braking.

1) Repeat period is under 100 s
2) Repeat period is over 100 s

Calculate the average loss and review the value.
The allowable braking energy is determined by the maximum regenerated capacity at braking. Chapter 6 " 6.5 Braking system (braking unit, braking resistor)" shows the list of allowances.
(5) Calculation of the motor RMS rating (refer to Section 9.1.2.3 for calculation details)

In metalworking machineries or conveying equipment which require positioning control, operation is repeated at high frequency in short duration rating conditions.
In these cases, calculate the maximum equivalent RMS current (actual current) and confirm that this value is within the tolerance (rated current value) of the motor.

## Precautions in reviewing capacity

When driving the FRENIC-VG exclusive motor, select the capacity such that the mean-square value of the torque is below $100 \%$ of the rated torque.
When driving general-purpose motors, select the capacity such that the mean-square value of the current, which takes into account the motor cooling efficiency, is less than the motor rated current. Select the inverter such that the mean-square value of the current is less than the inverter rated current value.

### 9.1.2 Equation for capacity selection

### 9.1.2.1 Calculation of load torque for rated operation

## (1) General equation

The details of the torque calculation method will be explained for cases where the motor drives a load which moves linearly.
When the force required to move a linear motion object at constant velocity $V[\mathrm{~m} / \mathrm{s}]$ is $\mathrm{F}[\mathrm{N}]$ and the motor speed driving this is $\mathrm{Nm}[\mathrm{r} / \mathrm{min}]$, the required motor output torque $\tau \mathrm{M}[\mathrm{N} \cdot \mathrm{m}]$ is defined by the following equation (9.1.2-1).

$$
\tau_{M}=\frac{60}{2 \pi \cdot N_{M}} \cdot \frac{F}{\eta_{G}}[N \cdot m] \quad \cdots \quad(9.1 .2-1)
$$

$\eta \mathrm{G}: \quad$ transmission efficiency
When the motor is in braking mode, the efficiency operates in the reverse direction. In this case, the required motor torque $\tau \mathrm{M}[\mathrm{N} \cdot \mathrm{m}]$ changes as described in equation (9.1.2-2).

$$
\tau_{M}=\frac{60 \cdot v}{2 \pi \cdot N_{M}} \cdot F \cdot \eta_{\mathrm{G}} \quad[N \cdot m] \quad \cdots \quad(9.1 .2-2)
$$

The expression $(60 \cdot V) /(2 \pi \cdot N m)$ is the equivalent rotation radius corresponding to the motor axis rotation speed $V$ [ $\mathrm{m} / \mathrm{s}]$. Additionally, the $\mathrm{F}[\mathrm{N}]$ in this general equation changes as follows depending on the type of load.

## (2) Approach for handling the required force $F$

## - Case of horizontal transport load

For simplicity, assume the physical configuration for horizontal transport as shown in Figure 9.1-6. If the table mass is WO [kg], payload is W [kg], and the coefficient of friction is $\mu$, then the frictional force $\mathrm{F}[\mathrm{N}]$ can be expressed by the equation (9.1.2-3).
This frictional force is the force required to drive the horizontal transport load.


Figure 9.1-6: General diagram of horizontal transport load

$$
F=(W o+W) \cdot g \cdot \mu[N] \quad \cdots \quad(9.1 .2-3)
$$

g: gravitational acceleration ( $\approx 9.8\left(\mathrm{~m} / \mathrm{s}^{2}\right)$ )
Therefore, the driving torque $\tau \mathrm{M}[\mathrm{N} \cdot \mathrm{m}]$ at the motor axis can be expressed as in equation (9.1.2-4).

$$
\tau_{M}=\frac{60 \cdot v}{2 \pi \cdot N_{M}} \cdot \frac{(W o+W) \cdot g \cdot \mu}{\eta_{G}}[N \cdot m] \quad \cdots \quad(9.1 .2-4)
$$

## Case of vertical elevator load

For simplicity, assume that the physical configuration for the vertical elevator is shown in Figure 9.1-7.
If the masses of the cage, payload, and the balance weight are $\mathrm{WO}, \mathrm{W}$, and $\mathrm{WB}[\mathrm{kg}]$ respectively, the force required for the vertical elevator load $\mathrm{F}[\mathrm{N}]$ can be expressed by equation (9.1.2-5) and equation (9.1.2-6).
[Ascent]

$$
\begin{equation*}
F=\left(W o+W-W_{B}\right) \cdot g[N] \cdots \tag{9.1.2-5}
\end{equation*}
$$

[Descent]

$$
F=\left(W o-W-W_{B}\right) \cdot g \quad[N] \cdots \quad(9.1 .2-6)
$$

When the maximum loading capacity is Wmax, the balance weight mass is generally $\mathrm{WB}_{\mathrm{B}}=\mathrm{Wo}+\mathrm{Wmax} / 2$.
Depending on the mass of the movable load, braking modes can exist in both ascending and descending movements where $\mathrm{F}[\mathrm{N}]$ can become negative, so exercise caution.
The calculation of the required torque $\tau$ at the motor axis should be performed using the appropriate formula from equation (9.1.2-1) and equation (9.1.2-2) according to the drive mode or the braking mode. In other words, when $\mathrm{F}[\mathrm{N}]$ is positive, use equation (9.1.2-1) and use equation (9.1.2-2) when the value is negative, to perform the calculation.


Figure 9.1-7: General diagram for vertical elevator load

## - Case of inclined elevator load

The case of inclined elevators is similar to the case of vertical elevators. However, the frictional force cannot be ignored, so the equation form changes between ascending and descending movements. When the inclination angle is $\theta$ as in Figure 9.1-8 and the coefficient of friction is $\mu$, the force $\mathrm{F}[\mathrm{N}]$ required to drive is shown by the following equations.
[Ascent]

$$
\begin{equation*}
F=\left[\left(W o+W-W_{B}\right)(\sin \theta+\mu \cdot \cos \theta)-W_{B}\right] \cdot g \quad[N] \cdots \tag{9.1.2-7}
\end{equation*}
$$

[Descent]

$$
F=\left[W_{B}-(W o+W)(\sin \theta+\mu \cdot \cos \theta)\right] \cdot g \quad[N] \quad \cdots \quad(9.1 .2-8)
$$

As in the case of vertical elevators, braking mode exists in both ascending and descending movements depending on the mass of the movable load. The calculation for the required motor axis torque is also identical.
In other words, use equation (9.1.2-1) when $\mathrm{F}[\mathrm{N}]$ is positive and use equation (9.1.2-2) when the value is negative, to perform the calculation.


Figure 9.1-8: General diagram for inclined elevator load

### 9.1.2.2 Calculation of acceleration and deceleration time

When an object with moment of inertia $\mathrm{J}\left[\mathrm{kg} \cdot \mathrm{m}^{2}\right]$ is rotating at speed $\mathrm{N}[\mathrm{r} / \mathrm{min}]$, the rotating object has kinetic energy defined by equation (9.1.2-9).

$$
E=\frac{J}{2} \cdot\left(\frac{2 \pi \cdot N}{60}\right)^{2}[J] \quad \cdots \quad(9.1 .2-9)
$$

In trying to accelerate this rotating object, the kinetic energy is enlarged. Conversely, in trying to decelerate this object, the kinetic energy must be released. The torque required to accelerate and decelerate is given in equation (9.1.2-10).

$$
\tau=J \cdot \frac{2 \pi}{60} \cdot\left(\frac{d_{N}}{d t}\right)[N \cdot m] \quad \cdots \quad(9.1 .2-10)
$$

In accelerating and decelerating movements, the mechanical moment of inertia is an important factor. The calculation method for the inertia is clarified first, and the description of calculation for acceleration and deceleration will follow.

## (1) Calculation of the moment of inertia

For objects rotating around a rotating axis, the moment of inertia for that object can be computed by first decomposing it to micro parts. Then, multiply the square of the distance from the rotating axis to the micro part with the mass and sum up all of the products. The moment of inertia of the object is the summation value. Moment of inertia J can be calculated by the following equation.

$$
J=\sum(W i \cdot r i 2)\left[k g \cdot \mathrm{~m}^{2}\right] \quad \cdots \quad(9.1 .2-11)
$$

Next, the calculation equation for the moment of inertia of the load or load systems with various shapes is described.

1) Cylinders and cylindrical columns

Cylinder is the most typical shape of rotating objects. Figure 9.1-9 shows an object with external and internal diameters at D1 and D2 [m] respectively and the total mass weighing $\mathrm{W}[\mathrm{kg}]$. The moment of inertia $\mathrm{J}\left[\mathrm{kg} \cdot \mathrm{m}^{2}\right]$ around the center axis of the cylinder can be calculated by the equation (9.1.2-12).

$$
J=\frac{\mathrm{W} \cdot\left(\mathrm{D} 1^{2}+\mathrm{D} 2^{2}\right)}{8}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right] \quad \cdots \quad(9.1 .2-12)
$$

Similarly, cylindrical columns are calculated with internal diameter D2 $=0$.


Figure 9.1-9: Cylinder
2) Case of general rotating objects

Table 9.1-1 shows equations for "calculating moment of inertia $\mathrm{J}\left[\mathrm{kg} \cdot \mathrm{m}^{2}\right]$ of various rotating objects" including the rotating cylindrical object described above.

Table 9.1-1: Moment of inertia of various rotating objects


## 3) Case of traveling load

Suppose that a moving table driven by a motor exists as shown in Figure 9.1-6. If the motor rotates at speed Nm [r/min] when the table speed is $V[\mathrm{~m} / \mathrm{s}]$ and the equivalent distance from the rotating axis is $60 \cdot V /(2 \pi \cdot \mathrm{Nm})$ [ m$]$, the moment of inertia of the table from the rotating axis can be calculated by equation (9.1.2-13).

$$
J=\left(\frac{60 \cdot v}{2 \pi \cdot N_{M}}\right)^{2} \cdot(W o+W)\left[k g \cdot \mathrm{~m}^{2}\right] \quad \cdots \quad(9.1 .2-13)
$$

4) Case of elevator load

For loads attached by rope as in Figure 9.1-7 and Figure 9.1-8, the moment of inertia is calculated by taking the summation of object mass in motion by equation (9.1.2-14), although the direction of motion differs.

$$
J=\left(\frac{60 \cdot v}{2 \pi \cdot N_{M}}\right)^{2} \cdot\left(W o+W+W_{B}\right)\left[\mathrm{kg} \cdot \mathrm{~m}^{2}\right] \cdots \quad(9.1 .2-14)
$$

## (2) Calculation of the acceleration time

Figure 9.1-10: Load model including transmission uses models of typical loads. These assume that the loads are attached via a transmission with efficiency $\eta \mathrm{G}$.
The time required to accelerate to $\mathrm{NM}[\mathrm{r} / \mathrm{min}]$ from stopped state with this load is given by equation (9.1.2-15).

$$
\begin{aligned}
t_{A C C}=\frac{J 1+J 2 / \eta_{G}}{\tau_{M}-\tau L / \eta_{G}} & : \frac{2 \pi\left(N_{M}-0\right)}{60}[\mathrm{~S}] \quad \cdots \quad(9.1 .2-15) \\
\mathrm{J} 1 & : \text { Moment of inertia of the motor axis }\left[\mathrm{kg} \cdot \mathrm{~m}^{2}\right] \\
\mathrm{J} 2 & : \text { Moment of inertia of the load axis converted to the motor axis }\left[\mathrm{kg} \cdot \mathrm{~m}^{2}\right] \\
\tau \mathrm{M} & : \text { Minimum value of motor output torque in drive mode }[\mathrm{N} \cdot \mathrm{~m}] \\
\tau \mathrm{L} & : \text { Maximum value of load torque converted to the motor axis }[\mathrm{N} \cdot \mathrm{~m}] \\
\eta \mathrm{G} & : \text { Efficiency of the transmission }
\end{aligned}
$$

As can be seen by these equations, the apparent moment of inertia is affected by transmission efficiency, becoming ( J 1 $+\mathrm{J} 2 / \eta \mathrm{G})$.


Figure 9.1-10: Load model including transmission

## (3) Calculation of the deceleration time

In the load system of Figure 9.1-10, the time required to stop the motor rotating at speed $\mathrm{NM}[\mathrm{r} / \mathrm{min}]$ can be typically calculated by equation (9.1.2-16).

$$
t_{D E C}=\frac{J 1+J 2 \cdot \eta_{G}}{\tau_{M}-\tau_{L} \cdot \eta_{G}} \cdot \frac{2 \pi\left(0-N_{M}\right)}{60}[S] \quad \cdots \quad(9.1 .2-16)
$$

In this equation, typically the output torque $\tau \mathrm{M}$ is negative and the load torque $\tau \mathrm{L}$ is positive, which reduces the deceleration time.
However, in the case of elevator loads, $\tau\llcorner$ may become negative in braking mode, extending the deceleration time.
Tip For elevator loads, calculate the deceleration time using the maximum negative value possible for the load torque $\tau \mathrm{L}$ converted to the motor axis when selecting the capacity.

## (4) Calculation of non-linear acceleration and deceleration time

For loads which are frequently accelerated and decelerated, all of the surplus motor torque may be used to accelerate and decelerate in the shortest time. Vector control allows this type of operation easily.
The acceleration and deceleration in these cases are non-linear, and the time required to complete acceleration and deceleration cannot be computed by one equation.
Therefore, speed N is subdivided into $\Delta \mathrm{N}$ parts and the acceleration and deceleration time of the parts are computed. Then the times of the parts are integrated until the end of acceleration and deceleration in order to compute the total time. The calculation of the parts increase in accuracy as the subdivision increases. Therefore, computers are used for calculating the actual acceleration and deceleration time.
The following shows the method to calculate.
Figure 9.1-11 shows an example of the driving equipment with constant output characteristics. The region below N0 shows constant torque while the region from N0 to N1 shows constant output. The acceleration time can be calculated using equation (9.1.2-17).

$$
t_{A C C}=\frac{J 1+J 2 / \eta_{G}}{\tau_{M}-\tau L / \eta_{G}} \cdot \frac{2 \pi \cdot \Delta N}{60}[S] \quad \cdots \quad \text { (9.1.2-17) }
$$



Figure 9.1-11: Example of functional characteristics for driving equipment with constant output

First, calculate the moment of inertia J 1 for the motor axis, the moment of inertia J 2 of the load axis converted to the motor axis, load torque $\tau \mathrm{L}$ converted to the motor axis, and the efficiency $\eta \mathrm{G}$ of the transmission. Then, calculate the maximum motor torque $\tau \mathrm{M}$ using the suitable equation below according to the speed range.
[ $\tau \mathrm{m}$ for $\mathrm{N} \leq \mathrm{N} 0$ ]: Constant torque

$$
\tau_{M}=\frac{60 \cdot P 0}{2 \pi \cdot N 0}[N \cdot m] \quad \quad \cdots \quad(9.1 .2-18)
$$

[ $\tau \mathrm{M}$ for $\mathrm{N} 0 \leq \mathrm{N} \leq \mathrm{N} 1$ ]: Constant output (torque inversely proportional to speed)

$$
\tau_{M}=\frac{60 \cdot P 0}{2 \pi \cdot N}[N \cdot m] \quad \quad \cdots \quad(9.1 .2-19)
$$

When the calculation results above do not meet the target values, the capacity of the driving equipment should be increased by one rank.
(5) Calculation of non-linear deceleration time

The calculation of the deceleration time can be performed using the same equations as for the acceleration time.

$$
t_{D E C}=\frac{J 1+J 2 \cdot \eta_{G}}{\tau_{M}-\tau L \cdot \eta_{G}} \cdot \frac{2 \pi \cdot \Delta N}{60}[S] \quad \cdots \quad(9.1 .2-20)
$$

In this equation, both $\tau \mathrm{M}$ and $\Delta \mathrm{N}$ are negative values, so in general, load torque $\tau \mathrm{L}$ assists deceleration.
However, in the case of elevator loads, modes exist where $\tau \mathrm{L}$ becomes negative. In these cases, the polarities of $\tau \mathrm{M}$ and $\tau\llcorner$ differ, impeding deceleration.

### 9.1.2.3 Calculation of the motor RMS rating

For loads which are frequently and repeatedly accelerated and decelerated, the load current varies widely and enters the region for the motor's short duration rating. In these cases, consideration and measures for heat tolerance are necessary. The heat generated by the motor is thought to be approximately proportional to the square of the load current, resulting in temperature rise proportional to the heat generated for FRENIC-VG exclusive motors with forced cooling fans.

For cases when the motor is repeatedly run in adequately short periods compared to the motor's thermal time constant, the following procedure can be followed to calculate the "equivalent current." Then, select the motor such that this "equivalent current" does not exceed the rated current.


Figure 9.1-12: Example of repeating operation

For these calculations, first find the required torque for each segment of the speed pattern. Next, use the motor torque current curve to convert to the load current pattern.

Then the motor's equivalent current leq can be computed using equation (9.1.2-21).

$$
I e q=\sqrt{\frac{I 1^{2} \cdot t 1+I 2^{2} \cdot t 2+I 3^{2} \cdot t 3+I 4^{2} \cdot t 4+I 5^{2} \cdot t 5}{t 1+t 2+t 3+t 4+t 5}}[A] \cdots \quad(9.1 .2-21)
$$

For the actual calculation, the motor torque current curve does not exist. Use the following equation (9.1.2-22) which calculates the load current I from load torque $\tau 1$, and then compute equivalent current leq.

$$
I=\sqrt{\left(\frac{\tau 1}{100} \cdot \operatorname{It} 100\right)^{2}+\operatorname{Im} 100^{2}} \quad[A] \quad \quad \cdots \quad(9.1 .2-22)
$$

$\tau 1$ : Load torque [\%], It100 = torque current (P09: M1 torque current), Im100 = excitation current (P08: M1 excitation current)

- Refer to Chapter 12 "Replacement Material" in separate volume, FRENIC-VG User's Manual Unit/Function Codes Edition (24A7-■-0019) for P08 and P09 function code data.
- Refer to the torque current and excitation current relevant to A code instead of the P code when using a second motor.


### 9.2 Inverter capacity selection

### 9.2.1 Overview of the control method

FRENIC-VG provides vector control with speed sensor (induction motor, synchronous motor), sensor-less vector control (induction motor), and $\mathrm{V} / \mathrm{f}$ control (induction motor).
The following provides a general description of these control modes.

### 9.2.1.1 Vector control with speed sensor (induction motor, synchronous motor)

In this control mode, the primary current of the AC motor is controlled by decomposing the primary current into the magnetic flux current and the torque current components to achieve control performance equivalent to that of DC motors.

Vector control with sensor is more suitable for quicker response and higher precision applications than V/f control mode.
(1) Good acceleration and deceleration characteristics
(2) Wide range of speed control
(3) Provision of torque control
(4) Quick control response

### 9.2.1.2 Sensor-less vector control (induction motor)

Vector control with speed sensor possesses superior performance such as quick response and high precision but requires speed sensors, necessitating attachment of and wiring to the speed sensor.
In comparison, this control mode is slightly inferior in performance than vector control with speed sensor. However, speed sensor-less vector control estimates the motor rotation speed from the motor terminal voltage or the primary current without using speed sensors, and uses the estimation as the speed feedback signal for vector control.

### 9.2.1.3 V/f control (induction motor)

This control mode operates the motor by varying the frequency and voltage according to the V/f pattern, without using speed sensors. The scheme is not suitable for systems requiring torque control, high precision speed control, and quick response. However, the adjustment is simple and provides only a few restrictions to the driving motor, making it suitable for numerous fan and pump applications as well as inverters.

### 9.2.2 Selection of MD/LD specification

### 9.2.2.1 Precautions for selection

FRENIC-VG is built to dual rating specifications. The applicable specification can be switched by altering the parameter settings between the MD (Medium Duty) specification and LD (Low Duty) specification. The MD specification can drive motors with capacities identical to the inverter, and the LD specification allows the inverter to drive motors with capacities which are one or two ranks higher.
Select the inverter capacity by reviewing the MD specification/LD specification in "9.2.2.2 Guidance for selection," the overloading characteristics, and the capacity of the motor to be used.
MD spec: Apply to equipment where the inverter's load current in normal operations is less than the inverter rated current (MD specification), and the load current in overload operation is less than $150 \%$ of the rated current (MD specification) for 1 minute.
LD spec: Apply to variable load equipment such as fans, pumps, and centrifugal machines where the inverter's load current in normal operations is less than the inverter rated current (LD specification), and the load current in overload operation is less than $110 \%$ of the inverter rated current (LD specification) for 1 minute.
The inverter rated current (LD specification) is based on a motor capacity which is one or two ranks higher than that of the inverter.
Note Replacement of FRENIC5000VG7S (HT specification) by FRENIC-VG:
FRENIC-VG does not provide a specification equivalent to the HT specification of VG7. When replacing VG7 HT specification by FRENIC-VG, use an inverter with one rank higher capacity.

### 9.2.2.2 Guidance for selection

Table 9.2-1 shows the functional differences between the MD specification and the LD specification. If the LD specification satisfies the requirements in your applications in view of overload capacity and functionality, you can select inverters with capacities (LD specification) which are one or two ranks lower than the motor capacity.

Table 9.2-1: MD specification/LD specification functional differences

| Function | MD spec | LD spec | Remarks |
| :---: | :---: | :---: | :---: |
| Use | General purpose load | Low overload applications |  |
| Motor capacity range | [400V class series] 30 to 315 kW 630 to $800 \mathrm{~kW}^{*}$ <br> [690V class series] 90 to 450 kW | [400V class series] <br> 37 to 355 kW <br> 710 to 1000 kW* <br> [690V class series] <br> 110 to 450 kW | * mark represents stack by phases |
| Function code setting (MD/LD spec switch) | $\mathrm{F} 80=0,2,3$ | $\mathrm{F} 80=1$ | Setting at factory shipping: $\mathrm{F} 80=0$ 0 and 2 are displayed as HD on keypad. |
| Inverter rated current level | Inverter and motor should have same capacity Rated current is based on motor | Rated current is based on motor capacity which is one or two ranks higher than that of inverter | In LD spec, the consecutive rated current rises by one or two ranks, but the \% of the consecutive rated current for overload capacity lowers. <br> For details, refer to Chapter 2 "Specifications." |
| Overload capacity | $150 \%$ of rated current for 1 minute | $110 \%$ of rated current for 1 minute | Rated currents differ between MD and LD specifications. |

Note (1) No output frequency range differs between MD and LD specifications.
(2) When constructing a system comprising converters and inverters, MD and LD specifications may co-exist. In this case, select rated capacities and overload capacities for the converters, which meet the required inverter capacities (rated and overload).

### 9.3 Converter selection

### 9.3.1 Converter model selection

Converter is available in diode rectifier and PWM converter. Please select the type of converter depending on load status of machinery system used, and harmonic currents regulation on the supply side.

Table 9.3-1: Advantages of various converters

| Item | Diode rectifier | PWM converter |
| :--- | :--- | :--- |
| Points for selection | - System with small capacity for regenerative energy <br> System using generators for power supply (no <br> regeneration) <br> System with restrictions in installation space | -System with large capacity for <br> regenerative energy <br> System with regulations on <br> power supply side harmonic <br> current (supply power factor) <br> Price <br> Installation space <br> Regenerative electric <br> power processing <br> $\left.\begin{array}{l}\text { Regeneration not possible only with the diode rectifier } \\ \text { Resistive regeneration can be applied } \\ \text { with braking resistor + braking unit }\end{array}\right)$ High |

Note
Price and installation space show comparison between diode rectifier and PWM converter.

### 9.3.2 Converter capacity selection

The converter capacity is selected based on the total capacity of inverters connected to the converter output or the total load capacity calculated from the motor operating conditions.
The following provides descriptions of converter capacity selection, taking in the event of one inverter and parallel connection of multiple units as an example.
Note Even if the capacity of the operated inverter is small, select a converter capacity which is more than $50 \%$ of the total capacity of all inverters connected to the converter.
Applied converter capacity $\geq$ (Capacity of all connected inverters $\times 50 \%$ )

### 9.3.2.1 Single unit operation

When driving one inverter, select a converter capacity (consecutive rating, basic rating, overload rating) which is identical to the inverter.
(Refer to No. 1 and No. 5 in Table 9.3-2)

### 9.3.2.2 Operation with multiple units connected

See below the example case of four inverters, $315 \mathrm{~kW}, 280 \mathrm{~kW}, 110 \mathrm{~kW}$, and 90 kW , connected. Calculate the converter capacity using "Equation (9.3.2-1)" and "Equation (9.3.2-2)."

Use the same equation for consecutive rating and overload rating (150\% or 110\%).

$$
\begin{aligned}
& \sum I N V=I N V 1+I N V 2+I N V 3+I N V 4 \\
& \sum I N V=I N V 1+I N V 2+I N V 3+(I N V 4 \times-0.95)
\end{aligned}
$$

: When all inverters operate in drive mode
...(9.3.2-2) : Only INV4 is in regenerative mode

[^15]Table 9.3-2: Consecutive rating

| No. | INV1 | INV2 | INV3 | INV4 | Total | Applied PWM converter type <br> (example) | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- | :--- |
| 1 | 315 | - | - | - | 315 | RHC315S-4D $\square$ | kW) |
| 2 | 315 | 280 | 110 | 90 | 795 | RHC800B-4D $\square$ | All units drive operation |
| 3 | 315 | 280 | 110 | 0 | 705 | RHC710B-4D $\square$ | Limited operation: 3 driven, 1 stopped |
| 4 | 315 | 280 | 110 | -86 | 620 | RHC630B-4D $\square$ | Limited operation: 3 driven, 1 <br> regenerating |

Table 9.3-3: Overload rating

| No. | INV1 | INV2 | INV3 | INV4 | Total | Applied PWM converter type <br> (example) | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- | :--- |
| 5 | 473 | - | - | - | 473 | RHC315S-4D $\square$ | Kingle unit drive operation |
| 6 | 473 | 420 | 165 | 135 | 1193 | RHC800B-4D $\square$ | All units drive operation |
| 7 | 315 | 420 | 165 | 0 | 900 | RHC710B-4D $\square$ |  |
| 8 | 315 | 420 | 165 | -128 | 772 | RHC630B-4D $\square$ | Limited operation: 3 driven, 1 stopped <br> Regenerating |

### 9.3.3 Capacity of resistive braking

### 9.3.3.1 Review of braking resistor rating

By using a PWM converter in combination with plural inverters, the regenerative energy generated during motor braking may be recycled to the power supply, or utilized as driving energy of other motors in driving operation.
On the other hand, the energy generated from the combination of diode rectifier and plural inverters may also be utilized as driving energy in other motors. However, as it is not revivable in power supply in principle, the unconsumed regenerative energy will cause the DC link bus voltage to increase, resulting in an alarm trip condition (overvoltage). For this reason a braking system (braking resistor + braking unit) will be required to convert the regenerative energy into thermal energy and dissipate the converted energy.
The method of capacity calculation of braking resistor is given in this chapter.


Figure 9.3-1: Flow of regenerative energy in combination with converter
The energies which can be regenerated in inverter operations are kinetic energy due to inertia or the potential energy of elevators.

1) Kinetic energy due to inertia

When an object with moment of inertia $\mathrm{J}\left[\mathrm{kg} \cdot \mathrm{m}^{2}\right]$ is rotating at rotational speed $\mathrm{N} 2[\mathrm{r} / \mathrm{min}]$, the kinetic energy of this rotating object is shown in equation (9.3.3-1).

$$
\begin{aligned}
E & =\frac{J}{2} \cdot\left(\frac{2 \pi \cdot N 2}{60}\right)^{2}[J=W s] & \cdots & (9.3 .3-1) \\
& \approx \frac{1}{182.4} \cdot J \cdot N 2^{2}[J] & \cdots & (9.3 .3-1)^{\prime}
\end{aligned}
$$

When decelerating this object to rotational speed N 1 [r/min], the released energy is shown in equation (9.3.3-2).

$$
\begin{aligned}
E & =\frac{J}{2} \cdot\left[\left(\frac{2 \pi \cdot N 2}{60}\right)^{2}-\left(\frac{2 \pi \cdot N 1}{60}\right)^{2}\right] \cdots \quad(9.3 .3-2) \\
& \approx \frac{1}{182.4} \cdot J \cdot\left(N 2^{2}-N 1^{2}\right)[J] \quad \cdots \quad(9.3 .3-2)^{\prime}
\end{aligned}
$$

In the case of a typical load model as shown in Figure 9.1-10, the energy regenerated to the inverter is calculated from the transmission efficiency $\eta \mathrm{G}$ and the motor efficiency $\eta \mathrm{M}$ by equation (9.3.3-3).

$$
E \approx \frac{1}{182.4} \cdot\left(J 1+J 2 \cdot \eta_{G}\right) \cdot \eta_{M} \cdot\left(N 2^{2}-N 1^{2}\right)[J] \quad \cdots \quad(9.3 .3-3)
$$

## 2) Potential energy of elevators

When descending an object of weight $W[k g]$ from height $h 2[m]$ to $h 1[m]$, the released potential energy can be expressed as equation (9.3.3-4).

$$
\begin{gathered}
E=W \cdot g \cdot(h 1-h 2)[J=W s] \\
g \approx 9.8065\left[\mathrm{~m} / \mathrm{s}^{2}\right]
\end{gathered}
$$

The energy regenerated to the inverter circuit is calculated from the transmission efficiency $\eta \mathrm{G}$ and motor efficiency $\eta \mathrm{M}$ by equation (9.3.3-5).

$$
E=W \cdot g \cdot(h 1-h 2) \cdot \eta_{G} \cdot \eta_{M} \quad[J=W s] \quad \cdots \quad(9.3 .3-5)
$$

### 9.3.3.2 Procedures for selection

The following selection conditions must be satisfied according to the repeating period.
(1) Period is less than 100 s : [Condition 1] and [Condition 3]
(2) Period is over $100 \mathrm{~s}: \quad$ [Condition 1] and [Condition 2]
[Cond 1]: "Maximum braking torque" must be smaller than the value specified in the table of Chapter 6 " 6.5 .3 Standard combination." If the "Maximum braking torque" exceeds the value in the table, select a capacity which is one rank larger.
[Cond 2]: The discharged capacity per braking must be smaller than the "Discharge withstand current rating kWs" in the table. For details of the calculation, refer to previous section "9.3.3.1 Review of braking resistor rating."
[Cond 3]: The average loss, which is the discharged capacity divided by the repeating period, must be smaller than the "Average loss kW" shown in Chapter 6 "6.5.3 Standard combination."

### 9.3.3.3 Precautions for selection

Braking time T 1 , repeat period T0, and utilization rate \%ED are converted under the conditions of deceleration braking by rated torque as shown in Figure 9.3-2. However, these values do not need to be used in the calculations for capacity selection.


Figure 9.3-2: Approach to utilization rate
Utilization Rate $\% E D=\frac{T 1}{T 0} \times 100[\%] \quad \cdots \quad(9.3 .3-6)$

### 9.4 Direct parallel connection system

Direct parallel connection is a method for controlling one motor by connecting 2 to 3 inverters that are identical in capacity.
<Features>
(1) A combination of plural inverters of smaller capacity allows easier restoration or replacement in breakdown as compared to a single unit of inverter of large capacity.
(2) Quick operation recovery is possible without any alterations to the wiring using inverters which have not failed.

- When failures occur during direct parallel operation, operation can be resumed using the remaining, normal inverters (operation with reduced number of units).
- Number of inverter units operated can be varied according to load conditions (operation with reduced number of units).


### 9.4.1 Restrictions of direct parallel connection system

There are some restrictions as follows.
(1) Number of direct parallel: 2 to 3 inverters with equal capacities units for connection
(2) Motor control mode : The direct parallel connection system is available under vector control with speed sensor and sensor-less vector control, and can be used for induction motors.
When controlling a motor using the direct parallel connection system, the optional high speed serial communication terminal block (OPC-VG1-TBSI) is necessary.
(3) Inverter output wiring
: Refer to "Chapter 9.4.8 Wiring inductance" (pages 9-29).
(4) Speed response, current 50 Hz speed control response
This scheme may not be able to support some conditions requiring very high speed responsiveness or torque control accuracy.
(5) Functional safety : The option card (OPC-VG1-SAFE) for supporting functional safety is not applicable.
(6) Operation with reduced : When operating with reduced number of units, contactors must be attached to the number of units inverter output side because the wiring for the motor and inverter will be detached.
(7) Auto-tuning function : This function enables the system to automatically determine the motor constant according to the direct parallel connection condition and store motor parameters depending on the motor constant.

### 9.4.2 Basic configuration of direct parallel connection

## Configuration

| Inverter |  | When using this control scheme, one OPC-VG1-TBSI (optional built-in terminal block supporting high speed serial communication) is required for every inverter. |
| :---: | :---: | :---: |
|  | Contactor Note1) | When running with reduced number of units, contactors are used to detach inverters which will not be operated. |
|  | Output circuit filter Note 2) | Refer to "9.4.8 Wiring inductance" (pages 9-29). |
|  | PG/NTC switcher | To be used for engine cutoff when PG vector control (vector control with speed sensor) or NTC thermistor (motor temperature detection) are used. MCA-VG7-CPG may be used for direct parallel connection of 2 units. |
|  | PLC | A section of the function code must be modified in changing to operate with reduced number of units, from 3 units to 2 units. Using PLC will automatically rewrite this function code. <br> Using PLC is recommended in systems for advanced operation with reduced number of units, which requires rewriting of parameter settings. |

Note 1) Select contactors and OFL filters whose capacity and type are appropriate for the inverters being used.
Note 2) Use of these options is not necessarily required for direct parallel connection system.
(It is however required in cases such as when using optional function of engine cutoff.)


- To determine some of the motor parameters, multiply by the inverse of the number of units connected in direct parallel connection.
Refer to "9.4.6 Motor constants" (pages 9-25).
- The master inverter exercises integrated control of operation and speed commands over the slaves.
- In the case of three units in the direct parallel connection system, up to three motor constants can be set in advance even when conducting operation with reduced number of units such as two or one. Switching among the motor constants is done by the X terminal input of the inverters.


### 9.4.3 Function code setup

When conducting direct parallel connection, the following function codes must be set up.
Table 9.4-1: Multiple system setup code

| F.No. | Function code name | Description |
| :--- | :--- | :--- |
| o33 | Multiple system control system | Setup of the multiple system control mode (direct parallel connection <br> system, etc.) |
| o34 | Multiple system slave exchange <br> number | Setup of the number of slave inverter exchanges (number of units) for the <br> multiple system |
| o50 | Multiple system exchange <br> number setup | Setup of exchange numbers for high speed serial communication <br> (OPC-VG1-TBSI) |

## 033

Multiple System Control System
Set the value according to the multiple system configuration below.
Also review the page on multiple system cancellations in E01 to E13 "X Function Selection."
Note) Available in inverters having a ROM version H1/2 0020 or later.
Specified value 0 : Invalid (single unit operation)
1 : Multi-winding system
2 : Multiple system 1 (direct parallel system)
3 : Multiple system 2 (unassigned)
4 : Reserve 1
5 : Reserve 2

When the multiple system is enabled, set the number of slave exchanges (number of units) excluding the master.
Setup value range 1 to 5
For configuring direct parallel connection systems
1: Two units configured in direct parallel connection (one slave unit)
2: $\quad$ Three units configured in direct parallel connection (two slave units)
3 to 5: Invalid (Not utilize for direct parallel connection)

## 050

Multiple system exchange number setup
Set exchange numbers for the terminal blocks supporting high speed serial communication (OPC-VG1-TBSI) in the multiple system.

$$
\text { Specified value } 0 \quad \text { : Master }
$$

1 to 5 : Slave
<Setup example>
(1) System with two units

Specify o34=1 for both the master INV and slave INV.
(2) System with three units

Specify o34=2 for both the master INV and slave INV.


Note For the multiple system exchange number setup (o50), set up in the order to connect to the master.
<Invalid setup example>
Master INV (o50 = 0), slave $1(050=2)$
Slave INV2 $(050=1)$, slave $3(o 50=3)$
*: *** show invalid setups.


Figure 9.4-2: Function code setup example

Note When the setup for o34 (Multiple System Slave Exchange Number) is wrong, the system may not operate and the alarm may not be activated. Reconfirm that the setup is correct.

### 9.4.4 Basic connection diagram

### 9.4.4.1 Configuration of 2 units in direct parallel connection

The following shows an example of two inverters used in direct parallel connection.
This connection diagram shows a configuration which has considered operation with reduced number of units. When operation with reduced number of units will not be conducted, elimination of inverter output contactors and simplification of operation sequence are possible.


Figure 9.4-3: Basic configuration for direct parallel connection system using two inverters

## <Supplementary explanation for the connection diagram>

## (1) Basic items

1) For safety, when alarm is activated ( $30 X$ actuated), input coast to a stop command $[B X]$ to the two inverter units. In the connection diagram shown, the coast to a stop command is confiqured to normally on (ordinarily closed, open signifies coast to a stop command). This input should be constructed by hardware circuit for safety.
2) Configure the two inverters such that after operation preparation is complete [RDY], FWD and REV can be turned ON. The diagram shows the case where the operation preparation complete function is allocated to relay output.
3) The alarm of slave inverters can be released by the reset command [RST] of the master inverter.
4) For installations into facilities which restart after instantaneous power failures, use the running restart function which searches the direction and speed of free running rotation and picks up smoothly to reengage drive.

## (2) Case of operation with reduced number of units

When running with reduced number of units, realize the following setup.

1) Realize the setup in "Table 9.4-2" below for $X$ terminal input ( Di ) and $Y$ terminal output (Do).

Table 9.4-2: Required X terminal functions for operation with reduced number of units

|  | Specified value / Setup name | Explanation of use in Operation with Reduced Number of Units |
| :---: | :---: | :---: |
| Di | 57 [MT-CCL] <br> Multiple system cancellation | Release direct parallel connection when turned ON. The system will be able to run on one independent inverter. When running independently on either of the two units, assign this function to both of the units. |
|  | $\begin{aligned} & 12 \text { [M-CH2] } \\ & \text { Motor M2 selection } \end{aligned}$ | When running on a single unit, the system is enabled to select the second motor constant and run the motor without changing the setting of the first motor constant. |
|  | $\begin{aligned} & 49 \text { [PG-CCL] } \\ & \text { PG alarm cancellation } \end{aligned}$ | Alarm is temporarily canceled for PG routing and NTC thermistor routing disconnection detecting function while preparing for operation with reduced number of units. |
|  | 75 [NTC-CCL] NTC thermistor alarm cancellation | used. In this case, reset the alarm when running aga |
|  | 4 [RT1] <br> Second ASR selection | If the system is running on a single unit using ASR constants (acceleration and deceleration times and $P$ gain and integral action time for the ASR) set for direct parallel operation, the load inertia may be too large. This can cause overload protection to be activated. <br> Avoid the overload trip by selecting the second ASR. <br> Using the torque restriction (torque current restriction) is also effective. |
| Do | $\begin{array}{ll}0 & {[\text { RUN }]} \\ & \text { Inverter operating }\end{array}$ | This signal signifies that the inverter is running. <br> During direct parallel connection operation, the system outputs a signal to signify that the master inverter is running. <br> During single unit operation, the system outputs signals to signify that respective inverters are running. |
|  | 16 [SW-M2] <br> Second motor selection complete | When the system receives a second motor selection signal and completes a transition to the second motor constant inside the inverters, the system outputs an ON signal. |

To switch to operation with reduced number of units, follow the steps below.


Figure 9.4-4: Flowchart for switching to operation with reduced number of units
2) For installations into facilities which restart after instantaneous power failures, use the running restart function which searches the direction and speed of free running rotation and picks up smoothly to reengage drive or use [IL] of the $X$ terminal
Use of the running restart function is recommended especially for PG vector control method.
3) For simple systems, hardware can be constructed as Figure 9.4-3. However, when a more complex process sequence is desired, construction of a system structure which operates on communication with PLC is recommended.

### 9.4.5 Configuration of 3 units in direct parallel connection

The circuit diagram of a direct parallel connection system using three inverters, where operation with reduced number of units is not conducted, is shown below.
In the case of two inverters in direct parallel connection system, the relay circuit is the same as in the diagram below if operation with reduced number of units is not conducted.


Figure 9.4-5: Basic configuration (without operation in reduced number of units) for direct parallel connection system using three inverters

## <Supplementary explanation for the connection diagram>

(1) For safety, when alarm is activated ( 30 X actuated), input coast to a stop command $[B X]$ to the three inverter units. This input should be constructed by hardware circuit for safety.
(2) Configure the three inverters such that after operation preparation is complete [RDY], FWD and REV can be turned ON.
(3) The alarm of slave inverters can be released by the reset command [RST] of the master inverter.
(4) When installing into facilities which restart after instantaneous power failures, use the running restart function which searches the direction and speed of free running rotation and picks up smoothly to reengage drive.

### 9.4.6 Motor constants

Direct parallel connection system is a control method where a single winding motor is operated in parallel by plural inverters. Therefore, the motor constant required for inverter to control the motor is " $1 /$ number of connected inverter units."
When an operation with reduced number of inverters, a characteristic of the direct parallel connection system, is performed, the motor constants need to be changed. FRENIC-VG allows the selection of up to three motor constants. Selection among the motor constants can be made by the motor constant switching function of X terminal.

Table 9.4-3 shows a setting method of motor parameters including the time of the operation with reduced number of inverters.
When performing operation with reduced number of inverters in the direct parallel connection system, set motor parameters after determining the definitions of motor constant codes.

## <Definitions>

- M1: Maximum number of

M1 code consists of motor parameters for single unit operation. connected units = 1 unit

- M2: Maximum number of connected units $=2$ units

M2 code consists of motor parameters for direct parallel connection system of 2 units.

- M3: Maximum number of connected units $=3$ units

M3 code consists of motor parameters for direct parallel connection system of 3 units.

Table 9.4-3: Explanation of change of motor parameters in the operation with reduced number of inverters

| Parameter name |  | Parameter code |  |  | Coefficient of setting value in operation with reduced number of inverters |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | M1 code | M2 code | M3 code |  |
| Control system |  | P01 | A01 | A101 |  |
| Motor selection |  | P02 | - | - |  |
| Maximum speed |  | F03 | A06 | A106 |  |
| Rated speed |  | F04 | A05 | A105 |  |
| Rated voltage |  | F05 | A04 | A104 |  |
| Rated capacity |  | P03 | A02 | A102 | $\times(1 /$ No. of units in direct parallel connection) |
| Rated current |  | P04 | A03 | A103 | $\times(1 /$ No. of units in direct parallel connection) |
| No. of poles |  | P05 | A07 | A107 |  |
| \%R1 |  | P06 | A08 | A108 |  |
| \%X |  | P07 | A09 | A109 |  |
| Exciting current |  | P08 | A10 | A110 | $\times(1 /$ No. of units in direct parallel connection) |
| Torque current |  | P09 | A11 | A111 | $\times(1 /$ No. of units in direct parallel connection) |
| Slip on driving, braking |  | P10, P11 | A12, A13 | A112, A113 |  |
| Iron loss coefficient 1 to 3 |  | P12 to P14 | A14 to A16 | A114 to A116 |  |
| Magnetic saturation coefficient 1 to 5 |  | P15 to P19 | A17 to A21 | A117 to A121 |  |
| Secondary time constant |  | P20 | A22 | A122 |  |
| Inductive voltage coefficient |  | P21 | A23 | A123 |  |
| R2 correction coefficient 1 to 3 |  | P22 to P24 | A24 to P26 | A124 to A126 |  |
| Exciting current correction coefficient |  | P25 | A27 | A127 |  |
| ACR <br> Constant | P gain | P26 | A28 | A128 |  |
|  | Integral action time | P27 | A29 | A129 |  |
| No. of PG pulses |  | P28 | A30 | A130 |  |
| Thermistor selection |  | P30 | A31 | A131 |  |
| Electronic thermal (activation selection) |  | F10 | A32 | A132 |  |

Note (1) Shaded parts $\square$ in Table show parameters which are set to different values between the M1 and M2 (M3) codes for the operation with reduced number of inverters.
Set the other parameters to same values among the M1, M2 and (M3) codes.
(2) ACR constants should be less than the standard set values when operating at direct parallel connection. (Adjust the constants while operating the motor.)
Use the standard set values in the operation reduced to one unit of the inverter.
(3) Use motor constants by assigning them to motor M2 selection and motor M3 selection [MCH2, MCH3] of the $X$ terminal function.

Table 9.4-4 shows setting values assigned to motor parameters in the cases of the direct parallel connection system of two or three inverters and a single inverter, taking the motor parameters of a 280 kW motor as an example.

Table 9.4-4: Setting example of motor parameters


Note (1) As a typical example, setting values assigned for the M1 code are shown. The same setting values will be shown when the M2 or M3 code is set/selected.
(2) Values set to P03, P04, P08, and P09 are floating-point numbers. Set the values by calculating them to settable decimal point. Set the values by rounding them when they cannot be divided.
(3) Set ACR constants to the setting values specified in this Table. Then, adjust the values while checking the operation status in test runs.

### 9.4.7 Protective functions in direct parallel connection system

This section describes protective functions (batch alarm, reset, disconnection detection) for direct parallel connection. For other protective functions, see Chapter 11 "Troubleshooting."

## (1) Batch alarm process

An alarm is indicated on all stations by optical link communication, 30X operation is executed and the inverter outputs are shut down. Alarm codes indicated on the keypad LED display enable the discrimination of a station which has caused the alarm. A function of the $Y$ terminal provides the monitoring of the multi-system self station failure [AL-SF].

## Example 1: When the master inverter goes into an alarm state (on occurrence of fin overheat (

Y terminal function: For the master inverter, the multi-system self station failure [AL-SF] is turned on.
LED display: "ロ" (other station) is prefixed to the alarm codes for the slave inverters 1 and 2.

| Inverter | Alarm code | Remark |
| :---: | :---: | :---: |
| Master | Slation which has caused alarm |  |
| Slave 1 | Other station |  |
| Slave 2 | Other station |  |

Example 2: When the slave inverter 2 goes into an alarm state (on occurrence of fin overheat (
Y terminal function: For the slave inverter 2, the multi-system self station failure [AL-SF] is turned on.
LED display: "ધ゙" (other station) is prefixed to the alarm codes for the master inverter and slave inverter 1.

| Inverter | Alarm code | Remark |
| :---: | :---: | :---: |
| Master | Other station |  |
| Slave 1 | Other station |  |
| Slave 2 | anini |  |

* Alarm sub codes (for manufacturers) are updated only on the station which has caused the alarm.


## (2) Reset process

In the direct parallel connection system, all stations are batch reset provided that the alarm cause is cleared. However, in the case of single unit operation, only a self station inverter is reset provided that the alarm cause is cleared. If the system is running on a single inverter, perform the reset process by inputting a reset command from an external device ( X terminal or communication by SX bus etc.) or by pressing the reset button on the keypad of the inverter.

Table 9.4-5: Reset target

|  | Direct parallel connection |  | Single unit operation <br> (Cancellation of direct parallel connection) | Reset target |
| :---: | :---: | :---: | :---: | :---: |
|  | Master INV | Slave INV |  |  |
| Master inverter reset process | Alarm trip | - | - | All inverters |
|  | - | Alarm trip | - | All inverters |
|  | - | - | Alarm trip | Master INV only |
| Slave inverter reset process | Alarm trip | - | - | All inverters |
|  | - | Alarm trip | - | All inverters |
|  | - | - | Alarm trip | Only slave INV |

## (3) Invalidation of disconnection detection

In the direct parallel connection system, the master inverter performs arithmetic operation of motor control integrally. Therefore, the slave inverters do not require motor detection signals through devices such as PG and NTC thermistor. Accordingly, PG disconnection detection and NTC disconnection detection are disabled under the conditions of "Multi-system" and "Slave."

[^16]
### 9.4.8 Wiring inductance

In some cases, control over the direct parallel connection cannot be normally performed owing to the influence of a surge voltage caused by the switching of the inverters. Therefore, it is recommended to install output circuit filters (OFL filters) that suppress the occurrence of the surge voltage.
If a space for storing OFL filters cannot be secured in your cabinet, however, motor operation by the direct parallel connection system becomes possible when suppressing the surge voltage to a level that causes no trouble to the direct parallel control by wiring inductance between the inverters and motor (regulated by wiring length).
This section explains the wiring inductance (wiring length) in the direct parallel connection system.
Output circuit filter (OFL filter)


Restrictions on wiring length in direct parallel connection system

- L1 = L2 (equal in wiring length)
- Refer to "9.4.8.1 Direct parallel connection combinations and wiring lengths" for wiring length by inverter capacity.

Figure 9.4-6 Explanatory drawing of restrictions on direct parallel connection

Note (1) In the figure above, two inverters in the direct parallel connection are shown. The same applies to the case of three inverters.
(2) If L1 and L2 are cabtire cables or shielded wires, the wiring length of them should be at least three times the length specified in the section 9.4.8.1.
(3) Make sure that L1 and L2 are equal in length.
(4) OFL filters can be installed on either primary or secondary side of contactors.
Make sure that the wiring length between the output circuit filters OFL-L1 and OFL-L2 is from 2 to 20 m if they are installed on the secondary side of the contactors.
(In the case of direct parallel connection of 3 units, the total wiring length among respective OFL filters should be within the range.)


Figure 9.4-7: Restrictions on use of OFL filters

### 9.4.8.1 Direct parallel connection combinations and wiring lengths

Table 9.4-6 shows specifications (rated currents, minimum wiring lengths) for direct parallel connection system combinations ( 2 units, 3 units). The rated current and minimum wiring length vary with the combination.

Table 9.4-6: Wiring lengths and combinations for direct parallel connection

|  |  | Configuration | Sing oper | unit ation | Direct parallel connection system |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 2 units |  |  | 3 units |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  | Inverter type |  |  | Rated cu | rrent [A] | Rated current [A] |  | Minimum wiring length (L) [m] | Rated current [A] |  | Minimum wiring length (L) [m] |
|  |  | MD spec |  | LD spec | MD spec | LD spec | MD spec |  | LD spec |  |
|  | FRN30SVG1S-4■ |  | 60 | 75 | 114 | 143 | 92 | 171 | 214 | 122 |  |
|  | FRN37SVG1S-4■ |  | 75 | 91 | 143 | 173 | 74 | 214 | 259 | 98 |  |
|  | FRN45SVG1S-4■ |  | 91 | 112 | 173 | 213 | 61 | 259 | 319 | 81 |  |
|  | FRN55SVG1S-4■ |  | 112 | 150 | 213 | 285 | 49 | 319 | 428 | 66 |  |
|  | FRN75SVG1S-4■ |  | 150 | 176 | 285 | 334 | 37 | 428 | 502 | 49 |  |
|  | FRN90SVG1S-4■ |  | 176 | 210 | 334 | 399 | 32 | 502 | 599 | 42 |  |
|  | FRN110SVG1S-4 $\square$ |  | 210 | 253 | 399 | 481 | 27 | 599 | 721 | 35 |  |
|  | FRN132SVG1S-4 $\square$ |  | 253 | 304 | 481 | 578 | 22 | 721 | 866 | 29 |  |
|  | FRN160SVG1S-4■ |  | 304 | 377 | 578 | 716 | 18 | 866 | 1074 | 25 |  |
|  | FRN200SVG1S-4 $\square$ |  | 377 | 415 | 716 | 789 | 15 | 1074 | 1183 | 20 |  |
|  | FRN220SVG1S-4 $\square$ |  | 415 | 468 | 789 | 889 | 14 | 1183 | 1334 | 18 |  |
|  | FRN250SVG1S-4 $\square$ |  | 468 | 520 | 889 | 988 | 12 | 1334 | 1482 | 16 |  |
|  | FRN280SVG1S-4 $\square$ |  | 520 | 585 | 988 | 1112 | 11 | 1482 | 1667 | 15 |  |
|  | FRN315SVG1S-4 $\square$ |  | 585 | 650 | 1112 | 1235 | 18 | 1667 | 1853 | 24 |  |
|  | FRN630BVG1S-4 $\square$ | Phasespecific | 1170 | 1370 | 2223 | 2603 | 4.7 | 3335 | 3905 | 6.3 |  |
|  | FRN710BVG1S-4 $\square$ |  | 1370 | 1480 | 2603 | 2812 | 4.0 | 3905 | 4218 | 5.3 |  |
|  | FRN800BVG1S-4 $\square$ |  | 1480 | 1850 | 2812 | 3515 | 3.7 | 4218 | 5273 | 4.9 |  |
|  | FRN90SVG1S-69■ |  | 100 | 130 | 190 | 247 | 85 | 285 | 371 | 114 |  |
|  | FRN110SVG1S-69■ |  | 130 | 140 | 247 | 266 | 66 | 371 | 399 | 88 |  |
|  | FRN132SVG1S-69■ |  | 140 | 161 | 266 | 306 | 61 | 399 | 459 | 81 |  |
|  | FRN160SVG1S-69■ |  | 161 | 216 | 306 | 410 | 53 | 459 | 616 | 71 |  |
|  | FRN200SVG1S-69■ |  | 216 | 265 | 410 | 504 | 40 | 616 | 755 | 53 |  |
|  | FRN250SVG1S-69■ |  | 265 | 295 | 504 | 561 | 33 | 755 | 841 | 43 |  |
|  | FRN280SVG1S-69■ |  | 295 | 330 | 561 | 627 | 29 | 841 | 941 | 39 |  |
|  | FRN315SVG1S-69■ |  | 330 | 365 | 627 | 694 | 26 | 941 | 1040 | 35 |  |
|  | FRN355SVG1S-69■ |  | 365 | 410 | 694 | 779 | 24 | 1040 | 1169 | 31 |  |
|  | FRN400SVG1S-69■ |  | 410 | 460 | 779 | 874 | 21 | 1169 | 1311 | 28 |  |
|  | FRN450SVG1S-69] |  | 460 | - | 874 | - | 19 | 1311 | - | 25 |  |

*1 The OPC-VG1-TBSI (sold separately as option) is necessary.

Note The minimum wiring lengths are specified on condition that the electric wires are in recommended wire sizes (FLSC electric wires). When substantially different electric wires or cabtire shielded wires are used, the wiring inductance changes. Thus, the wiring length should be reviewed.

In the case of a cabtire shield wire, the wiring length should be approximately three times the minimum wiring length specified in this table.

### 9.4.9 Precautions for use

This section explains precautions in setting function codes and during operation. In the direct parallel connection system, restrictions are placed on some functions, such as control interface functions, function codes and monitor codes. See the following details.

### 9.4.9.1 Powering ON

There is no restriction on the order in which the main power (direct current) is supplied to each inverter. However, when some of the inverters in direct parallel connection are not ready to operate, entering an operation command (FWD, REV) causes an alarm trip condition.

### 9.4.9.2 Setting before operation

The function codes listed in Table 9.4-7 should each be set to same setting values among the master inverter and the slave inverters.

Note The motor will not operate normally if the codes each are set to different values.
Table 9.4-7: Function codes requiring same settings

| Function code | Function | Remarks |
| :--- | :--- | :--- |
| F03 to F05, <br> P, A all codes | Motor parameters | Ensure the same setting. |
| F36 | 30Ry mode | Required to design a failure sequence externally. |
| F80 | Current rating switching | Ensure the same setting. |
| H04, H05 | Retry operation | Same setting is required when retry operation is made valid. |
| 033, o34 | Multiple system setting code | Ensure the same setting. |

### 9.4.9.3 Command input

Input an operation command, a speed command or a torque limit, etc. to only the master inverter in the direct parallel connection system. The specification (scale etc. of speed command etc.) of command input is the same with the standard specification.

When the multiple system is canceled by means of a setting made to the $X$ terminal function, operation and speed commands need to be input to the inverters to be driven.


Figure 9.4-8: Command input

### 9.4.9.4 Input/output interface (I/O functions)

When the direct parallel connection system is selected, the input/output interface functions of the slave inverters are restricted. (No restriction is placed on the functions of the master inverter.)

Table 9.4-8 indicates the input/output interface functions available on the slave inverters.
Note When the multiple system is canceled by a setting made to the $X$ terminal, restrictions on the functions are removed.

Table 9.4-8: Restrictions on I/O functions (direct parallel connection system is selected)

| Category | Available functions even on slave (Functions not listed are invalid) | Terminal symbol | Remark |
| :---: | :---: | :---: | :---: |
| Di | Coast to a stop command | [7: BX] | Causes all units of the system to coast to a stop. |
|  | Error reset | [8: RST] | Resets all units of the system. |
|  | External alarm | [9: THR] |  |
|  | Motor M2 selection | [12: M-CH2] |  |
|  | Motor M3 selection | [13: M-CH3] |  |
|  | Keypad edit permission command | [19: WE-KP] |  |
|  | Universal DI | [25: U-DI] |  |
|  | Short voltage cancel | [50: LU-CCL] |  |
|  | Multi-system cancel | [57: MT-CCL] |  |
|  | External simulated failure | [74: FTB] |  |
|  | Life prediction cancel | [76: LF-CCL] |  |
|  | Safety function input terminal | $\begin{aligned} & \text { [EN1] } \\ & \text { [EN2] } \end{aligned}$ | Terminal used exclusively for controlling safety function input. <br> Causes all units of system to coast to a stop. <br> However, output is shut down by hardware for only the units into which the signal is inputted. |
| Do | Operating | [0: RUN] | Operated by operation information from master inverter. |
|  | Stopping under short voltage | [7: LU] |  |
|  | Stopping | [13: STOP] |  |
|  | Operation preparation completion | [14: RDY] | Operation preparation completion signal of self inverter is outputted. |
|  | Motor M2 selection state | [16: SW-M2] |  |
|  | Motor M3 selection state | [17: SW-M3] |  |
|  | Alarm contents | $\begin{array}{\|l\|} \hline \text { [19: AL1] } \\ \text { [20: AL2] } \\ \text { [21: AL4] } \\ \text { [22: AL8] } \\ \hline \end{array}$ | Alarm information about master inverter and self inverter are added on 4 bits and outputted. |
|  | Cooling fan operating | [23: FAN] |  |
|  | Universal DO | [25: U-DO] |  |
|  | Cooling fin overheat prediction | [26: INV-OH] |  |
|  | Life prediction | [28: LIFE] |  |
|  | Inverter overload prediction | [31: INV-OL] |  |
|  | DB overload prediction | [34: DB-OL] |  |
|  | Transmission error | [35: LK-ERR] |  |
|  | Multi-system communication established | [51: MTS] |  |
|  | Multi-system cancel response | [52: MEC-AB] |  |
|  | Multi-system self station failure | [54: AL-SF] |  |
|  | Batch alarm | [56: ALM] |  |
|  | Light failure | [57: L-ALM] |  |
|  | Maintenance prediction | [58: MNT] |  |
|  | DC fan lock signal | [60: DCFL] |  |
|  | 73 input command | [71: PRT-73F] |  |
|  | Y terminal test output ON | [72: Y -ON] |  |
|  | Y terminal test output OFF | [73: Y-OFF] |  |
|  | Clock battery life | [75: BATT] |  |
|  | EN terminal detection circuit error | [80: DECF] |  |
|  | EN terminal OFF | [81: ENOFF] |  |
|  | Safety function operating | [82: SF-RUN] |  |
|  | Motor stopping by safety function | [83: SF-STP] |  |
|  | During STO test by safety function | [84: SF-TST] |  |
| Ai | Universal Ai | [14: U-Ai] |  |
|  | Others, invalid |  |  |
| Ao | Motor current | [I-AC] |  |
|  | Motor voltage | [ V -AC] |  |
|  | DC intermediate voltage | [VDC] |  |
|  | +10, -10 V test | [P10, N10] |  |

[^17]
### 9.4.9.5 Keypad functions

When the direct parallel connection system is selected, the keypad functions of the slave inverters are restricted. (No restriction is placed on the functions of the master inverter.)

Table 9.4-9 indicates keypad functions available on the slave inverters.
Note - When the multiple system is canceled by a setting made to the $X$ terminal function, restrictions on the functions are removed.

- All other functions work effectively such as I/O check, maintenance information, load rate measurement, I/O status upon alarm, alarm history and copy function.

Table 9.4-9: Restrictions on keypad monitor display (direct parallel connection system is selected)

| Category | Name | Remarks |
| :---: | :---: | :---: |
|  | Output current detection value | Displays current detection value of self inverter |
|  | Output voltage detection value | Displays voltage detection value of self inverter |
|  | DC intermediate voltage detection value | Displays intermediate voltage detection value of self inverter |
|  | Output current detection value | Displays current detection of self inverter |
|  | Output voltage detection value | Displays voltage detection of self inverter |
|  | Output current detection value upon alarm occurrence | Displays current detection value of self inverter upon alarm trip |
|  | Output voltage detection value upon alarm occurrence | Displays current detection value of self inverter upon alarm trip |
|  | Accumulated operation time upon alarm occurrence | Displays voltage detection value of self inverter upon alarm trip |
|  | Motor output command value upon alarm occurrence | Outputs motor output command value multiplied by the number of inverters upon alarm trip |
|  | Inverter inside air upon alarm occurrence | Displays inside air temperature of self inverter upon alarm trip |
|  | Cooling fin temperature upon alarm occurrence | Displays cooling fin temperature of self inverter upon alarm trip |
|  | Communication status upon alarm occurrence (4 points) |  |

### 9.4.9.6 Function codes (F to U)

When the direct parallel connection system is selected, the function codes ( $F$ to $U$ ) of the slave inverters are restricted. (No restriction is placed on the functions of the master inverter.)
Table 9.4-10 to Table 9.4-14 below summarize restrictions on the slave inverters. Beware of the

0: Setting becomes invalid
1: Setting becomes valid (Code that has to be set to same value as master inverter)
2: Setting becomes valid (Code that does not have to be set to same value as master inverter)
3: Setting becomes valid (Code for which setting specific to multi-winding is required) details.
Note that certain function codes must be set to the same value for both the master and slave inverters.
Table 9.4-10: Slave inverters: Categories for F00 to F85

| Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F00 | 2 | F11 | 0 | F24 | 0 | F42 | 0 | F51 | 2 | F60 | 2 | F69 | 0 | F80 | 1 |
| F01 | 0 | F12 | 0 | F26 | 0 | F43 | 0 | F52 | 2 | F61 | 0 | F70 | 0 | F81 | 0 |
| F02 | 2 | F14 | 0 | F27 | 0 | F44 | 0 | F53 | 2 | F62 | 0 | F73 | 0 | F82 | 0 |
| F03 | 1 | F17 | 0 | F36 | 1 | F45 | 0 | F54 | 2 | F63 | 0 | F74 | 0 | F83 | 0 |
| F04 | 1 | F18 | 0 | F37 | 0 | F46 | 0 | F55 | 2 | F64 | 0 | F75 | 0 | F84 | 2 |
| F05 | 1 | F20 | 0 | F38 | 0 | F47 | 0 | F56 | 2 | F65 | 0 | F76 | 0 | F85 | 0 |
| F07 | 0 | F21 | 0 | F39 | 0 | F48 | 0 | F57 | 2 | F66 | 0 | F77 | 0 |  |  |
| F08 | 0 | F22 | 0 | F40 | 0 | F49 | 0 | F58 | 2 | F67 | 0 | F78 | 0 |  |  |
| F10 | 0 | F23 | 0 | F41 | 0 | F50 | 0 | F59 | 2 | F68 | 0 | F79 | 2 |  |  |

Table 9.4-11: Slave inverters: Categories for E01 to E118

| Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E01 | 2 | E14 | 2 | E27 | 2 | E40 | 0 | E53 | 0 | E66 | 0 | E79 | 2 | E106 | 0 |
| E02 | 2 | E15 | 2 | E28 | 2 | E41 | 0 | E54 | 0 | E67 | 0 | E80 | 2 | E107 | 0 |
| E03 | 2 | E16 | 2 | E29 | 0 | E42 | 0 | E55 | 0 | E68 | 0 | E81 | 2 | E108 | 0 |
| E04 | 2 | E17 | 2 | E30 | 0 | E43 | 0 | E56 | 0 | E69 | 2 | E82 | 2 | E109 | 0 |
| E05 | 2 | E18 | 2 | E31 | 0 | E44 | 0 | E57 | 0 | E70 | 2 | E83 | 2 | E110 | 0 |
| E06 | 2 | E19 | 2 | E32 | 0 | E45 | 0 | E58 | 0 | E71 | 2 | E84 | 2 | E114 | 0 |
| E07 | 2 | E20 | 2 | E33 | 0 | E46 | 0 | E59 | 0 | E72 | 2 | E90 | 0 | E115 | 0 |
| E08 | 2 | E21 | 2 | E34 | 0 | E47 | 0 | E60 | 0 | E73 | 2 | E91 | 0 | E116 | 0 |
| E09 | 2 | E22 | 2 | E35 | 2 | E48 | 0 | E61 | 0 | E74 | 2 | E101 | 0 | E117 | 0 |
| E10 | 2 | E23 | 2 | E36 | 2 | E49 | 0 | E62 | 0 | E75 | 2 | E102 | 0 | E118 | 0 |
| E11 | 2 | E24 | 2 | E37 | 2 | E50 | 0 | E63 | 0 | E76 | 2 | E103 | 0 |  |  |
| E12 | 2 | E25 | 2 | E38 | 0 | E51 | 0 | E64 | 0 | E77 | 2 | E104 | 0 |  |  |
| E13 | 2 | E26 | 2 | E39 | 0 | E52 | 0 | E65 | 0 | E78 | 2 | E105 | 0 |  |  |

Note - Only the functions listed in "Section 9.4.9.4" (Pages 9-31) are effective for E01 to E13, E15 to E27 and E69 to E73.

- C01 to C73: All 0
- P01 to P27: 1, P28 to P58: 0

Table 9.4-12: Slave inverters: Categories for H 01 to H 227

| Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| H01 | 0 | H20 | 0 | H36 | 2 | H53 | 0 | H74 | 0 | H90 | 0 | H118 | 1 |  |  |
| H02 | 2 | H21 | 0 | H37 | 2 | H55 | 0 | H75 | 0 |  |  | H142 | 2 |  |  |
| H03 | 2 | H22 | 0 | H38 | 2 | H56 | 0 | H76 | 2 |  |  | H149 | 0 |  |  |
| H04 | 1 | H23 | 0 | H39 | 2 | H57 | 0 | H77 | 2 | H105 | 2 |  |  |  |  |
| H05 | 1 | H24 | 0 | H40 | 2 | H58 | 0 | H78 | 2 | H106 | 2 |  |  |  |  |
| H06 | 2 | H25 | 0 | H41 | 0 | H60 | 0 | H79 | 2 | H107 | 2 |  |  |  |  |
| H08 | 0 | H26 | 0 | H42 | 0 | H61 | 0 | H80 | 2 | H108 | 2 |  |  |  |  |
| H09 | 0 | H27 | 0 | H43 | 0 | H62 | 0 | H81 | 2 | H109 | 2 |  |  |  |  |
| H10 | 0 | H28 | 0 | H44 | 0 | H63 | 0 | H82 | 2 | H110 | 2 |  |  |  |  |
| H11 | 0 | H29 | 2 | H46 | 0 | H64 | 0 | H83 | 2 | H111 | 2 |  |  |  |  |
| H13 | 0 | H30 | 1 | H47 | 0 | H65 | 0 | H84 | 2 | H112 | 1 |  |  |  |  |
| H14 | 0 | H31 | 2 | H48 | 0 | H66 | 0 | H85 | 2 | H113 | 1 |  |  |  |  |
| H15 | 0 | H32 | 2 | H49 | 0 | H67 | 0 | H86 | 2 | H114 | 1 |  |  |  |  |
| H16 | 0 | H33 | 2 | H50 | 0 | H68 | 2 | H87 | 2 | H115 | 1 |  |  |  |  |
| H17 | 0 | H34 | 2 | H51 | 0 | H70 | 0 | H88 | 2 | H116 | 1 |  |  |  |  |
| H19 | 0 | H35 | 2 | H52 | 0 | H71 | 0 |  |  | H117 | 1 |  |  |  |  |

Note - H2O1 to H227: All 0

- A01 to A29, A32 to A34: 1
- A30, A31, A51, A71 to A74, A101 to A129, A132 to A134: 1, A130, A131, A151, A171 to A174: 0

Table 9.4-13: Slave inverters: Categories for o01 to o50

| Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 001 | 0 | O04 | 0 | o07 | 0 | o13 | 0 | O16 | 0 | o19 | 0 | o32 | 2 | o50 | 3 |
| -02 | 0 | -05 | 0 | -08 | 0 | -14 | 0 | 017 | 0 | o30 | 2 | o33 | 3 |  |  |
| 003 | 0 | o06 | 0 | 012 | 0 | o15 | 0 | o18 | 0 | o31 | 2 | o34 | 3 |  |  |

Note - L01 to L15: All 0

- U code: All 2


### 9.4.9.7 Function codes (S: command data)

When the direct parallel connection system is selected, the function codes (S: command data) of the slave inverters are restricted. (No restriction is placed on the functions of the master inverter.)
Only S06 "Operation command 1" and S07 "Universal DO" of the slave inverters work effectively.
Note, however, that only the functions listed in "Section 9.4.9.4" (Pages 9-31) are valid.

### 9.4.9.8 Function codes (M: monitor codes)

When the direct parallel connection system is selected, the function codes (M: monitor codes) of the slave inverters are restricted. (No restriction is placed on the functions of the master inverter.)
Table 9.4-14 below summarizes restrictions on the slave inverters. Beware of the details.
Table 9.4-14: Slave inverters: Categories for M01 to M222

| Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category | Code | Category |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M01 | 0 | M22 | 0 | M43 | 1 | M65 | 1 | M86 | 1 | M114 | 0 | M139 | 1 | M162 | 0 |
| M02 | 0 | M23 | 1 | M44 | 1 | M66 | 1 | M91 | 1 | M115 | 1 | M140 | 1 | M163 | 0 |
| M03 | 1 | M24 | 1 | M45 | 1 | M67 | 1 | M92 | 1 | M116 | 1 | M141 | 1 | M164 | 0 |
| M04 | 0 | M25 | 1 | M46 | 1 | M68 | 1 | M93 | 1 | M119 | 1 | M142 | 1 | M165 | 0 |
| M05 | 1 | M26 | 1 | M47 | 1 | M69 | 1 | M94 | 1 | M120 | 1 | M143 | 1 | M166 | 1 |
| M06 | 1 | M27 | 0 | M48 | 1 | M70 | 1 | M95 | 1 | M121 | 1 | M144 | 1 | M167 | 1 |
| M07 | 1 | M28 | 0 | M49 | 0 | M71 | 1 | M96 | 1 | M123 | 1 | M147 | 0 | M168 | 1 |
| M08 | 1 | M29 | 1 | M50 | 0 | M72 | 1 | M100 | 1 | M124 | 1 | M148 | 1 | M169 | 1 |
| M09 | 1 | M30 | 0 | M51 | 0 | M73 | 1 | M101 | 1 | M125 | 1 | M149 | 1 | M170 | 1 |
| M10 | 2 | M31 | 1 | M52 | 1 | M74 | 1 | M102 | 0 | M126 | 1 | M150 | 1 | M171 | 1 |
| M11 | 1 | M32 | 1 | M53 | 1 | M75 | 1 | M103 | 1 | M127 | 1 | M151 | 1 | M172 | 1 |
| M12 | 1 | M33 | 1 | M54 | 1 | M76 | 0 | M104 | 1 | M128 | 1 | M152 | 1 | M177 | 0 |
| M13 | 1 | M34 | 1 | M55 | 1 | M77 | 1 | M105 | 1 | M129 | 1 | M153 | 1 | M178 | 0 |
| M14 | 1 | M35 | 1 | M56 | 1 | M78 | 0 | M106 | 0 | M130 | 0 | M154 | 1 | M179 | 0 |
| M15 | 1 | M36 | 2 | M57 | 1 | M79 | 1 | M107 | 0 | M132 | 1 | M155 | 1 | M180 | 0 |
| M16 | 1 | M37 | 1 | M58 | 1 | M80 | 1 | M108 | 0 | M133 | 1 | M156 | 1 | M185 | 0 |
| M17 | 1 | M38 | 1 | M59 | 1 | M81 | 1 | M109 | 0 | M134 | 1 | M157 | 1 | M186 | 1 |
| M18 | 1 | M39 | 1 | M60 | 1 | M82 | 1 | M110 | 0 | M135 | 1 | M158 | 1 | M221 | 0 |
| M19 | 1 | M40 | 1 | M62 | 1 | M83 | 1 | M111 | 1 | M136 | 1 | M159 | 1 | M222 | 0 |
| M20 | 1 | M41 | 1 | M63 | 1 | M84 | 1 | M112 | 0 | M137 | 1 | M160 | 1 |  |  |
| M21 | 1 | M42 | 1 | M64 | 1 | M85 | 1 | M113 | 0 | M138 | 1 | M161 | 0 |  |  |

### 9.5 Motors

### 9.5.1 Vibration, noise and vibration proof

Vibration level, noise level and vibration proof of the vector dedicated motors are as specified in Table 9.5-1.
Table 9.5-1: Vibration level, noise level and vibration proof of vector dedicated motors

| Dedicated applicable motor Note <br> 1) [kW] |  | Type | Vibration level [ $\mu \mathrm{m}$ ] |  | Noise level [dB (A)] Note 2) |  | Vibration proof [ $\mathrm{m} / \mathrm{s}^{2}$ ] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MVK_ | Base speed 1500 [r/min] | Maximum speed <br> Note 3) 3600 [r/min] | Base speed 1500 [r/min] | Maximum speed 3600 [r/min] |  |
| 22 | 4 | 8185A | 5 or less | 7 or less | 71 | 73 | 7 or less Note 4) |
| 30 |  | 8187A |  | 7 or less |  | 73 |  |
| 37 |  | 8207A |  |  |  |  |  |
| 45 |  | 8208A | 5 or less | 7 or less Note 5) | 71 | 73 |  |
| 55 |  | 9224A | Note 5) | 15 or less | Note 5) | Note 5) |  |
| 75 |  | 9254A |  |  |  |  |  |
| 90 |  | 9256A |  |  |  |  |  |
| 110 |  | 9284A |  |  |  |  |  |
| 132 |  | 9286A |  |  |  |  |  |
| 160 |  | 528KA |  |  |  |  |  |
| 200 |  | 528LA |  |  |  |  |  |
| 220 |  | 531FA |  |  |  |  |  |
| 250 |  | 531GA |  |  |  |  |  |
| 280 |  | 531 HA |  |  |  |  |  |
| 300 |  | 535GA |  |  |  |  |  |
| 315 |  | 535GA |  |  |  |  |  |
| 355 |  | 535HA |  |  |  |  |  |
| 400 |  | 535JA |  |  |  |  |  |

Note 1) See the section "2.3.1 Dedicated motor specifications" in Chapter 2 for the specifications and external shape drawings of the dedicated motors.
Note 2) Values are the levels measured at the position 1 [ m ] away from the motor in the direction of terminal box.
Note 3) Maximum speed is $3000[\mathrm{r} / \mathrm{min}]$ for 30 to $45[\mathrm{~kW}], 2400[\mathrm{r} / \mathrm{min}]$ for 55 to $75[\mathrm{~kW}]$ and $2000[\mathrm{r} / \mathrm{min}]$ for 90 to 220 [kW].
Note 4) If actual vibration exceeds the values above, a separate anti-vibration measure is required.
Note 5) Contact us individually.

### 9.5.2 Allowable radial load on shaft end



Maximum allowable values of radial load applied by the belt are shown in the Figure below for each frame number and rotation speed.
The allowable values in the Figure indicate that, when the point determined by the radial load FA $[\mathrm{kN}]$ acting on the motor shaft and the length $L[\mathrm{~mm}]$ from the stepped part of the shaft end to the center of the pulley (the distance between FA loaded points) is within the curve, the motor can be driven by that pulley.

Refer to the technical leaflet of induction motors for the details.
Contact us individually when using a motor ( 55 kW or larger) exceeding the Frame No. 200L.

Figure 9.5-1: Explanation of load applied point


### 9.5.3 Allowable thrust load

Allowable thrust loads on the vector dedicated motors are as specified in Table 9.5-2.

Table 9.5-2: Allowable thrust loads on vector dedicated motors Unit: kN (kgf)


Note (1) In Frame No. 250S and larger, allowable thrust loads on the motors for direct connection are specified.
(2) The allowable thrust loads in this table are calculated based on the assumption that the radial load is borne by the normal sized half coupling.

### 9.5.4 List of special combinations

### 9.5.4.1 Combination list of 380 V series

When building a system comprising our vector dedicated motor, FRENIC-VG inverters and RHD-D series diode rectifier converters, and if the system receives an incoming voltage of 380 VAC, select inverters with capacities which are one rank higher than the capacity of the motor as specified in Table 9.5-3.

Table 9.5-3: Reference table in the case of incoming voltage of 380 V (only in the case of FRENIC-VG + RHD-D series)

| Type |  | 4-pole non-standard special motor |  |  | 4-pole standard motor |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base speed [r/min] |  | 1500 |  |  | Base speed: 1,500 [r/min], <br> Max. speed: 1,500 [r/min] |  |  |
| Max. load torque [\%] |  | 150 |  |  | 150 |  |  |
| Model/Item |  |  | odel | Max. speed Nmax [r/min] | Model |  | Potential max speed Nmax [r/min] Note 2) |
|  |  | Motor MVK $\qquad$ | Inverter <br> FRN $\qquad$ |  | Motor <br> MVK $\qquad$ | Inverter <br> FRN $\qquad$ |  |
| Output | 22 | 8185A | 30SVG1S-4■ | 3600 | 8185A | - | 2000 |
|  | 30 | 8187A | 37SVG1S-4■ |  | 8187A | 30SVG1S-4 $\square$ | 2200 |
|  | 37 | 8207A | 45SVG1S-4■ |  | 8207A | 37SVG1S-4 $\square$ | 1600 |
|  | 45 | 8208A | 55SVG1S-4■ |  | 8208A | 45SVG1S-4 $\square$ | 2100 |
|  | 55 | 9224A | 75SVG1S-4■ | 2400 | 9224A | 55SVG1S-4 $\square$ | 1600 |
|  | 75 | 9254A | 90SVG1S-4■ |  | 9254A | 75SVG1S-4 $\square$ | 2000 |
|  | 90 | 9256A | 110SVG1S-4 $\square$ | 2000 | 9256A | 90SVG1S-4 $\square$ | 2000 |
| [kW] | 110 | 9284A | 132SVG1S-4 $\square$ |  | 9284A | 110SVG1S-4 $\square$ | 2000 |
|  | 132 | 9286A ${ }^{\text {Note1) }}$ | 160SVG1S-4 $\square$ |  | 9286A | 132SVG1S-4 $\square$ | 1500 |
|  | 160 | 528KA ${ }^{\text {Note1) }}$ | 200SVG1S-4 $\square$ |  | 528KA | 160SVG1S-4 $\square$ | 1500 |
|  | 200 | 528LA ${ }^{\text {Note1) }}$ | 220SVG1S-4 $\square$ |  | 528LA | 200SVG1S-4 $\square$ | 1500 |
|  | 220 | 531FA ${ }^{\text {Note1) }}$ | 280SVG1S-4■ |  | 531FA | 220SVG1S-4 $\square$ | 1500 |

Note 1) The electrical characteristics of the motor are the same with those of the standard motor. The motor is combined with inverter with higher capacity.
Note 2) The maximum rotation speed is specified at which the $150 \%$ overload rated torque can be obtained with 380 V input. When a $150 \%$ overload constant is required at the speed or faster, select one rank higher inverter to increase the capacity.

This table is not applicable when PWM converters (RHC-D series) are used. (Inverters are applicable in the combination of standard specifications.)

### 9.5.4.2 Combination list of low base speed series

When driving a low base speed motor of which base rotation speed is slower than that of the standard vector dedicated motor, see Table 9.5-4 to select an applicable inverter.

Table 9.5-4: Combinations of inverters and low base speed motors

| No. of poles, standard/ non-standard |  | 6-pole non-standard special motor |  |  |  |  |  | 4-pole standard motor |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base speed |  | 500 [r/min] | 650 [r/min] | 750 [r/min] | 850 [r/min] | 1,000 [r/min] |  | 1,000 [r/min] |  |
| Max. speed |  | 2,000 [r/min] | 2,000 [r/min] | 1,800 [r/min] | 1,700 [r/min] | 2,000 [r/min] | 2,400 [r/min] | 3,000 [r/min] | 3,600 [r/min] |
| Output <br> [kW] | 22 | MVK9284A <br> FRN37SVG1S -4 $\square$ | MVK9250A FRN30SVG1S -4 $\square$ | MVK8207A FRN30SVG1S -4 $\square$ |  | MVK8187A FRN30SVG1S -4 $\square$ |  | MVK8207A FRN37SVG1S -4 $\square$ |  |
|  | 30 | MVK9284A <br> FRN45SVG1S -4 $\square$ | MVK9256A FRN37SVG1S -4 $\square$ |  | MVK9221A FRN37SVG1S -4 $\square$ | MVK8207A FRN37SVG1S -4 $\square$ |  | MVK8208A FRN45SVG1S $-4 \square$ |  |
|  | 37 | MVK9286A FRN55SVG1S -4 $\square$ | MVK9284A FRN45SVG1S -4 $\square$ |  | MVK9224A FRN45SVG1S -4 $\square$ | MVK9221A FRN45SVG1S -4 $\square$ |  |  |  |
|  | 45 | MVK528KA FRN75SVG1S -4 $\square$ | MVK9284A FRN55SVG1S -4 $\square$ |  | MVK9250A FRN55SVG1S -4 $\square$ | MVK9224A FRN55SVG1S $-4 \square$ |  |  |  |
|  | 55 | MVK528LA <br> FRN75SVG1S -4 $\square$ | MVK9286A FRN75SVG1S$4 \square$ |  | MVK9256A FRN75SVG1S -4 $\square$ | MVK9250A FRN75SVG1S -4 $\square$ |  |  |  |
|  | 75 | MVK531GA <br> FRN110SVG1S -4 $\square$ | MVK528LA FRN90SVG1S$4 \square$ |  | MVK9284A FRN90SVG1S -4 $\square$ | MVK9256A FRN90SVG1S -4 $\square$ |  |  |  |
|  | 90 | MVK531HA FR132SVG1S -4 $\square$ | MVK531GA FRN110SVG1S $-4 \square$ |  | MVK9286A FRN110SVG1S -4 $\square$ | MVK9284A FRN110SVG1S $-4 \square$ |  |  |  |
|  | 110 |  | MVK531HA FRN132SVG1S -4 $\square$ |  | MVK528KA FRN132SVG1S -4 $\square$ | MVK9286A FRN132SVG1S -4 $\square$ |  |  |  |
|  | 132 |  | MVK531HA FRN200SVG1S -4 $\square$ |  | MVK528LA FRN160SVG1S $-4 \square$ | MVK528KA FRN160SVG1S -4 $\square$ |  |  |  |
|  | 160 |  |  |  |  | MVK528LA FRN200SVG1S -4■ |  |  |  |
|  | 200 |  |  |  |  | Note 1) |  |  |  |

Note 1) Contact us separately.

### 9.6 Conversion from SI units

The SI units are used for all calculation formulae given in this chapter "Model Selection." This section explains conversion formulae and calculation formulae to other units.

### 9.6.1 Conversion of units

(1) Force

- $1[k g f] \approx 9.8 \quad[\mathrm{~N}]$
- $1[N] \approx 0.102[k g f]$
(2) Torque
- $1[\mathrm{kgf} \cdot \mathrm{m}] \approx 9.8[N \cdot \mathrm{~m}]$
- $1[\mathrm{~N} \cdot \mathrm{~m}] \approx 0.102[\mathrm{kgf} \cdot \mathrm{m}]$
(3) Work and energy
- $1[\mathrm{kgf} \cdot \mathrm{m}] \approx 9.8[\mathrm{~N} \cdot \mathrm{~m}]=9.8[\mathrm{~J}]=9.8[\mathrm{~W} \cdot \mathrm{~s}]$
(4) Power
- $1[\mathrm{kgf} \cdot \mathrm{m} / \mathrm{s}] \approx 9.8[\mathrm{~N} \cdot \mathrm{~m} / \mathrm{s}]=9.8[\mathrm{~J} / \mathrm{s}]=9.8 \quad[\mathrm{~W}]$
- $1[N \cdot \mathrm{~m} / \mathrm{s}] \approx 1[\mathrm{~J} / \mathrm{s}]=1[\mathrm{~W}] \approx 0.102[\mathrm{kgf} \cdot \mathrm{m} / \mathrm{s}]$
(5) Rotation speed
- $1[\mathrm{r} / \mathrm{min}]=\frac{2 \pi}{60}[\mathrm{rad} / \mathrm{s}]=0.1047[\mathrm{rad} / \mathrm{s}]$
- $1[\mathrm{rad} / \mathrm{s}]=\frac{60}{2 \pi}[\mathrm{r} / \mathrm{min}]=9.549[\mathrm{r} / \mathrm{min}]$


### 9.6.2 Calculation formulae

(1) Torque, power, and rotation speed

- $P[W] \approx \frac{2 \pi}{60} \cdot N \quad[r / \mathrm{min}] \cdot \tau \quad[N \cdot m]$
- $P[W]=1.026 \cdot N \quad[r / \mathrm{min}] \cdot T \quad[\mathrm{~kg} f \cdot \mathrm{~m}]$
- $\tau[N \cdot m] \approx 9.55 \cdot \frac{P[W]}{N[r / \mathrm{min}]}$
- $T[\mathrm{kgf} \cdot \mathrm{m}] \approx 0.974 \cdot \frac{P[W]}{N[r / \mathrm{min}]}$
(2) Kinetic energy
- $E[W] \approx \frac{1}{182.4} \cdot J \quad\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right] \cdot N^{2}\left[(\mathrm{r} / \mathrm{min})^{2}\right]$
- $E[W] \approx \frac{1}{730} \cdot G D^{2}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right] \cdot N^{2}\left[(\mathrm{r} / \mathrm{min})^{2}\right]$
(3) Torque of linear moving load [Driving mode]
- $\tau[N \cdot m] \approx 0.159 \cdot \frac{V[\mathrm{~m} / \mathrm{min}]}{N_{M}[\mathrm{r} / \mathrm{min}] \cdot \eta_{G}} \cdot F \quad[\mathrm{~N}]$
- $T[\mathrm{kgf} \cdot \mathrm{m}] \approx 0.159 \cdot \frac{V[\mathrm{~m} / \mathrm{min}]}{N_{M}[\mathrm{r} / \mathrm{min}] \cdot \eta_{G}} \cdot F \quad[\mathrm{kgf}]$
[Braking mode]
- $\tau[N \cdot m] \approx 0.159 \cdot \frac{V[\mathrm{~m} / \mathrm{min}]}{N_{M}[r / \mathrm{min}] /} \cdot F \quad[N]$
- $T[\mathrm{kgf} \cdot \mathrm{m}] \approx 0.159 \cdot \frac{V[\mathrm{~m} / \mathrm{min}]}{N_{M}[\mathrm{r} / \mathrm{min}] / \eta_{G}} \cdot F \quad[\mathrm{~kg} f]$
(6) Inertia constant
- J $\left[\mathrm{kg} \cdot \mathrm{m}^{2}\right] \quad:$ Moment of inertia
- $G D^{2}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]$ : Flywheel effect
- $G D^{2}=4 J$
- $J=\frac{G D^{2}}{4}$
(7) Pressure and stress
- $1[m m A q] \approx 9.8[P a] \approx 9.8\left[\mathrm{~N} / \mathrm{m}^{2}\right]$
- $1[\mathrm{~Pa}] \approx 1\left[\mathrm{~N} / \mathrm{m}^{2}\right] \approx 0.102[\mathrm{mmAq}]$
- $1[\mathrm{bar}] \approx 100000[\mathrm{~Pa}] \approx 0.102\left[\mathrm{~kg} \cdot \mathrm{~cm}^{2}\right]$
- $1\left[\mathrm{~kg} \cdot \mathrm{~cm}^{2}\right] \approx 98000[\mathrm{~Pa}] \approx 980[\mathrm{mbar}]$
- 1 atmosphere $=1013[\mathrm{mbar}]=760[\mathrm{mmHg}]$

$$
=101300[\mathrm{~Pa}] \approx 1.033\left[\mathrm{~kg} / \mathrm{cm}^{2}\right]
$$

[Driving mode]

- $\tau[N \cdot m] \approx \frac{J\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{9.55} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}]}{\Delta t s[s] \cdot \eta_{G}}$
[Braking mode]
- $\tau[N \cdot \mathrm{~m}] \approx \frac{J\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{9.55} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}] \cdot \eta_{G}}{\Delta t s[s]}$
- $T[\mathrm{kgf} \cdot \mathrm{m}] \approx \frac{G D^{2}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{375} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}] \cdot \eta_{G}}{\Delta t s[\mathrm{~s}]}$
(5) Acceleration time
- $t_{A C C}[s] \approx \frac{J 1+J 2 / \eta_{G}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{\tau M-\tau L / \eta_{G}[\mathrm{~N} \cdot \mathrm{~m}]} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}]}{9.55}$
- $t_{A C C}[s] \approx \frac{G D 1^{2}+G D 2^{2} / \eta_{G}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{T_{M}-T_{L} / \eta_{G}[\mathrm{kgf} \cdot \mathrm{m}]} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}]}{375}$
(6) Deceleration time
- $t_{D E C}[s] \approx \frac{J 1+J 2 \cdot \eta_{G}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{\tau M-\tau L / \eta_{G}[N \cdot \mathrm{~m}]} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}]}{9.55}$
- $t_{D E C}[s] \approx \frac{G D 1^{2}+G D 2^{2} \cdot \eta_{G}\left[\mathrm{~kg} \cdot \mathrm{~m}^{2}\right]}{T_{M}-T_{L} \cdot \eta_{G}[\mathrm{~kg} f \cdot \mathrm{~m}]} \cdot \frac{\Delta N[\mathrm{r} / \mathrm{min}]}{375}$


## FRENIC-VG

10

## Chapter 10Maintenance and

## Inspection

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### 10.1 Inspection cycle

Perform inspections based on the details and cycle shown in Table 10.1-1.
Table 10.1-1 List of periodic inspections

| Name of inspection | Cycle | Details of inspection |
| :--- | :--- | :--- |
| Daily inspection | Every day | See Daily inspection |
| Periodic inspection | Once every year | See Periodic inspection |
| 10-year inspection *1 | Once every 10 years | Replacement of the cooling fans of the inverter and some converters *2 <br> Replacement and detailed check of the capacitors of the main circuit |

*1 The 10-year inspection must be performed by a person who has received training by Fuji Electric. Contact your Fuji Electric representative. (Except for replacement of the cooling fans.)
*2 For the standard replacement frequency of the cooling fans, see "10.4 Periodic replacement parts."

For stack-type models, the service life of each component is estimated when the model is used under an ambient temperature of $30^{\circ} \mathrm{C}$ and a load rate of $100 \%$ for the MD spec and $80 \%$ for the LD spec.
The replacement cycle may be shortened in an environment where the ambient temperature is higher than the environment spec of $30^{\circ} \mathrm{C}$ or where exposed to heavy dust.
The standard replacement frequency is for reference only, and not meant to guarantee service life.

### 10.2 Daily inspection

Visually inspect the inverter from outside whether there is any failure while it is in operation and powered on and the covers remain installed.
Perform the following inspections:
Table 10.2-1 List of daily inspections

| Location | Item | Method | Criteria |
| :---: | :---: | :---: | :---: |
| Ambient environment | (1) Check the ambient temperature, humidity, vibration, atmosphere (dust, gas, oil mist, drop of water, etc.). <br> (2) Check if there is any tool and/or hazardous material around the inverter. | (1) Check them visually and make measurement using gauges. <br> (2) Check them visually. | (1) The specifications stipulated in "2.2.1 Installation environment" of Chapter 2 must be satisfied. <br> (2) No tools and hazardous materials must be left. |
| External appearance, etc. | (1) Check if the fixing screws of the main circuit and control wiring are loosened. (*Check them before the inverter is powered on.) <br> (2) Check if there is any trace of overheat and/or discoloration, etc. <br> (3) Check if there is any abnormal noise, abnormal vibration, and/or offensive smell, etc. | (1) Tighten the screws firmly. <br> (2) Check them visually. <br> (3) Check them by listening, viewing, and smelling. | (1) The screws must not be loosened. If they are loosened, tighten them firmly. <br> 2) \& 3) There must be no such faults. |
| Cooling fan | Check if any abnormal noise and/or abnormal vibration is generated while they are in operation. | Check them by listening and viewing. | There must be no such faults. |
| Display on keypad | Check if any alarm appears on the keypad. | Check it visually. | For the alarms, see Chapter 11 "Troubleshooting". |
| Performance | Check if the expected performance (which meets the standard specifications) is obtained. | Check the monitor of the keypad. | There must be no fault in the operation data including the operation frequency, current, and voltage, etc. |
| Door (cabinet) | Check if the door is opened and closed smoothly. <br> Check if the handle moves without any problems. <br> Check if the bolts of the hinges and hooks are not loosened. <br> Check if there is no hole in the air filter. | Check them visually and actually operate them. | (1) The door must be opened and closed smoothly. <br> (2) The screws must not be loosened, and the filter must not get dirty outstandingly and have holes. |

### 10.3 Periodic inspection

In the periodic inspection, the inspection items and methods vary according to the power condition, etc. This section explains the inspection items for each power condition.

### 10.3.1 Periodic inspection 1 (Before power is on or after operation is stopped)

Among the periodic inspection items, those that must be checked before the power is on and immediately after the operation is stopped are explained in Table 10.3-1. Regarding the inspection items for immediately after the operation is stopped, be sure to shut down the power and detach the front cover before performing the inspection.
It takes time until the capacitors of the main circuit discharge after the power is turned OFF.
For safety, after the charge lamp (CHARGE) of the inverter is turned OFF, check that the DC voltage is lowered to the safe level ( $\mathrm{DC}+25 \mathrm{~V}$ or less) using a tester, etc., and then start the inspection.

Table 10.3-1 List of periodic inspections 1

|  | Location | Item | Method | Criteria |
| :---: | :---: | :---: | :---: | :---: |
| Structural parts including cases and covers of cabinet and inverter |  | 1) Check if the bolts (tightening sections) are not loosened. <br> 2) Check if there is any deformation and breakage. <br> (Check if the cabinet is not deformed.) <br> 3) Check if there is any discoloration caused by overheat. <br> 4) Check if any dirt and/or dust is affixed. | 1) Tighten the bolts firmly. <br> 2), 3), 4) Check them visually. | 1), 2), 3), 4) There must be no such faults. <br> If any dirt is affixed, wipe it with a soft cloth. |
| Air suction filter (cabinet) |  | Check if there is any hole on the filter. Check if significant dust is affixed. Check if the air filer is hardened. | 1), 2) Check them visually. <br> 3) Touch the filter by hand. | 1), 2) There must be no such faults. <br> 3) The fabric must not be damaged. |
|  | Common | 1) Check if the bolts, etc. are not loosened or dropped. <br> 2) Check if there is any arc mark, deformation, crack, breakage, and/or discoloration caused by overheat and/or deterioration on the devices and insulation materials (insulation sheets, insulation tubes, and other insulators). <br> 3) Check if any dirt and/or dust is affixed. | 1) Tighten them firmly. <br> 2), 3) Check them visually. | 1), 2), 3) There must be no such faults. <br> If any dirt is affixed, wipe it with a soft cloth. <br> It might be difficult to find arc marks on the devices because they have a protection cover, etc. |
|  | Conductor/ Electric wire | 1) Check if there is any discoloration and/or warp caused by overheat on the conductors. <br> 2) Check if there is any tear, crack, or discoloration on the covers of the electric wires. | 1), 2) Check them visually. | 1), 2) There must be no such faults. |
|  | Terminal block | Check if it is damaged. | Check it visually. | There must be no such fault. |
|  | Capacitors in main circuit | 1) Check if there is any liquid leakage, discoloration, crack, and extension of the cases. <br> 2) Check if the safety valve sticks out and if any valve extends too much. <br> 3) Measure the electrostatic capacity, if necessary. | 1), 2) Check them visually. | 1), 2) There must be no such faults. |
|  | Braking resistor | 1) Check if there is any offensive smell and/or crack of insulators caused by overheat. <br> 2) Check if the wires are disconnected. | 1) Check them visually and by smelling. <br> 2) Check it visually or detach the connection at one side and make measurement using a tester. | 1) There must be no such faults. <br> 2) The value displayed on the resistor must be within $\pm 10 \%$. |


|  | PCB | 1) Check if any screw or connector is loosened. <br> 2) Check if there is any offensive smell and/or discoloration. <br> 3) Check if there is any crack, breakage, deformation, and outstanding rust. <br> 4) Check if there is any liquid leakage from and/or deformation of the capacitors. <br> * Detection of the service life based on the maintenance information. | 1) Tighten them firmly. <br> 2) Check them visually and by smelling. <br> 3) Check them visually. <br> 4) Check them visually. | 1), 2), 3), 4) There must be no such faults. |
| :---: | :---: | :---: | :---: | :---: |
|  | Cooling fan | 1) Check if there is any fault. <br> 2) Check if the bolts, etc. are not loosened. <br> 3) Check if there is any discoloration caused by overheat. <br> * Detection of the service life based on the maintenance information. | 1) Rotate the fan by hand. (Be sure to turn the power OFF beforehand.) <br> 2) Tighten them firmly. <br> 3) Check it visually. | 1) The fan must rotate smoothly. <br> 2), 3) There must be no such faults. |
|  | Ventilation opening | Check if the cooling fin, air suction opening, and/or exhaust opening is clogged, and if any foreign material is affixed to them. | Check it visually. | No dust and foreign material are affixed. If they are, remove them by a brush or air, etc. |

### 10.3.2 Periodic inspection 2 (After power is on, inverter is energized)

Visually inspect the inverter from the outside to check if there is any failure in the operation while it is powered on and the covers remain attached.

Perform the periodic inspection 2 in accordance with the items listed in Table 10.3-2 List of periodic inspections 2.
Table 10.3-2 List of periodic inspections 2

| Location | Item | Method | Criteria |
| :--- | :--- | :--- | :--- |
| Voltage | Check if the main circuit voltage and control <br> circuit voltage are correct. | Measure the voltage using a <br> tester, etc. | The voltage must meet the <br> standard specifications. |
| Structural parts including <br> cases and covers | Check if there is any abnormal noise and/or <br> abnormal vibration during operation. | Check them visually and by <br> listening. | There must be no such <br> faults. |
| Transformer and reactor | Check if there is any abnormal roaring noise <br> and/or offensive smell during operation. | Check them visually and by <br> listening and smelling. | There must be no such <br> faults. |
| Electromagnetic contactor <br> and relay | Check if there is any chattering noise during <br> operation. | Check it by listening. | There must be no such <br> faults. |

## [Additional Information]

(1) The frequency of the periodic inspection (once a year) shown in Table 10.3-1 and Table 10.3-2 is reference information. You can determine the frequency according to the environment where the inverter is used.
(2) Save the results of the periodic inspection and keep the logs, and use them to determine the operation and maintenance, and estimate the service life of the equipment.
(3) Check the accumulated operation time on the keypad upon inspection and use it to determine the replacing timing of parts.
(See Inverter Instruction Manual.)
(4) Even if the inverter is stored in a cabinet, dust may enter the inverter. Be sure to check if dust settles on the cooling fans or cooling fins of the inverter upon periodic inspection.
(If the cooling fans and/or cooling fins are covered with a lot of dust, the cooling performance is lowered, and the temperature protection function of the inverter might work. In addition, the temperature around the electronic parts rises, and it affects some consumable parts, lowering their service life.)

### 10.4 Periodic replacement parts

Some parts used in the inverter are consumable owing to their characteristics. While their service life varies according to the surrounding environment and use conditions, it is recommended to replace them based on the standard replacement frequency shown in Table 10.4-1. Some of them need knowledge for replacement.

Table 10.4-1 Replacement parts

| Replacement part |  | Standard replacement frequency | Remarks |
| :---: | :---: | :---: | :---: |
|  | Capacitors of main circuit | Every 10 yrs |  |
|  | Electrolytic capacitors on PCB | Every 10 yrs |  |
|  | Cooling fan | Every 10 yrs |  |
|  | Fuse | Every 10 yrs |  |
|  | Battery for memory backup | Every 5 yrs |  |
| Cooling fan (for cabinet) |  | Every 3 to 5 yrs (reference) | Contact the manufacturer of the cooling fan and determine the replacement frequency. <br> It is 3 years for a cooling fan of general specifications. |
| Air filter |  | - | The replacement frequency varies according to the use conditions. <br> Clean the air filter or replace it with a brand-new one. (For details, see the next page.) |
| Fuse |  | Every 10 yrs |  |

(Note) The estimated service life is calculated using the following conditions for MD and LD specifications respectively. In an environment where the ambient temperature is higher than $30^{\circ} \mathrm{C}$ or there is a lot of dust, the standard replacement frequency might become shorter.

- MD specification: Inverter ambient temperature: $30^{\circ} \mathrm{C}$; Load rate: $100 \%$
- LD specification: Inverter ambient temperature: $30^{\circ} \mathrm{C}$; Load rate: $80 \%$

Note the following matters for operation:
(1) The standard replacement frequencies listed in the table above are the reference values. If you replace the parts with new ones at these frequencies, failures can be prevented at high probabilities. They do not guarantee the complete operation during the specified number of years.
(2) The above table is not applied to the unused spare parts in stock.

It can be applied only if the unused spare parts are stored in a ventilated cool and dark place and they are powered on approx. every one year.
(3) You can replace the cooling fans and batteries. On the other hand, other parts must be replaced by those who have received training by Fuji Electric. Contact your Fuji Electric representative for purchase of replacement parts of the cooling fans and batteries or request for replacement of other parts.

## Replacement of air filter

An air filter to be mounted on the air suction opening (our standard filter is mounted on the door) collects dust inhaled together with air from outside. If the air filter is clogged, the ventilation performance is lowered (the cooling air volume is lowered), and the temperature in the panel rises, causing overheat and/or failures.
For this reason, you need to perform periodical inspection, and clean or replace the air filter when it gets dirty substantially.

## <Reference>

Recommended air filter: Viledon air filter (PS/400) by Japan Vilene Co., Ltd.
(1) Mounting example


Mount the air filter so that the left side of the air filter faces the outer side of the panel as shown in the figure below. Failure to do so impairs the performance of the air filter.


Figure 10.4-2 Air filter mounting direction

## (2) Example of reuse

The air filter recommended by Fuji Electric is reusable.

- Wash the air filter in a water tank by gently pressing it.
- Clean the filter by spray.
- Blow the dirt on the filter with compressed air or suck it using a vacuum cleaner.

If you use neutral detergent, oily dust, etc. can be also removed.
To prevent deterioration of the air filter during cleaning, do not rub and squeeze when you wash it. Be sure to dry the air filter naturally after cleaning.
While the number of times that the filter can be reused varies according to the use condition and cleaning method, the performance of the filter is lowered after it is reused.
Therefore, it is recommended to replace the air filter with a new one after cleaning and reusing it three times.

## FRENIC-

## Chapter 11 Troubleshooting

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### 11.1 Protective functions

The FRENIC-VG series of inverters has various protective functions as listed below to prevent the system from going down and reduce system downtime.
(1) The protective functions marked with an asterisk "*" in the table below are disabled by default. Enable them according to your needs.
(2) The FRENIC-VG has roughly three protective functions and lightning surge protection function. The inverter performs any of these functions according to the status of its operation, input interface setting, input signal, and communication interface:

1) The "heavy alarm" detection function which, upon detection of an abnormal state, displays the alarm code and causes the inverter to trip
2) The "light alarm" detection function which displays the alarm code but lets the inverter continue the current operation
3) Other "warning signal" output functions
4) Lightning surge protection function

If any problem arises, understand the protective functions listed below and follow the procedures given in the following sections for troubleshooting.

Table: 11.1-1 Description of protective functions

| Protective functions |  | Description |
| :---: | :---: | :---: |
| Heavy alarm (detection) |  | This function detects an abnormal state, causes the inverter to trip, and displays an alarm code corresponding to each factor on the keypad. See Table: 11.3-1 " Abnormal states detectable (heavy alarm and light alarm objects)" for alarm codes. For details, see description corresponding to each alarm code in the troubleshooting. <br> The inverter retains and displays the latest and the last 10 alarm codes and the latest and the last three pieces of detail information. <br> For more information, see Sections 3.4.4.8 and 3.4.4.9 in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". |
| Light alarm * |  | This function detects an abnormal state and displays " $L-1,1 / \overline{\prime \prime}$ " for a "light alarm," and lets the inverter continue the current operation without tripping. <br> It is possible to define which abnormal states should be categorized as a "light alarm". (See Table: 11.3-1.) <br> For instructions on how to check and release light alarms, see Section 3.4.3.5 in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". |
| Warning | Stall prevention | When the torque command value exceeds the torque limiter level (F44, F45) during acceleration/deceleration or constant speed running, this function limits the torque generated by the motor in order to avoid an overcurrent trip. |
|  | Motor overload early warning ${ }^{*}$ | When the inverter output current has exceeded the specified level, this function issues the motor overload early warning signal [M-OL] before the motor electronic thermal function causes the inverter to trip for motor protection. |
|  | Retry ${ }^{*}$ | When the inverter has stopped because of an alarm trip, this function allows the inverter to automatically reset and restart itself. <br> (The number of retries and the latency between stop and reset can be specified.) |
| Surge protection |  | This function protects the inverter from a surge voltage invaded between main circuit power lines and the ground. |

Note) If the DC link bus voltage drops below the undervoltage level, alarm information is not saved.

### 11.2 Before proceeding with troubleshooting

## $\triangle$ WARNING

- If any of the protective functions has been activated, first remove the cause. Then, after checking that all the run commands are set to OFF, release the alarm. If the alarm is released while any run commands are set to ON, the inverter may supply the power to the motor, running the motor, which could be dangerous.


## Injury may occur.

- Even if the inverter has interrupted power to the motor, voltage may be output to inverter output terminals $\mathrm{U}, \mathrm{V}$, and $W$ if any voltage is applied to the main power supply input terminals.
- Before inspection, perform the following: Turn OFF the power supply and wait at least ten minutes. Make sure that the LED monitor and charging lamp are turned OFF. Further, make sure, using a tester or a similar instrument, that the DC link bus voltage between the main circuit terminals $P(+)$ and $N(-)$ has dropped to the safe level (+25 VDC or below).


## Electric shock may occur.

Follow the procedure below to solve problems.
(1) First, check that the inverter is correctly wired. Refer to Chapter 2, "Section 2.4.1 Connection diagrams."
(2) Check whether an alarm code or the "light alarm" indication ( $1, T_{1}^{\prime \prime \prime \prime}$ ) is displayed on the LED monitor.

- If an alarm code appears on the LED monitor
- If the "light alarm" indication ( 1, -FNㅡㄴ) appears on the LED monitor
- If neither an alarm code nor "light alarm"

Abnormal motor operation

Go to Section 11.3.
Go to Section 11.4.
[1] The motor does not rotate
[2] The motor rotates, but the speed does not change
[3] The motor runs in the opposite direction to the command
[ 4 ] Speed fluctuation or current oscillation (e.g. hunting) occurs during running at constant speed
[5] Grating sound is heard from the motor or the motor sound fluctuates
[6] The motor does not accelerate or decelerate within the specified time
[7] The motor does not restart even after the power recovers from a momentary power failure
[8] The motor abnormally heats up
[9] The motor does not run as expected
[ 10 ] When the motor accelerates or decelerates, the speed is not stable
[ 11 ] The motor stalls during acceleration
[ 12 ] When the T-Link communications option is in use, neither a run command nor a speed command takes effect
[ 13 ] When the SX-bus communications option is in use, neither a run command nor a speed command takes effect
[ 14 ] When the CC-Link communications option is in use, neither a run command nor a speed command takes effect
[ 15 ] Under bar (_) appears
Problems with inverter settings
Go to Section 11.5.2. (Page 11-38)
[1] Nothing appears on the keypad
[2] The desired function code
[3] Data of function codes cannot be changed from the keypad
[4] Data of function codes cannot be changed via the communications link

If any problems persist after the above recovery procedure, contact your Fuji Electric representative.

## 11．3 If an alarm code appears on the LED monitor

If an alarm is detected，check the alarm cord displayed on the 7－segment LED of the keypad．Some alarm codes are followed by alarm sub codes that denote the detailed error causes．

For the alarm sub code checking procedure，refer to＂Section 3．4．4．8 Reading alarm information＂in Chapter 3 of separate volume＂Unit Type／Function Codes Edition（24A7－$\square$－0019）＂．
（1）For alarm codes followed by alarm sub codes，the alarm sub code is indicated with a 4－digit numeric value（0001 to 믐）in the bracket［ ］．
（2）For alarm codes not followed by alarm sub codes，the alarm sub code is set at＂ 0000 ＂，and＂－－＂is written in the table below．

## 11．3．1 List of alarm codes

Table：11．3－1 Abnormal states detectable（heavy alarm and light alarm objects）

| Alarm code | Error cause | Heavy alarm objects | Light alarm objects | Retry objects | Alarm sub code | Remarks | Ref． page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 水， | DC fuse disconnection | 0 | － | － | － | If DCF1 and DCF2 are not connected，an error cannot be detected | 11－5 |
| ロいて | Excessive positioning deviation | $\bigcirc$ | － | － | － |  | 11－5 |
| $E_{1}$ | Encoder communication error | $\bigcirc$ | － | － | 0001 to 2000 | When OPC－VG1－SPGT is installed | 11－6 |
| ERCO | ENABLE circuit（safety stop circuit）failure | 0 | － | － | 0001 | Input timing mismatch between EN1 and EN2 terminals | 11－6 |
|  |  |  |  |  | 0002 | PCB failure |  |
|  |  |  |  |  | 0005 to 0008 | CPU error |  |
| E， | Ground fault | $\bigcirc$ | － | － | － |  | 11－7 |
| E，－ | Memory error | $\bigcirc$ | － | － | 0001 to 0008 | For manufacturers | 11－7 |
| ミーシ | Keypad communications error | 0 | － | － | 0001 | Detection of wire break | 11－8 |
|  |  |  |  |  | 0002 | Detection of wire break（during operation by way of TP） |  |
| Er－ | CPU error | $\bigcirc$ | － | － | 0001 to 0008 | For manufacturers | 11－8 |
| E，－ | Network error | $\bigcirc$ | $\bigcirc$ | － | 0001 to 0004 |  | 11－9 |
| ミーム | RS－485 communications error | $\bigcirc$ | $\bigcirc$ | － | 0001 | Communications error（timeout） | 11－10 |
|  |  |  |  |  | 0002 | Communications error （transmission error） |  |
| 荗旨 | Operation error | 0 | － | － | 0001 | Error in mounting of option（s） | 11－11 |
|  |  |  |  |  | 0002 | Auto－tuning malfunction |  |
|  |  |  |  |  | 0008 to 8000 | For manufacturers |  |
| $8-7$ | Output wiring fault | 0 | － | － | 0001 | Output wiring fault during tuning | 11－12 |
|  |  |  |  |  | 0002 | Speed not attained during rotation－tuning |  |
|  |  |  |  |  | 0004 to 0040 | For manufacturers |  |
| にーム | A／D converter error | $\bigcirc$ | － | － | 0001 to 0004 | For manufacturers | 11－12 |
| E－G | Speed not agreed | 0 | $\bigcirc$ | － | 0001 | Motor 1 speed deviation | 11－13 |
|  |  |  |  |  | 0002 | Motor 2 speed deviation |  |
|  |  |  |  |  | 0004 | Motor 3 speed deviation |  |
|  |  |  |  |  | 0008 | Machine runaway detected by H149 |  |
| E，－17 | UPAC error | 0 | － | － | 0001 to 0004 |  | － |
| EーG | Inter－inverter communications link error | $\bigcirc$ | － | － | 0002 to 0400 | For manufacturers | 11－14 |
| Er－イ | Hardware error | $\bigcirc$ | － | － | 0001 to 1000 | For manufacturers | 11－14 |
| E，－－ | Mock alarm | $\bigcirc$ | 0 | － | － |  | 11－14 |
| É i | Encoder error 1 | $\bigcirc$ | － | － | － | When OPC－VG1－SPGT is installed | 11－14 |

（To be continued）

Table：11．3－1 Abnormal states detectable（Heavy alarm and light alarm objects）（Continued）

| Alarm code | Error cause | Heavy alarm objects | Light alarm objects | Retry objects | Alarm sub code | Remarks | Ref． page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lill | Start delay | $\bigcirc$ | $\bigcirc$ | － | － |  | 11－15 |
| íi | Undervoltage | $\bigcirc$ | － | － | － |  | 11－16 |
| －וּ | NTC thermistor wire break | $\bigcirc$ | $\bigcirc$ | － | － |  | 11－16 |
| 行－ | Overcurrent | $\bigcirc$ | － | $\bigcirc$ | 0001 to 0004 | For manufacturers | 11－17 |
|  |  |  |  |  | 0100 | Overcurrent to demagnetizing limiting current for PMSM |  |
| ＇늑＇＇ | Heat sink overheat | $\bigcirc$ | － | $\bigcirc$ | 0001 to 0008 | Protection by thermistor | 11－18 |
|  |  |  |  |  | 0010 to 0200 | For manufacturers |  |
| ［1711） | External alarm | $\bigcirc$ | $\bigcirc$ | － | 0001 | Protection by THR signal | 11－19 |
| ［111行 | Inverter internal overheat | $\bigcirc$ | － | $\bigcirc$ | 0001 to 0008 | Protection by thermistor | 11－19 |
|  |  |  |  |  | 0010 | For manufacturers |  |
| ［717－1， | Motor overheat | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | － |  | 11－20 |
| 统！ | Motor 1 overload | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | － |  | 11－21 |
|  | Motor 2 overload | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | － |  | － |
| 促 7 | Motor 3 overload | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | － |  | － |
| ＇는＇ | Inverter overload | $\bigcirc$ | － | $\bigcirc$ | 0001 to 0010 | For manufacturers | 11－22 |
|  | Output phase loss detection | $\bigcirc$ | － | － | 0001 | Loss of one or more phases | 11－23 |
|  |  |  |  |  | 0002 | Loss of two or more phases |  |
| \％1\％ | Overspeed | $\bigcirc$ | － | － | － |  | 11－23 |
| ［171 | Overvoltage | $\bigcirc$ | － | － | 0001 | For manufacturers | 11－24 |
| 17 | PG wire break | $\bigcirc$ | － | － | 0001 | Detection of wire break（inverter PA，PB） | 11－25 |
|  |  |  |  |  | 0002 | Detection of wire break（option） |  |
|  |  |  |  |  | 0004 | Detection of power supply disconnection （inverter） |  |
|  |  |  |  |  | 0010 to 0400 | Failure in PG wiring for PMSM |  |
|  | E－SX bus tact synchronization error | $\bigcirc$ | $\bigcirc$ | － | － |  | 11－26 |
| 171 | （PLC）Toggle abnormality error | 0 | 0 | － | － |  | 11－26 |
| Sı，－ | Functional safety card error | $\bigcirc$ | － | － | $\begin{aligned} & \hline 0001 \text { to 000d } \\ & (8001 \text { to } 800 \mathrm{~d}) \\ & \hline \end{aligned}$ | When OPC－VG1－SAFE is installed <br> ＊For details，refer to the OPC－VG1－SAFE instruction manual （INR－SI47－1541－JE）． | － |
| S1： |  | $\bigcirc$ | － | － | 000e to 0015 <br> （800e to 8015） |  |  |
| Sッル－ |  | － | $\bigcirc$ | － | $\begin{gathered} \hline 0016 \text { to } 0018 \\ (8016 \text { to } 8018) \\ \hline \end{gathered}$ |  |  |

### 11.3.2 Possible causes of alarms, checks and measures

## [1] 1 ルII DC fuse disconnection

Problem The DC fuse connected to the input terminals $P(+)$ and $N(-)$ of the FRENIC-VG blew.
Note (1) Connect microswitch (b-contact) provided for DC fuse to input terminals (DCF1, DCF2) for detecting DC fuse disconnection.
(2) If the fuse has been disconnected, the internal elements may be broken. NEVER turn the power ON to prevent secondary damage. Contact your Fuji Electric representative.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The fuse blew | Check whether there has been any excess surge or noise coming from outside. <br> $\rightarrow$ Take measures against surges and noise. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) |
|  | Disconnect the wiring from the output terminals [U], [V] and [W] and perform a Megger test on the inverter and the motor. <br> $\rightarrow$ Find and remove the ground fault parts. (Check the wiring, etc. as well.) If the DC fuse was disconnected due to ground faults that have occurred at the inverter and/or motor, repair and inspection might be required. (Ask your Fuji Electric representative.) |
| (2) Are the input terminals $P(+)$ and $\mathrm{N}(-)$ short circuited? | Modify the structure of the cabinet. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) |
| (3) Is wiring of microswitch disconnected? | $\rightarrow$ Check for disconnection of cable by using tester, etc. <br> $\rightarrow$ Check for any loose wiring. (Also check for any loose terminal screw.) |

## [2] 2 ㄴㄱ Excessive positioning deviation

Problem An excessive positioning deviation has occurred.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Wrong wiring to the motor | Check the wiring to the motor. <br> $\rightarrow$Connect the inverter output wiring U, V, and W to the motor <br> wiring U, V, and W, respectively. (It is also possible to use H75: <br> phase sequence configuration of main circuit output wiring). <br> (2) The motor cannot rotate mechanically. <br> (3) Output torque is too small. <br> Check whether the brake is applied. |
| (4) Deviation override width is too smallInsufficient gain in positioning control <br> system. $\rightarrow$ Revease the torque limiter level (F44, F45). <br> (6) The acceleration/deceleration by pulse  <br> train command is too rapid. $\rightarrow$ Readjust the positioning loop gain. (o16) |  |

## [3] EL Encoder communication error

Problem Communication error. (When OPC-VG1-SPGT is installed)

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Communications with the ABS encoder are interrupted. | $\rightarrow$ Check for disconnection of cable using a tester, etc. <br> $\rightarrow$ Check for any loose wiring. (Also check for any loose terminal screw.) |
| (2) Disconnection (poor connection) of ABS encoder cable | $\rightarrow$ Check if the encoder is a model specified for OPC-VG1-SPGT. <br> $\rightarrow$ Communication error might have occurred due to ringing in communication data. <br> Install a terminating resistor ( $220 \Omega, 1 / 4 \mathrm{~W}$ ). <br> $\rightarrow$ Malfunction might have occurred due to noise. Insert a ferrite core. |
| (3) OPC-VG1-SPGT is not installed properly. | Check that the option card is properly engaged with the connector of the inverter. <br> $\rightarrow$ Reinstall the option card properly. |

For more information, see "Section 6.8 OPC-VG1-SPGT" in Chapter 6 of separate volume "Option Edition (24A7- $\square$-0045)".

## [4] ELI ENABLE circuit (safety stop circuit) failure

(1) Alarm sub-code 0001

Problem A failure occurred in the enable input circuit.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Poor contact of control circuit terminal block | Check that the control circuit terminal block is securely fitted on the inverter. |
| (2) Enable input circuit faulty logic | Check the ON/OFF state of EN1 and EN2 using I/O check. <br> $\rightarrow$ Check that wiring is properly installed between the EN1 and PS terminals as well as between the EN2 and PS terminals. <br> $\rightarrow$ Operate the relay so as to synchronize ON/OFF between EN1 and EN2. <br> $\rightarrow$ Check the relay for fusion of the contacts and any problem. If a problem exists, replace the relay. <br> $\rightarrow$ Check the ON/OFF timing between EN1 and EN2 for a time lag. Make sure that the time lag is less than 50 ms . |
| (3) Failure in enable input circuit | A failure occurs even after measures in (2) are taken. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) * Inform the representative of the alarm sub code displayed. |

(2) Alarm sub-code 0002, 0005 to 0008

Problem A failure or any other error occurred in PCB or CPU.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Inverter affected by <br> strong electrical noise | Check if appropriate noise control measures have been implemented (e.g. correct <br> grounding and routing of signal wires, communication cables and main circuit wires). <br> $\rightarrow$ Improve the noise control measures. |
| (2)Short circuit on the <br> printed circuit board(s) | Check the printed circuit board(s) for short circuits, dust and any adherents. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) <br> * Inform the representative of the alarm sub code displayed. |

Note To remove the
The error cannot be removed by pressing the ereser key.

## [5] EF Ground fault

Problem A ground fault current flew from the output terminal of the inverter.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :---: |
| (1) Ground faults have <br> occurred at the inverter <br> output terminal(s). | Disconnect the wiring from the inverter output terminals [U], [V] and [W] and perform <br> a Megger test on the inverter and the motor. <br> $\rightarrow$ Remove the ground fault parts (including replacement of the wires, relay <br> terminals and motor). |
| (2) The setting of the motorrated current (P04, A03, <br> A103) is small relative to <br> the inverter rated current. | The motor rated current is set at a value that is too small to the inverter rated current. <br> $\rightarrow$ Check the setting of the motor rated current (P04, A03, A103). <br> Disable the ground fault detection by setting "0" to the hundreds digit of H103 <br> (Protection/maintenance function 1). |

## [6] E/ 'Memory error

Problem Error occurred in writing data to the memory in the inverter.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) When writing function code data (especially initializing or copying data), the inverter was shut down so that the voltage to the control PCB has dropped. | Initialize the function code data by setting H03 to "1." After initialization, check if pressing the (esse) key can release the alarm. <br> $\rightarrow$ Revert the initialized function code data to their previous customized settings (Note), then restart the operation. |
| (2) Inverter affected by strong electrical noise when writing function code data (especially initializing data) | - Check if appropriate noise control measures have been implemented (e.g. correct grounding and routing of control and main circuit wires). <br> - Perform the same check as described in (1) above. <br> $\rightarrow$ Implement noise control measures. Revert the initialized function code data to their previous customized settings, then restart the operation. |
| (3) Control circuit failure [Sub code: 0001 to 0008] | Initialize the function code data by setting H03 to "1," then reset the alarm by pressing the ${ }^{\text {restrfic}}$ ) key and check that the alarm goes on. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) The PCB (CPU) failed and needs to be replaced. <br> * Inform the representative of the alarm sub code displayed. |
| (4) High-frequency rewriting to the non-volatile memory has reached the limit of the electronic device (approx. 1,000,000 times). <br> [Sub code: 0001 to 0008] | Function code data setting has been frequently changed. <br> $\rightarrow$ Request for repair work on inverter. (Please contact our service department.) The PCB (non-volatile memory) failed and needs to be replaced. *Inform the representative of the alarm sub code displayed. <br> $\rightarrow$ Decrease the frequency of rewriting. Decrease the frequency of full save operations. <br> Note When you access H02 (full save) using PLC, etc., do not perform the full save operation every task cycle of PLC. |

(Note) Function code data can be easily reverted to the previously customized settings by using the backup data copied in the keypad memory with "Menu \#10 Copying data" in Programming mode. (Refer to "Section 3.4.4.10 Copying data" in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)".)

## [7] Er-こ Keypad communications error

Problem A communications error occurred between the keypad and the inverter.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Disconnection or poor contact <br> of communications cable <br> [Sub code: 0001] | Check continuity of the cable, contacts and connections. <br> $\rightarrow$ Re-insert the connector firmly. <br> $\rightarrow$ Replace the communication cable. |
| (2) The keypad is not properly <br> installed. <br> [Sub code: 0001] | Many control wires are connected, and consequently the front cover is lifted. <br> The keypad is not inserted properly into the front cover. <br> $\rightarrow$ Use wires of the recommended size ( $\left.0.75 \mathrm{~mm}^{2}\right)$ for wiring. <br> $\rightarrow$ Change the wiring layout inside the unit so that the front cover can be <br> mounted firmly. |
| (3) Inverter affected by strong |  |
| electrical noise |  |$\quad$| Check if appropriate noise control measures have been implemented (e.g. |
| :--- |
| correct grounding and routing of communication cables and main circuit wires). |
| $\rightarrow$ Implement noise control measures. |

## [8] Er-3CPU error

Problem A CPU error occurred.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Inverter affected by strong |  |
| electrical noise |  |$\quad$| Check if appropriate noise control measures have been implemented (e.g. |
| :--- |
| correct grounding and routing of signal wires, communications cables, and main |
| circuit wires). |
| $\rightarrow$ Implement noise control measures. |

[^18]
## [9] Eーム'Network error

Problem The connected option card detected an error.

| Possible Causes |  | What to Check and Suggested Measures |
| :---: | :---: | :---: |
|  | (1) Wrong wiring | $\rightarrow$ Check if the wiring is correct. If not, correct the wiring. <br> - The specified cable is used. <br> - There is no wire break. <br> - The wiring length is within the range of the specification. <br> - The shielded wires are properly treated. <br> - The signal lines are not wired in parallel with the power lines. <br> - The maximum extension cable length, inter-station cable length, and the number of devices connected are as specified. |
|  | (2) Wrong address (station number) setting | $\rightarrow$ Set a new link address. (After a new link address is set, reset the power.) |
| $\begin{aligned} & \text { 음 } \\ & \text { 흥 } \\ & \text { 듣 } \\ & \text { in } \end{aligned}$ | (1) The power to the MICREX IO terminal is OFF. | Check the power to the MICREX IO terminal. <br> $\rightarrow$ Turn ON the power to the MICREX IO terminal and reset the inverter alarm state. |
|  | (2) Wrong wiring | Check if the wiring is correct. <br> - The T-Link network has terminating resistors. (1 resistor at each end: $100 \Omega$ ) <br> - The SD terminal of the T-Link is not connected to a frame ground (FG). <br> - A crimp terminal is used for connection. |
|  | (1) The SX-bus power is shut down or the PLC's CPU module is down. | Check the power to the SX (E-SX) bus and the status of the PLC's CPU module. <br> $\rightarrow$ Turn ON the power to the SX-bus or E-SX bus, recover the PLC's CPU module, and reset the inverter alarm state. <br> Check if the power capacity is sufficient. <br> $\rightarrow$ If not, add an electric repeater on the SX bus (E-SX bus). |
|  | (2) An error has occurred at any other station. | Check the detailed RAS information on the PLC's CPU module to find a faulty station. <br> $\rightarrow$ Recover the faulty station and reset the inverter alarm state. |
|  | (3) SX bus terminating connector is not inserted. | $\rightarrow$ Insert an SX bus terminating connector at each end of the bus. <br> Note E-SX bus does not use a terminating connector. <br> (If it is used, the devices connected to the E-SX bus might get broken.) |
|  | (1) The power to the PLC is shut down or the PLC's CPU module is down. | Check the power to the PLC and the status of the PLC's CPU module. <br> $\rightarrow$ Turn ON the power to the PLC, recover the PLC's CPU module, and reset the inverter alarm state. |
|  | (2) An error has occurred at any other station. | Check the detailed RAS information on the PLC's CPU module to find a faulty station. <br> $\rightarrow$ Recover the faulty station and reset the inverter alarm state. |
|  | (3) Wrong wiring | Check if the following wiring is correct. <br> - The CC-Link network has terminating resistors (1 resistor at each end: $110 \Omega$ ). <br> - The minimum cable length between CC-Link stations is as specified. <br> - Connection to the terminal block is proper. |

[^19]
## [ 10 ] $\Sigma_{1}-5$ RS-485 communications error

Problem A communications error occurred during RS-485 communication.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Communication conditions of the inverter do not match that of the host equipment. <br> [Sub code: 0002] | Compare the settings of function codes H 32 to H 40 (for communications) with those of the host equipment. <br> $\rightarrow$ Correct any settings that differ. |
| (2) Even though no-response error detection time (H38) has been set, communication is not performed within the specified cycle. <br> [Sub code: 0001] | Check the host equipment side. <br> $\rightarrow$ Change the settings of host equipment software or disable the no-response error detection time ( $\mathrm{H} 38=0$ ). |
| (3) The host equipment did not operate due to defective software, settings, or defective hardware. <br> [Sub code: 0002] | Check the host equipment (e.g. PLCs and computers). <br> $\rightarrow$ Remove the cause of the host equipment error. |
| (4) The RS-485 converter did not operate due to incorrect connections and settings, or defective hardware. | Check the RS-485 converter (e.g. check for poor contact or incorrect wiring). <br> $\rightarrow$ Change the various RS-485 converter settings, reconnect the wires, or replace hardware with recommended devices as appropriate. |
| (5) Disconnection or poor contact of communications cable | Check the continuity of the cables, contacts and connections. <br> $\rightarrow$ Replace the cable. |
| (6) Inverter affected by strong electrical noise | - Check if appropriate noise control measures have been implemented (e.g. correct grounding and routing of communications cables and main circuit wires). <br> - Check if decreasing the communication speed (H34) down to 2400 bps causes no alarm. <br> $\rightarrow$ Implement noise control measures. <br> $\rightarrow$ Implement noise reduction measures on the host equipment. <br> $\rightarrow$ Replace the RS-485 converter with a recommended insulated one. <br> $\rightarrow$ Keep the inverter running, using the selection of operation when error occurs (H32). |
| (7) Terminating resistor not properly configured | Check that the inverter serves as a terminating device in the RS485 network. <br> $\rightarrow$ Configure the terminating resistor switch (SW4) for RS-485 communication correctly. <br> (To use the inverter as a terminating device, turn the switch (SW4) to the ON position.) <br> For more information, see "Section 3.3.3.9 Setting up the slide switches" in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". |
| (8) Response interval does not match the send/receive switching time of the RS-232C-RS-485 converter. | Check whether the specified response interval (H39) matches the specification of the actual converter. <br> $\rightarrow$ Match the response interval (H39) with the specification of the converter. |

## [ 11] $E_{1}-5$ Operation error

Problem An incorrect operation was attempted, resulting in an error.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Restrictions on mounting of option(s) not observed <br> [Sub code: 0001] | Check the model of option(s) mounted. <br> $\rightarrow$ Check the restrictions on mounting of the option(s). <br> This error cannot be shown as mounting status of control options in "Menu \#4 I/O check" on the keypad. Check whether the configurations of the customizing switches (SW) on the two option boards are the same. <br> $\rightarrow$ Change the SW configuration. |
| (2) Auto-tuning not performed in accordance with correct procedure <br> [Sub code: 0002] | Check whether tuning started with digital input BX, STOP1, STOP2 or STOP3 being ON . <br> $\rightarrow$ With all of digital input BX, STOP1, STOP2 and STOP3 being OFF, start tuning. <br> Check whether tuning started with digital input EN1 or EN2 being opened. <br> $\rightarrow$ With each of digital input EN1 and EN2 connected with PS, start tuning. Check whether 20 seconds or more have elapsed immediately after writing to H01 until the key is pressed. <br> $\rightarrow$ Press the key on the keypad within 20 seconds immediately after writing to H 01 . <br> $\rightarrow$ Before writing to H 01 , make sure that $\mathrm{F} 02=0$ and $\mathrm{H} 30=0$ or 1 . |
| (3) The PG detection circuit self-diagnosis function (H74) has been performed with the PG (SD)/PGo (SD) card being mounted. <br> [Sub code: 0080] | Check whether the PG (SD)/PGo (SD) card is mounted. <br> $\rightarrow$ Remove the PG (SD)/PGo (SD) card, then perform the self-diagnosis function of the PG detection circuit. |
| (4) When the multiplex system is selected ( $o 33 \neq 0$ ), the multiplex system station number ( 050 ) is greater than the number of multiplex system slave stations (o34). <br> [Sub code: 0100] | $\rightarrow$ Review the settings of o50 and o34. |
| (5) When the multiplex system is selected (o33 $\neq 0$ ), the motor control mode setting is not proper. <br> [Sub code: 0200] | Some motor control modes are not available under the multiplex system. <br> $\rightarrow$ Review the selected control mode (P01, A01, A101). <br> For available control mode, refer to "Section 6.6 OPC-VG1-TBSI" in Chapter 6 of separate volume "Option Edition (24A7- $\square$-0045)". |
| (6) The multiplex system control mode setting (o33) has been changed either from the setting 1 to the setting 2 or vice versa. <br> [Sub code: 0800] | The alarm cannot be released until the inverter is turned off and on. <br> $\rightarrow$ Review the setting of o33 and turn the inverter off and on. |
| (7) Mismatch between the multiplex system control mode setting (o33) and the number of multiplex system slave stations setting (034) <br> [Sub code: 4000] | Multiplex systems have restrictions on the number of slave stations. <br> $\rightarrow$ Review the settings of o33 and o34. <br> For available control mode, refer to "Section 6.6 OPC-VG1-TBSI" in Chapter 6 of separate volume "Option Edition (24A7- $\square-0045$ )". |

## [12] $\Sigma_{-}$TOutput wiring fault

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) A phase was missing (There was a phase loss) in the connection between the inverter and the motor. <br> [Sub code: 0001] <br> [Sub code: 0020, 0040] | $\rightarrow$ Properly connect the motor to the inverter. <br> $\rightarrow$ Check the state of the contactor connected at the inverter output side. |
| (2) A tuning operation involving motor rotation ( $\mathrm{H} 01=4$ ) was attempted while the brake was applied to the motor. <br> [Sub code: 0002] | Check that the brake can be released. <br> $\rightarrow$ Specify the tuning that does not involve the motor rotation ( $\mathrm{H} 01=2$ or 3 ). <br> $\rightarrow$ Release the brake before tuning that involves the motor rotation ( $\mathrm{H} 01=4$ ). |
| (3) Tuning of magnetic pole position offset value has failed. <br> [Sub code: 0010] | $\rightarrow$ Correct the wiring of the PG. <br> $\rightarrow$ Adjust the settings of the pull-in current (H161) and pull-in frequency (H162). <br> For more information, refer to the following sections in separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". <br> - "Section 3.5.4.2 [3] Setting the magnetic pole position offset value" in Chapter 3 <br> - "Section 3.5.4.2 [3] (2) Automatic adjustment of the magnetic pole position offset value" in Chapter 3 |

## [ 13 ] $E$ - $B \mathrm{~A} / \mathrm{D}$ converter error

Problem An error occurred in the A/D converter circuit.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Inverter affected by strong |  |
| electrical noise |  |$\quad$| Check if appropriate noise control measures have been implemented (e.g. |
| :--- |
| correct grounding and routing of signal wires, communications cables, and main |
| circuit wires). |
| $\rightarrow$ Implement noise control measures. |

## [ 14 ] $E_{1}-$ SSpeed mismatch

Problem An excessive deviation has occurred between the speed command and the detected speed.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Incorrect setting of function code data <br> [Sub code: 0001 to 0004] | Check the settings of the following function codes: P05, A07 and A107 (Motor, No. of poles), P28, A30 and A130 (Return (Feedback input) encoder pulse count), P29, A51 and A151 (Return (Feedback input) pulse correction factor 1), and H149 (Machine runaway detection speed setting). <br> $\rightarrow$ Specify motor parameters in accordance with the motor and PG. <br> $\rightarrow$ Review the data of the following function codes. <br> - E43 (Speed agreement, Detection width) <br> - E44 (Speed agreement, Off-delay timer) <br> - E45 (Speed disagreement, Alarm use/disuse) |
| (2) Overload <br> [Sub code: 0001 to 0004] | Measure the inverter output current. <br> $\rightarrow$ Reduce the load. <br> $\rightarrow$ Increase the inverter capacity. <br> Check whether any mechanical brake is working. <br> $\rightarrow$ Release the mechanical brake. |
| (3) Mismatch between function code data settings and the motor characteristics <br> [Sub code: 0001 to 0004] | Check the motor parameters. <br> $\rightarrow$ Perform auto-tuning, using H 01 . |
| (4) Wrong wiring of the PG <br> [Sub code: 0001 to 0004] | Check the wiring between the PG and the inverter. <br> $\rightarrow$ Correct the wiring. |

Check that the relationships between the PG feedback signal and the run command are as follows:

- For the FWD command: the B phase pulse is in the High level at rising edge of the A phase pulse
- For the REV command: the B phase pulse is in the Low level at rising edge of the A phase pulse
$\rightarrow$ If the relationship is wrong, interchange the $A$ and $B$ phase wires.
$\rightarrow$ Note that if the digital input signal IVS ("normal/inverse operation") is active, the above operation is reversed.
(5) Wrong wiring to the motor
[Sub code: 0001 to 0004]
Check the wiring to the motor.
$\rightarrow$ Connect the inverter output wiring $\mathrm{U}, \mathrm{V}$, and W to the motor wiring $\mathrm{U}, \mathrm{V}$, and $W$, respectively. (It is also possible to use H75: Phase sequence configuration of main circuit wiring.)
[Under vector control with/without speed sensor]

Check the setting of the torque limiter (operation level) (F44, F45).
$\rightarrow$ Change the F44 or F45 data to an appropriate value. If no torque limiter operation is required, disable the torque limiter ( $\mathrm{F} 40=0$ ).
(6) The motor speed does not rise due to the torque limiter operation.
[Sub code: 0001 to 0004]
(7) During running of the motor (after the mechanical brake is released), the deviation between the speed command value (Reference speed 4, ASR input) and the actual speed exceeds the setting of E43.
[Sub code: 0008]

## ［15］Er－b Inter－inverter communications link error

Problem A communications link error occurred between high－speed serial communication terminal options．

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| （1）The optical cable is disconnected or inserted poorly into the connector． <br> ［Sub code： 0001 to 0020］ | $\rightarrow$ Connect the optical cable fully． |
| （2）The optical cable is bundled or bent with the bend radius of 35 mm or less． <br> ［Sub code： 0001 to 0020］ | Increase the bend radius of the optical cable to more than 35 mm ． |
| （3）The optical cable or connectors on the inverter were exposed to intense light （e．g．direct sunlight or strobe light）． <br> ［Sub code： 0001 to 0020］ | Do not expose the optical cable or the connectors on the inverter to intense light． |
| （4）Discrepancy in capacity between master and slave inverters <br> ［Sub code：0200］ | The multiplex system cannot be configured with inverters of different capacities． |
| （5）Discrepancy in current rating（F80） between master and slave inverters <br> ［Sub code：0400］ | The multiplex system cannot be configured with inverters of different current rating settings（F80）． <br> $\rightarrow$ Review the current rating settings（F80）． |

## ［ 16 ］Еール＇Hardware error

Problem The LSI on the power supply printed circuit board（PCB）malfunctions．

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| The control PCB or power supply |  |
| PCB is defective． | The control PCB or power supply PCB（including the gate PCB）needs to be <br> replaced． <br> $\rightarrow$ Request for repair work on inverter．（Please contact our service <br> department．） <br> ＊Inform the representative of the alarm sub code displayed． |

## ［17］Er－I－Mock alarm

Problem The LED displays İール．

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
|  down for more than 5 seconds． | $\rightarrow$ To escape from this alarm state，press the（riser）key． |

## ［18］EL／＇Encoder error 1

Problem ABS encoder position detection data error．（When OPC－VG1－SPGT is installed）

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| （1）Data received from the ABS <br> encoder is wrong． | $\rightarrow$ Use shielded wire to prevent being affected by noise． <br> Recommended shielded wire：WSC－P06PPa－ロ（twisted 6－pair shielded <br> wire） |
| （2）The ABS encoder has been <br> broken． | $\rightarrow$ Replace the ABS encoder． |
| ＊For more information，see＂Section 6．8 OPC－VG1－SPGT＂in Chapter 6 of separate volume＂Option Edition |  |
| $(24 A 7-\square-0045) "$. |  |

## [19] LoL Start delay

Problem At the startup, an excessive deviation has occurred between the speed command and the detected speed.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Incorrect setting of function code data | Check the settings of the following function codes: P05, A07 and A107 (Motor, No. of poles), P28, A30 and A130 (Return (Feedback input) encoder pulse count), and P29, A51 and A151 (Return (Feedback input) pulse correction factor 1). <br> $\rightarrow$ Specify motor parameters in accordance with the motor and PG. <br> $\rightarrow$ Review the data of the following function codes. Related function code: <br> - H140 Start delay detection (Start delay detection level) <br> - H141 Start delay detection (Start delay detection timer) |
| (2) Overload | Measure the inverter output current. <br> $\rightarrow$ Reduce the load. <br> $\rightarrow$ Increase the inverter capacity. <br> Check whether any mechanical brake is working. <br> $\rightarrow$ Release the mechanical brake. |
| (3) Mismatch between function code data settings and the motor characteristics | Check the motor parameters. <br> $\rightarrow$ Perform auto-tuning, using H 01 . |
| (4) Wrong wiring of the PG | Check the wiring between the PG and the inverter. <br> $\rightarrow$ Correct the wiring. <br> Refer to Chapter 3, "Section 3.5.2 Powering ON and checking" of separate volume "Unit Type/Function Codes Edition (24A7- $\square-0019$ )". |

Check that the relationships between the PG feedback signal and the run command are as follows:

- For the FWD command: the B phase pulse is in the High level at rising edge of the A phase pulse
- For the REV command: the B phase pulse is in the Low level at rising edge of the A phase pulse
$\rightarrow$ If the relationship is wrong, interchange the $A$ and $B$ phase wiring.
$\rightarrow$ Note that if the digital input signal IVS ("normal/inverse operation") is active, the above operation is reversed.
(5) Wrong wiring to the motor

Check the wiring to the motor.
$\rightarrow$ Connect the inverter output wiring $\mathrm{U}, \mathrm{V}$, and W to the motor wiring $\mathrm{U}, \mathrm{V}$, and W , respectively. (It is also possible to use H 75 : Phase sequence configuration of main circuit wiring.)
Check the setting of the torque limiter (operation level) (F44, F45).
$\rightarrow$ Change the F44 or F45 data to an appropriate value. If no torque limiter operation is required, disable the torque limiter ( $\mathrm{F} 40=0$ ).

Check the wiring to the motor.
$\rightarrow$ Connect the inverter output wiring $\mathrm{U}, \mathrm{V}$, and W to the motor wiring $\mathrm{U}, \mathrm{V}$, and W , respectively.
(6) The motor speed does not rise due to the torque limiter operation.
(7) During running of the motor (after the mechanical brake is released), the torque current command value exceeds the specified level (function code H 140 ) and the actual speed drops below the specified "stop speed" (function code F37), and then the state is kept for the specified duration (function code H141).

## [20] ĹL'Undervoltage

Problem DC link bus voltage has dropped below the undervoltage level.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) A momentary power failure occurred. | $\rightarrow$ Release the alarm. <br> $\rightarrow$ To restart running the motor without treating this condition as an alarm, set the data of F14 (Restart mode after momentary power failure (mode selection)) to "3," "4," or "5," depending on the load type. |
| (2) The power to the inverter was switched back to ON too soon (when F14 = 1). | Check if the power to the inverter was switched back to ON after the inverter was shut down while the control power was still alive. (Check whether the LEDs on the keypad light.) <br> $\rightarrow$ Turn the power ON again after all LEDs on the keypad go off. |
| (3) The power supply voltage does not reach the inverter's specification range. | Measure the input voltage. <br> $\rightarrow$ Increase the power supply voltage to within the specified range. |
| (4) Peripheral equipment for the power circuit malfunctioned, or the wiring is incorrect. | Measure the input voltage to find which peripheral equipment malfunctioned or which wiring is incorrect. <br> $\rightarrow$ If any, replace the faulty peripheral equipment and/or correct the incorrect wiring. |
| (5) Any other load(s) connected to the same power supply system has required a large starting current, causing a temporary power supply voltage drop. | Measure the input voltage and check the voltage fluctuation. <br> $\rightarrow$ If any, reconsider the power supply system configuration. |
| (6) Insufficient capacity of the power supply transformer increases load, causing a power supply voltage drop. | Measure the output current. <br> $\rightarrow$ Reduce the load. <br> $\rightarrow$ Reconsider the capacity of the power supply transformer. |
| (7) No power is supplied to the auxiliary power supply (RO-TO). | Measure the input voltage of the auxiliary power supply. <br> $\rightarrow$ Insert various circuit breakers or magnetic contactor (MC). <br> $\rightarrow$ Check for voltage drop, connection failure, poor contact and other problems, and then take measures against them. |

## [21] ] NTC thermistor wire break

Problem A wire break is found in the NTC thermistor detection circuit.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The NTC thermistor cable is broken. | Check whether the motor cable is broken. <br> $\rightarrow$ Replace the motor cable. |
| (2) The temperature around the motor is extremely low (lower than $-30^{\circ} \mathrm{C}$ ). | Measure the temperature around the motor. <br> $\rightarrow$ Reconsider the use environment of the motor. |
| (3) The NTC thermistor is broken. | Measure the resistance of the NTC thermistor (including a spare thermistor). <br> $\rightarrow$ Connect a spare thermistor to the motor. <br> $\rightarrow$ If the spare thermistor is also broken, replace the motor. |

[^20]
## [22] 红 Overcurrent

Problem The inverter momentary output current exceeded the overcurrent level.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) The inverter output lines were |  |
| short-circuited. |  | | Disconnect the wiring from the inverter output terminals (U, V and W) and |
| :--- |
| measure the interphase resistance of the motor wiring. Check if the |
| resistance is too low. |
| $\rightarrow$ Remove the short-circuited part (including replacement of the wiring, |
| relay terminals and motor). |


| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| [Under vector control with speed | Check whether the inverter internal control circuit (PG input circuit) is faulty, <br> sensor] |
| using the self-diagnosis function of the PG detection circuit (H74).  <br> (10)PG defective If the result is "Normal," replace the PG. |  |
|  | $\rightarrow$ If it is "Abnormal," contact your Fuji Electric representative. |
|  | Check the PG waveform using an oscilloscope. |
|  | $\rightarrow$ Replace the PG. |

## [ 23] ] ' 'Heat sink overheat

Problem Temperature around heat sink has risen abnormally.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The surrounding temperature exceeded the range of the inverter specification. <br> [Sub code: 0001 to 0008] | Measure the temperature around the inverter. <br> $\rightarrow$ Lower the temperature around the inverter (e.g. ventilate the panel where the inverter is mounted). |
| (2) Ventilation path is blocked. [Sub code: 0001 to 0008] | Check if there is sufficient clearance around the inverter. <br> Change the mounting place to ensure the clearance. |
|  | Check if the heat sink is not clogged. <br> $\rightarrow$ Clean the heat sink. (For the cleaning procedure, contact your Fuji Electric representative.) |
| (3) Cooling fan's airflow volume decreased due to the service life expired or failure. <br> [Sub code: 0001 to 0008] <br> [Sub code: 0010 to 0200] | Check the cumulative run time of the cooling fan.* <br> $\rightarrow$ Replace the cooling fan. (Contact your Fuji Electric representative.) |
|  | Visually check whether the cooling fan rotates normally. <br> $\rightarrow$ Replace the cooling fan. (Contact your Fuji Electric representative.) |
| (4) Overload <br> [Sub code: 0001 to 0008] | Measure the output current. <br> $\rightarrow$ Reduce the load (Use the heat sink overheat early warning [INV-OH] (E15 to E27) or the inverter overload early warning [INV-OL] (E15 to E27) to reduce the load before the overload protection is activated.). |

* Refer to "Section 3.4.4.6 Reading maintenance information" in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7-■-0019)".


## ［24］ 动化 External alarm

Problem External alarm（＂THR＂）was inputted．（When the external alarm signal＂THR＂has been assigned to any of digital input terminals．）

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| （1）An alarm function of external equipment was activated． | Check the operation of external equipment． <br> $\rightarrow$ Remove the cause of the alarm that occurred in external equipment． |
| （2）Wrong connection or poor contact in external alarm wiring | Check if the＂external alarm＂signal wiring is correctly connected to the terminal to which the＂External alarm＂（function code data $=9$ ）has been assigned．（Any of E01 through E09 should be set to＂9．＂） <br> Connect the external alarm wiring correctly． |
| （3）Incorrect setting of function code data | Check whether the normal／negative logic of the external signal matches that of the＂THR＂command specified by E14． <br> $\rightarrow$ Ensure the matching of the normal／negative logic． |
| （4）The surrounding temperature exceeded the range of the braking resistor temperature specification． | Measure the temperature around the braking resistor． <br> $\rightarrow$ Lower the surrounding temperature（e．g．ventilate the inverter）． |
| （5）The capacity of the braking resistor is insufficient． | Reconsider the capacity and \％ED of the braking resistor． <br> $\rightarrow$ Review the braking resistor． |
| （6）Diode rectifier RHD－D is overheated | When a diode rectifier RHD－D is being used，please check all possible reasons and countermeasures discribed in［23］OH1 heat sink overheat． |
| （7）PWM converter RHC－D is tripped | When a PWM converter RHC－D is being used，please remove the possible alarm reasons according to chapter 6．3．10．2 trouble shooting． |
| （8）AC fuse has blown | Confirm if the AC fuse has blown or not． <br> $\rightarrow$ Request the repair of inverter．（Contact the service department of our company） <br> $\rightarrow$ Confirm the ground fault part and remove it．（The wiring should also be checked．）If the AC fuse blown is caused by ground fault，it may be necessary to have inverter repaired and inspected．（Contact the service department of our company） <br> Confirm if the wire of microswitch is disconnected or not． <br> $\rightarrow$ Confirm the wire with tester． <br> $\rightarrow$ Confirm if any bolt is loosened．（Confirm bolts of terminals．） |

## ［ 25 ］ ำนプ Inverter internal overheat

Problem Temperature inside the inverter has exceeded the allowable limit．

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| （1）The surrounding temperature exceeded the inverter＇s specification limit． <br> ［Sub code： 0001 to 0008］ | Measure the surrounding temperature． <br> $\rightarrow$ Lower the temperature around the inverter（e．g．ventilate the panel where the inverter is mounted）． |
| （2）Temperature detection circuit failure（Thermistor wire break） <br> ［Sub code：0010］ | $\rightarrow$ Request for repair work on inverter．（Please contact our service department．） <br> ＊Inform the representative of the alarm sub code displayed． |

## [ 26 ] ค

Problem Temperature of the motor has risen abnormally.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The temperature around the motor exceeded the range of the motor specification. | Measure the temperature around the motor. <br> $\rightarrow$ Lower the surrounding temperature. |
| (2) Cooling system for the motor failed. | Check if the cooling system of the motor is operating normally. <br> $\rightarrow$ Repair or replace the cooling system of the motor. |
| (3) Overload | Measure the output current. <br> $\rightarrow$ Reduce the load (e.g. Use the motor overload early warning (E34) to reduce the load before the overload protection is activated.). <br> Lower the temperature around the motor. |
| (4) The activation level (E32) of the PTC thermistor for motor overheat protection was set inadequately. | Check the PTC thermistor specifications and recalculate the detection voltage. <br> $\rightarrow$ Modify the data of function code. |
| (5) The activation level (E30) of the NTC thermistor for motor overheat protection was set inadequately. | Check the data of function code E30 (motor overheat protection level). <br> $\rightarrow$ When a motor exclusive to vector control is used, set E30 to $150^{\circ} \mathrm{C}$ (Factory default). <br> $\rightarrow$ When the motor temperature is entered via any of analog input terminals [Ai1] to [Ai4], set E30 to the protection level matching the motor specification. |
| (6) Settings for the PTC/NTC thermistor are improper. | Check the setting of the thermistor mode selection (function code P30, A31, A131). <br> $\rightarrow$ Change the data of P30, A31 or A131 in accordance with the thermistor used. |
| (7) NTC thermistor model (characteristics) is not correct. | Check the NTC thermistor model (characteristics). <br> $\rightarrow$ Use the NTC thermistor incorporated in a motor exclusive to vector control. |
| [Under V/f control] <br> (8) Excessive torque boost specified (P35, A55, A155) | Check whether decreasing the torque boost (function code P35, A55, A155) does not stall the motor. <br> $\rightarrow$ If no stall occurs, decrease the data of P35, A55 or A155. |
| [Under V/f control] <br> (9) The V/f pattern did not match the motor. | Check whether the motor rated speed (F04, A05, A105) and the motor rated voltage (F05, A04, A104) match the values on the motor's main nameplate. <br> $\rightarrow$ Match the function code data with the values on the motor's main nameplate. |
| (10) Incorrect setting of function code data | Although no PTC thermistor is used, the thermistor mode selection is enabled (function code P30, A31, A131). <br> $\rightarrow$ Change the data of the thermistor mode selection (P30, A31 or A131) to "0" (Disable). |
| (11) The input voltage of the motor cooling fan is out of the range of the specification. | Check the input voltage of the motor cooling fan. <br> $\rightarrow$ Review the power supply system. |
| (12) The air passage of the motor cooling fan is clogged. | Check the air passage of the motor cooling fan. <br> $\rightarrow$ Perform cleaning. (For the cleaning procedure, contact your Fuji Electric representative.) |
| (13) Mismatch of motor parameters | For exclusive motors for the FRENIC-VG: Check whether the data of function code P02 matches the connected motor. <br> $\rightarrow$ Correct the data of P02. <br> $\rightarrow$ For other motors: Perform auto-tuning. |

## 

Problem Electronic thermal protection for motor 1，2，or 3 activated．
ilil i ：Motor 1 overload
バルース ：Motor 2 overload
ハIII＝：Motor 3 overload

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| （1）The electronic thermal <br> characteristics do not match <br> the motor overload <br> characteristics． | Check the motor characteristics． <br> $\rightarrow$ Reconsider the data of function codes F10，F12，A32，A34，A132 and <br> A134． |
| （2）The activation level for the <br> electronic thermal protection <br> is not appropriate． | Recheck the continuous allowable current of the motor． <br> $\rightarrow$ Reconsider and change the data of function code F11，A33 or A133． |
| （3）The specified acceleration／ |  |
| deceleration time is too short． |  | | Recalculate the acceleration／deceleration torque and time needed for the load， |
| :--- |
| based on the moment of inertia for the load and the acceleration／deceleration |
| time． |
| $\rightarrow$ Increase the acceleration／deceleration time（F07，F08，C46，C47，C56， |
| C57，C66，C67）． |

## [28] Lik'Inverter overload

Problem Electronic thermal overload protection for inverter activated.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) The surrounding temperature <br> exceeded the range of the <br> inverter specification. | Measure the temperature around the inverter. <br> $\rightarrow$ Lower the surrounding temperature (e.g. ventilate the panel where the <br> inverter is mounted.). |
| [Under V/f control] <br> (2) Excessive torque boost <br> specified | Check whether decreasing the torque boost (P35, A55, A155) does not stall the <br> motor. <br> $\rightarrow$ If no stall occurs, decrease the torque boost (P35, A55, A155). |
| (3) The specified <br> acceleration/deceleration time <br> was too short. | Recalculate the acceleration/deceleration torque and time needed for the load, <br> based on the moment of inertia for the load and the acceleration/deceleration <br> time. |
| (4) Overload | Increase the acceleration/deceleration time (F07, C35, C46, C56, C66). |

## [29] 1 겐ㄴㄴ Output phase loss

Problem Output phase loss occurred.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Inverter output wiring is <br> broken. | Measure the output current. <br> $\rightarrow$ Replace the output wiring. |
| (2) The motor winding is broken. | Measure the output current. <br> $\rightarrow$ Replace the motor. |
| (3) The inverter output terminals <br> or motor input terminals are <br> weakly tightened. | Check if any screws on those terminals have become loose. <br> $\rightarrow$ Tighten the terminal screws to the recommended torque. |
| (4) A single-phase motor has <br> been connected. | Single-phase motors cannot be used. (The FRENIC-VG is a drive for <br> three-phase motors.) |

## [ 30 ] 05 Overspeed

Problem The motor rotates in an excessive speed. (When Motor speed $\geq$ Maximum reference speed $\times \mathrm{H} 90 \div 100$ )

| Possible Causes | What to Check and Suggested Measures |
| :--- | ---: |
| [Under vector control with/without <br> speed sensor] | Check the maximum speed setting (function code F03, A06, A106). <br> $\rightarrow$ Modify the data of F03, A06 or A106 in accordance with the machinery. |
|  |  |

(1) Incorrect setting of function code data
[Under vector control with/without speed sensor]
(2) Insufficient gain of the automatic speed regulator (ASR)
[Under vector control with/without speed sensor]
(3) The overspeed alarm detection level is not appropriate.
[Under vector control with speed sensor]
(4) Noises superimposed on the PG signal.
[Under vector control with/without speed sensor]
(5) Droop gain too large
[Under vector control with/without speed sensor]
(6) The motor parameters do not match the connected motor.
[Under vector control without
speed sensor] speed sensor]
(7) Breaks in the inverter output circuit
[Under vector control with speed sensor]
(8) PG waveform abnormal

Check the setting of the speed limiter (F76 to F78).
$\rightarrow$ Enable the speed limiter (F76 to F78).
Check whether the actual speed overshoots the commanded one in higher speed operation.
$\rightarrow$ Increase the ASR gain (F61).
(Depending on the situations, reconsider the setting of the filter constants or the integral time.)

Check the setting of the overspeed alarm detection level (H90/Factory default 120\%).
$\rightarrow$ Set the data of H90, taking into account the maximum allowable speed for the machinery.

Check the PG signal input monitor and check whether appropriate noise control measures have been implemented (e.g. correct grounding and routing of signal wires and main circuit wires).
$\rightarrow$ Implement noise control measures. (For details, refer to "Appendix 5.")
Check whether the droop gain is appropriate.
$\rightarrow$ Decrease the droop gain (H28).

For motors exclusive to the FRENIC-VG: Check whether the setting of function code P02 matches the connected motor.
$\rightarrow$ Correct the data of P02.
For other motors:
Perform auto-tuning.
Check the inverter output circuit.
$\rightarrow$ Correct the wiring.

Measure the PG waveform.
$\rightarrow$ Replace the PG.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| [Under vector control with speed <br> sensor] | Check the function code setting. <br> (9) Mismatch between the PG's <br> pulse resolution specification <br> and the function code setting |
| Match the function code settings (P28, A30, A130) with the PG |  |
| specifications. |  |

## [31] $L^{\prime}$ 'Overvoltage

Problem The DC link bus voltage exceeded the overvoltage detection level.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The power supply voltage exceeded the range of the inverter specification. | Measure the input voltage. <br> $\rightarrow$ Decrease the power supply voltage to within the specified range. |
| (2) A surge current entered the input power supply. | In the same power supply system, if a phase-advancing capacitor is turned ON/OFF or a thyristor converter is activated, a surge (momentary large increase in the input voltage) may be caused in the input power. <br> $\rightarrow$ Install a DC reactor. |
| (3) The deceleration time was too short for the moment of inertia of the load. | Recalculate the deceleration torque based on the moment of inertia of the load and the deceleration time. <br> $\rightarrow$ Increase the deceleration time (F08, C36, C47, C57, C67). <br> $\rightarrow$ Consider the use of a braking resistor or PWM converter. <br> $\rightarrow$ Decrease the moment of inertia of the load. <br> $\rightarrow$ Enable the overvoltage suppression function (H57). <br> $\rightarrow$ Select the power limit function (F40 = 2). <br> [Under vector control with speed sensor] <br> $\rightarrow$ Enable the torque limiter (F40 to F45). |
| (4) The acceleration time was too short. | Check if an overvoltage alarm occurs after acceleration. <br> $\rightarrow$ Increase the acceleration time (F07, C35, C46, C56, C66). <br> $\rightarrow$ Select the S-curve acceleration/deceleration (F67 to F70). <br> $\rightarrow$ Consider the use of a braking resistor or PWM converter. <br> $\rightarrow$ Decrease the moment of inertia of the load. |
| (5) Braking load was too heavy. | Compare the braking torque of the load with that of the inverter. <br> $\rightarrow$ Consider the use or enhancement of a braking resistor (DBR) or the use of PWM converter. |
| (6) Malfunction caused by noise | Check if the DC link bus voltage was below the protective level when the overvoltage occurred. <br> $\rightarrow$ Implement noise control measures. (For details, refer to "Appendix 5.") <br> $\rightarrow$ Enable the auto-reset (H04). <br> $\rightarrow$ Connect a surge absorber to magnetic contactor's coils or other solenoids (if any) causing noise. |
| (7) The inverter output lines were short-circuited. | Disconnect the wiring from the inverter output terminals ( $\mathrm{U}, \mathrm{V}$ and W ) and measure the interphase resistance of the motor wiring. Check if the resistance is too low. <br> $\rightarrow$ Remove the short-circuited part (including replacement of the wiring, relay terminals and motor). |
| (8) Wrong connection of the braking resistor | Check the connection. <br> $\rightarrow$ Correct the connection. |
| (9) Large, rapid decrease of the load | Check whether the inverter runs at the time of rapid decrease of the load. <br> $\rightarrow$ Consider the use or enhancement of a braking resistor (DBR) or the use of PWM converter. |

## [ 32 ] ISPG wire break

Problem The pulse generator (PG) wiring has been broken somewhere in the circuit.

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Break in the PG wiring Inverter PA, PB: [Sub code: 0001] Inverter power supply: [Sub code: 0004] <br> Option: [Sub code: 0002] (OPC-VG1-PG, OPC-VG1-PMPG) | Check whether the PG is correctly connected to the option or any wire is broken. <br> $\rightarrow$ Check whether the PG is connected correctly. Or, tighten up the related terminal screws. <br> $\rightarrow$ Check whether any joint or connecting part bites the wire sheath. <br> $\rightarrow$ Replace the wire. |
| [PMSM] <br> When the option card (OPC-VG1-PMPG) is used: <br> (2) Connection failure of speed/magnetic pole position sensor <br> (3) Mismatch between the motor rotation direction and sensor output <br> [Sub code: 0010 to 0400] | Check the output wiring of the speed/magnetic pole position sensor for poor contact or the phase sequence of the AB phases and UVW phases. <br> $\rightarrow$ Correct the connection between the option card and the speed/magnetic pole position sensor. <br> Check the motor wiring for poor contact or the phase sequence. <br> $\rightarrow$ Correct the connection between the inverter and the motor. |
| (4) Connection failure of option card (OPC-VG1-PG, OPC-VG1-PMPG) | Check whether the connector of the option card engages with that of the inverter unit. <br> $\rightarrow$ Mount the option card on the inverter unit correctly. |
| (5) PG related circuit affected by strong electrical noise | Check if appropriate noise control measures have been implemented (e.g. correct grounding and routing of signal wires, communication cables, and main circuit wires.). <br> $\rightarrow$ Implement noise control measures. <br> $\rightarrow$ Separate the control circuit wiring from the main circuit wiring as far as possible. |
| (6) Motor drive control mode wrongly selected | Check the motor drive control mode currently selected. <br> $\rightarrow$ If no speed sensor is mounted, select the vector control without speed sensor. |
| (7) Mismatch between the PG power voltage (specification) and the voltage setting of PGP terminal | Check the PG power supply voltage (specification) and the voltage setting of PGP terminal (switchable with SW6). <br> $\rightarrow$ Set SW6 properly. <br> For details, refer to Chapter 3, "Section 3.3.3.9 Setting up the slide switches" of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". |
| (8) PG wires small in size | Check whether the PG wires satisfy the recommended wire size. <br> $\rightarrow$ Replace the wires with the recommended one. |
| (9) PG waveform abnormal | Check whether the inverter internal control circuit (PG input circuit) is faulty, using the self-diagnosis function of the PG detection circuit $(\mathrm{H} 74)$. <br> $\rightarrow$ If the result is "Normal," replace the PG. <br> $\rightarrow$ If it is "Abnormal," contact your Fuji Electric representative. <br> Check the PG waveform using an oscilloscope. <br> $\rightarrow$ Replace the PG. |

## [ 33 ] $A 1-E$ E-SX bus tact synchronization error

Problem E-SX bus tact synchronization error occurred during operation.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| Alarm occurred due to noise. | Check if noise entered the E-SX bus.  <br>  $\rightarrow$ Check if the E-SX bus is mounted in parallel with the main circuit <br>  cable. If so, modify the wiring route. <br>  $\rightarrow$ Insert the ferrite core. <br>  $\rightarrow$ Lower the tact frequency if possible. |

* For more information, see Section 6.14, Chapter 6 in separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)" of separate volume "Option Edition (24A7- $\square$-0045)".


## [ 34 ] $\mathscr{S i}^{-1}$ Toggle abnormality error

Problem A toggle abnormality monitoring error occurred. (Available when T-Link, SX bus, or E-SX bus is used.)

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| Toggle abnormality monitoring error <br> occurred. | $\rightarrow$ Check if the CPU of the host PLC is stopped. |

### 11.4 If the "light alarm" indication ( $1-1 / 2)$ appears on the LED monitor

If the inverter detects a minor abnormal state "light alarm," it can continue the current operation without tripping. (Light alarm function)
When a light alarm occurs, the "light alarm" indication $L-F_{1 / \prime \prime}^{\prime}$ is displayed on the LED monitor, the LED under the (ewd) key blinks, and the "light alarm" signal "L-ALM" is output to a general-purpose output terminal. (To use the L-ALM, it is necessary to assign the signal to any of the digital output terminals by setting any of function codes E15 through E19 to "57.")
Function codes H106 through H110 specify which alarms should be categorized as "light alarm." The available "light alarm" codes are check-marked in the "Light alarm" object column in Table: 11.3-1 (page 11-3).
For the "light alarm" factors and the alarm removal procedure, refer to Chapter 3, "Section 3.4.3.5 Monitoring light alarms" of separate volume "Unit Type/Function Codes Edition (24A7- $\square-0019)$ ".

### 11.5 If neither an alarm code nor "light alarm" indication ( $L-1 / L)$ appears on the LED monitor

### 11.5.1 Abnormal motor operation

## [ 1 ] The motor does not rotate

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) No power supplied to the inverter | Check the input voltage and interphase voltage unbalance. <br> $\rightarrow$ Check if the input devices work properly and if the wiring is correct, etc. <br> $\rightarrow$ Check for voltage drop, phase loss, poor connections, or poor contacts, and fix them if necessary. <br> $\rightarrow$ If only the auxiliary control power input is supplied, also supply the main power to the inverter. <br> $\rightarrow$ Check the converter for any faults. |
| (2) No run forward/reverse command was inputted, or both the commands were inputted simultaneously (terminal block operation). | Check the input status of the forward/reverse command with Menu "I/O check" on the keypad. <br> $\rightarrow$ Input a run command. <br> $\rightarrow$ Set either the forward or reverse operation command to off. <br> $\rightarrow$ Correct the run command source. (Set the data of F02 to "1.") <br> $\rightarrow$ Connect the external circuit wiring to control circuit terminals [FWD] and [REV] correctly. <br> $\rightarrow$ Make sure that the sink/source slide switch (SW1) on the printed circuit board (PCB) is properly configured. <br> For details, refer to Chapter 3, "Section 3.3.3.9 Setting up the slide switches" of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)". |
| (3) A run command with higher priority than the one attempted was active, and the run command was stopped. | Referring to the run command block diagram*, check the higher priority run command using Menu "DATA CHECK" and Menu "I/O check" with the keypad. <br> $\rightarrow$ Correct the wrong setting of function code data of Communications link function (Mode selection) (H3O) or cancel the higher priority run command. |
| (4) No analog speed command input. | Check whether the analog speed command has been entered correctly, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Connect the external circuit wiring to terminals [13], [12], [11], [Ai1] and [Ai2] correctly. <br> $\rightarrow$ Inspect the speed command potentiometers, signal converters, switches and relay contacts. Replace defective one(s), if any. |
| [Under V/f control] <br> (5) The reference speed was below the starting or stop speed. | Check whether the speed command has been entered correctly, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Set the reference speed at the same or higher than the starting speed (F23). <br> $\rightarrow$ Reconsider the starting speed (F23), and if necessary, change it to the lower value. <br> $\rightarrow$ Inspect the speed command potentiometers, signal converters, switches and relay contacts. Replace defective one(s), if any. <br> $\rightarrow$ Connect the external circuit wiring to terminals [13], [12], [11], [Ai1] and [Ai2] correctly. |
| (6) A reference speed with higher priority than the one attempted was active. | Referring to the run command block diagram*, check the higher priority run command using Menu "DATA CHECK" and Menu "I/O check" with the keypad. <br> $\rightarrow$ Correct the wrong setting of function code data (e.g. cancel the higher priority run command). <br> $\rightarrow$ Correct the wrong setting of function code data of Communications link function (Mode selection) (H30) or cancel the higher priority run command. |

[^21]| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (7) The speed limiter settings were made incorrectly. | Check the data of function codes F76 (Speed limiter mode selection), F77 and F78 (Speed limiter levels 1 and 2). <br> $\rightarrow$ Correct the data of F76 through F78. |
| (8) The coast-to-stop command was effective. | Check the data of function codes E01 through E09 and the input status of $X$ terminals, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Release the coast-to-stop command setting. |
| (9) No enable input on [EN1] or [EN2] | Check the input status of the EN terminal, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Connect terminals [EN1] and [EN2]. <br> - To make inverters not compliant with the Functional Safety Standard (STO), short-circuit each of terminals [EN1] and [EN2] with [PS]. <br> (Refer to "Section 3.3.3.8 Wiring of control circuit terminals, [EN1] [EN2]" in Chapter 3 of separate volume "Unit Type/Function Codes Edition (24A7-■-0019)".) <br> - To make inverters compliant with the Functional Safety Standard (STO), refer to the instruction manual. Refer to FRENIC-VG Instruction Manual. |
| (10) Broken wires, incorrect connection or poor contact with the motor. Or the motor defective. | Check the wiring and the motor. (Measure the output current.) <br> $\rightarrow$ Repair the wiring to the motor, or replace them. <br> $\rightarrow$ Repair the motor or replace it. When the motor needs to be repaired, contact your Fuji Electric representative. |
| (11) Overload | Measure the output current. <br> $\rightarrow$ Reduce the load (In winter, the load tends to increase.) <br> $\rightarrow$ Increase the inverter and motor capacities. <br> Check whether any mechanical brake is activated. <br> $\rightarrow$ Release the mechanical brake, if any. |
| (12) Torque generated by the motor is insufficient. | Check that the motor switching signal (selecting motor 1,2 or 3 ) is correct with Menu "I/O check" using the keypad and that the data of function codes matches each motor. <br> $\rightarrow$ Correct the motor switching signal. <br> $\rightarrow$ Modify the function code data to match the connected motor. |
| [Under V/f control] <br> (13) Torque generated by the motor is insufficient. | Check whether the reference speed is below the slip-compensated speed of the motor. <br> (Function codes P10 and P11 for M1, A12 and A13 for M2, and A112 and A113 for M3). <br> $\rightarrow$ Change the reference speed so that it becomes higher than the slip-compensated speed of the motor. <br> Check whether increasing the toque boost (Function code P35, A55, A155) starts rotating the motor. <br> $\rightarrow$ Increase the data of P35, A55 or A155. <br> Check the data of function code F04, A05 or A105. <br> $\rightarrow$ Change the V/f pattern setting to match each motor. |
| (14)No reference speed setting (keypad operation) | Check the reference speed on the keypad. <br> $\rightarrow$ Modify the reference speed by pressing [ $\uparrow$ ] key. |
| [Under vector control with speed sensor] <br> (15) Incorrect setting of the number of poles of the motor | Check whether the setting of function code P05, A07 or A107 (No. of poles) matches the number of poles of the actual motor. <br> $\rightarrow$ Set the data of $\mathrm{P} 05, \mathrm{~A} 07$ or A 107 to the correct number of poles. |
| [Under vector control with speed sensor] <br> (16) Wrong wiring between the motor and pulse generator (PG) | Check the motor wiring (phase sequence) and the polarity of the PG. <br> $\rightarrow$ Correct the wiring. |


| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| [Under vector control with/without speed sensor] <br> (17) Incorrect setting of the torque limiter level | Check whether the torque limiter level is set to zero (0). <br> $\rightarrow$ Modify the torque limiter level to the appropriate value. |
| [Under vector control with/without speed sensor] <br> (18) Incorrect setting of the torque command value | Check whether the torque command value is zero (0) under torque control mode. <br> $\rightarrow$ Modify the torque command value to the appropriate value. |
| [Under vector control with speed sensor] <br> (19)Mismatch between the PG's specification and the function code setting | Check whether the setting of function code P28, A30 or A130 matches the pulse resolution specification of the actual PG. <br> $\rightarrow$ Modify the data of P28, A30 or A130 to the appropriate value. <br> Check whether the voltage setting of terminal PGP (SW6) matches the power supply voltage specification of the actual PG. <br> $\rightarrow$ Set SW6 to the appropriate position. <br> For details, refer to Chapter 3, "Section 3.3.3.9 Setting up the slide switches" of separate volume "Unit Type/Function Codes Edition (24A7-■-0019)". |
| (20)The magnetic pole position of the synchronous motor (PMSM) is out of place. | Check the magnetic pole position. <br> $\rightarrow$ Adjust the magnetic pole position (o10, A60, A160). * |

* Refer to Chapter 3, "Section 3.5.3.3 Adjusting the magnetic pole position" of separate volume "Unit Type/Function Codes Edition (24A7-■-0019)".


## [ 2 ] The motor rotates, but the speed does not change

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The setting of the maximum speed was too low. | Check the data of function code F03, A06 or A106 (Maximum speed). <br> $\rightarrow$ Modify the data of F03, A06 or A106 to the appropriate value. |
| (2) The setting of the speed limiter was too low. | Check the setting of the speed limiter (F76 to F78). <br> $\rightarrow$ Modify the data of F76 to F78 to the appropriate value. |
| (3) The reference speed did not change.(Analog setting) | Check whether the reference speed has been entered correctly, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Increase the reference speed. <br> $\rightarrow$ Inspect the speed command potentiometers, signal converters, switches, and relay contacts. Replace any ones that are faulty. <br> $\rightarrow$ Connect the external circuit wiring to terminals [13], [12], [11], [Ai1] and [Ai2] correctly. |
| (4) The external circuit wiring to terminals [X1] to [X9] or signal assignment to those terminals is wrong. | Check whether the reference speed has been entered correctly, using Menu "I/O check" on the keypad. <br> $\rightarrow$ Connect the external circuit wiring to terminals [X1] to [X9] correctly. <br> $\rightarrow$ Correct the data of E01 to E14. <br> $\rightarrow$ Correct the data of C 05 to C 21 . (Multistep speed settings) |
| (5) A reference speed (e.g. multistep speed or via communications link) with higher priority than the one attempted was active and the reference speed was too low. | Referring to the speed command block diagram*, check the function code data check and Menu "I/O check" with the keypad. <br> $\rightarrow$ Correct any incorrect data of function code data (e.g. cancel the higher priority reference speed). |
| (6) The acceleration or deceleration time was too long or too short. | Check the settings of the acceleration/deceleration time (function codes F07, F08, C35, C36, C46, C47, C56, C57, C66 and C67). <br> $\rightarrow$ Change the acceleration/deceleration time to match the load. |


| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (7) Overload | Measure the output current. <br> $\rightarrow$ Reduce the load. <br> Check whether any mechanical brake is activated. <br> $\rightarrow$ Release the mechanical brake. |
| [Under V/f control] <br> (8) Function code settings do not agree with the motor characteristics. | If auto-torque boost (Function code P35, A55, A155) is enabled, check whether the data of P03, P04, P06, P07 and P08 for M1, A02, A03, A08, A09 and A10 for M2, A102, A103, A108, A109 and A110 for M3 matches the parameters of the motor. <br> $\rightarrow$ Perform auto-tuning of the inverter for the motor to be used. |
| [Under V/f control] <br> (9) The output frequency does not increase due to the current limiting operation. | Decrease the value of the torque boost (Function code P35, A55, A155), then run the motor again and check if the speed increases. <br> $\rightarrow$ Adjust the value of the torque boost (P35, A55, A155). <br> Check the data of function codes F04, A05 and A105 to ensure that the V/f pattern setting is right. <br> $\rightarrow$ Match the V/f pattern setting with the motor ratings. |
| (10) The motor speed does not increase due to the torque limiter operation. | Check whether the data of torque limiter level related function codes F40 through F45 is correctly configured. <br> Check the "TL2/TL1" terminal command ("Select torque limiter level $2 / 1$ ") is correct. <br> $\rightarrow$ Correct the data of F44 or F45 or enter the "F40-CCL" terminal command (Cancel F40 (Torque limiter mode 1)). |
| (11) Incorrect settings of bias and gain for analog input. | Check the data of function codes F17, F18 and E53 to E60. <br> $\rightarrow$ Correct the bias and gain settings. |
| (12) The reference speed did not change. (Keypad operation) | Check whether modifying the reference speed setting on the keypad changes the reference speed. <br> $\rightarrow$ Modify the reference speed setting by pressing the [ $\uparrow$ ] and [ $\downarrow$ ] keys. |
| [Under vector control with speed sensor] <br> (13) Wrong wiring of the PG | Check the wiring between the PG and the inverter for the phase sequence, wire breaks, shielding and twisting. <br> $\rightarrow$ Correct the wiring. |
| [Under vector control with speed sensor] <br> (14)Wrong wiring between the inverter and the motor | Check the phase sequence ( $\mathrm{U}, \mathrm{V}$, and W ) of the motor wiring. <br> $\rightarrow$ Connect the inverter output terminals $\mathrm{U}, \mathrm{V}$, and W to the motor input terminals $\mathrm{U}, \mathrm{V}$, and W , respectively. |
| [Under vector control with/without speed sensor] <br> (15)Function code settings do not agree with the motor characteristics. | For motors exclusive to the FRENIC-VG: Check whether the data of function code P02 matches the specification of the connected motor. <br> $\rightarrow$ Correct the data of P02. <br> For other motors: <br> $\rightarrow$ Perform auto-tuning. |

* Refer to "Section 4.1 Block diagrams for control logic" in Chapter 4 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)".


## [3] The motor runs in the opposite direction to the command

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| [Under V/f control] <br> [Under vector control without <br> speed sensor] <br> (1) Wrong wiring to the motor | Check the wiring to the motor. <br> $\rightarrow$ Connect the inverter output terminals U, V, and W to the motor input <br> terminals U, V, and W, respectively. |
| (2) The rotation direction <br> specification of the motor is <br> opposite to that of the <br> inverter. | The rotation direction of IEC-compliant motors is opposite to that of the <br> FRNIC-VG1 dedicated motors. <br> $\rightarrow$ Switch the "FWD"/"REV" signal setting. |
| (3) Incorrect setting of speed <br> command related function <br> code data | Check the data of the speed command related function codes, referring to the <br> speed command selection block diagram*1. <br> $\rightarrow$ Correct the data of the related function codes. |
| [Under vector control with speed |  |
| sensor] |  |
| (4) Wrong wiring of the PG | Check the wiring to the motor. <br> $\rightarrow$ Correct the wiring. ${ }^{* 2}$ |

*1 For details, refer to Chapter 4 of separate volume "Unit Type/Function Codes Edition (24A7- $\square-0019$ )".
*2 Refer to Chapter 3, "Section 3.5.2 Mounting direction of a pulse encoder (PG) and PG signals" separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)".

## [4] Speed fluctuation or current oscillation (e.g. hunting) occurs during running at constant speed

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The analog speed command fluctuates. | Check the signal status for the speed command with Menu "I/O check" using the keypad. <br> $\rightarrow$ Increase the filter constants (F83, E61 to E64) for the speed command. <br> $\rightarrow$ Take measures to keep the speed command value constant. |
| (2) An external speed command potentiometer is used. | Check that there is no noise on the signal wires connecting to external sources. <br> $\rightarrow$ Separate the control circuit wiring from the main circuit wiring as far as possible. <br> (Do not install the main circuit wires and control circuit wires side by side.) <br> $\rightarrow$ Use shielded or twisted wires for control circuit wiring. <br> $\rightarrow$ Set a ferrite core on the signal wire. (In the case of 1 MHz or higher: ACL-40B) <br> $\rightarrow$ Use an insulation converter. <br> Check whether the speed command potentiometer is malfunctioning due to noise from the inverter. <br> $\rightarrow$ Connect a capacitor ( 0.22 uF or less) to the output terminal of the speed command potentiometer or set a ferrite core on the signal wire. |
| (3) Speed switching or multistep speed command was enabled. | Check whether the relay signal for switching the speed command is chattering. <br> If the relay contact is defective, replace the relay. |
| [Under V/f control] <br> (4) The wiring length between the inverter and the motor is too long. | Check whether auto-torque boost is enabled (P35, A55, A155). <br> $\rightarrow$ Perform auto-tuning. <br> Disable the auto-torque boost (select manual torque boost), then check that the motor vibration stops. <br> $\rightarrow$ Make the output wiring as short as possible. |
| (5) The machinery is hunting due to vibration caused by low rigidity of the load side. Or the current is irregularly oscillating due to special motor parameters. | Once disable all the automatic control systems (speed control, auto-torque boost, current limiting, torque limiter and droop control), then check that the motor vibration comes to a stop. <br> $\rightarrow$ Under vector control with/without speed sensor, readjust the speed control system. (F61 to F66, C40 to C45, C50 to C55) <br> $\rightarrow$ Disable the automatic control system(s) causing the vibration. |
| (6) Function code settings do not agree with the motor characteristics. | For motors exclusive to the FRENIC-VG: Check whether the setting of function code P02 matches the specification of the connected motor. <br> $\rightarrow$ Correct the data of P02. <br> For other motors: <br> $\rightarrow$ Perform auto-tuning. |
| [Under vector control with/without speed sensor] <br> (7) Load is fluctuating. | Check whether the automatic speed regulator (ASR) is properly configured. (F61 to F66, C40 to C45, C50 to C55) <br> $\rightarrow$ Readjust the speed control system. (F61 to F66, C40 to C45, C50 to C55) |
| (8) Output voltage of PWM converter is not stable. | $\rightarrow$ Refer to Instruction Manuals for PWM converter. You may be required to change the setting of function code U04 (AVR control response), for example. |

## [5] Grating sound is heard from the motor or the motor sound fluctuates

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Resonance with the load | Check the machinery mounting accuracy of the load side or check whether <br> there is resonance with the mounting base. <br> $\rightarrow$ |
|  | Disconnect the motor from the machinery and run it alone to find where <br> the resonance comes from. Upon locating the cause, improve the <br> characteristics of the source of the resonance. |
| $\rightarrow$Adjust the jump speed (C01 to C04) to avoid continuous running in the <br> frequency range causing resonance. |  |
| $\rightarrow$Specify the observer (H47 to H52, H125 to H127) to suppress vibration. <br> (Depending on the characteristics of the load, this may take no effect.) |  |
| $\rightarrow$Decrease the P gain of the auto speed regulator (ASR). (F61, C40, C50, <br> C60) |  |

## [6] The motor does not accelerate or decelerate within the specified time

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The inverter runs the motor with S-curve acceleration/deceleration. | Check the data of function codes F67 to F70 (S-curve acceleration/deceleration pattern). <br> $\rightarrow$ Select the linear pattern. (F67 to $F 70=0$ ) <br> $\rightarrow$ Decrease the acceleration/deceleration time (F07, F08, C46, C47, C56, C57, C66, C67). |
| [Under V/f control] <br> (2) The current limiting operation prevented the frequency from increasing (during acceleration). | Check whether the acceleration time and torque boost are properly specified. <br> $\rightarrow$ Increase the data of F07, C35, C46, C56 or C66 (acceleration time). <br> $\rightarrow$ Decrease the torque boost (P35, A55, A155) and restart the inverter to check that the speed increases. |
| (3) Overload | Measure the output current. <br> $\rightarrow$ Reduce the load. |
| [Under V/f control] <br> (4) Torque generated by the motor was insufficient. | Check that increasing the torque boost (P35, A55, A155) starts the motor. <br> $\rightarrow$ Increase the value of the torque boost (P35, A55, A155). |
| (6) Torque generated by the motor is limited by the torque limiter operation. | Check whether data of torque limiter level related function codes (F40 to F45) is correctly configured and the "TL2/TL1" terminal command ("Select torque limiter level $1 / 2^{\prime \prime}$ ) is correct. <br> $\rightarrow$ Correct the data of F40 to F45 or reset them to the factory defaults. Check whether the speed command potentiometer is malfunctioning due to noise from the inverter. <br> $\rightarrow$ Set the torque limiter (TL2 or TL1) switching signal correctly. <br> $\rightarrow$ Increase the acceleration/deceleration time (F07, F08, C35, C36, C46, C47, C56, C57, C66, C67). |
| (7) The specified acceleration or deceleration time was incorrect. | Check the terminal commands "RT1" and "RT2" for acceleration/deceleration times using the X terminal (digital input terminal). <br> $\rightarrow$ Correct the signal settings. |
| (8) Current limiting settings on PWM converter were changed. | $\rightarrow$ Refer to Instruction Manuals for the PWM converter. Check that no change is made on the settings of H 15 to H 18 . (If limit value is set lower than it should be.) |

## [ 7 ] The motor does not restart even after the power recovers from a momentary power failure

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) The data of function code F14 is either " 0, " " 1, ," or " 2. " | Check if an undervoltage trip ( $\left.1 \begin{array}{l}L \\ L\end{array}\right)$ occurs. <br> $\rightarrow$ Change the data of F14 (Restart mode after momentary power failure, Mode selection) to "3," "4," or "5." |
| (2) The run command remains OFF even after the power has been restored. | Check the input signal with Menu "I/O check" using the keypad. <br> $\rightarrow$ Check the power recovery sequence with an external circuit. If necessary, consider the use of a relay that can keep the run command ON. |
|  | In 3-wire operation, the power to the inverter control circuit has been shut down once because of a long momentary power failure time, or the self-holding selection signal "HOLD" has been turned OFF once. <br> $\rightarrow$ Change the design or the setting so that a run command can be issued again within 2 seconds after the power has been restored. |

## [8] The motor abnormally heats up

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Airflow volume of the motor's cooling fan decreased due to the service life expired or failure. | Visually check whether the cooling fan rotates normally. <br> $\rightarrow$ Repair or replace the cooling fan. (Contact your Fuji Electric representative.) |
| [Under V/f control] <br> (2) Excessive torque boost specified | Check whether decreasing the torque boost (P35, A55, A155) decreases the output current but does not stall the motor. <br> $\rightarrow$ If no stall occurs, decrease the torque boost (P35, A55, A155). |
| (3) Continuous running in extremely slow speed | Check the running speed of the inverter. <br> $\rightarrow$ Change the running speed setting or replace the motor with an exclusive motor for inverters (motor with separately powered cooling fan). |
| (4) Overload | Measure the inverter output current. <br> $\rightarrow$ Reduce the load. <br> $\rightarrow$ Increase the inverter capacity and motor capacity. |
| [Under vector control with/without speed sensor] <br> (5) Function code settings do not agree with the motor characteristics. | For exclusive motors for the FRENIC-VG: Check whether the setting of function code P02 matches the specification of the connected motor. <br> $\rightarrow$ Correct the data of P02. <br> For other motors: <br> $\rightarrow$ Perform auto-tuning. |
| (6) Motor defective | Check whether the inverter output voltages ( $\mathrm{U}, \mathrm{V}$ and W ) are well-balanced. <br> $\rightarrow$ Repair or replace the motor. (Contact your Fuji Electric representative.) |

## [ 9 ] The motor does not run as expected

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Incorrect setting of function <br> code data | Check that function codes are correctly configured and no unnecessary <br> configuration has been done. <br> $\rightarrow$ Configure all the function codes correctly. |
|  | Make a note of function code data currently configured and then initialize all <br> function code data using H03. <br> $\rightarrow$ After the above process, reconfigure function codes one by one, checking <br> the running status of the motor. |
| (2) Under torque control, the |  |
| inverter keeps output although |  |
| the run command is OFF. | Check the setting of the automatic operation OFF function (H11). <br> $\rightarrow$ Set the data of H11 to "2" (Coast to a stop when a run command is turned <br> OFF) or "4" (Coast to a stop when a run command is turned OFF under <br> torque control). |

## [ 10 ] When the motor accelerates or decelerates, the speed is not stable

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| [Under vector control with/without | Check whether the automatic speed regulator (ASR) is properly adjusted under <br> speed control. |
| speed sensor] <br> The ASR constants are <br> inadequate. | $\rightarrow$ Readjust the function codes (F61 to F66, C40 to C45, C50 to C55). |

## [ 11] The motor stalls during acceleration

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| [Under vector control with/without speed sensor] <br> (1) Function code settings do not agree with the motor characteristics. | For exclusive motors for the FRENIC-VG: Check whether the setting of function code P02 matches the connected motor. <br> $\rightarrow$ Correct the data of P02. <br> For other motors: <br> $\rightarrow$ Perform auto-tuning. |
| (2) The specified acceleration time is too short. | Check the data of F07, C35, C46, C56 or C66 (acceleration time). <br> $\rightarrow$ Increase the acceleration time. |
| (3) The moment of inertia of the load is large. | Measure the inverter output current. <br> $\rightarrow$ Decrease the moment of inertia of the load. <br> $\rightarrow$ Increase the inverter capacity. |
| (4) Large voltage drop on wires | Check the terminal voltage of the motor. <br> $\rightarrow$ Use larger size wires between the inverter and motor or make the wiring distance shorter. |
| (5) The torque of the load is large. | Measure the output current. <br> $\rightarrow$ Decrease the torque of the load. <br> $\rightarrow$ Increase the inverter capacity. |
| [Under V/f control] <br> (6) Torque generated by the motor was insufficient. | Check that increasing the torque boost (P35, A55, A155) starts the motor. <br> $\rightarrow$ Increase the value of the torque boost (P35, A55, A155). |

[ 12 ] When the T-Link communications option is in use, neither a run command nor a speed command takes effect

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) Incorrect setting of the <br> communications link <br> operation (H30) | Check whether the setting of the communications link operation is correct (H3O). <br> $\rightarrow$ Correct the data of H30. <br> $\rightarrow$ Check the status of the X terminal to which the communications link <br> operation selection [LE] is assigned. |
| (2) Incorrect setting of the <br> transmission format (o32) | Check whether the setting of the transmission format is correct (o32). <br> $\rightarrow$ Correct the data of o32 (4W + 4W or 8W + 8W). |
| (3) Incorrect setting of the link |  |
| number | Check the current setting of the link number (that should be configured in <br> hexadecimal). <br> $\rightarrow$ Review the function code list. |
| (4) Data not written to the I/O |  |
| relay area as assigned |  |$\quad$| Check the data held in the I/O relay area, using the MICREX loader. |
| :--- |
| $\rightarrow$ Investigate writing into the I/O relay area. |

[13] When the SX-bus communications option is in use, neither a run command nor a speed command takes effect

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Incorrect setting of the communications link operation (H30) | Check whether the setting of the communications link operation is correct (H30). <br> $\rightarrow$ Correct the data of H 30 . |
| (2) Terminal command [LE] is assigned to an X terminal, but the terminal is OFF. | Check the status of the X terminal (digital input terminal) to which the [LE] command is assigned. <br> $\rightarrow$ Turn the corresponding $X$ terminal input ON . |
| (3) Incorrect setting of the transmission format selection (U11) | Check whether the transmission format selected by U11 is identical with the one selected in the system configuration definition. <br> $\rightarrow$ Correct the setting of the transmission format. |
| (4) Incorrect setting of the link number | Check the current setting of the link number (that should be configured in hexadecimal). <br> $\rightarrow$ Review the function code list. |
| (5) Data not written to the I/O memory area as assigned to the address | Check the data in application programs, using the SX loader. <br> $\rightarrow$ Investigate writing into the I/O memory area. |

[ 14 ] When the CC-Link communications option is in use, neither a run command nor a speed command takes effect

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) Incorrect setting of the communications link operation (H30) | Check whether the setting of the communications link operation is correct (H3O). <br> $\rightarrow$ Correct the data of H3O. |
| (2) Terminal command [LE] is assigned to an $X$ terminal, but the terminal is OFF. | Check the status of the $X$ terminal (digital input terminal) to which the LE command is assigned. <br> $\rightarrow$ Turn the corresponding $X$ terminal ON . |
| (3) Incorrect setting of the transmission format selection (o32) | Check whether the transmission format selected by o32 is identical with the one selected in the system configuration definition. <br> $\rightarrow$ Correct the setting of the transmission format. |
| (4) Incorrect setting of the link number | Check the current setting of the link number (that should be configured in hexadecimal). <br> $\rightarrow$ Review the function code list. |
| (5) Data not written to the I/O memory area as assigned to the address | Check the data in application programs, using the PLC loader. <br> $\rightarrow$ Investigate writing into the I/O memory area. |

## [ 15 ] Under bar (_) appears

Problem Although you pressed the key or key or entered a run forward command "FWD" or a run reverse command "REV", the motor did not start and an under bar ( $\_$) appeared on the LED monitor.

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) The DC link bus voltage |  |
| was low. |  |$\quad$| Select Menu "MAINTENANCE" in Programming mode on the keypad and check the |
| :--- |
| DC link bus voltage which should be 400 VDC or less for three-phase 400V class |
| series, and 580 VDC or less for three-phase 690 V class series. |
| $\rightarrow$ Connect the inverter to a power supply that meets its input power supply |
| voltage specifications. |
| $\rightarrow$ Check if converter is operating normally. |

### 11.5.2 Problems with inverter settings

## [1] Nothing appears on the keypad

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) No power (neither main power nor auxiliary control power) supplied to the inverter | Measure the input voltage and check the voltage and interphase unbalance. <br> $\rightarrow$ Turn ON a molded case circuit breaker (MCCB), an earth leakage circuit breaker (ELCB) (with overcurrent protection) or a magnetic contactor (MC). <br> $\rightarrow$ Check for voltage drop, phase loss, poor connections, or poor contacts and fix them if necessary. |
| The keypad was not properly connected to the inverter. | Check whether the keypad is properly connected to the inverter. <br> $\rightarrow$ Remove the keypad, put it back, and see whether the problem recurs. <br> $\rightarrow$ Replace the keypad with another one and check whether the problem recurs. |
|  | When running the inverter remotely, ensure that the extension cable is securely connected both to the keypad and to the inverter. <br> $\rightarrow$ Disconnect the cable, reconnect it, and see whether the problem recurs. <br> $\rightarrow$ Replace the keypad with another one and check whether the problem recurs. |

## [2] The desired function code does not appear

| Possible Causes | What to Check and Suggested Measures |
| :--- | :---: |
| (1) The function code does not | Check whether the function code is located in a different directory. |
| appear. | $\rightarrow$ Display the function codes in the directory, referring to Chapter 3, "Section |
|  | 3.4.4 Programming mode" of separate volume "Unit Type/Function Codes |
|  | Edition (24A7- $\square-0019) . "$ |

## [ 3] Data of function codes cannot be changed from the keypad

| Possible Causes | What to Check and Suggested Measures |
| :---: | :---: |
| (1) An attempt was made to change function code data that cannot be changed when the inverter is running. | Check if the inverter is running with Menu "OPR MNTR" using the keypad and then confirm whether the data of the function codes can be changed when the motor is running, referring to the list of function codes. <br> $\rightarrow$ Stop the motor and then change the data of the function codes. |
| (2) The data of the function codes is protected. | Check the data of function code F00 (Data protection). <br> $\rightarrow$ Change the data of FOO from "Enable data protection" (FOO = 1) to "Disable data protection" ( $\mathrm{FOO}=0$ ). |
| (3) The "WE-KP" terminal command ("Enable data change with keypad") is not entered, though it has been assigned to a digital input terminal. | Check the data of function codes E01 to E09 and the input signal status with Menu "I/O check" using the keypad. <br> $\rightarrow$ Input a "WE-KP" command through a digital input terminal. |
| (4) The (1anc) key was not pressed. | Check whether you have pressed the key after changing the function code data. <br> $\rightarrow$ Press the key after changing the function code data. Check that "STORING..." is displayed on the LCD monitor. |
| (5) The data of function code F02 cannot be changed. | Check if either one of the "FWD" and "REV" terminal signals is turned ON. <br> $\rightarrow$ Turn OFF both "FWD" and "REV" terminal signals. |

## [ 4 ] Data of function codes cannot be changed via the communications link

| Possible Causes | What to Check and Suggested Measures |
| :--- | :--- |
| (1) An attempt was made to <br> change function code data <br> that cannot be changed <br> when the inverter is running. | Check if the inverter is running with Menu "OPR MNTR" using the keypad and <br> then confirm whether the data of the function codes can be changed when the <br> motor is running, referring to the list of function codes. <br> $\rightarrow$ Stop the motor and then change the data of the function codes. |
| (2) The data of the function |  |
| codes is protected. |  |$\quad$| Check the data of function code H29 (Data protection). |
| :--- |
| $\rightarrow$ Change the data of H29 from "Enable data protection" (H29 = 1) to "Disable |
| data protection" (H29 = 0). |

## FRENIC-

## Chapter 12 Cabinet Construction

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### 12.1 Installation environment

The inverter is housed in a cabinet (board made of steel sheets) to protect against the surrounding environment and as countermeasures for EMI, human protection, and other concerns. The environments where the cabinets are installed vary, and the installation environment can affect the life and performance of the inverter. In Japan, the "Switchboard and Control Panel Ratings and Tests (JEM1460:2008)" standard of Japan Electrical Manufacturers' Association defines the use conditions. (Refer to Appendix 2.)
JEM1460 specifies normal use conditions and special use conditions. Unless special provisions are specified, normal use conditions are assumed.
The inverter is designed for indoor use under normal use conditions. Therefore, countermeasures are implemented on the cabinet for use in special environment or outdoors. However, quantitative understanding of the conditions and phenomena for special use conditions is difficult and the criteria for judgment is unclear in many cases, as can be seen from JEM1460. Therefore, countermeasures are not always adequate.
In these situations, the most effective, economic and maintenance-friendly countermeasure is to install the inverter where normal use conditions apply. Therefore in cabinet design, care must be taken to make sure that the use conditions adequately meet the actual inverter installation environment.
This chapter describes the countermeasures for the cabinet installed under typical, special conditions.

| Item |  | Concerns for installation location |
| :---: | :---: | :---: |
| Temperature |  | Vicinity of heat generating objects such as blast furnaces, thermostatic ovens, and boilers; sealed rooms and boxes (such as containers); tropical regions, freezers, and cold districts |
| Humidity |  | Food processing factories, inside drying facilities such as for wood, transportation facilities such as for frozen materials, inside tunnels, locations with snow and ice, locations using water and vapor |
| Vibration/Impact |  | Installation on vehicles, ships, and machines such as press machines and cranes |
|  | Dust | Vicinity of casting factories, cement factories, spinning mills, fertilizer plants, flour mills, steel mills, sawmills, construction sites, garbage incinerators, and grinder facilities |
|  | Oil mist | Locations where oil mist exists such as in casting factories, at press machines, and at machine tools |
|  | Salt | Locations affected by sea-salt particles such as seashores and ships |
|  | Flammable gas, Corrosive gas (sulfuration gas) | Chemical factories, petroleum refineries, fuel gas facilities, gasoline stations, water purification plants, hot springs, geothermal power plants, and coal mines |
| Outdoor |  | Outdoor installation location |

### 12.1.1 Ambient temperatures

The ambient temperature of the control board (hereafter called cabinet) is in the range of -10 to $+40^{\circ} \mathrm{C}$ in accordance with the inverter specifications.
Additionally, "No condensation and freezing due to sudden temperature changes" is a condition.
The cabinet houses instruments which use electronic devices such as CPUs and memories, and the ambient temperature is determined from the operating temperature range of these parts. (Aluminum electrolytic capacitor life is calculated based on the operating temperature.)
For this reason, malfunction and decrease of product life occur when the ambient temperature of the inverter exceeds the allowable range. If the temperature does not fall within the allowable range, perform the following measures.

|  | (1) Suppress temperature increase inside the cabinet by increasing ventilation volume (cooling air flow). |
| :--- | :--- | :--- | :--- | :--- | :--- |
| (1) When the heat generated by the instruments inside the cabinet affects the temperature, increase the |  |

### 12.1.2 Humidity (condensation)

High humidity can cause decrease of insulation and erosion, resulting in spatial dielectric breakdown in worst cases when the humidity becomes extremely low. Also, relative humidity can increase rapidly and cause condensation when the temperature changes quickly and the water vapor pressure in the air cannot follow the change.
The inverter has an electronic circuit that has a very little insulation distance between the circuits, causing short circuit when condensations occur. Countermeasures for condensation are necessary for this reason.

| High humidity <br> condensation <br> countermeasure | (1) Install a space heater inside the cabinet. <br> Caution: Beware of local overheating when installing space heaters. <br> (2) Request the user to keep the power on constantly (even when switched off). <br> (3) Move to a location with normal temperature surroundings or a location with air conditioning. <br> (4) Apply anti-dust measures to the cabinet and use panel coolers. |
| :--- | :--- |
| Low humidity <br> countermeasure | Under typical environment, the humidity will not drop below 5\% in most cases. <br> Static electricity occurs easily when humidity is below 5\%, and it can affect various instruments. <br> Move the equipment to a location where the humidity is within the operating range (i.e., the <br> humidity is 5\% or higher). |

[Selection of the space heater]
As a simple condensation countermeasure, the relative humidity inside the cabinet can be lowered by increasing the temperature inside the cabinet $(\Delta \mathrm{T})$ with respect to the external temperature.
The temperature increase $(\Delta \mathrm{T})$ setting can be used to mitigate the humidity.
The following are rough guidelines.

- When $\Delta \mathrm{T}=5 \mathrm{~K}$, relative humidity decreases by $20 \%$
- When $\Delta T=10 \mathrm{~K}$, relative humidity decreases by $40 \%$


## Selection of space heater capacity (for cabinets without a ventilation outlet)

Specify $\Delta \mathrm{T}$ and determine heater capacity from the natural heat dissipation capacity of the cabinet and Figure 12.1-1.

- Example of heater capacity selection (calculation example) ${ }^{\text {(Note 1) }}$
(1) Cabinet external dimensions

Width (L) $\quad=800 \mathrm{~mm}$
Depth (D) $\quad=600 \mathrm{~mm}$
Height (H) $\quad=2300 \mathrm{~mm}$
Note 1 The channel base is not included.



Figure 12.1-1: Selection of space heater (1)
(2) Calculation of cabinet heat dissipation surface area

The heat dissipation area (bottom side area is subtracted from the total external area) of the cabinet is calculated below.

$$
\begin{aligned}
S & =[(L \times H) \times 2]+[(D \times H) \times 2]+[(L \times D) \times 1] \\
& =[(0.8 \times 2.3) \times 2]+[(0.6 \times 2.3) \times 2]+[(0.8 \times 0.6) \times 1]=6.92\left[\mathrm{~m}^{2}\right]
\end{aligned}
$$

(3) Selection of the space heater capacity

Space heater capacity can be selected based on the cabinet heat dissipation area (S) and the specified temperature increase value.

- $S=6.92\left[\mathrm{~m}^{2}\right]$
- Specified temperature increase value $\Delta T=5 \mathrm{~K}$

Reading from the graph in Figure 12.1-2, the space heater capacity should be 155 [W].
Given the above, a space heater with a similar capacity of 150 W or higher, is selected.
If instruments that are continuously powered exist (for example, power supply transformers), subtract the heat loss by the continuously powered instrument from the space heater capacity selected above to derive the final space heater capacity.

## Selection of space heater capacity for cabinets with a ventilation outlet

When the cabinet has a ventilation outlet, Figure 12.1-1: Selection of space heater (1) and Figure 12.1-2: Selection of space heater (2) can be used to calculate the heater capacity.

When the ventilation outlet area is $0.8 \%$ of the heat dissipation area, T (temperature increase with ventilation outlet/temperature increase without ventilation outlet) becomes $50 \%$ reading from Figure 12.1-2. Therefore, to increase the temperature inside the cabinet by $\Delta \mathrm{T}=5 \mathrm{~K}$,

$$
T=\frac{\Delta T_{\mathrm{H}}}{\Delta T_{\mathrm{L}}} \times 100[\%] \cdots \text { Equation 12.1-1 }
$$

From Equation 12.1-1, the following equation is derived:

$$
\Delta T_{L}=\frac{\Delta T_{\mathrm{H}}}{\Delta T_{\mathrm{L}}} \times 100[\%]=\frac{5 K}{50[\%]} 100[\%]=10 \mathrm{~K}
$$

When converted to the value for cabinets without a ventilation outlet, a space heater capable of increasing the temperature by $\Delta T=10 \mathrm{~K}$ should be selected.

Then, calculate the space heater capacity by following the steps for "Selection of space heater capacity (for



Figure 12.1-2: Selection of space heater (2) cabinets without a ventilation outlet)".
<Electrochemical migration behavior (ion migration behavior)>
When humidity is high, electrochemical migration behavior (also called ion migration behavior) can progress, causing short circuit between electronic instruments. Care should be taken to keep humidity within the inverter specifications to avoid condensation.
What is electrochemical migration behavior?
Electrochemical migration behavior begins when water molecules attach to the metal sections of electronic circuits such as semiconductors. The metal sections rise in temperature when current flows and metal ions start to dissolve into the water molecules. The dissolved metal ions become metal films while being attracted to adjacent metals, extending towards nearby conductors. In the end, metal (conductor) short circuit is created.

## <Relationship between humidity and corrosion>

The relationship between humidity and corrosion of steel materials is shown in Figure 12.1-3. When humidity increases as shown, the amount of corrosion increases.
Copper is commonly used for conductors, but copper erodes as well. Corrosion of the section contacting the conductor decreases the conductive area.
Plate the conductor protection to protect against corrosion.

## <Condensation>

The graph of Figure 12.1-4: Relationship between humidity and temperature difference summarizes the conditions causing condensation (humidity and temperature difference). As can be seen, large temperature difference can cause condensation at relatively low humidity level. Caution is necessary on the temperature difference between the inside of the cabinet and the surroundings.


Figure 12.1-3: Relationship between humidity and corrosion

( $\Delta \mathrm{T}$ : ambient temperature - temperature inside cabinet)

Figure 12.1-4: Relationship between humidity and temperature difference

### 12.1.3 Altitude

Insulation and cooling depend on air. Lower air pressure increases the possibility for insulation breakdown, reducing insulation durability. Thin air also reduces cooling effect, making the operating inverter rise in temperature more easily. For these reasons, reduce the voltage tolerance test value (not the rated voltage) and the rated current value (applicable motor capacity) by applying the factors shown in Table 12.1-1 when using at altitudes above 1000 meters.

Table 12.1-1: Reduction factor for the altitudes

| Altitude | Output current <br> (motor capacity) <br> reduction factor | Voltage tolerance <br> test reduction <br> factor |
| :--- | :---: | :---: |
| 1000 m or <br> lower | 1.00 | 1.00 |
| 1001 to <br> 1500 m | 0.97 | 0.95 |
| 1501 to <br> 2000 m | 0.95 | 0.90 |
| 2001 to <br> 2500 m | 0.91 | 0.85 |
| 2501 to <br> 3000 m | 0.88 | 0.80 |

### 12.1.4 Vibration

Vibration durability is expressed in terms of externally applied vibration amplitude and acceleration rate by operating frequency. When vibrations exceeding allowable limits are applied, instruments are exposed to mechanical stress, causing "loosening of the mechanical sections" or "breakage due to mechanical fatigue". For installations in high vibration locations, implement the following anti-vibration measures.

## (1) Anti-vibration measure

1) Attach anti-vibration rubber.

When protecting only the inverter from vibration, attach to the inverter fastening section. When protecting the entire cabinet, attach as shown in Figure 12.1-5.
2) Use a cabinet structure which does not transmit vibration. Use flexible structure and absorb the transmitted vibration.
3) Install at a location distant from the vibration source.

## (2) Overview of vibrational acceleration

Vibrational acceleration is not known commonly, and quantitative understanding is difficult. The following explains vibrational acceleration using the example of a simple harmonic oscillation (sine wave vibration).
Displacement changes over time for simple harmonic oscillation, as depicted in Figure 12.1-6. Equation 12.1-2 describes this displacement.
$x=a \bullet \sin \omega t \cdots$ Equation 12.1-2
$\chi$ : Displacement at arbitrary time [m]
$a$ : Amplitude on one side [m]
$\omega$ : Angular velocity [ $\mathrm{m} / \mathrm{s}$ ]
$t$ : Time [s]


Figure 12.1-5: Example of anti-vibration rubber application


Figure 12.1-6: Waveform of simple harmonic oscillation

Vibrational acceleration can be derived by differentiating Equation 12.1-2 twice.

$$
d x^{2} / d t^{2}=-\omega^{2} a \bullet \sin \omega t \cdots \text { Equation 12.1-3 }
$$

Substitute $\omega=2 \pi f$ into Equation 12.1-3.
(f: vibration frequency [Hz])

$$
\begin{aligned}
d x^{2} / d t^{2} & =-(2 \pi f)^{2} a \bullet \sin 2 \pi f t \\
& =\alpha\left[m / s^{2}\right]
\end{aligned}
$$

Maximum value of vibrational acceleration $\alpha$ is derived when $\sin 2 \pi \mathrm{ft}=-1$, so it can be calculated by the following equation (Equation 12.1-5):

$$
\alpha=(2 \pi f)^{2} \cdot a \cdots \quad \text { Equation 12.1-5 }
$$

Example: When a vibration of $10[\mathrm{~Hz}]$ vibrational frequency and $1.5[\mathrm{~mm}]$ amplitude on one side is applied to the inverter ( $\mathrm{a}=0.0015 \mathrm{~m}, \mathrm{f}=10$ Hz ),

$$
\alpha=\left(2 \times \pi \times 10_{\mathrm{Hz}}\right)^{2} \times 0.0015_{m}=5.9\left[\mathrm{~m} / \mathrm{s}^{2}\right]
$$

## <Reference>

To express the value relative to gravitational acceleration, divide by gravitational acceleration $\mathrm{G}=9.8 \mathrm{~m} / \mathrm{s}^{2}$

$$
\alpha=5.9 / 9.8=0.6 \mathrm{G}
$$

In other words, when a sine wave of 10 Hz vibrational frequency and 1.5 mm amplitude on one side is applied, the vibrational acceleration is $5.9 \mathrm{~m} / \mathrm{s}^{2}\{0.6 \mathrm{G}\}$.

### 12.1.5 Surrounding environment

The cabinet housing the inverter should be installed in places which suit the specified inverter specification environment, such as electric rooms.
However, there are occasions when it is unavoidable to install the inverter at locations not fitting the inverter specifications. The following explains typical measures to implement in such cases.

## Dust and oil mist

In environments with high level of dust and oil mist, these may stick to and accumulate inside the cabinet, causing contact failures, deterioration of insulation, and corrosion in electrical instruments. If the dust contains humidity, the cooling fins of the inverter may become clogged and cause degradation of cooling capacity and inverter overheat alarm.
Additionally, conductive and humid dust can cause failures in electrical instruments quickly, and oil mist considerably reduces the life of electronic components.

## Salt [seashore]

Sea-salt particles are scattered in the air on ships, coastal cranes, and factories on seashores. When these sea-salt particles accumulate, moisture absorption phenomenon of the sea-salt particles (occurrence increases when relative humidity exceeds $75 \%$ ) causes reduction in the surface resistance of insulators, increasing the occurrence of flashovers even at rated voltages. The particles also cause corrosion from the contacted areas when attached to metals. Fuji Electric inverters are designed assuming 0.01 [ $\left.\mathrm{mg} / \mathrm{cm}^{2}\right]$ per year of permeating salt volume. Measures must be implemented to contain salt volume within this limit when installing close to seashores.
Fuji Electric offers inverters and electric instruments (MCCB and contactors) with enhanced resistance to the effects of salt damage and humidity, in the product lineup. For details, contact your Fuji Electric representative.

## Corrosive gas (sulfuration gas)

Corrosive gas such as hydrogen sulfide gas and chlorine exist in the air in petroleum chemical factories, sewage plants, and hot spring areas.
Corrosive gas invokes erosion of metal, rust, and deterioration of insulation, causing failures in and markedly reducing the life of electric and electronic instruments.
As hydrogen sulfide gas is heavier than air and is gaseous, preventing cabinet entry is difficult with typical cabinet construction.
Fuji Electric offers inverters and electric instruments (MCCB and magnetic contactors) with enhanced resistance to the effects of sulfuration gas, in the product lineup. For details, contact your Fuji Electric representative.

## Flammable (combustive) gas, vapor, and powder dust

In flour mills where flammable gas and powder dust are produced, electrical instruments which use mechanical structures such as contactors and relays may cause sparks when contact points are opened and closed. Danger of explosion exists in these cases. All instruments for installation in locations with danger of explosion must be examined according to explosion-proof construction examination regulations for electric machinery and appliance. A certification organization specified by the government performs the tests for explosion-proof performance on the product submitted for examination and determines acceptability. For a product passing the examination, an acceptance number is issued.
When installing in locations with danger of explosion, electrical instruments which use mechanical structures such as inverters and relays must be tested for explosion-proof performance as a stand-alone unit. When instruments not certified on explosion-proof performance are used, the cabinet housing the electrical instruments must be examined for explosion-proof performance.

Creating cabinets with explosion-proof construction is difficult, and cabinets with typical construction cannot be used in dangerous locations. Therefore, install them in safe locations.
Additionally, when installing only the motor in dangerous locations, the inverter and the motor as a set must be examined for explosion-proof performance of the motor.
(Regardless of whether a new or existing motor is used, the motor must be combined with the inverter for the explosion-proof performance examination.)
Fuji Electric manufactures explosion-proof motors and submits them for examinations on requested orders. For details, contact your Fuji Electric representative.


Figure 12.1-7: Certification label

### 12.2 Construction

In the design and manufacturing of cabinets, protection levels, heat dissipation of the housed instruments, and the layout of the housed instruments affect the safety, dimensions, and construction of the cabinet. This section describes the protective construction of the cabinet, the cooling system of the instruments, and the layout of the instruments.

### 12.2.1 Protective construction

### 12.2.1.1 Protective construction by IP class

The cabinet protection level is compliant to "JEM1267 (2008) Protection Levels for Switchboards and Control Panels (2008)" of Japan Electrical Manufacturers' Association. Protective construction matching the installation location should be determined.
This standard includes the following two categories.
(1) Protection of instruments inside the cabinet against penetration by solid, external objects and protection of humans against nearing dangerous sections inside the cabinet
(2) Protection of instruments inside the cabinet against harmful effects by water penetration


Table 12.2-1: Protection levels for "Nearing dangerous sections" and "Solid, external objects" expressed by the first numerical parameter

| First symbol IP $\square \mathrm{x}$ (protection against foreign objects and dust) |  |  |  |
| :---: | :---: | :---: | :---: |
| Symbol | Protection from | Test method | Criteria |
| 0 | Unprotected | - | - |
| 1 | Solid, foreign objects larger than 50 mm |  | Does not pass through openings, and maintains appropriate clearance against live sections and moving sections |
| 2 | Solid, foreign objects larger than 12.5 mm |  | Maintains appropriate clearance against live sections and moving sections (withstanding voltage warranty) |
| 3 | Solid, foreign objects larger than 2.5 mm |  | Does not enter housing |
| 4 | Solid, foreign objects larger than 1.0 mm |  | Same as above |
| 5 | Dust-protected | Visual inspection <br> Visual inspection defined in terms of installation requirements ${ }^{\text {(Note 1) }}$ | Lack of dust accumulation which impedes normal operation |
| 6 | Dust-tight | Visual inspection <br> Visual inspection defined in terms of installation requirements ${ }^{\text {(Note 2) }}$ | Dust does not penetrate into the housing |

Remarks: $\quad X$ should be used when the degree of protection is not specified (ex. IP2X, IPX3)
Note 1) IP5X installation requirements
Construction has shielded external surfaces all around and is carefully designed for dust protection at small crevices on doors and ventilation openings. The construction may allow dust accumulation but not on insulators.

Note 2) IP6X installation requirements
Construction has shielded external surfaces all around and has packings attached on doors and bonding sections of the cabinet. Ventilation openings should be normally not created, but they can be constructed if adequate measures to prevent dust penetration, such as filters, are implemented.

Table 12.2-2: Protection level against water expressed by the second numerical parameter

| Second symbol IPx $\square$ (protection against water) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Symbol | Protection from | Test method |  | Criteria |
| 0 | Unprotected | - |  | - |
| 1 | Dripping water |  | - Precipitation: 3 to $5 \mathrm{~mm} / \mathrm{min}$ <br> - Time: 10 min <br> - Precipitation: 3 to $5 \mathrm{~mm} / \mathrm{min}$ <br> - Tilt sample by $15^{\circ}$, in 4 directions <br> - Time: 10 min |  |
| 2 | Water dripping with $15^{\circ}$ inclination |  |  |  |
| 3 | Water spray from vertical to $60^{\circ}$ |  | - Jet water: $10 \mathrm{~L} / \mathrm{min}$ <br> - Water pressure: 80 to 100 kPa <br> - Time: 5 min or longer <br> - With $30^{\circ}$ shield |  |
| 4 | Spray from all directions |  | Same as above (without shield) |  |
| 5 | Jet water from all directions | 3 m from nozzle to housing | - $D=6.3$ <br> - Jet water: $12.5 \mathrm{~L} / \mathrm{min}$ <br> - Water pressure: 30 kPa (Water spray 2.5 m ascent) <br> - Time: 3 min at minimum |  |
| 6 | Jet water from all directions |  | - $D=12.5$ <br> - Jet water: $100 \mathrm{~L} / \mathrm{min}$ <br> - Water pressure: 100 kPa (Water spray 8 m ascent) <br> - Time: 3 min at minimum |  |
| 7 | Immersion in water |  | - Time: 30 min |  |
| 8 | Submerged | As agreed on between manufacturer and user |  |  |

### 12.2.1.2 Protective construction by NEMA standard class

In some cases, protection levels are expressed in terms of NEMA standards along with IP class. This section describes the protection level by NEMA standards and approximate IP classes.

NEMA standards was defined by NEMA (National Electrical Manufacturers Association: USA), and the relevant container type is defined by NEMA250 (Enclosure for Electrical Equipment (1000 V Maximum).
The container type is commonly expressed as NEMA 4 or NEMA Type 4.

Major types of NEMA standards include explosion-proof and non-explosion-proof types as well as indoor and outdoor types which are classified by type numbers.

|  | Indoor | Indoor and outdoor |
| :--- | :--- | :--- |
| Non-explosion-proof | Type 1, 2, 5, 12, 12K, 13K | Type 3, 3R, 3S, 4, 4X, 6, 6P |
| Explosion-proof | Type 7, 8, 9, 10 |  |


| Type | Overview | Approximate IP code |
| :---: | :---: | :---: |
| 1 | Indoor use primarily to provide a degree of protection against contact with the enclosed equipment and against a limited amount of falling dirt. | IP30 |
| 2 | Indoor use to provide a degree of protection against limited amounts of falling water and dirt. (IP31) | IP31 |
| 3 | Outdoor use to provide a degree of protection against windblown dust, rain, and sleet; undamaged by the formation of ice on the enclosure | IP64 |
| 3R | Outdoor use to provide a degree of protection against falling rain and sleet: undamaged by the formation of ice o the enclosure. | IP32 |
| 3 S | Outdoor use to provide a degree of protection against windblown dust, rain and sleet; external mechanisms remain operable while ice laden. |  |
| 4 | Indoor or outdoor use to provide a degree of protection against splashing water, windblown dust and rain, hose directed water; undamaged by the formation of ice on the enclosure. | IP66 |
| 4X | Indoor or outdoor use to provide a degree of protection against splashing water, windblown dust and rain, hose directed water; undamaged by the formation of ice on the enclosure, resists corrosion. | IP66 |
| 5 |  |  |
| 6 | Indoor or outdoor use to provide a degree of protection against the entry of water during temporary submersion at a limited depth; undamaged by the formation of ice on the enclosure. |  |
| 6 P | Indoor and outdoor use to provide a degree of protection against the entry of water during prolonged submersion at a limited depth. |  |
| 11 | Indoor use to provide by oil immersion a degree of protection of the enclosed equipment against the corrosive effects of corrosive liquids and gases. |  |
| 12,12K | Indoor use to provide a degree of protection against dust, falling dirt and dripping noncorrosive liquids. (IP65) | IP65 |
| 13 | Indoor use to provide a degree of protection against dust and spraying of water, oil and noncorrosive coolants. (IP65) | IP65 |

Table 12.2-3: Target of protection for non-explosion-proof containers

| Target of protection | 1 | 2 | 3 | $3 R$ | $3 S$ | 4 | 4 X | 5 | 6 | 6 P | $12,12 \mathrm{~K}$ | 13 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Prevention of accidental contact with internal parts | O | O | O | O | O | O | O | O | O | O | O | O |
| Protection from falling dust | O | O | O | O | O | O | O | O | O | O | O | O |
| Protection from accumulation of floating dust in the circulating air flow |  |  |  |  |  |  |  | O |  |  |  |  |
| Protection from floating dust in the circulating air flow |  |  |  |  |  |  |  |  |  |  | O | O |
| Protection from blown dust |  |  | O |  | O | O | O |  |  |  |  |  |
| Protection from dripping and light spraying |  | O |  |  |  |  |  | O |  |  | O |  |
| Protection from spraying |  |  |  |  |  | O | O |  |  |  |  |  |
| Protection from spraying of water and non-corrosive lubricants |  |  |  |  |  |  |  |  |  |  |  | O |
| Protection from jet streams |  |  |  |  |  | O | O |  | O | O |  |  |
| Protection from rain, sleet, and snow |  |  | O | O | O | O | O |  |  |  |  |  |
| Protection from temporary immersion in water |  |  |  |  |  |  |  |  | O |  |  |  |
| Protection from intermittent immersion in water |  |  |  |  |  |  |  |  |  | O |  |  |
| Maintenance of function after exterior is frozen |  |  | O | O |  | O | O |  | O | O |  |  |
| Maintenance of function after exterior is frozen |  |  |  |  | O |  |  |  |  |  |  |  |
| Protection from corrosion |  |  |  |  |  |  | O |  |  |  |  |  |
| Reference IP codes (refer to text) | 10 | 11 | 54 | 14 | 54 | 56 | 56 | 52 | 67 | 67 | 52 | 54 |

### 12.3 Cabinet

The cabinet construction can be modified to adapt to individual installation environments. This section describes the modifications to the cabinet construction to adapt to installation environments.

### 12.3.1 Indoor cabinet

Generally, control cabinets which house electrical instruments such as inverters use cabinet constructions made of steel sheets. The steel sheets shield the components from penetration by foreign objects and for human safety. Since the electrical instruments each generate heat, ventilation openings should be created to cool the inside of the cabinets. On the ventilation openings, air filters should be attached to prevent dust penetration, other than in specially cleaned environments such as clean rooms.
Typical indoor cabinets must implement IP protective construction which does not allow penetration of a cylindrical rod with 12.5 mm diameter from ventilation openings or crevices in the casing. The IP code for this level of protection will be IP2X.
For water, the unprotected IPXO is common. However, construction that does not allow direct penetration to the interior by small amounts of sprayed water drops, or that does not allow wetting of the conductive parts and the insulators around the conductive parts in the case of indirect penetration, is required.

### 12.3.2 Outdoor cabinet

Cabinets installed outdoors are affected by direct sunlight, rain, wind, and snow, so the construction must be able to withstand all weather conditions, in principle.
Typically, protective construction is added to cabinet construction for indoors.
<Example of countermeasure: IP33W equivalent without direct sunlight>
(1) Attach the roof and create a construction which does not allow rain to seep in from the door, bonding surfaces, or the ventilation openings.
Attach gallery structure and air filter to the intake opening to prevent rain from wetting the air filter.
(When the air flow speed at the intake section is fast, ) rain and dust can easily be drawn in. The intake area should be made larger compared to installations in indoor electric rooms.


Figure 12.3-1: Outdoor cabinet example
(2) Attach wire screens to openings such as the ventilation opening to prevent intrusion by small animals.
(3) For the tools to attach to the door, use outdoor types. Otherwise, attach a window to the door and make the tools operable with direct view from the window.
(The desirable construction for the operating tools will shield the board even when the window is open.)
(4) On the bonding surfaces for the roof, door, and the cabinet, "attach packing and water drain", or use a "labyrinthine structure".

## Direct sunlight

From the heat of the direct sunlight, the cabinet surface temperature rises and may reach up to $70^{\circ} \mathrm{C}$ on the roof section at noon in the summer time. When the surface temperature rises, internal temperature also rises, and the tolerable upper level temperature of the housed instruments may be exceeded.
<Example of countermeasure>
(1) For the roof section where direct sunlight affects the most, use "Double layer roof construction" or "Construction with heat insulating material".
(2) Use light color for the cabinet surfaces to reduce heat absorption or use heat insulating paint.
(3) Increase the cabinet volume as much as possible. Use large ventilation (cooling) fans.
(4) Install at shaded locations where the effect of direct sunlight is small.

## Countermeasures for condensation

When the inside of the cabinet is subjected to sudden temperature changes as in the case of direct sunlight after rain or vice versa, condensation can result.
Condensations on the inside roof portion of the cabinet can cause water drops which cause damage on electrical instruments.

The following construction is recommended for installation in such environments.
<Example of (1) Implement high humidity and condensation countermeasures 1) and 2) described in "12.1.2 countermeasure> Humidity (condensation)".
(2) Change the roof section to double layer roof construction or construction with heat insulating material.
(3) Tilt the roof to avoid buildup of rain.

## Snow

For outdoor installations in snowfall areas, construction enhancements are necessary in order to prevent penetration of powder snow in addition to rain and to withstand the load of accumulated snow. Since powder snow can penetrate from small crevices, snow countermeasures for the cabinet with openings require a considerable amount of cost and labor.
Additionally, the condensation may result in the inside of the cabinet during early spring when the temperature changes suddenly.
Therefore, avoid outdoor cabinet installations in snowfall areas. Indoor installation is recommended.

## Wind pressure

The cabinet door can open and close due to effects of wind pressure when the cabinet is installed in strong wind areas and in high locations such as on seacoast cranes.
(The worker may suffer injury if the door closes due to wind pressure while conducting maintenance checkup.)
When installing the cabinet in strong wind pressure areas, attaching devices such as door stoppers and latches is recommended.


Figure 12.3-2: Example of cabinet internal temperature rise due to direct sunlight


Figure 12.3-3: Example of countermeasure to prevent door opening and closing due to wind pressure

### 12.3.3 Cabinet installation in indoor special environment

## Water drop proof cabinet

When installing the cabinet at indoor locations close to water and oil ducts, protection levels such as IP21 and IP22 are required.
In this case, water protection of the construction must prevent internal penetration by small volume of water drops at angles within $15^{\circ}$ from vertical.
(1) Add a simple lean-to on the top of a cabinet with protection level equivalent to indoor installation.
(2) Attach gallery to the intake opening.
(3) Create a construction that allows quick water discharge when cables and cable terminal surroundings become wet.

## Dust-protected, dust-tight, and water-proof cabinet

When installing the cabinet where mist is dispersed such as mineral stopes, tunnel digging sites, and cement factories, protection levels (dust-protected and water-proof levels) equivalent to IP51 and IP54 are required.
(1) Fabricate the contacting surface between the cabinet frame and the door in a water draining structure, and attach airtight packing with cushion on the contacting surface between the cabinet frame and the door.
(2) Fill in the gaps on the outside screws using caulking compound.
(3) Cool the inside of the cabinet using panel coolers and heat exchangers for cabinets which support IP51 and IP54.
(4) Apply plating to wires and conductors and use SUS type screws.
(5) Use polyurethane or epoxy type resin paint to paint the cabinet. (This reduces corrosion of the cabinet.)
(6) For moving parts of the cabinet, make adjustments such that the hook on the handle will not scratch off the paint. (Use SUS cover plate or resin caps.)

Dust-tight IP6X level can be implemented depending on the amount of dust. To comply with IP6X equivalent level, cabinet must be air purged, and the pressure inside the cabinet must be raised. When the amount of heat generated by the housed instruments is large, the modifications become extensive. For this reason, installation of the cabinet in environments requiring IP6X protection level is not recommended.

## Corrosion protection and corrosion resistant cabinets

Specialized cabinet construction is necessary to prevent corrosion of electrical instruments housed in the cabinet from corrosive gas such as sulfuration gas. (To increase the pressure inside the cabinet, treatments such as air purge are necessary.)
When installing, use electrical instruments treated for anti-corrosive gas and implement the measures for dust-protected, dust-tight, and waterproof cabinet in the previous section.

## Salt tolerant cabinets

When installing close to seashores, the following measures are effective. However, maintenance checkups and frequent cleaning may be necessary.
(1) Use salt tolerant filters for ventilated cabinets.

- Salt tolerant filters have very fine openings, resulting in very mild air flow velocity. Therefore, the intake area must be made large.
- Also, the salt tolerant filters cannot be recycled.
(2) Fabricate the contacting surface between the cabinet frame and the door in a water draining structure, and attach airtight packing with cushion on the contacting surface between the cabinet frame and the door.
(3) Cool the inside of the cabinet using panel coolers and heat exchangers for cabinets which support IP51 and IP54.
(4) Apply plating to wires and conductors and use SUS type screws.
(5) Use polyurethane or epoxy type resin paint to paint the cabinet. (This reduces corrosion of the cabinet.)
(6) For moving parts of the cabinet, make adjustments such that the hook on the handle will not scratch off the paint. (Use SUS cover plate or resin caps.)


### 12.4 Cooling

The inverter generates heat in the switching operation in the IGBT main circuit when driving the motor. Even when housed in cabinets, the inside temperature will not rise if all of the amount of heat generated can be dissipated. However, when the cabinets use constructions close to full enclosure, the internal temperature rises.
The inverters and the peripheral instruments housed in the cabinets have individual tolerances for ambient temperature. Cabinet heat dissipation and cooling are important because the performance and the life of the housed instruments degrade when these tolerances are exceeded.

### 12.4.1 Cooling method

Commonly used cooling methods are categorized and their characteristics are shown (in Tables 12.4-1 to 12.4-3).

## (1) Natural cooling

Cooling method using heat dissipation by natural convection current and cooling fans of housed instruments.
Table 12.4-1: Types and characteristics of cooling methods (1)

| Type | Natural ventilation |
| :---: | :--- |
| Overview | - Forced ventilation by the inverter cooling fan <br> - Construction which circulates natural air |
| Characteristics | Economical. <br> easily from cabinet top surface if exhaust air does not flow.) <br> considerably. (The calculation of the intake opening area is difficult.) <br> In cases where the cooling fan attached to the inverter is used for forced exhaust. Exhaust ducts <br> and hoods may need to be attached by occasion. |
|  |  |

## (2) Forced cooling

The cabinet is force-cooled using fans, panel coolers, and heat exchangers.
The cabinet will not grow larger even when the amount of heat generated inside is large. The methods are applicable from small to large capacity inverter boards.

Table 12.4-2: Types and characteristics of cooling methods (2)

| Type | Forced cooling by ventilation fan (exhaust method) |
| :---: | :--- |
| Overview | Cooling method using an exhaust fan attached to the roof of the cabinet |
| Characteristics | $\bullet$ An air filter that collects dust is necessary for the intake opening. |
|  | Phe number of parts for maintenance increases: <br> $\quad$ Periodic maintenance is necessary. |
|  |  |
| Application | Installation to typical indoor environment <br> Measures for outdoor installation are necessary for outdoor applications |

Table 12.4-3: Types and characteristics of cooling methods (3)

| Type | Forced cooling by ventilation fan (pressurized <br> air method) | Cooling by panel cooler/heat exchanger |
| :---: | :--- | :--- |
| Overview | Air purge cooling using fresh air (pressurized <br> fan) | Cooling method using panel coolers and heat <br> exchangers |
| Characteristics |  |  |
| Vaised by increasing the air flow volume of |  |  |
| the pressurizing fan. (Air purge) Suction of |  |  |
| dust and mist into the cabinet can be |  |  |
| prevented. |  |  |

### 12.4.2 Installation condition specification and selection of cooling system

The cabinet cooling method is selected considering the installation environment, operation load conditions (amount of heat generated), and others.

| Condition 1)Ambient <br> temperature: | $40^{\circ} \mathrm{C}$ (Typical indoor condition) JEM1460 specifies ambient temperature to be $40^{\circ} \mathrm{C}$ <br> for both indoor and outdoor. <br> If ambient temperature can be lowered depending on the installation environment, <br> this should be reflected in the selection conditions. |  |
| :--- | :--- | :--- |
| Condition 2)Allowable internal <br> temperature: | $50^{\circ} \mathrm{C}$ (Typical allowable temperature upper limit for instruments housed in cabinets) <br> Out of the housed instruments, the temperature of the instrument with the lowest <br> allowable temperature upper limit should be used as a reference. |  |
| Condition 3) | Total amount of <br> heat generated by <br> housed <br> instruments: | The amount of heat generated by the inverter varies with loading capacity, <br> operation cycle pattern (calculation of average load), and carrier frequency. |

## Amount of heat generated (heat loss) by internally housed instruments

Calculate the heat loss (amount of heat) incurred by the entire cabinet. Follow the steps below in calculating the amount of heat generated.
(1) Calculate the heat loss of the inverter and the other heat generating instruments individually and add.

The amount of heat generated by the inverter becomes larger with increasing capacity. If the loading capacity and the operation cycle pattern can be specified, these should be considered. The amount of heat generated also differs depending on the carrier frequency.
(2) The heat loss of wires and small parts (frequency setting device and fuses) is difficult to digitize. Based on historical data with safety factor, estimate 10 to $15 \%$ of the value calculated in (1).
(3) If the cabinet is heated by radiant heat from the surroundings and direct sunlight, convert the amount of heat received to loss [W].

Add the values found in (1), (2), and (3) to obtain the total heat loss of the cabinet.
The actual cooling is difficult to estimate using only theory because heat dissipation varies slightly depending on the cabinet construction and the placement of the instruments. Accumulated data and experience should be factored into specific designs.

### 12.4.3 Examples of cooling calculations by cooling system

### 12.4.3.1 Forced cooling by ventilation fan

A typical forced cooling by ventilation fan (exhaust method) will be used as an example for the illustration. In this cooling method, heat dissipation from ventilation fan is much larger than the heat dissipation from cabinet surfaces, so the heat dissipation from the cabinet surface using natural convection will be ignored. JEM-TR148 defines the equation for ventilation fan cooling. This equation will be used.

$$
q=\rho \times C \times Q(T o-T a) \quad \cdots \text { Equation 12.4-1 }
$$

$$
Q=\frac{q}{\rho \times C(T o-T a)}
$$

$q$ : Total amount of heat generated by the entire cabinet [kW]
$\cdots$ Equation 12.4-2 $\rho$ : Air density 1.057 (to 1.251 ) $\left[\mathrm{kg} / \mathrm{m}^{3}\right]$ (at 50 to $0^{\circ} \mathrm{C}$ )
C: Specific heat of air $1.0\left[\mathrm{~kJ} / \mathrm{kg} \cdot{ }^{\circ} \mathrm{C}\right]$
Q : Ventilation air volume [ $\mathrm{m}^{3} / \mathrm{s}$ ]
To : Air temperature at exhaust opening (cabinet internal temperature) [ $\left.{ }^{\circ} \mathrm{C}\right]$
Ta : Air temperature at intake opening (ambient temperature) $\left[{ }^{\circ} \mathrm{C}\right]$

## Calculation example

Substituting into Equation 12.4-2,

$$
\begin{aligned}
& Q=\frac{q}{\rho \times C(T o-T a)}=\frac{1080 \times 0.001}{1.057 \times 1.0(50-40)} \\
& \fallingdotseq 0.103\left[\mathrm{~m}^{3} / \mathrm{s}\right] \\
& Q=6.2\left[m^{3} / \mathrm{min}\right] \\
& \text { (Conditions) } \rho=1.057\left[\mathrm{~kg} / \mathrm{m}^{3}\right] \\
& \mathrm{C}=1.0\left[\mathrm{~kJ} / \mathrm{kg} \cdot{ }^{\circ} \mathrm{C}\right] \\
& \mathrm{Ts}=50\left[{ }^{\circ} \mathrm{C}\right] \\
& \mathrm{Ta}=40\left[^{\circ} \mathrm{C}\right]
\end{aligned}
$$

Hence, regardless of cabinet dimensions, using a fan with $6.2\left[\mathrm{~m}^{3} / \mathrm{min}\right]$ air flow will make cooling possible.
The results show that the cooling can be done if cooling fan and the intake area can cool the heat generated inside the cabinet.

The cooling construction using the inverter cooling fan, which is one method of natural cooling, can be calculated similarly using Equation 12.4-2 in this section.
With this method, however, exhaust from the inverter flows back into the cabinet if there is quite a distance between the exhaust opening and inverter cooling fan, and therefore an exhaust duct should be fitted to prevent back-flow.
And as heat dissipation results from natural convection, very little heat is dissipated. Consequently, application is only possible for inverter boards for which little heat is generated.


Figure 12.4-3: Forced cooling by ventilation fan (pressurized air method)

The case of pressurized air method can be calculated similarly using the equation in this section (Equation 12.4-2).
When air is pressurized by a cabinet mounted fan, air filters are typically attached before and after the fan. If the distance between the fan and the filters is short, the fan will not be able to produce the rated air flow.

Also, if the air filter comparable in size to the fan is used, the air flow speed through the filter increases, shortening the cleaning and replacement cycle of the filter.


Figure 12.4-1: Forced cooling by ventilation fan (exhaust method)


Figure 12.4-2: Natural ventilation (forced cooling with inverter cooling fan)

### 12.4.3.2 Cooling by heat exchanger

The cooling performance when heat exchangers are used can be calculated using technical information from heat exchanger manufacturers and "Board Heat Exchanger Technical Council Documents No. 003 Selection Method for Board Heat Exchanger Model".

The heat exchangers which can be attached to cabinets have size limitations, and the rated capacities are relatively small in most cases. (Heat dissipation capacity is low compared to forced cooling fans.) For this reason, the heat dissipation from cabinet surfaces is also included in the heat calculations.

Also, the cabinet internal temperature cannot be lowered to below the ambient temperature.

$$
R=\frac{q}{T s-T a}-h \times A \quad \cdots \quad \text { Equation 12.4-3 }
$$

q : Total amount of heat generated by the entire cabinet [W]
R : Rated cooling capacity of heat exchanger [W/ $\left.{ }^{\circ} \mathrm{C}\right]$
h : Thermal conductivity (heat loss coefficient) 5 to $6\left[\mathrm{~W} / \mathrm{m}^{2} \cdot{ }^{\circ} \mathrm{C}\right]$
A : Effective heat dissipation area of cabinet [ $\mathrm{m}^{2}$ ]
Ts : Cabinet internal temperature $\left[{ }^{\circ} \mathrm{C}\right]$
Ta : Ambient temperature [ $\left.{ }^{\circ} \mathrm{C}\right]$

## Calculation example

Substituting the values into Equation 12.4-3,

$$
\begin{aligned}
& R=\frac{q}{T s-T a}-h \times A \\
& =\frac{1080}{50-40}-5.4 \times 6=75.6\left[W /{ }^{\circ} \mathrm{C}\right]
\end{aligned}
$$



Figure 12.4-4: Cooling by heat exchanger

Hence, select a board heat exchanger with rated cooling capacity of $75.6\left[\mathrm{~W} /{ }^{\circ} \mathrm{C}\right]$ or higher from heat exchanger catalogues.

### 12.4.4 Cooling by panel cooler

The cooling capacity when panel coolers are used can be calculated using technical documents from panel cooler manufacturers.

The cooling capacity differs depending on ambient temperature and the configured temperature of the panel cooler.

$$
P=q+h \times A(T a-T s) \quad \cdots \quad \text { Equation 12.4-4 }
$$

Equation 12.4-4 shows that the cabinet surface area exposed to the ambient temperature affects the required cooling capacity of the cooler.
When the configured temperature of the panel cooler is set below ambient temperature, the cabinet surface is affected by radiant heat of the ambient temperature, adding radiant heat to the total amount of heat generated by housed instruments.
When ambient temperature is higher than the configured panel cooler temperature, cabinet surface radiates heat and this amount is subtracted (dissipated).

## Calculation example

Substituting the values into Equation 12.4-4,

$$
\begin{aligned}
& P=q+h \times A(T a-T s) \\
& =1080+5.4 \times 6(40-50)=756[\mathrm{~W}]
\end{aligned}
$$

Hence, select a panel cooler with cooling capacity of 756 [W] or higher when ambient temperature $=40^{\circ} \mathrm{C}$ and the configured panel cooler temperature $=50^{\circ} \mathrm{C}$, from panel cooler catalogues.

### 12.5 Selection of cooling fan

This section describes the selection and verification of cooling fans to be used on cabinets with forced cooling by ventilation fans.
For more details, refer Appendix 3.

## <Procedures>

(1) Calculate the total heat loss of the instruments housed in the cabinet.
(2) Determine the temperature rise value within the cabinet and calculate ventilation volume (air flow) Q [ $\mathrm{m}^{3} / \mathrm{s}$ ] according to "12.4.3 Forced cooling by ventilation fan".
(3) Estimate the pressure loss due to the air flow through the cabinet (air flow speed) using analogical reasoning on the air flow characteristics inside the cabinet and accumulated operation data. Deriving pressure loss from the equation is difficult, so actual data measurements will be necessary.
(4) Calculate the required ventilation volume (air flow) $\mathrm{Q}\left[\mathrm{m}^{3} / \mathrm{s}\right]$ using the fan characteristic curves (Q-Ps curve) listed in fan catalogues and technical documents and the estimated pressure loss from (3). Determine the fan to use.
The resistance curve is a diagram based on pressure loss. The fan is operated at the intersection of the fan characteristic curve and the resistance curve shown in Figure 12.5-1. The air flow of this intersection (operating point) becomes the ventilation volume of the cabinet.
(5) Attach the selected fan, and verify the temperature rise inside the cabinet at full load operation. Typically, internal temperature of the cabinet is $50^{\circ} \mathrm{C}$ when ambient temperature is $40^{\circ} \mathrm{C}$. In this case, the allowable temperature rise in the cabinet will be up to 10 K .
(6) If the temperature rise inside the cabinet exceeds 10 K , perform the following countermeasures.

1) Improve the air flow inside the cabinet and reduce pressure loss.
2) Replace with a larger fan.
3) If the temperature surrounding the inverter is high despite the low temperature at the exhaust opening, attach partitioning boards to increase the air flow around the inverter.


Figure 12.5-1: Fan operating characteristics


Figure 12.5-2: Case when ventilation volume is insufficient

### 12.5.1 Air filter size calculation

When drawing in external air using a fan, use a dust air filter on the intake opening, because dust may be suctioned from the intake opening. The recommended air filters are shown below.
<Recommended air filter information>
Manufacturer: Japan Vilene http://www.vilene.co.jp
Product name: Viledon ${ }^{\circledR}$ air filter regenerative type for general use Specifications:

| Item | Part No. | PS/150N | PS/300N | PS/400N | PS/600N |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Material | Polyester/modern acrylic |  |  |  |  |  |
| Std size <br> W x L | $[\mathrm{m}]$ | $1.6 \times 30$ |  | $1.6 \times 20$ |  |  |
| Thickness | $[\mathrm{mm}]$ | $8 \pm 3$ | $10 \pm 2$ | $14 \pm 2$ | $20 \pm 3$ |  |
| Typical air speed | $[\mathrm{m} / \mathrm{s}]$ | 2.5 |  |  |  |  |
| Init pressure loss | $[\mathrm{Pa}]$ | 30 | 54 | 64 | 90 |  |
| Avg collection <br> efficiency | $[\%]$ | 63 | 73 | 76 | 82 |  |
| Operating <br> temperature | $[\mathrm{mm}]$ | 8 |  |  |  |  |

The recommended part number is PS/400N.
Select part types, according to installation environment.


Table 12.5-1: Relationship between air flow speed and pressure loss

Calculate the air filter effective area and ventilation opening area using the following equation.

$$
A f=\frac{Q}{V f} \cdots \quad \text { Equation } 12.5-1
$$

In the specification of the air filter, the air flow speed through the air filter is $2.5 \mathrm{~m} / \mathrm{s}$. As time passes, dust begins to clog the path through the filter. Maintaining the same air flow volume increases air flow speed along with increase in pressure loss. When the maximum dust retention volume is exceeded, pressure loss exceeds the limit and the ventilation volume decreases.

Therefore, at Fuji Electric, air flow speed of $1 \pm 0.5[\mathrm{~m} / \mathrm{s}]$ is used to calculate the effective area of filters.
(Depending on the installation location, large exhaust volume from the exhaust opening may have the exhaust heat suctioned from the intake opening.)
Air filters should be replaced or cleaned and reused before the ventilation volume (air flow) lower limit is reached. Also, the cooling fan requires static pressure commensurate with the pressure loss of the air filter, so select the air filter considering this pressure loss.

## Calculation example

Substituting $\mathrm{Q}=0.103\left[\mathrm{~m}^{3} / \mathrm{s}\right]$ and $\mathrm{Vf}=0.75[\mathrm{~m} / \mathrm{s}]$ from Equation 12.5-1,

$$
A f=\frac{Q}{V f}=\frac{0.103}{0.75}=0.137\left[\mathrm{~m}^{2}\right] \quad \begin{aligned}
& \mathrm{Q}=0.103 \mathrm{~m}^{3} / \mathrm{s} \\
& \mathrm{Vf}=0.75 \mathrm{~m} / \mathrm{s}
\end{aligned}
$$

Hence, create an intake opening which will allow an effective air filter area of over 0.137 [ $\left.\mathrm{m}^{2}\right]$.
Additionally, a construction which positions the intake opening at the bottom of the cabinet and the exhaust opening on the roof as shown in Figure 12.5-3 is recommended.


Figure 12.5-3: Control cabinet with intake and exhaust openings

### 12.5.2 Principles in designing layout in cabinets

(1) Ascertain that instruments, parts, and materials which are vulnerable to heat are cooled.

The exhaust heat from the inverter cooling fan can reach up to $60^{\circ} \mathrm{C}$. The reactor also reaches high temperature.
Therefore, the electrical instruments should not be placed at locations where the exhaust heat from the inverter hits, at locations close to the reactor, and at locations on route of air flow carrying emitted heat from the reactor.
(2) Avoid local temperature increase.

The air flow inside the cabinet moves towards the direction where the area of the air flow path is larger. (Air flows in the route of least flow resistance.)
Positioning high heat generating instruments together will cause local build-up of heat.
For this reason, place the instruments in the cabinet such that the fresh air drawn in from the intake opening will flow towards the high heat generating instruments. Be creative to implement improvements such as attaching air stirring fans inside the cabinet and furnishing ventilation openings and ducts where hot air builds up.
(3) Avoid heat interaction between instruments.

Place instruments with high heat generation towards the top, and place instruments apart.
Inverters may intake and exhaust from the sides. For details, refer to the inverter technical documents or the users' manual and secure distance between instruments.
(4) Exercise caution against the surrounding environment.

In space confined installations, the exhaust heat from the cabinet (radiant heat from the cabinet surface) will increase room temperature. If heat generating objects (furnaces and machines which heat up) are close, the cabinet will be affected by the heat dissipated from the objects.
Reconsider room ventilation, cooling methods, and installation location.
Be careful that the cabinet will not draw in its own exhaust heat.
(5) Exercise caution to prevent dust from entering through crevices. (use of packing and sealing) Seal crevices using packings for doors and construction wiring clay for cable lead-in sections, even for cases of forced cooling using ventilation fans.

## Forced cooling by ventilation fan (exhaust method)

(1) Construct such that the parts requiring cooling are in the path of air flow. Air passes through sections with lower resistance. If the ventilation fan and the inverter are positioned as in Figure 12.5-4, most of the fresh air drawn in from the intake opening will pass directly to the exhaust opening without passing through the inverter. In these cases, install dampers or partitioning boards to guide air flow to the heated sections.
(2) For inverters with cooling fans, be careful of the air flow direction between the ventilation fans and the cabinet cooling fans. When the air flow directions oppose, air flow cancel each other out, reducing cooling air volume.
(3) When attaching multiple inverters or instruments with high heat generation, position side-by-side as in Figure 12.5-5.

If dimensional restrictions make vertical positioning of the instruments unavoidable, create a construction with partitioning boards to prevent heat effect. Without the partitioning boards, the exhaust heat from the lower inverter will be drawn into the upper inverter.


Figure 12.5-4: Example of damper attachment

(a) Side-by-side placement

Figure 12.5-5: Multiple inverters

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## Appendix 1 Guideline concerning safety of switchboards

## Appendix -1.1 Introduction

Product liability law (PL law enforced on July, 1995) is a short law consisting of six articles which contain the following two main points.
(1) When human life, body, or property is infringed due to "defects" of the manufactured product, then the damage must be compensated.
(2) "Defect" refers to the state where normally available safety is lacking for normally presumable usage, and product liability is an enactment of the new rule concerning responsibility for product defects.

The following three points are the most important responsibilities of manufacturers defined by PL law.
(1) Establishment of internal company structure
(2) Specific implementation items for product safety

Eliminating danger in design to fundamentally secure safety is the most important in securing product safety. Secondly, protective covers, safety devices, and safety mechanisms are implemented when safety cannot be secured in design or for technical reasons, or when the cost is not economically reasonable. Thirdly, warning labels are attached, but this should be done only as the last resort. Preferably, the warning labels should not be attached, and frequent use should be avoided.
(3) Education on product safety

This guideline describes the fundamental items to be respected (establishment of internal company structure, specific items to be implemented for product safety, and market support) by JSIA member companies in securing product safety.

## Appendix -1.2 Establishment of company internal structure

Every company must clarify their corporate philosophy concerning product safety. Company internal structure concerning product safety should be established, work should be allotted, and safety standards should be defined. "Product safety policy" must be defined stating that "product safety is the highest priority in corporate management." Effort must be made to inform all employees on safety while requiring conformance. Structure for product safety must be established in the company as a whole.

## Appendix -1.3 Specific implementation items for product safety

## Appendix -1.3.1 Considerations for safety when signing contracts

(1) Confirmation of contract conditions
(2) Related parties will discuss thoroughly on contract conditions such as product specification. Agreements should be made on product safety items, especially for instruments requiring periodic maintenance and instruments for which service life may cause issues.
(3) Confirmation of responsibility allotment

Agreements should be made on the method of solution and cost allotment, when a third party other than the contracting parties incurs damages arising from product defects.

## Appendix -1.3.2 Securing safety in planning, development, and design phases

Perform the following product safety measures during the planning, development, and design phases when much of the functions and performance related to product safety are determined.
(1) Forecasting dangers of the product During product design, effort should be made for research, development and improvement for enhancement of safety along with conformance to various safety standards. Also, perform the following to forecast dangers of the relevant product.

1) Forecast dangers of the product for various phases from distribution, use, to disposal. Also forecast dangers due to product deterioration, and consider effects to the environment.
2) During the initial design phase, consider the actual method of use by the customer and forecast dangers in use conditions (including unintended use of product and alterations).
(2) Comparison of product usefulness and danger

Compare the usefulness to society and the dangers which can arise from the relevant product, and determine the validity of productization.
(3) Specifying the technical level concerning safety

1) List related laws and standards, and conduct technical study to adapt to laws and public standards.
2) For the technical level for product safety, consider the safety level of similar products in similar price range or the possibility of alternate designs at reasonable price (for example, the dewatering bin in washing machines have possibility of injury if hands touch the dewatering bin while still turning; terminating the rotation upon opening of the washing machine lid is an alternate design which can be implemented within reasonable cost increase range) and avoid falling short of industry standards. Rather, attempt to secure levels surpassing the industry standards. Collect and research information concerning safety technologies for this purpose.
(4) Securing safety

Prioritize measures to secure safety through design and keep in mind that warning indications are last resorts. Depending on the level of possible damage, eliminate and reduce the danger, and provide warnings according to the following procedures.

1) When occurrence of danger in the relevant product can be predicted, secure fundamental safety by attempting to eliminate the cause through design.
2) When fundamental safety cannot be secured, implement protective covers, safety devices, and safety mechanisms to reduce danger, as necessary.
3) When occurrence of danger still remains, implement appropriate measures by attaching warning labels and providing warnings in user manuals.
4) Avoid using materials containing hazardous substances and dangerous substances. When these are used inevitably, research related laws and public standards, and implement appropriate measures to prevent danger and to protect the environment.

## Appendix -1.3.3 Securing safety in manufacturing and inspection phases

(1) Procurement

When purchasing raw materials or parts and when outsourcing all or part of the product, request the supplier to take necessary measures to secure product safety.
(2) Manufacturing

Provide and maintain control standards, work orders, manufacturing facilities, jigs, and tools for securing the required safety level in manufacturing phase. In addition, implement necessary measures such as clarifying the process management method, to ensure that safety is not lost as a result of causes in manufacturing phase.
(3) Inspection

Specify inspection standards, determine inspection methods, and maintain inspection technology and inspection instruments considering the actual use of the product.

## Appendix -1.3.4 Securing safety in storage, wrapping and packaging, transport, assembly, installation, and adjustment phases

(1) Storage, wrapping and packaging, and transport Implement necessary prevention measures in storage, wrapping and packaging as well as transport phases to avoid loss of safety functions of the product and occurrence of damage to the operator and surroundings due to damaged product.
(2) Assembly, installation, and adjustment

Implement necessary prevention measures at assembly, installation, and adjustment phases to avoid loss of safety functions of the product and occurrence of damage to the operator and surroundings while considering the use conditions and the environment conditions surrounding the relevant product.

## Appendix -1.3.5 Securing safety in maintenance, checkup, and repair phases

Provide necessary work standards or work manuals to prevent damage to the operator and surroundings and loss of product safety functions while maintenance, checkups, and repairs are conducted. Items for periodic checkup should be clearly stated in the work manual on the frequency and range.

## Appendix -1.3.6 Securing safety in used products and in the disposal phase

When selling used products, implement product safety measures according to the product liability law for new products. Implement necessary and appropriate measures to secure safety related to product disposal such as disposal method, disposal procedures, and avoidance of generation of hazardous substances at product disposal phase.

## Appendix -1.4 Market support

When a deficiency is found in the product after shipping or delivery, inform the customer on methods to circumvent danger. At the same time, implement appropriate measures such as repair, adjustment, and collection of the relevant product including the stock.

## Appendix -1.5 Accident cause analysis and measures to prevent recurrence

In the event that an accident is caused by the product, implement necessary measures to identify the cause, to prevent expansion of damage, and to prevent recurrence of similar accidents.

## Appendix -1.6 Information management

Accumulate information and technologies related to product safety, and implement appropriate measures to check and store necessary information and discard it when no longer necessary. For the storage period, create storage standards according to the importance of the information and the ten year responsibility period specified in the product liability law, and store accordingly.

## Appendix -1.7 Education on product safety

In order to fully inform and to require conformance by various sections on product safety concept, conduct company internal education on the importance of product safety measures and the implementation methods. Also conduct awareness campaigns as necessary.

## Appendix -1.8 Closing remarks

The product liability law is expected to be effective in changing mindsets of product manufacturers and consumers on product safety and in relieving the burden of proof for the aggrieved party, among others. However, electrical facilities such as switchboards are manufactured based on laws and technical standards. As care has been exercised historically for safety, there is no universal way to identify what are "defects" and where they lie. Therefore, the only way to improve safety is for individual companies to enhance the safety of products on their own. As precedents are accumulated, the relationship between product liability law and switchboards should become clearer.
Japan Electrical Manufacturers' Association will establish a new product liability committee to propose a fundamental policy concerning product liability measures, to implement and to disseminate specific measures, to collect information, and to research on product liability insurances.
(End of appendix)

Reference document: "Guidelines concerning product safety of heavy electrical machinery" issued by Japan Electrical Manufacturers' Association

## Appendix 2 Excerpt from switchboard and control board standards by Japan Electrical Manufacturers' Association

This appendix describes Japan Electrical Manufacturers' Association standard (JEM standard) related to cabinets housing inverters.

# Appendix -2.1 Rating and testing for switchboards and control boards (excerpt) 1460: 2008 

Japan Electrical Manufacturers' Association standard JEM<br>Rating and testing for switchboards and control boards (excerpt) 1460: 2008<br>Rating and testing for low voltage switchgear and control gear assemblies (boards)

## 4. Use conditions

Unless otherwise specified, the cabinet will be used in the standard use condition defined in 4.1 along with the major circuit and control circuit constituting the cabinet.
When the actual use condition differs from the standard use condition, the main circuit instruments and the control circuit instruments used for cabinet must be designed for the special use condition required by the user or appropriate measures must be implemented.

### 4.1 Standard use condition

The standard use condition for the cabinet is specified by either one of the following.

### 4.1.1 Indoor

a) Ambient temperature range is between $-5^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ and the average temperature measured for 24 hours is below $35^{\circ} \mathrm{C}$.
b) Altitude is below 1000 meters.
c) Relative humidity range is between 45 to $85 \%$. No dew condensation is allowed.

### 4.1.2 Outdoor

a) Ambient temperature range is between $-25^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ and the average temperature measured for 24 hours is below $35^{\circ} \mathrm{C}$.
b) Altitude is below 1000 meters.
c) Relative humidity outside the cabinet is not defined. However, the condensation inside the cabinet must be at a level which does not affect the internal instruments.
d) Wind pressure is below 1000 Pa (equivalent to wind speed $40 \mathrm{~m} / \mathrm{s}$ ).

### 4.2 Special use condition

Special use condition is specified by any of the following. When using in this condition, the user will specify the conditions to the manufacturer and the countermeasures will be determined through discussion between the user and the manufacturer. Additionally, if the temperature and humidity differ from 4.1 during transportation, storage, and installation, countermeasures will be determined through discussion between the user and the manufacturer.
a) Ambient temperature, humidity, and altitude exceed the definitions in 4.1.
b) Temperature or air pressure changes rapidly.
c) Excessive vapor, oil mist, smoke, dust, salt, and corrosive substance is in the air.
d) Explosive, flammable, and other hazardous gas is in the air.
e) Cabinet is exposed to excessive snow fall, fog, or wind pressure.
f) Cabinet is exposed to strong electrical or magnetic fields.
g) Cabinet is exposed to abnormal vibration or impact.
h) Cabinet is mounted on vehicles for transportation during operation.

# Appendix -2.2 Construction and dimensions of switchboards and control boards (excerpt) 1459: 2005 

Japan Electrical Manufacturers' Association standard JEM

Construction and dimensions of switchboards and control boards (excerpt) 1459: 1998
General requirements for construction and external dimensions of switchgear and control gear assemblies (Control)

## 4. Cabinet construction

4.1 Typical construction For the typical construction, the following requirements apply:
a) The casing shall be made of robust metal with construction capable of withstanding the weight of the housed instruments and the impact in operation.
b) The casing shall be treated to prevent rust and be painted with durable paint.
c) If the temperature of the housed instruments exceeds allowable temperature due to temperature increase in the cabinet, appropriate ventilation opening or ventilation device shall be installed.
d) For cabinets installed outdoors or in comparable locations, heaters or other condensation prevention devices shall be installed if possibility of failure exists due to internal condensation.
e) Construction other than a) to d) shall adequately meet the protection levels defined in 4.3.

### 4.2 Construction of individual parts

4.2.1 Door For the door construction, the following requirements apply:
a) Construction
b) Hinge
c) Stopper
d) Monitoring window

Use a construction which resists deformation and non-alignment, supported by hinges and with doors machined to "L" or "[" shape. For outdoor cabinets, door handles and hinges shall use material resisting or treated for corrosion.

Door hinge shall be made of metal. Install stopper to hold the open position on doors for self-standing, outdoor cabinets. Use glass or durable, transparent material when installing monitoring windows.

### 4.2.2 Detachable cover

The detachable cover shall have construction and weight for easy detachment. The cover shall be such that it can be attached to avoid falling due to vibrations. Addition of handles for attachment and detachment is desirable, if necessary.

### 4.2.3 Ceiling board

When installing ceiling boards, consider the need of a ventilation and/or cable outlet opening, and the protection level.

### 4.2.4 Roof

The roof shall be inclined or otherwise designed to resist buildup of rain and snow on the top. Also, add a lean-to or the like to resist penetration of rain and snow into the casing.

### 4.2.5 Floor board

When installing a floor board, consider the safety of the access to the inside of the cabinet, dropping of objects into the cable outlet opening, and prevention of intrusion by small animals into the cabinet.

### 4.2.6 Base

When installing a base, consider the floor thickness of the installation location, cabinet construction, and the relationship to adjacent cabinets. Use base construction and material which eases installation of the casing.

### 4.2.7 Posts

Posts shall possess enough rigidity to support the casing. Also, consider making the inside of the posts available for wires and cables.

### 4.2.8 Ventilation opening cover

When installing ventilation opening covers, consider the classification of the protection level and ventilation efficiency.

### 4.3 Protection level

Follow JEM1267 for names and inspection methods for the protection levels.

# Appendix -2.3 Grounding of switchboards and control boards (excerpt) 1323: 2005 

Japan Electrical Manufacturers' Association standard JEM

Grounding of switchboards and control boards (excerpt) 1323: 2005
Earthing for low-voltage switchgear and control gear assemblies (boards)

## 1. Scope of application

This standard defines the grounding for switchboards using electrical circuit with alternating current below 600 V or direct current below 750 V and control boards (hereafter called boards) electrical circuit with alternating current below 1000 V or direct current below 1200 V . However, the definition does not apply to the grounding of the main circuit.

## 4. Types of cabinet grounding

### 4.1 Grounding of the main board

a) Inside the board, grounding terminals or grounding buses which are connected to the main board electrically by welding or tightening metal screws in order to ground the board. The grounding terminals or the grounding buses are grounded through the grounding wire.
b) For door casings with attaching instruments, connection by wire to the cabinet main body is desirable. However, electrically equivalent connections (use of metal hinges treated to prevent corrosion, use of toothed washers, or use of metal screws to tighten metal supporting surfaces) can also be used for grounding.
c) For door casings without attaching instruments, secure conduction using metal screws and metal hinges.

### 4.2 Grounding of the casing of instruments attached to cabinets and instrument mounting brackets

When grounding is necessary for safety and performance guarantee reasons, connect the casing of attached instruments to the grounding terminal or grounding bus using the cabinet internal grounding wire. For casings of general instruments attached to the cabinet and instrument mounting brackets, metal screw tightening method may be used to connect to the cabinet body electrically. However, for attaching brackets to moving instruments, connection with the cabinet body through electrical wire is desirable, but electrically equivalent connections (use of metal hinges with corrosion protection) may also be used.

### 4.3 Grounding of circuit

For measurement and control circuits requiring grounding, connect to the grounding terminal or grounding bus using cabinet internal grounding wire.

## 5. Construction of the ground terminal

The grounding terminal shall use crimped terminal tightening type construction or electrical wire tightening type construction which can be connected by cabinet internal grounding wire and grounding wire.

## 6. Construction of the ground bus

The grounding bus shall be $25 \mathrm{~mm} \times 3 \mathrm{~mm}$ or greater if made of copper and shall use crimped terminal tightening type construction or electrical wire tightening type construction which can be connected by cabinet internal grounding wire and grounding wire.
Remark: If the grounding bus is not made of copper, equivalent heat and mechanical requirements shall be met.

## 7. Thickness of cabinet internal ground

The thickness of cabinet internal grounding wire shall meet the requirements shown in Table 2.3-1.
Table 2.3-1: Thickness of cabinet internal grounding wire

| Applicable circuit |  | Thickness of cabinet <br> internal grounding wire ${ }^{(1)}$ <br> $\left[\mathrm{mm}^{2}\right]$ | Remarks (Types of <br> grounding construction) |
| :--- | :--- | :---: | :---: |
| Casing of <br> attached <br> instruments | 300 VAC or less, 300 VDC or less | 2 or greater | Class D grounding work |
|  | More than 300 VAC and 600 VAC or less <br> More than 300 VDC and 750 VDC or less | 2 or greater | Class C grounding work |
|  | More than 600 VAC, more than 750 VDC | 5.5 or greater | Class A grounding work |
| Secondary and tertiary circuits of transformers for special <br> high voltage instruments | 5.5 or greater | Class A grounding work |  |
| Secondary and tertiary circuits of transformers for high <br> voltage instruments | 2 or greater | Class D grounding work |  |

Note (1) The thicknesses for cabinet internal grounding wire in this table show the minimum values for copper lines.

JEM 1323:2005
Grounding of switchboards and control boards (excerpt)

## 2. Contents of individual constituting elements

### 2.3 Grounding of cabinet body (4.1 of main body)

a) To ground the cabinet body, it is desirable to create grounding terminals in cabinets with few cabinet internal grounding wires and create grounding bus in cabinets with many cabinet internal grounding wires or cabinets placed side by side. However, if grounding terminals are created on each board and the grounding wire connects the grounding terminals, grounding buses are not required. Figure 2 shows examples of cabinet body grounding.


Figure 2: Example of cabinet body grounding
b) For metal casings such as cabinet doors allowing instrument attachment, connecting the cabinet body (or the grounding terminal and grounding bus installed on the cabinet body) and the door casing by electrical wire is desirable. It is deemed that grounding between the cabinet body and the brackets can be secured through electrically equivalent connections which allow conduction (for example, metal hinges with corrosion protection, toothed washers, use of sliding contacts, tightening by metal screw on metal support surface) [refer to JIS C 8480 7.4.3.1.5 b) and c)]. When using insulating hinges, however, the cabinet body and the casing must be connected by electrical wire. Figure 3 shows examples of door casing grounding of the cabinet with attached instrument.


Figure 3: Example of casing grounding for cabinet with attached instruments
c) For casings such as cabinet doors, side panels, and roof panels not requiring instrument attachment, metal screw and metal hinge connections are considered adequate for securing conduction [refer to JIS C 8480 7.4.3.1.5 c)]. Electrical wire connections are also unnecessary when attaching instruments built with circuits not requiring countermeasures for electric shock and using voltages within the limit of very low voltage [refer to JIS C 8480 7.4.3.1.5 C) and IEC60439-1]. Figure 4 shows examples for casings of cabinets with instruments not requiring countermeasures for electric shock and casings of boards without attaching instruments.

a) Example of no instrument attached to door casing
b) Example of attaching only instruments not requiring countermeasures for electric shock to door casing

Figure 4: Example of case grounding for door casing without attached instruments and for door casing attaching only instruments not requiring countermeasures for electric shock
d) Cabinet bodies made of insulator are rare these days, but grounding through grounding terminals or grounding buses will be adequate also for these cases.

### 2.4 Grounding of the casing of instruments attached to cabinets and instrument mounting brackets (main body 4.2)

When the casings of instruments attached to cabinets and the mounting brackets have metal surfaces, and when the pressure exerted on the surface is adequately high, the surface is deemed to adequately secure conduction for the protective circuit. Therefore, metal casings of typical cabinet attached instruments can be considered to be electrically connected to the cabinet body by metal screw connections, making grounding by dedicated wires unnecessary. To guarantee good conductivity, however, caution should be exercised on the following points.
a) When ground connection attachment sections (such as frame grounding terminals) are available on the casings of cabinet attached instruments requiring grounding for safety and for performance guarantee, connect the ground connection sections on instrument casings to the grounding terminal or the grounding bus of the cabinet using cabinet internal grounding wire. Figure 5 a) shows an example.
b) When ground connection attachment sections (such as frame grounding terminals) are not available on the casings of cabinet attached instruments, and when the casings of cabinet attached instruments are equipped with metal support surfaces, the connection made by the metal screws can be considered to provide adequate electrical connection to the cabinet, making grounding by dedicated wires unnecessary. Figure 5 b ) shows an example.
c) When the casings of cabinet attached instruments are not connected with the cabinet grounding terminals or grounding buses using cabinet internal grounding wire but instead are connected to the instrument mounting brackets, and when the mounting brackets are not equipped with metal support surfaces, connect the mounting brackets and the cabinet grounding terminals or the grounding buses by cabinet internal grounding wire. Figure 5 c ) shows an example.
d) When the casings of cabinet attached instruments are not connected to the cabinet grounding terminals or grounding buses using cabinet internal grounding wire but instead are connected to the instrument mounting brackets, and when the mounting brackets are equipped with metal support surfaces, the connection made by the metal screws can be considered to provide adequate electrical connection to the cabinet body, making grounding by dedicated wires unnecessary. Figure 5 d ) shows an example.
e) When the casings of cabinet attached instruments are not connected to the cabinet grounding terminals or grounding buses using cabinet internal grounding wire but instead are connected to the moving instrument mounting brackets, and when conduction cannot be secured due to hinges using isolation, connect the moving mounting brackets and the cabinet grounding terminals or the grounding buses by cabinet internal grounding wire. Figure 5 e) shows an example.
f) When the casings of cabinet attached instruments are not connected to the cabinet grounding terminals or grounding buses using cabinet internal ground wire but instead are connected to the moving instrument mounting brackets, and when conduction can be secured through metal hinges, grounding by dedicated wires is unnecessary. Figure 5 f) shows an example.

a) Example of Connecting Instrument Casing by Ground Wire
b) Example of Connection by Tightening Metal Screws on Instrument Casing

c) Example of Connection by Ground Line to Instrument Mounting Bracket
d) Example of Connection by Tightening Metal Screws on Instrument Mounting Bracket

f) Example of Connection Using Metal Screws on Moving Mounting Brackets of Instrument

Figure 5: Example of grounding instruments and instrument mounting brackets

### 2.5 Construction of ground terminal (main body 5)

The crimped terminal tightening type construction cited in the main body uses electrical wires with crimped terminals attached on terminations. The crimped terminals are fastened by metal screws onto the switchboard. A representative example of this construction is defined in JIS C 2811 as "screw terminal block" and "stud terminal block", and is shown with a sample figure. The wire tightening method fastens wire terminations by using clamping blocks on the switchboard or by fastening with the metal screw tips. A representative example of this construction is defined in JIS. C. 2811 as "clamp terminal block" and "press-clamping terminal block", and is shown with a sample figure.
For sharing by grounding types or grounding using combined grounding terminals, refer to indoor wiring regulations 1350. Figure 6 shows examples of ground terminals.


Figure 6: Examples of ground terminals

### 2.6 Construction of grounding bus (main body 6)

When cabinets are placed side by side and when a grounding bus is to be created, implement a grounding bus for the group. For the grounding bus size, follow the definitions in JEM 1265.

### 2.7 Thickness of cabinet internal grounding wire (main body 7)

The thickness of grounding wires have been defined to match various ground construction details in Articles 10 and 11 in Guidebook of Electrical Equipment and Articles 19, 20, 27, and 29 in Interpretation of Guidebook of Electrical Equipment. To make cabinet internal ground wire effective, considerations are needed not only for the inside of the cabinet but also for ground construction outside the cabinet. The basics on ground construction have been listed in the remarks column of Table 1 in the main body.
Table 1 of the main body shows only thickness of grounding wires in terms of cross-section area ( $\mathrm{mm}^{2}$ ) only. Equivalent diameters ( $\varphi \mathrm{mm}$ ) are shown in indoor wiring regulations 1350-3, Table 2 and Table 3. This standard also considers these values effectively equivalent, and the values should be used in implementation. Table 1 in the main body shows the minimum values of grounding wire thicknesses in the case of copper wire. Table 2 and Table $\mathbf{3}$ show excerpts of selection criteria for thickness, according to indoor wiring regulations.

Table 2: Thickness of ground wires for C type and D type constructions (excerpt from Internal line regulations 1350-3)

| Smallest rated current capacity of overcurrent breaker installed on the power supply side of the low voltage path in the metal outer casing for instruments to be grounded | Typical cases |  |  | When using cords or cabtyre cables for sections requiring flexibility in grounding machines which are moved for use |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Aluminum | Thickness of single-core | Thickness of one core when using 2 cores for grounding |
| Below 20 A | $ø 1.6 \mathrm{~mm}$ or more | $2 \mathrm{~mm}^{2}$ or more | $ø 2.6$ mm or more | $1.25 \mathrm{~mm}^{2}$ or more | $0.75 \mathrm{~mm}^{2}$ or more |
| Below 30 A | $\varnothing 1.6 \mathrm{~mm}$ or more | $2 \mathrm{~mm}^{2}$ or more | $\emptyset 2.6 \mathrm{~mm}$ or more | $2 \mathrm{~mm}^{2}$ or more | $1.25 \mathrm{~mm}^{2}$ or more |
| Below 50 A | $\emptyset 2.0$ mm or more | $3.5 \mathrm{~mm}^{2}$ or more | $ø 2.6 \mathrm{~mm}$ or more | $3.5 \mathrm{~mm}^{2}$ or more | $2 \mathrm{~mm}^{2}$ or more |
| Below 100 A | $ø 2.6$ mm or more | $5.5 \mathrm{~mm}^{2}$ or more | $ø 3.2 \mathrm{~mm}$ or more | $5.5 \mathrm{~mm}^{2}$ or more | $3.5 \mathrm{~mm}^{2}$ or more |

Table 3: Thickness of ground wires for A type constructions (excerpt from Internal line regulations 1350-4)

| Ground line section of A type grounding construction | Copper | Aluminum |  |
| :--- | :--- | :--- | :--- |
| For grounding electric machines used while fixed in <br> location and grounding electric machines used while <br> moving and without requirement for flexibility | $\varnothing 2.6 \mathrm{~mm}$ or more | $5.5 \mathrm{~mm}^{2}$ or more | ø3.2 mm or more |

## Appendix 3 Characteristics of fan

Understanding the fan characteristics and the route of air is necessary to use the fan. This appendix describes the main points of the characteristics.

## Appendix -3.1 Relationship between air volume and air pressure (static)

"Fan characteristic curve" shows the relationship between air volume and air pressure, which is an important characteristic in the fan specification.
This characteristic curve is described in catalogs and technical documentations provided by the fan manufacturer.
(Hereafter, air pressure will be referred to as static pressure, and the fan characteristic curve will be referred to as the P-Q curve Figure 3.1-1.)

When air passes through the cabinet, pressure loss occurs. The loss is affected by the area, length, and turns of the air path and the congested state of the internal structural parts which result as resistance. The relationship between the pressure loss and air volume expressed as an equation is as follows.
Figure 3.1-2 shows the "Resistance curve" which plots this equation.

$$
P=K Q^{n} \cdots \quad \text { Equation 3-1 }
$$

P: Pressure loss in $[\mathrm{Pa}]$ or $\{\mathrm{mm} \cdot \mathrm{Ag}\}$
K: Constant
Q: Air volume [ $\mathrm{m}^{3} / \mathrm{min}$ ]
n : Constant determined by air volume (use 2 for cabinets)
(Note) Constant K changes depending on the state of the air path, and calculating the value from theoretical formulas is difficult. Estimation from real measurements is the only good way. This is true not only for cabinets but also for other machines and equipment. Using the fan requires accumulation of measurement data, and this accumulated data becomes the know-how of manufacturers.

The relationship between the P-Q curve of the fan and the resistance curve of the air path is as follows.
When the fan rotates, air flows through the air path and pressure loss results.
To create air flow, the air must be pushed with a pressure matching the pressure loss which will occur. This pressure is called the static pressure (Ps).
Therefore, the fan, as shown in Figure 3.1-3, operates at the intersection of the P -Q curve and the resistance curve. This crossing point (point a) is called the operating point, and the fan cannot be operated at any other point. To operate at a combination of air flow volume and static pressure other than at point a, only the following two methods exist.

Figure 3.1-2: Air path resistance curve


Figure 3.1-3: Operating point

1) Change the property of the resistance curve. (change the flow of air)
2) Change the fan rotation speed, or replace with another fan with different specification and change the P-Q curve (fan characteristics).

Figure 3.1-4 shows case 1 ) and point $b$ is the operating point.
$b^{\prime}$ increases resistance characteristics and b" decreases resistance characteristics.
To realize b' characteristic curve, "decrease the area of the air path" or "increase the resistance of the air path by using dampers, etc".
To realize b", "increase the area of air path" or "eliminate the objects which impede air flow".

Figure 3.1-5 shows case 2). To realize the characteristic curve of c', "reduce the rotation speed", or "replace with a smaller fan" etc.
To realize c", "increase the rotation speed", or "replace with a larger fan" etc.
Next, the explanation of a countermeasure to problems in installation to real facilities follows.
Select the fan, considering the required air flow in the cabinet and the pressure loss. Attach to the cabinet and test run.
Sometimes, the temperature inside the cabinet rises beyond expectation, and the characteristic shifts from the calculated curve.
In order to cool according to the calculations, it is recommended to use actual operating data (resistance curves) fully to select the fan.


Figure 3.1-4: Changing resistance characteristics


Figure 3.1-5: Changing fan characteristics


Figure 3.1-6: Insufficient air volume

The following items summarize the main points.

## [Main points]

- The fan has the P-Q characteristics and the air flow route has resistance characteristics. Both characteristics exist independently.
- Without changing the air flow route, the resistance characteristics will not change even if the fan may be replaced.
- The fan cannot be operated other than at the operating point. Operating point refers to the intersection of the $\mathrm{P}-\mathrm{Q}$ curve and the resistance curve.
- When air flow volume is insufficient, check to see if the resistance characteristics of the air flow route differ from the estimation at design.


## Appendix -3.2 Serial and parallel operation of the fan

When one fan does not produce enough air flow, multiple fans should be used. However, $1+1$ does not necessarily mean twice the volume, so care is necessary in the design. The following shows characteristics when two fans are used in parallel or series.

## (1) Combined fan characteristics of parallel operation

Figure 3.2-1 shows the characteristic curve when two fans with different P-Q curves are operated in parallel.
Keeping the static pressure constant, seek the air flow value Q1 and Q2 for each fan on the individual P-Q curves. The combination of the two values (Q1+Q2) is the combined fan characteristic point. Combining the P-Q curves for FAN1 and FAN2 will result in the combined fan P-Q curve.

When using fans with different characteristics together, and if Ps1 < Ps2 (when the air flow of FAN1 = zero (static pressure of fan at cutoff)), then FAN1 will exhibit "reverse flow characteristics" in this range.
The reverse flow characteristic curves of fans are not described normally in catalogs, so contact the fan manufacturer.

As can be seen from the above, even if ventilation is designed to extremely reduce intake volume and exhaust high volume, adequate ventilation will not occur.

## (2) Combined fan characteristics of serial operation

Figure 3.2-2 shows the characteristic curve when two fans with different P-Q curves are operated in series. For serial operation, if no crevices exist in the cabinet other than at the fans, then FAN1 and FAN2 will have the same air flow volume. Keeping air flow volume constant, seek the static pressure value Ps1 and Ps2 for each fan on the individual P-Q curves. The combination of the two values (Ps1 + Ps2) is the combined fan characteristic point. Combining the $P-Q$ curves for FAN1 and FAN2 will result in the combined fan $P-Q$ curve.

When using fans with different characteristics together, and if Q1 < Q2 (static pressure of FAN1 = zero (fan blowing)), then FAN1 will exhibit "turbine characteristics" in this range.
The reverse flow characteristic curves of fans are not described normally in catalogs, so contact the fan manufacturer.

As can be seen from the above, a cabinet design with extremely low static pressure (very low fan air flow volume due to the relationship between the fan air flow volume and cabinet capacity) will not ventilate adequately.


Figure 3.2-1: P-Q curve for parallel operation



Figure 3.2-2: P-Q curve for serial operation

## (3) Relationship between combined fan characteristics and resistance characteristic

The explanations in the previous paragraphs ((1), (2)) consider only the fans in the P-Q curves, but in reality, resistance characteristics exist. For this reason, the air flow volumes verified in real cabinets differ.
The following describes specific effects, using parallel operation as an example.

Point C in Figure 3.2-3 is the combined fan characteristic operating point for parallel operation. At this point, the fan air flow volumes are A' and B'.
If the fans are operated independently, the air flow volumes will be A and B along the resistance curve.
The relationship can be described as follows.

$$
C=A^{\prime}+B^{\prime}<A+B
$$

Therefore, operating two fans in parallel does not deliver the sum of the two.
This trait becomes more pronounced as the resistance curve rises more steeply. When the resistance of the air flow path is low and the resistance curve rises gradually, along the horizontal axis, the delivered air flow volume becomes approximately the sum of the two.
The air flow volume increase at points $C$ and $C^{\prime}$ in Figure 3.2-4 show the difference.

In the case of serial operation where the operating point will be at the intersection of the resistance curve and the combined fan P-Q curve, the air flow volume of the two fans will be less than the simple addition of air flow volumes of the individual fans.
Refer to $C$ and $C^{\prime}$ in Figure 3.2-5.


Figure 3.2-3: Air flow volume in parallel operation


Figure 3.2-4: Parallel operation of 2 identical fans


Figure 3.2-5: Serial operation of 2 identical fans

As can be seen from above, when placing fans in parallel or in series, the expected effect cannot be achieved without carefully studying the relationship with resistance characteristics.
Consider the following items prior to cooling by fans in parallel or in series.
(1) Use safety factor to make the combined air flow volume, which can be achieved by serial or parallel operation, lower than the sum of air volumes from individual operations. (Unless the air flow path is fixed, installing two units will not deliver twice the volume of one unit.)
(2) For parallel operation, create cabinet construction which will allow gradual rise of the resistance curve. (Consider enlarging the area of passage in the cabinet.)
(3) Serial operation is not so effective in terms of air flow volume, but is more effective in increasing static pressure for constructions as the following where the resistance curve rises steeply.

- Cabinet construction which does not allow large intake or exhaust openings
- Cabinets with small passage area inside (cabinet housing instruments at high density)

Also consider using fans with large air flow volume.
(4) Analyze P-Q curves and resistance curves for multiple fan usage also.
(5) Using identical fans are recommended when installing multiple units. When different fans are used, "reverse flow characteristics" may occur in parallel operation and "turbine characteristics" may occur in serial operation.

## Appendix 4 Input to inverters

## Appendix -4.1 Input current (Harmonic current)

Figure 4.1-1 shows the main circuit of the inverter. The input side consists of a three-phase full wave rectification diode converter. The diode rectification and capacitor Cs perform the conversion to direct current.

In diode converters, distortion wave current as shown in Figure 4.1-2 flows close to the peaks of the power-supply voltage waveform.
The peak input current value ip and the conduction time ton of this distortion wave current depends not only on the power dissipation of the load but also on the size of the power supply side impedance (especially the reactance component).
For example, if the motor load is constant, the smaller the power supply impedance, the higher the peak values and shorter the conduction time become, as in Figure 4.1-2 (a).
On the other hand, the larger the power supply impedance, the lower the peak values and longer the conduction time become, as in Figure 4.1-2 (b).

The frequency components of the input current are shown in Figure 4.1-3. When the output of the electric motor is $100 \%$, changes in

- Fundamental wave current I1
- Harmonic current I5 to I19 (Various harmonic current from 5th harmonic to 19th harmonic)
- Total effective current leff
caused by the power supply reactance is shown.
Fundamental wave current I1 barely changes while the harmonic current and the total effective current vary widely.

The power supply reactance \% Xs in Figure 4.1-3 was converted to reference capacity base, assuming inverter capacity as the reference, by using the following equation.

$$
\% X_{S}=\% X_{T} \times \frac{P_{I N V}}{P_{T}}[\%] \quad \cdots \quad \text { Equation 4-1 }
$$

\%Xs : Power supply reactance based on inverter capacity [\%]
\% $X_{T}$ : Power supply reactance [\%]
Pinv: Inverter rated capacity [kVA]
$P_{T}$ : Power supply transformer capacity [kVA]
However, when \% $X_{T}$ is expressed in terms of power supply system reference capacity, $\mathrm{P}_{\mathrm{T}}$ will be expressed in terms of power supply system reference capacity.
If the wiring reactance is small and can be neglected, the power supply transformer \% reactance becomes \% $\mathrm{X}_{\mathrm{T}}$.

This harmonic wave adversely affects the input side power supply system and the electricity generators.


Figure 4.1-1: Inverter main circuit

(a) Case of low impedance

(b) Case of high impedance


Figure 4.1-2: Inverter input current waveform


Figure 4.1-3: Power supply reactance-input current characteristics

## Appendix -4.2 Input power factor

The input power factor of the inverter is given below.

$$
\begin{aligned}
& \begin{array}{l}
\text { Inverter input power } \\
\text { factor }
\end{array}=\frac{\text { Effective power }}{\text { Apparent power }}=\frac{\sqrt{3} \times E \times I_{1} \times \cos \theta_{1}}{\sqrt{3} \times E \times I_{e f f}} \\
& =\frac{I_{1} \times \cos \theta_{1}}{I_{e f f}} \quad \cdots \cdots \ldots . \text { Equation 4-2 } \\
& \text { E : Effective power supply voltage [V] } \\
& 11 \text { : Effective fundamental wave current [Arms] } \\
& \text { leff : Total effective current [Arms] } \\
& \cos \theta \text { : Fundamental wave power factor }
\end{aligned}
$$



Figure 4.2-1: Inverter input power factor

Figure 4.2-1 shows the result of computing Equation 4-2. The figure shows that as the power supply reactance (\%Xs) increases, the harmonic component decreases, improving the input power factor.

## Appendix -4.3 Improvement of the input power factor

When the inverter is operated, the decrease in power factor on the input power supply side is due to the inverter input current described in the previous section. It is not due to the phase difference between the voltage and current of the input system, so phase advancing capacitors will not improve power factor. (The phase advancing capacitors may be burned due to this harmonic current.)
To improve input power factor, suppression (reduction) of the harmonic current is necessary. Use a direct current reactor (DCR) as in Figure 4.3-1.
Alternating current reactor (ACR) also improves power factor to a degree, but it is inferior to DCR. For details, refer to "Appendix 7 Harmonics guideline".
Additionally, using Fuji Electric's PWM converter will improve power factor.


Figure 4.3-1: Locations to insert reactor

## Appendix -4.4 Generator (synchronous generator)

When supplying the inverter input power supply using a generator, the harmonic current of the inverter may cause induced current (negative-phase-sequence current) in the damper coils of the generator and cause the generator to burn. "JEM1354 2003: Synchronous land generator for driving diesel engines" states that generators must withstand negative-phase-sequence current up to $15 \%$. This negative-phase-sequence current can be computed by converting to negative phase equivalent current using Equation 4-3.

$$
\begin{gathered}
I 2 e g=\sqrt{\sum_{\gamma}\left[\sqrt[4]{\frac{\gamma}{2}} \times I \gamma\right]^{2}}=\sqrt{\left[\sqrt[4]{\frac{6}{2}\left(\mathrm{I}_{5}+I_{7}\right)}\right]^{2}+\left[\sqrt[4]{\frac{12}{2}\left(\mathrm{I}_{11}+I_{13}\right)}\right]^{2}+\left[\sqrt[4]{\frac{18}{2}\left(\mathrm{I}_{17}+I_{19}\right)}\right]^{2}+\left[\sqrt[4]{\frac{24}{2}\left(\mathrm{I}_{23}+I_{25}\right.}\right)^{2}} \cdots \\
\text { I2eg: } \\
\text { : Equivalent negative phase current } \\
\text { I5,I.I7..... } 125 \\
\text { : nth harmonic current }
\end{gathered}
$$

Equation 4-3

When using a generator as the power source, the rated current of the generator to select should be approximately three times when using a direct current reactor, and approximately four times when using an alternating current reactor. Some generators have enhanced damper windings, so contact the generator manufacturer for details.
LC filters, PWM converters, and active filters can reduce harmonic current.
<Calculation example>

| ¢ | Input voltage: $3 \varphi 220 \mathrm{VAC} / 60 \mathrm{~Hz}$ <br> Motor: 45 kW <br> Inverter: FRN45VG1S-2 $\square$ (DCR2-45) |
| :---: | :---: |

$$
\begin{aligned}
\text { Generatorcapacityrequired } & =\sqrt{3} \times V \times \frac{I 2 e g}{15 \%}=\sqrt{3} \times 220 \times \frac{89}{0.15} \\
& =226[\mathrm{kVA}]
\end{aligned}
$$

Generator capacity required is $226[\mathrm{kVA}]$ or greater.

Using Equation 4-3

$$
\begin{aligned}
I 2 e g & =\sqrt{\left[\sqrt[4]{\frac{6}{2}\left(\mathrm{I}_{5}+I_{7}\right)}\right]^{2} \cdots+\left[\sqrt[4]{\frac{24}{2}\left(\mathrm{I}_{23}+I_{25}\right)}\right]^{2}} \\
& =\sqrt{\sqrt{3}\left(\mathrm{I}_{5}+\mathrm{I}_{7}\right)^{2}+\sqrt{6}\left(I_{11}+I_{13}\right)^{2}+\sqrt{9}\left(I_{17}+I_{19}\right)^{2}+\sqrt{12}\left(I_{23}+I_{25}\right)^{2}} \\
& =\sqrt{\sqrt{3}(39+20)^{2}+\sqrt{6}(13+8.4)^{2}+\sqrt{9}(7.5+5.5)^{2}+\sqrt{12}(5.1+4.0)^{2}} \\
& =89[A]
\end{aligned}
$$

## Appendix 5 Proficient way to use inverters (on electric noise)

This appendix describes the contents of "Proficient way to use inverters (on preventing electric noise): 2010 revised edition" published by Japan Electrical Manufacturers' Association with supplementary information. Please implement noise countermeasures referencing this section and Chapter 7 "EMC Compatible Peripherals".

## Proficient way to use inverters (on preventing electric noise)

Japan Electrical Manufacturers' Association (JEMA)
Excerpt from Technical Document (Dec 2010)

## Appendix -5.1 Effect of inverters on other instruments

This section describes the effects of the inverter on existing electronic instruments and instruments embedded in the same system as the inverter, and countermeasures. (For details, refer to "Appendix -5.4 Cases of noise countermeasures".)

## 1. Effect on AM radios

Phenomenon : When the inverter is operating, noise sometimes enters nearby AM radios. (FM radios and televisions are basically not affected).
Probable Cause: The radio is receiving the noise radiated from the inverter.
Countermeasure: Installing noise filter on the inverter power supply side is effective.
2. Effect on telephones

Phenomenon : When the inverter is operating, noise sometimes enters the telephone in use, making hearing difficult.
Probable Cause: Harmonic leak current from the inverter or motor enters the telephone cable shielded wires, causing noise.
Countermeasure: Connecting the motor grounding terminals to one point in common and attaching the point to inverter grounding terminal is effective.
3. Effect on pressure sensors

Phenomenon : The pressure sensor sometimes malfunctions when the inverter is operating.
Probable Cause: Noise enters the signal line through the grounding wire.
Countermeasure: Installing noise filter on the inverter power supply side and separating the I/O wires, grounding wires, and control circuit wiring are effective.
4. Effect on position detectors (pulse encoder)

Phenomenon : The pulse encoder sometimes malfunctions when the inverter is operating, causing shifts in stop position.
Probable Cause : Phenomenon occurs more readily when the motor power line and the encoder lines are bundled.
Countermeasure: Separately route the motor power line and the encoder lines can reduce the effect of induction noise and radiated noise. Adding noise filter on the I/O terminals of the inverter is also effective.
5. Effect on proximity switches

Phenomenon : When the inverter is operating, proximity switches (static capacitance type) sometimes malfunction.
Probable Cause : Noise immunity of the static capacitance type switches may be low.
Countermeasure: Installing noise filter on the inverter power supply side and attaching grounding capacitors to the zero volt side (common side) of the proximity switch power supplies are effective. Also, replacement to magnetic type switches which have high noise immunity is also effective.

## Appendix -5.2 Definition of noise

This section describes the noise generated by the inverter, the principles of occurrence, and the instruments which can be affected by noise readily.

## 1. Inverter operation principles and noise generation

Figure 5.2-1 shows the overview of an inverter. The inverter converts alternating current to direct current (forward conversion) in the converter section. The control circuit uses the six IGBTs in the inverter section in PWM switching to convert (reverse conversion) to variable voltage and variable frequency alternating current to control the motor at various speeds.
At this time, the high speed switching of the IGBTs turns direct current voltage on and off, creating switching noise. This switching noise flows through the inverter, the I/O wires, and the stray capacitance (C) between the motor and the earth as noise current (i).
The magnitude of the noise current is given by the following:

$$
i=C \bullet \frac{d v}{d t}
$$

It is related to stray capacitance (C) and dv/dt (switching speed of IGBT). This noise current flows every time IGBT switches on and off, so it depends also on the carrier frequency.
The DC/DC converter also performs switching, so it is also a noise source.

The frequency bandwidth of the noise spans approximately tens of MHz , affecting AM radios, factory radios, telephones, and communication instruments.

## 2. Types of noise

The switching noise generated by the inverter propagates through the inverter wiring to power supplies and motors, affecting a wide range of instruments from the power transformer to the motor.
Figure 5.2-2 shows the possible various noise transmission routes.
Noise can be categorized into three types: transmission noise, induction noise, and radiated noise.


Figure 5.2-1: Inverter overview


Figure 5.2-2: Noise propagation route

## (1)Transmission noise

For transmission noise, the switching noise generated inside the inverter is transmitted to and affects peripheral instruments via electric wires and conductors.
(1) Route through the main circuit and the power supply
(2) Route possible when the grounding wire is used commonly by instruments
(3) Route via sensor signal lines and shielded wires


Figure 5.2-3: Transmission noise

## (2) Induction noise

The inverter main circuit wires (wiring around the input and output sides) contain current with inverter switching components.
The output side direct current bus (DC bus) carries a lot of switching noise.
Wraparound of distorted electric current caused by harmonics and inverter leak current occurs on the input side.

Therefore, peripherals and signal lines placed close to the main circuit wires are affected by electromagnetic induction noise in Figure 5.2-4 and static induction noise in Figure 5.2-5.

## (3) Radiated noise

Noise generated inside the inverter uses the power and grounding wires on the input and output sides as antennas to radiate into the air. Peripheral instruments and radio communication are affected by radiated noise (5). Radiated noise uses not only wires, but also the cabinet housing the inverter and the motor surfaces as antennas.


Figure 5.2-4: Electromagnetic induction noise

Figure 5.2-5: Static induction noise


Figure 5.2-6: Radiated noise

## Appendix -5.3 Noise countermeasures

The effectiveness of noise countermeasures is proportional to the degree of improvement. However, sometimes simple solutions fit the problems best. Implementing economic measures matching the level of noise and facility conditions is required.
Prior consideration for noise is important even in the case of housing inverters in cabinets. Substantial time and cost will be necessary for resolving troubles, once the troubles caused by noise occur.

## (1) Prior treatment

The following lists prior treatments for noise:

1) Separate the wiring of main circuit power lines and control circuit lines.
2) Wire main circuit power lines in metal pipes (conduit pipe).
3) Use shielded wires and twisted shielded wires for control circuit.
4) Construct grounds and ground wiring appropriately.

The above treatments should avoid most of the noise troubles.

## (2) Implementation of countermeasures

Noise countermeasures can be implemented on the instruments being affected by noise and on the transmission routes.

## (2)-1.1. Instruments affected by noise

1) Separate from the inverter main circuit wiring.
2) When the peripheral instrument requires power, insulate it from the inverter main power supply. (Use isolation transformers. Use isolation transformer with short proof shield between primary and secondary coils.)
3) Attach LC filters on power lines for PLC (programmable sequencer) and POD (programmable operation display).
(2)-1.2. Inverter, the noise generation source
4) Attach noise filter to reduce the noise level.
5) Contain noise level by using metal wiring pipes and metal cabinets.
6) Always bundle power lines when wiring. For the input side and the output side direct current buses, wire separately. (Do not bundle.)
Table 5.3-1 summarizes the methods to prevent noise trouble, the purpose, and the noise transmission route which is the target of the countermeasures.

Table 5.3-1 : Noise trouble prevention methods

| Methods to prevent noise trouble |  | Purpose of countermeasure |  |  |  | Propagation Route |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { әs!̣ou oł } \\ \text { ә\|q!̣dəosns ssə әyew } \end{gathered}$ |  |  |  |  |  |  |
| Wiring and installation | Separate wiring of main circuit and control circuit | $\bigcirc$ |  |  |  |  | $\bigcirc$ |  |
|  | Wiring with minimum wiring distance | $\bigcirc$ |  |  | $\bigcirc$ |  | $\bigcirc$ | $\bigcirc$ |
|  | Wiring in parallel and avoid bundling | $\bigcirc$ |  |  |  |  | $\bigcirc$ |  |
|  | Appropriate grounding | $\bigcirc$ |  |  | $\bigcirc$ | O | $\bigcirc$ |  |
|  | Use shielded wires and twisted shielded wires | $\bigcirc$ |  |  |  |  | $\bigcirc$ | $\bigcirc$ |
|  | Use shielded cable for main circuit |  |  | $\bigcirc$ |  |  | $\bigcirc$ | $\bigcirc$ |
|  | Use metal wiring pipes |  |  | $\bigcirc$ |  |  | $\bigcirc$ | $\bigcirc$ |
| Cabinet | Appropriate placement of housed instruments in cabinet | $\bigcirc$ |  |  |  |  | O | O |
|  | Metal control board |  |  | $\bigcirc$ |  |  | $\bigcirc$ | $\bigcirc$ |
| Instruments for countering noise | Line filter | $\bigcirc$ |  |  | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |
|  | Isolation transformer |  | $\bigcirc$ |  |  | $\bigcirc$ |  | $\bigcirc$ |
| Treatment on instruments affected by noise | Use bypass capacitor on control circuit | $\bigcirc$ |  |  |  |  | $\bigcirc$ | $\bigcirc$ |
|  | Use ferrite core on control circuit | $\bigcirc$ |  |  | $\bigcirc$ |  | $\bigcirc$ | $\bigcirc$ |
|  | Line filter | $\bigcirc$ |  | $\bigcirc$ |  | $\bigcirc$ |  |  |
| Other | Separate power systems | $\bigcirc$ | $\bigcirc$ |  |  | $\bigcirc$ |  |  |
|  | Lower carrier frequency |  |  |  | $\triangle$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |

In the table, $\quad$ O mark denotes high effect. $\triangle$ mark denotes low effect.
Blank denotes no effect.

The following shows trouble countermeasures when constructing inverter drives.

## (2)-2.1. Wiring and ground

On the inside and outside of the cabinet housing the inverter, separate the wiring for the main circuit and the control circuit as much as possible. Use wires which are less susceptible to noise, such as shielded wires and twisted shielded wires, for the control circuit wiring and wire at minimum distance. (Refer to Figure 5.3-1: Example of separated wiring.)
Do not bundle the wiring for main circuit and control circuit, and avoid parallel wiring.


Figure 5.3-1: Example of separated wiring

Use metal wiring pipes for the main circuit wiring and ground the metal pipe to prevent propagation of noise (refer to Figure 5.3-2).
For the shield sheath (net) of the shielded wire, always connect only one point to the signal ground line reference (common) side to avoid creating loops with multiple point connection. (Refer to Figure 5.3-3.)
Grounding is effective in preventing electric shock due to earth leakage, noise penetration and noise radiation. Construct ground according to the main circuit voltage, using Type 3 Ground Construction ( 300 VAC or lower) or Special Type 3 Ground Construction (300 VAC to 600 VAC) rules. Create dedicated grounds or lay individual ground lines for the various ground wiring.


Figure 5.3-2: Grounding metal wiring


Figure 5.3-3: Treatment of shielded wires

## (2)-2.2. Control cabinet

Cabinets housing inverters are typically made of metal. Installation of the metal box shields the surroundings from radiated noise of the inverter.
When attaching electronic instruments such as the programmable controller to the cabinet, exercise caution on the placement of each instrument. Installation of shielding plates between the inverter and the peripheral instruments may be necessary in some cases.

## (2)-2.3. Instruments for noise countermeasures

Line filters and power transformers are used to reduce transmission noise which propagates along the wiring, noise which propagates along the electric circuit and noise which radiates to the air from the main circuit wiring (refer to Figure 5.3-4).

Simple types of filter include capacitive filters which are connected in parallel to power lines and inductive filters which are connected in series. More elaborate filters (LC filter) corresponding to radio noise regulations also exist, and the filters are selected according to the target noise reduction effect. Power transformer types include the typical isolation transformers, shield transformers, and noise cut transformers, delivering different effects in preventing noise transmission.


Figure 5.3-4: Various filter and connection methods

## (2)-3. Treatment on instruments affected by noise

Noise immunity enhancement is important for the electronic instruments housed in the same cabinet as the inverter or installed in the periphery. Use line filters, shielded wires, and twisted shielded wires for the signal lines of these instruments to prevent intrusion of noise. Additionally,
(1) Reduce circuit impedance by adding capacitors and resistors in parallel to the I/O terminals of the signal circuit.
(2) Insert choke coils in series to the signal circuit and route wire through ferrite core beads to increase the impedance against noise. Enlarging the signal reference line (OV line) and the grounding wire are also effective noise countermeasures.

## (2)-4. Others

The level of the noise which propagates (occurs) is also dependent on the carrier frequency. Higher carrier frequencies make higher noise generation levels. For inverters which allow carrier frequency change, reducing the carrier frequency while keeping balance with the noise level generated by the motor when driving, will reduce the occurrence of noise.

## Appendix -5.4 Cases of noise countermeasures

This section describes cases implemented against noise generated by inverters.
Table 5.4-1: Cases of noise countermeasures

| No. | Target instrument | Phenomenon | Countermeasure | Points |
| :---: | :---: | :---: | :---: | :---: |
| 1 | AM radio | When the inverter was operated, noise appeared on AM radio broadcast (500 to 1500 kHz ). <br> <Probable cause> AM radio probably received the noise radiated from the power supply side or the output side wiring of the inverter. | 1) Install LC filter on the power supply side of the inverter. (Simple attachment of capacitive filter may be also done) <br> 2) Use metal wiring pipe between the motor and inverter. <br> Note) <br> The wiring between the LC filter and inverter will be shortened (to within 1 m ). | - Reduce the radiated noise from the wiring. <br> - Reduce transmission noise to the power supply side. <br> - Or, use shielded wires. <br> Note) <br> Adequate improvement may not result in areas where radio waves are weak, such as in the mountains. |
| 2 | AM radio | When the inverter was operated, noise appeared on AM radio broadcast (500 to 1500 kHz ). <br> <Probable cause> AM radio probably received the noise radiated from the power lines of the inverter power supply side. | 1) Attach inductive filters (zero phase reactor) to the input and output sides of the inverter. <br> Note) <br> Maximize the number of windings on the zero phase reactor. Also make the wiring between the inverter and inductive filter short. (within 1 m ). <br> 2) For even more improvement, attach LC filter. | Reduce the radiated noise from the wiring. |

Table 5.4-1: Cases of noise countermeasures (Continued)

| No. | Target instrument | Phenomenon | Countermeasure | Points |
| :---: | :---: | :---: | :---: | :---: |
| 3 | $\left(\begin{array}{l}\text { Telephone } \\ \text { A house 40 } \\ \text { m away }\end{array}\right)$ | When the ventilator was driven by the inverter, noise appeared on the telephone of a house 40 m away. <br> <Probable cause> <br> The high frequency leakage current from the inverter and motor flowed into the shield ground section of the telephone cable when returning through the ground of the transformer on the electric pole. Static induction probably occurred and created noise in the telephone line. | 2) Connect the grounding terminals of the motors in common and connect to the inverter board. <br> 3) Attach $1 \mu \mathrm{~F}$ grounding capacitor to the inverter input terminal. | - Inductive filters and LC filters may not be appropriate in the voice frequency band. <br> - If the power transformer forms a V -connection and is a 200 V system, due to the difference in voltage to ground, caution must be exercised in connecting the capacitors as in the diagram below. |
| 4 | Photoelectric relay | When the inverter was operated, the photoelectric relay malfunctioned. <br> <Probable cause> <br> The wiring of the inverter power input line and the photoelectric relay were wired in parallel for 30 to 40 m with 25 mm spacing. Induction noise is estimated to have caused the malfunction. (The installation conditions do not allow separation of wiring.) | 1) As a temporary measure, attach a $0.1 \mu \mathrm{~F}$ capacitor between the 0 V terminal of the power circuit (belonging to the detection section of the photoelectric relay in the roof section) and the roof section board frame. <br> 2) As a permanent measure, move the 24 V power supply on the ground to the roof section, and use contact signals to the ground. | - Wire separately. ( 30 cm or more). <br> - When separation is not possible, use dry contact signals to transmit and receive signals. <br> - Parallel wiring of power system wires and small signal lines in close spacing must be avoided. |

Table 5.4-1: Cases of noise countermeasures
(Continued)

| No. | Target instrument | Phenomenon | Countermeasure | Points |
| :---: | :---: | :---: | :---: | :---: |
| 5 | Photoelectric relay | When the inverter was operated, the photoelectric relay malfunctioned. <br> <Probable cause> <br> The inverter and the photoelectric relay are adequately separated. Because the power supply is connected in common, however, transmission noise probably entered from the power lines. | Attach $0.1 \mu \mathrm{~F}$ capacitor between the output common terminal of the photoelectric relay amplifier and the frame. | Low cost countermeasure is sometimes possible and relatively easy. Focus on the weak section of the circuit belonging to the malfunctioning instrument. |
| 6 | Proximity switch (static capacitance type) | Proximity switch malfunctioned. <br> <Probable cause> Static capacitance type proximity switch has low noise immunity. The switch may be susceptible to electric circuit transmission noise and radiated noise. | 1) Install LC filter on the inverter output side. <br> 2) Install capacitive filter on the inverter input side. <br> 3) Connect the DC supply 0 V (common) line of the proximity switch and the casing of the machine via a capacitor. | - Reduce the generated noise at the inverter side. <br> - Replace with a proximity switch (such as magnetic type) which has high noise immunity. |
| 7 | Pressure sensor | Pressure sensor malfunctioned. <br> <Probable cause> <br> Noise wrapped around from the casing via the shielded wire and caused the pressure sensor to malfunction. | 1) Install LC filter on the inverter input side. <br> 2) Switch the connection of the pressure sensor shielded wire from the machine casing to the pressure sensor 0 V line (common). | - Connect the shielded wire of sensor signals to the common point of the system. <br> - Reduce the transmission noise from the inverter. |

Table 5.4-1: Cases of noise countermeasures
(Continued)

| No. | Target instrument | Phenomenon | Countermeasure | Points |
| :---: | :---: | :---: | :---: | :---: |
| 8 | Position detector $\binom{$ Pulse }{ encoder } | The pulse encoder output an erroneous pulse which shifted the crane stop position. <br> <Probable cause> <br> The motor line and the encoder signal line were bundled in the wiring. Induction noise probably distorted the pulse waveform. | 1) Install LC filter and capacitive filter on the inverter input side. <br> 2) Install LC filter on the inverter output side. | - This countermeasur $e$ is for cases when power lines and signal lines cannot be separated. <br> - Reduce the induction noise and radiated noise on the inverter output side. |
| 9 | Programmable controller (PLC) | PLC program failed in operation. <br> <Probable cause> <br> Noise probably propagated to PLC through the power supply, since the power supplies of the inverter and PLC use the same power system. | 1) Install LC filter and capacitive filter on the inverter input side. <br> 2) Install LC filter on the inverter output side. <br> 3) Lower the carrier frequency of the inverter. <br> 4) Install LC filter on the PLC power supply. | Reduce overall electric circuit transmission noise and induced noise. |

## Appendix 6 Grounding as noise countermeasure and ground noise

Signal ground (hereafter referred to as SG) establishes the reference potential (zero potential) of electronic circuits and enables stable operation. Frame ground (hereafter referred to as FG) is the construction, such as the casing (metal) of the equipment, which provides a shield protecting SG from noise. By connecting these grounds to the earth (grounding), noise entering from the outside, such as the input power supply, is transmitted to the earth to reduce noise interference. In another case, internally generated noise is prevented from transmission to the outside to reduce noise interference. However, grounds may generate noise related to grounding.

## (1) Noise due to difference in ground potential

Impedance consisting of direct current resistance and inductance exists between the earth, SG and FG. The voltage of the earth differs by location because the earth is a resistor with conductivity. Therefore, when leakage current flows to the grounding wire or the earth, the reference potential changes and creates potential difference, which may cause noise.
To prevent this noise, the potential difference between the electronic circuit reference potential (SG) and the earth must be eliminated. In other words, the impedance of the grounding circuit must be minimized.

## (2) Noise due to common impedance of the grounding circuit

When the grounding wire is connected as in Figure 6-2, the inverter and the electronic instrument will share the common impedance. When common impedance exists in the grounding circuit, leakage current (ground potential) shift on one side affects the ground potential on the other side, generating noise though mutual interference.
Therefore, separate the grounding circuit for each instrument and avoid sharing common impedance.

## (3) Noise due to inductive coupling

When long grounding wires are wired in parallel to other wires such as power lines, induction voltage (induction noise) results in the grounding wires due to static capacitance $C$ or mutual inductance M. (Refer to Figure 6-3.)
Induction voltage has high frequency and increases as the wires get closer. To avoid induction voltage, wire separately from wires which are noise sources.

## (4) Example of ground noise generation

For example, when leak current $\mathrm{I}_{1}$ flows in the inverter grounding wire as in Figure 6-4, ground voltage $\mathrm{Vg}_{1}$ is generated. When frequency $f_{1}$ of current $I_{1}$ rises, impedance ( $2 \pi f_{1} L_{1}$ ) of inductance $L_{1}$ increases and $V g_{1}$ rises.
When $I_{1}$ or $f_{1}$ vary, $\mathrm{Vg}_{1}$ also varies, generating noise due to ground potential difference.
Additionally, when an electronic instrument is connected, rise in $\mathrm{Vg}_{1}$ increases the potential difference with $\mathrm{FG}_{2}$. Then, current $\mathrm{I}_{3}$ flows through the signal line casing (shield cover of shielded wires) and the common impedance $L_{2} \cdot R_{2}$ and noise is generated by the common impedance.
When la flows, induction noise occurs by the voltage induced in the core wire due to inductive coupling between the signal line casing and the core wire (signal line).

## Appendix 7 Harmonics guideline

## Appendix -7.1 How to comply with "Guideline on measures to suppress harmonics for users serviced by high voltage or special-high voltage" (general-purpose inverters)

The following two notifications were issued by the Ministry of International Trade and Industry, Agency for Natural Resources and Energy, Public Utilities Department on September 30, 1994.
(1) "Guideline on measures to suppress harmonics in home Appliances and General Purpose Products"
(2) "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage"

The use of electronic instruments generating harmonic current is expected to increase. The aim of these guidelines is to prevent harmonic interference to instruments connected to the system by providing regulations beforehand. These guidelines apply to all electric and electronic instruments generating harmonic current operated on commercial power supplies, but the following explanation is limited to "general purpose inverters".

## Appendix -7.1.1 Application of the "general purpose inverter"

## [ 1] Case of "other than special users"

The "Guideline on measures to suppress harmonics in home appliances and general purpose products" issued by the Ministry of Economy, Trade, and Industry in September 1994 states that general purpose inverters (input current under 20 A ) are not subject to the regulation from January 2004. Users who do not fall under the "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage" are recommended to attach "direct current reactor" as described in the past on inverter catalogs and user manuals.

## [ 2] Case of "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage"

Users of high voltage or special high voltage power services are corresponded using the "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage". Harmonic current generating instruments, such as the "general purpose inverters", are not directly controlled, but the regulation is enforced by users of electricity. Calculation of the amount of harmonic current generated is necessary for each instrument.
(1) Targets of regulation

Regulation applies when the following two conditions are satisfied.

- Receiving voltage is either high voltage or special high voltage.
- "Equivalent capacity" of the converter loading exceeds the reference value for the receiving voltage ( 50 kVA for 6.6 kV receiving voltage).
For calculating the "equivalent capacity" according to the guideline, supplementary explanation is available in the B. 2 "[1]
"Calculation of equivalent capacity"."


## (2) Regulating method

The magnitude (calculated value) of the harmonic current flowing to the system from the user's point of receiving voltage is controlled. The regulated value is proportional to the contract demand. The regulated values of the guideline are shown in Table 7.1-1.
Supplementary explanation for calculating "harmonic current" according to the guideline is available in Appendix -7.1.2 (Correspondence to "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage").

Table 7.1-1: Maximum harmonic current outflow per 1 kW of contract demand (mA/kW)

| Receiving voltage | $5^{\text {th }}$ | $7^{\text {th }}$ | $11^{\text {th }}$ | $13^{\text {th }}$ | $17^{\text {th }}$ | $19^{\text {th }}$ | $23^{\text {rd }}$ | Beyond $25^{\text {th }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.6 kV | 3.5 | 2.5 | 1.6 | 1.3 | 1.0 | 0.90 | 0.76 | 0.70 |
| 22 kV | 1.8 | 1.3 | 0.82 | 0.69 | 0.53 | 0.47 | 0.39 | 0.36 |

(3) Implementation timing

Application of the new guidelines has already begun.
With the application of the new guidelines, the calculation of the "voltage distortion rate" which was formerly performed when signing the power contract, is no longer needed.

## Appendix -7.1.2 Correspondence to "Guideline on measures to suppress harmonics for users serviced by high voltage or special high voltage"

When calculating for the "general purpose inverter" according to the guideline, please compute in the following fashion. The contents described in this section are based on the "Technical guide on harmonic suppression measures" (JEAG 9702-1995) issued by Japan Electric Association.

## [1] "Calculation of equivalent capacity"

Equivalent capacity is computed by (rated input capacity) x (conversion factor). However, general purpose inverter catalogs in the past do not specify the rated input capacity value, so it is described below.
(1) "Inverter rated capacity" which corresponds to "Pi"

- In the guidelines, a 6-pulse converter is defined as the reference with conversion factor 1 . The rated input capacity of general purpose inverters must be expressed in terms of harmonic current corresponding to conversion factor 1.
- Specifically, the fundamental harmonic input current $I_{1}$ is computed from the load motor's rated kW , motor efficiency, and inverter efficiency. Then, calculate rated input capacity $=\sqrt{3} \times$ (Supply voltage) $\times l_{1} \times 1.0228 / 1000(\mathrm{kVA}) .1 .0228$ is (effective current) / (fundamental harmonic current) for the 6-pulse converter.
- When general purpose motors and inverter motors are used, the values in Table 7.1-2 can be used. Use the rated kW of the motor used regardless of inverter type in selecting the value.

Note Be cautioned that the "rated input capacity" mentioned here can be used only for the calculation in harmonic guidelines and cannot be used in selecting inverter supply side instruments and wiring size.
(1) Refer to the manufacturer's catalog or technical documents for selecting the capacity of peripheral instruments.

Table 7.1-2: General purpose inverter "rated input capacity" determined by the applied motor

| Applied motor (kW) |  | 0.4 | 0.75 | 1.5 | 2.2 | 3.7 | 5.5 | 7.5 | 11 | 15 | 18.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{Pi} \\ (\mathrm{kVA}) \end{gathered}$ | 200 V | 0.57 | 0.97 | 1.95 | 2.81 | 4.61 | 6.77 | 9.07 | 13.1 | 17.6 | 21.8 |
|  | 400 V | 0.57 | 0.97 | 1.95 | 2.81 | 4.61 | 6.77 | 9.07 | 13.1 | 17.6 | 21.8 |


| Applied motor (kW) |  | 22 | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pi <br> $(\mathrm{kVA})$ | 200 V | 25.9 | 34.7 | 42.8 | 52.1 | 63.7 | 87.2 | 104 | 127 |  |  |
|  | 400 V | 25.9 | 34.7 | 42.8 | 52.1 | 63.7 | 87.2 | 104 | 127 | 153 | 183 |


| Applied motor (kW) |  | 200 | 220 | 250 | 280 | 315 | 355 | 400 | 450 | 500 | 630 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pi <br> $(\mathrm{kVA})$ | 200 V |  |  |  |  |  |  |  |  |  |  |
|  | 400 V | 229 | 252 | 286 | 319 | 359 | 405 | 456 | 512 | 570 | 718 |

(2) Magnitude of "Ki (conversion factor)"

Use the conversion factors included in the document attached to the guideline, according to the use of optional ACR (alternating current reactor) and DCR (direct current reactor). The magnitude of the conversion factor is shown in Table 7.1-3.

Table 7.1-3: General purpose inverter "conversion factor Ki" determined by reactor

| Circuit category |  | Circuit classification | Conversio <br> n factor Ki | Major use cases |
| :---: | :---: | :---: | :---: | :---: |
| 3 | 3 phase bridge (capacitor smoothing) | No reactor | K31 = 3.4 | - General purpose inverter <br> - Elevator <br> - Refrigeration and air conditioning equipment <br> - Other general purpose equipment |
|  |  | With reactor (AC side) | $\mathrm{K} 32=1.8$ |  |
|  |  | With reactor (DC side) | K33 $=1.8$ |  |
|  |  | With reactor (AC and DC sides) | K34 $=1.4$ |  |

[^22]
## [ 2 ] "Calculation of harmonic current"

(1) Magnitude of "fundamental harmonic current"

- "Fundamental harmonic current" needs to be computed separately when performing calculations using "Table 2, in the document attached to the guideline".
- Use Table 7.1-4 below according to the rated kW of the motor used, regardless of inverter type and availability of reactors.
Note When the input voltage differs, values are calculated in inverse proportion to the voltage value.
Table 7.1-4: "Fundamental harmonic input current" of general purpose inverters determined by applied motor

| Applied motor (kW) |  | 0.4 | 0.75 | 1.5 | 2.2 | 3.7 | 5.5 | 7.5 | 11 | 15 | 18.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fundamental harmonic input current (A) | 200 V | 1.62 | 2.74 | 5.50 | 7.92 | 13.0 | 19.1 | 25.6 | 36.9 | 49.8 | 61.4 |
|  | 400 V | 0.81 | 1.37 | 2.75 | 3.96 | 6.50 | 9.55 | 12.8 | 18.5 | 24.9 | 30.7 |
| 6.6 kV conversion value (mA) |  | 49 | 83 | 167 | 240 | 394 | 579 | 776 | 1121 | 1509 | 1860 |


| Applied motor (kW) |  | 22 | 30 | 37 | 45 | 55 | 75 | 90 | 110 | 132 | 160 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fundamental <br> harmonic input <br> current (A) | 200 V | 73.1 | 98.0 | 121 | 147 | 180 | 245 | 293 | 357 |  |  |
|  | 400 | 36.6 | 49.0 | 60.4 | 73.5 | 89.9 | 123 | 147 | 179 | 216 | 258 |
| 6.6 kV conversion value (mA) | 2220 | 2970 | 73.5 | 4450 | 5450 | 7450 | 8910 | 10850 | 13090 | 15640 |  |


| Applied motor (kW) |  | 200 | 220 | 250 | 280 | 315 | 355 | 400 | 450 | 500 | 630 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fundamental harmonic input current (A) | 200 V |  |  |  |  |  |  |  |  |  |  |
|  | 400 V | 323 | 355 | 403 | 450 | 506 | 571 | 643 | 723 | 804 | 1013 |
| 6.6 kV conversion value (mA) |  | 19580 | 21500 | 24400 | 27300 | 30700 | 34600 | 39000 | 43800 | 48700 | 61400 |

(2) Calculation of harmonic current

Generally, use "Table 2-3 in the document attached to the guideline, 3 phase bridge (capacitor smoothing)" to compute. The contents of the document attached to the guideline are shown in Table 7.1-5.

Table 7.1-5: Amount of harmonic current generated (\%) 3 phase bridge (capacitor smoothing)

| Order | $5^{\text {th }}$ | $7^{\text {th }}$ | $11^{\text {th }}$ | $13^{\text {th }}$ | $17^{\text {th }}$ | $19^{\text {th }}$ | $23^{\text {rd }}$ | $25^{\text {th }}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No reactor | 65 | 41 | 8.5 | 7.7 | 4.3 | 3.1 | 2.6 | 1.8 |
| With reactor (AC side) | 38 | 14.5 | 7.4 | 3.4 | 3.2 | 1.9 | 1.7 | 1.3 |
| With reactor (DC side) | 30 | 13 | 8.4 | 5.0 | 4.7 | 3.2 | 3.0 | 2.2 |
| With reactor (AC and DC sides) | 28 | 9.1 | 7.2 | 4.1 | 3.2 | 2.4 | 1.6 | 1.4 |

- AC side reactor $: 3 \%$
- DC side reactor : Accumulated energy corresponds to 0.08 to $0.15 \mathrm{~ms}(100 \%$ load conversion)
- Smoothing capacitor : Accumulated energy corresponds to 15 to 30 ms ( $100 \%$ load conversion)
- Load : 100\%
nth order harmonic current $(A)=$ fundamental harmonic current $(A) x$ $\qquad$ 100

Compute harmonic current for each order as shown above
(3) Maximum rate of operation

- For elevators where the loading requires intermittent operation and where the design uses overrated motors, the "maximum rate of operation" is multiplied to reduce the current.
- According to the document attached to the guideline, "The maximum rate of operation for instruments is the ratio of the total capacity of the equipment generating harmonics to the capacity which maximizes the actual operation of the instrument. The capacity of the actually operating equipment is the average value in 30 minutes".
- Generally, calculation is performed according to this definition. However, for building facilities, the standard values in Table 7.1-6 are recommended. The values can probably be referenced for similar facilities.

Table 7.1-6: Rate of operation for building facility inverters (standard values)

| Type of facility | Instrument capacity | Stand-alone instrument rate of operation |
| :---: | :--- | :---: |
| Air conditioning facility | 200 kW or less | 0.55 |
|  | Over 200 kW | 0.60 |
| Sanitary pump | - | 0.30 |
| Elevator | - | 0.25 |
| Refrigeration and freezing equipment | 50 kW or less | 0.60 |
| UPS (6 pulse) | 200 kVA | 0.60 |

## Correction factor according to scale of contract demand

When scale increases such as in buildings, the overall rate of operation decreases. In such cases, calculation of harmonic reduction using correction factor $\beta$ in Table 7.1-7 is approved.

Table 7.1-7: Correction factor by scale

| Contract demand (kW) | Correction factor $\beta$ |
| :---: | :---: |
| 300 | 1.00 |
| 500 | 0.90 |
| 1,000 | 0.85 |
| 2,000 | 0.80 |

(Note) When the contract demand is between the numbers shown in Table 7.1-7, then calculate by interpolation.
(Note) For users whose receiving voltage is especially high or over 2000 kW , value must be determined in discussions with the power company.
(4) Harmonic order to calculate

The characteristic for the amount of harmonic current generated by general purpose inverters decreases as the order increases. The characteristic corresponds to the "case which does not cause special problems" which is shown in 3. (3) in the document attached to the guideline.
Therefore, only " 5 th and the 7 th components of the harmonic current need to be calculated".

## [3] Specific calculation examples

(1) Calculation example for "equivalent capacity"

|  | Sample load | Input capacity | Conversion factor | Equivalent capacity |
| :--- | :--- | :--- | :--- | :---: |
| [Ex 1] | $400 \mathrm{~V}, 3.7 \mathrm{~kW}, 10$ units <br> With AC and DC reactors | $4.61 \mathrm{kVA} \times 10$ units | $\mathrm{K} 32=1.4$ | $4.61 \times 10 \times 1.4=64.54 \mathrm{kVA}$ |
| [Ex 2] | $400 \mathrm{~V}, 1.5 \mathrm{~kW}, 15$ units <br> With AC reactors | $2.93 \mathrm{kVA} \times 15 \mathrm{units}$ | $\mathrm{K} 34=1.8$ | $2.93 \times 15 \times 1.8=79.11 \mathrm{kVA}$ |
|  |  | Refer to Table 7.1-2. | Refer to Table 7.1-3. |  |

(2) Calculation example for "harmonic current for various orders"

Example 1: $400 \mathrm{~V}, 3.7 \mathrm{~kW}, 10$ units (with AC reactor), max rate of operation 0.55

| Fundamental harmonic current on 6.6 <br> kV side (mA) | Harmonic current on 6.6 kV side (mA) |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $394 \times 10=3940$ | $5^{\text {th }}$ | $7^{\text {th }}$ | $11^{\text {th }}$ | $13^{\text {th }}$ | $17^{\text {th }}$ | $19^{\text {th }}$ | $23^{\text {rd }}$ | $25^{\text {th }}$ |
|  | $(38 \%)$ | $(14.5 \%)$ | $(7.4 \%)$ | $(3.4 \%)$ | $(3.2 \%)$ | $(1.9 \%)$ | $(1.7 \%)$ | $(1.3 \%)$ |
|  | 823.5 | 314.2 |  |  |  |  |  |  |
| Refer to Table 7.1-4 and Table 7.1-6. | Refer to Table 7.1-5. |  |  |  |  |  |  |  |

Example 2: $400 \mathrm{~V}, 3.7 \mathrm{~kW}, 15$ units (with AC and DC reactors), max rate of operation 0.55

| Fundamental harmonic current on $6.6 \text { kV side (mA) }$ | Harmonic current on 6.6 kV side (mA) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $394 \times 15=5910$ | $\begin{gathered} 5^{\text {th }} \\ (28 \%) \end{gathered}$ | $\begin{gathered} 7^{\text {th }} \\ (9.1 \%) \end{gathered}$ | $\begin{gathered} 11^{\text {th }} \\ (7.2 \%) \end{gathered}$ | $\begin{gathered} 13^{\text {th }} \\ (4.1 \%) \end{gathered}$ | $\begin{gathered} 17^{\text {th }} \\ (3.2 \%) \end{gathered}$ | $\begin{gathered} 19^{\text {th }} \\ (2.4 \%) \end{gathered}$ | $\begin{gathered} 23 \text { rd } \\ (1.6 \%) \end{gathered}$ | $\begin{gathered} 25^{\text {th }} \\ (1.4 \%) \end{gathered}$ |
|  | 910.1 | 295.8 |  |  |  |  |  |  |
| Refer to Table 7.1-4 and Table 7.1-6. | Refer to Table 7.1-5. |  |  |  |  |  |  |  |

## Appendix 8 Effect on insulation when driving general purpose motor with a 400 V class inverter

When the inverter drives the motor, surge voltage created by IGBT switching superposes on the inverter output voltage and is applied on the motor terminals. When this surge voltage is high, the motor insulation can be affected, leading to damage in some cases.
This document describes the inverter surge voltage generation mechanism and the countermeasure in order to prevent these instances.
For the inverter operating principles, refer to Appendix 5 "Proficient way to use inverters (on electric noise) ".

## Appendix -8.1 Surge voltage generation mechanism

The inverter rectifies and smooths commercial power supply. The direct voltage $E$ is approximately $\sqrt{\mathbf{2}}$ times the commercial power supply voltage (approximately 620 V for 440 VAC input). The peak value of the output voltage is normally around this direct voltage.
However, inductance (L) and stray capacitance (C) exist in the wiring between the inverter and the motor. The voltage changes caused by the switching of the inverter components resonate with LC, causing surge voltage. This surge voltage applies high voltage on the motor terminals. (Refer to Figure 8.1-1.)

This voltage, which varies depending on the switching speed of inverter components and wiring conditions, can reach up to approximately twice the inverter direct current voltage ( 620 V x $2=1200 \mathrm{~V}$


Figure 8.1-1: Voltage waves of various parts approximately).
"Figure 8.1-2: Actual measurement sample of wiring length and voltage peak value at motor terminal" shows an actually measured example of the relationship between the wiring length between the inverter and motor and the voltage peak value at the motor terminal. This figure shows that the peak value of the motor terminal voltage rises as the wiring lengthens, saturating at approximately twice the inverter direct current voltage. Also, shorter ramp time increases the motor terminal voltage, even for short wiring length.


Figure 8.1-2: Actual measurement sample of wiring length and voltage peak value at motor terminal

## Appendix -8.2 Effect of surge voltage

The surge voltage generated by LC resonation of the wiring is applied on the motor input terminals. Depending on the magnitude of the surge voltage, motor insulation may be damaged. When driving with 200 V class inverters, the direct current voltage is around 300 V . At this level, insulation strength will not cause problems even if the motor terminal voltage peak values due to surge voltage reach twice the DC voltage.
However, when driving with 400 V class inverters, the direct current voltage becomes approximately 600 V . The surge voltage can magnify depending on the wiring length and may lead to insulation damage.

## Appendix -8.3 Countermeasure for surge voltage

The following methods exist as countermeasures for insulation damage due to surge voltage when driving motors with 400 V class inverters.

## Appendix -8.3.1 Suppressing surge voltage

Surge voltage can be suppressed by suppressing the ramp up of voltage and by suppressing the peak value.

## (1) Output LC filter (OFL filter)

Including cases of long wiring, generally, motor terminal voltage peak values are suppressed by installing LC filter (OFL filter) on the output side of inverters.
For details, refer to Chapter 7 "EMC Compatible Peripherals".

## (2) Output reactor

When the wiring is relatively short, install AC reactor on the inverter output side to suppress the ramp up of voltage (dv/dt) to reduce surge voltage.


Figure 8.3-1: Methods to suppress surge voltage

## Appendix -8.3.2 Using motors with enhanced insulation

The insulation in motor windings can be strengthened to improve surge durability.

## Appendix -8.3.3 On existing products

## Case of motors already driven by 400 V class inverters

Research for the past five years on motor insulation damage instances due to inverter generated surge voltages reveal that the occurrence rate is $0.013 \%$. When damages occur, the voltages are above 1100 V and they tend to occur within a few months after inverter driven operation begins.
Therefore, the probability of insulation damage in motors which have been in operation for more than a few months is considerably low.

## Case of driving existing motor with a new $\mathbf{4 0 0} \mathrm{V}$ class inverter

Suppressing surge voltage by using the method described in "Appendix -8.3.1 Suppressing surge voltage" is recommended.

## Appendix 9 Wire permissible current (IEC 60364-5-52)

## Appendix -9.1 Permissible current based on ambient temperature, cable laying method

Table 9.1-1: Permissible current of a PVC (polyvinyl chloride) wire (maximum permissible temperature $70^{\circ} \mathrm{C}$ ) (for 3-core cables with copper conductor)

|  | $\begin{gathered} \text { Aerial wiring } \\ \text { (number of cables: } 1 \text { ) } \end{gathered}$ |  |  | Electric duct wiring (number of cables: 2) |  |  | Electric duct wiring (number of cables: up to 9) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $30^{\circ} \mathrm{C}$ <br> (Io) <br> [A] | $\begin{gathered} 40^{\circ} \mathrm{C} \\ (10 \times 0.87) \end{gathered}$ $[\mathrm{A}]$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ (\mathrm{I} \times \times 0.71) \\ {[\mathrm{A}]} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{3 0 ^ { \circ }} \mathbf{C} \\ (102=10 \times 0.87) \end{gathered}$ <br> [A] | $\begin{gathered} 40^{\circ} \mathrm{C} \\ (\mathrm{I} 02 \times 0.87) \end{gathered}$ <br> [A] | $\begin{gathered} 50^{\circ} \mathrm{C} \\ (102 \times 0.71) \end{gathered}$ <br> [A] | $\begin{gathered} \mathbf{3 0 ^ { \circ }} \mathbf{C} \\ (\mathrm{IO}=\mathrm{Io} \times 0.78) \\ {[\mathrm{A}]} \end{gathered}$ | $\begin{gathered} 40^{\circ} \mathrm{C} \\ (103 \times 0.87) \end{gathered}$ $[\mathrm{A}]$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ (103 \times 0.71) \end{gathered}$ $[\mathrm{A}]$ |
| 1.5 | 18.5 | 16 | 13 | 16 | 14 | 11 | 14 | 13 | 10 |
| 2.5 | 25 | 22 | 18 | 22 | 19 | 15 | 20 | 17 | 14 |
| 4 | 34 | 30 | 24 | 30 | 26 | 21 | 27 | 23 | 19 |
| 6 | 43 | 37 | 31 | 37 | 33 | 27 | 34 | 29 | 24 |
| 10 | 60 | 52 | 43 | 52 | 45 | 37 | 47 | 41 | 33 |
| 16 | 80 | 70 | 57 | 70 | 61 | 49 | 62 | 54 | 44 |
| 25 | 101 | 88 | 72 | 88 | 76 | 62 | 79 | 69 | 56 |
| 35 | 126 | 110 | 89 | 110 | 95 | 78 | 98 | 86 | 70 |
| 50 | 153 | 133 | 109 | 133 | 116 | 95 | 119 | 104 | 85 |
| 70 | 196 | 171 | 139 | 171 | 148 | 121 | 153 | 133 | 109 |
| 95 | 238 | 207 | 169 | 207 | 180 | 147 | 186 | 162 | 132 |
| 120 | 276 | 240 | 196 | 240 | 209 | 170 | 215 | 187 | 153 |
| 150 | 319 | 278 | 226 | 278 | 241 | 197 | 249 | 216 | 177 |
| 185 | 364 | 317 | 258 | 317 | 276 | 225 | 284 | 247 | 202 |
| 240 | 430 | 374 | 305 | 374 | 325 | 266 | 335 | 292 | 238 |
| 300 | 497 | 432 | 353 | 432 | 376 | 307 | 388 | 337 | 275 |

* lo: Reference value for permissible current
* Shows the permissible current for each of the ambient temperatures of $30^{\circ} \mathrm{C}, 40^{\circ} \mathrm{C}$, and $50^{\circ} \mathrm{C}$ and for each of 1 -, 2 -, and 9 -cable configurations.
If the use conditions are different, refer to IEC 60364-5-52:2001(JIS C 60364-5-52:2006).
Table 9.1-2: Permissible current of an XLPE (cross-linked polyethylene) and EP (ethylene-propylene rubber) wires (maximum permissible temperature $90^{\circ} \mathrm{C}$ ) (for 3-core cables with copper conductor)

|  | Aerial wiring(number of cables: 1) |  |  | Electric duct wiring (number of cables: 2) |  |  | Electric duct wiring (number of cables: up to 9) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $30^{\circ} \mathrm{C}$ <br> (lo) <br> [A] | $\begin{gathered} \hline 40^{\circ} \mathrm{C} \\ (10 \times 0.87) \\ {[\mathrm{A}]} \\ \hline \end{gathered}$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ (\mathrm{I} \times 0.71) \\ {[\mathrm{A}]} \end{gathered}$ | $\begin{gathered} \hline \mathbf{3 0 ^ { \circ }} \mathrm{C} \\ (\mathrm{I} 2=\mathrm{I} \times 0.87) \\ {[\mathrm{A}]} \end{gathered}$ | $\begin{gathered} \hline 40^{\circ} \mathrm{C} \\ (\mathrm{I} 2 \times 0.08) \\ {[\mathrm{A}]} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{5 0 ^ { \circ }} \mathrm{C} \\ (\mathrm{I} 2 \times 0.71) \\ {[\mathrm{A}]} \\ \hline \end{gathered}$ | $\begin{array}{c\|} \hline 30^{\circ} \mathrm{C} \\ (\mathrm{IO}=10 \times 0.78) \\ {[\mathrm{A}]} \end{array}$ | $\begin{gathered} \hline 40^{\circ} \mathrm{C} \\ (\mathrm{I} 03 \times 0.87) \\ {[\mathrm{A}]} \\ \hline \end{gathered}$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ (103 \times 0.71) \end{gathered}$ <br> [A] |
| 1.5 | 23 | 20 | 16 | 20 | 17 | 14 | 18 | 16 | 13 |
| 2.5 | 32 | 28 | 23 | 28 | 24 | 20 | 25 | 22 | 18 |
| 4 | 42 | 37 | 30 | 37 | 32 | 26 | 33 | 29 | 23 |
| 6 | 54 | 47 | 38 | 47 | 41 | 33 | 42 | 37 | 30 |
| 10 | 75 | 65 | 53 | 65 | 57 | 46 | 59 | 51 | 42 |
| 16 | 100 | 87 | 71 | 87 | 76 | 62 | 78 | 68 | 55 |
| 25 | 127 | 110 | 90 | 110 | 96 | 78 | 99 | 86 | 70 |
| 35 | 158 | 137 | 112 | 137 | 120 | 98 | 123 | 107 | 88 |
| 50 | 192 | 167 | 136 | 167 | 145 | 119 | 150 | 130 | 106 |
| 70 | 246 | 214 | 175 | 214 | 186 | 152 | 192 | 167 | 136 |
| 95 | 298 | 259 | 212 | 259 | 226 | 184 | 232 | 202 | 165 |
| 120 | 346 | 301 | 246 | 301 | 262 | 214 | 270 | 235 | 192 |
| 150 | 399 | 347 | 283 | 347 | 302 | 246 | 311 | 271 | 221 |
| 185 | 456 | 397 | 324 | 397 | 345 | 282 | 356 | 309 | 253 |
| 240 | 538 | 468 | 382 | 468 | 407 | 332 | 420 | 365 | 298 |
| 300 | 621 | 540 | 441 | 540 | 470 | 384 | 484 | 421 | 344 |

* Io: Reference value for permissible current
* Shows the permissible current for each of the ambient temperatures of $30^{\circ} \mathrm{C}, 40^{\circ} \mathrm{C}$, and $50^{\circ} \mathrm{C}$ and for each of $1-, 2-$, and 9 -cable configurations.
If the use conditions are different, refer to IEC 60364-5-52:2001(JIS C 60364-5-52:2006).


# High Performance Vector Control Inverter <br> <br> FRENIC-VG 

 <br> <br> FRENIC-VG}

## User's Manual (Stack type edition)

First Edition, March 2013 5th Edition, July 2019

Fuji Electric Co., Ltd

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[^0]:    Correspondence Method to "Guideline on Measures to Suppress Harmonics for Users Serviced by High Voltage or Special High Voltage" (General Purpose Inverters)

[^1]:    *1 comming soon

[^2]:    *1 Available when the ROM version is $\mathrm{H} 1 / 20021$ or later.

[^3]:    Note (1) Frame 3-and 4 size stacks ( 400 V : 132 to $800 \mathrm{~kW}, 690 \mathrm{~V}$ : 132 to 450 kW ) are provided with casters. Install caster guides on the cabinet. If caster guides are painted, the paint may come off when setting or drawing out stacks. It is advisable to use SUS panels or plated steel panels.
    (2) Create the fixation attachment on the front face of the stack according to the recommended dimensions. (See Figure 4.2.1-14 (on page 4-16) and Figure 4.2.1-15 (on page 4-17).)
    Design the cooling fan of the stack to be detached without removing this fixation attachment.
    (3) The upper area of the stack is designed to attach a DC fuse. Lay out this area so that this DC fuse can be easily attached and detached.
    (4) Do not fix the stack aslant.

[^4]:    Website of System Sacom Industry Corp.: http://www.sacom.co.jp/

[^5]:    Set point current value at $20^{\circ} \mathrm{C}$
    $\frac{\text { Set point current value at } 20^{\circ} \mathrm{C}}{\text { Correctioncoefficient for installation condition (cabinet internaltemperatue) }}=$ Set point value of thermalrelay

[^6]:    ( BW400EAN: 50 kA .
    (Note 3) The specifications of class 2 heat resistant type is different from the value listed above table. For details, refer to the list of Fuji heat resistant type equipment catalog (No AH060).
    (Note 4) The product is not applicable to the 400 V -circuit.
    (Note 5) For details about UL ratings, refer to the list of specifications (page 20).

[^7]:    Note

    - The contact outputs (terminals Y5A/C, 30A/B/C, 73A/C) are mechanical contacts. Frequent ON/OFF operations cannot be permitted. Signals turned ON/OFF at high frequency at terminal Y5A/C should be output from terminals Y 1 to Y 3 .
    Furthermore, even if using an AC power supply, the contact life may be shorter with loads for which the contact current direction is fixed (loads with half-wave rectifier circuit, etc., e.g., timers, power supply devices for motor electromagnetic brakes).
    In cases such as this, instead of connecting the load directly to the contact output terminals, connect a control relay, etc. (separately installed) which satisfies load conditions to the contact output terminals, and then connect to the load via this relay.

[^8]:    ＊For information on peripherals for RHC630B to 800B－4DJ，refer to＂6．3．12．2 List of peripherals with no filter stack used＂．

[^9]:    *1 Requires the option OPC-VG7-SIR.
    *2 To connect PWM converters in parallel (so that all of them have the same output), ensure that they all have the same capacity.

[^10]:    * The generated loss of the filters shown above is the value for all quantities.

[^11]:    Note (1) The 3 phases ( $\mathrm{U}, \mathrm{V}, \mathrm{W}$ ) and the dedicated grounding wire for the motor are taken into consideration for the wires in the above table.
    (2) The use conditions given in the above table are applied when the wires specified in this manual are used. (IV, HIV, and FLSC wires)

[^12]:    (Note 1) Value within parenthesis is quasi-standard.

[^13]:    Note - Connect shielded wires to the inverter side.

[^14]:    (*1) Available when ROM version is newer than H1/2 0067.

[^15]:    Note For regenerative mode, multiply by the coefficient -0.95 .

[^16]:    Note When "PG vector control" and "NTC thermistor: Valid" are selected in the motor control system at the time of conducting single unit operation, disconnection detection function works and an alarm trip results.

[^17]:    Note
    Even when functions not described are selected in AO, output (monitor) is ' 0 ' (displays ' 0 ').

[^18]:    Note
    To remove the
    The error cannot be removed by pressing the (erser) key.

[^19]:    * For more information on the option cards, see Chapter 6 of separate volume "Option Edition (24A7-■-0045)".

[^20]:    * A negative temperature coefficient (NTC) thermistor is used to protect the motor from overheat, and under vector control, to compensate for the temperature in the motor parameters.
    A dedicated motor (VG motor) for Fuji vector control has a built-in NTC thermistor.

[^21]:    * Refer to "Section 4.1 Block diagrams for control logic" in Chapter 4 of separate volume "Unit Type/Function Codes Edition (24A7- $\square$-0019)".

[^22]:    Note Be cautioned that some models come with a reactor as standard.
    When the converter you use is a diode rectifier (RHD-D series), a DCR (direct current reactor) is contained in the diode rectifier. Therefore, the conversion factor K33=1.8 with a reactor (on the DC side) as shown in Table 7.1-3 should be used in calculation. Also, the conversion factor K34=1.4 can be applied when an optional ACR (alternate current reactor) is added.

